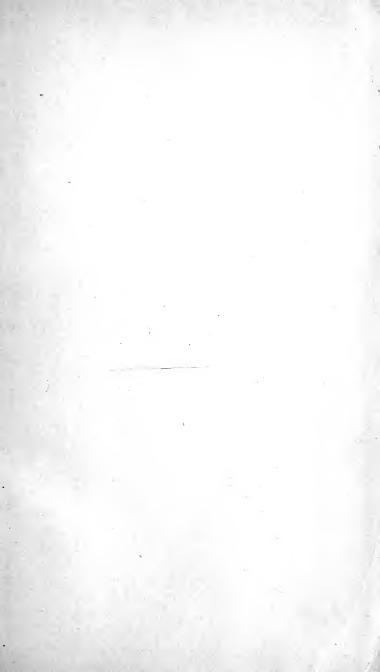
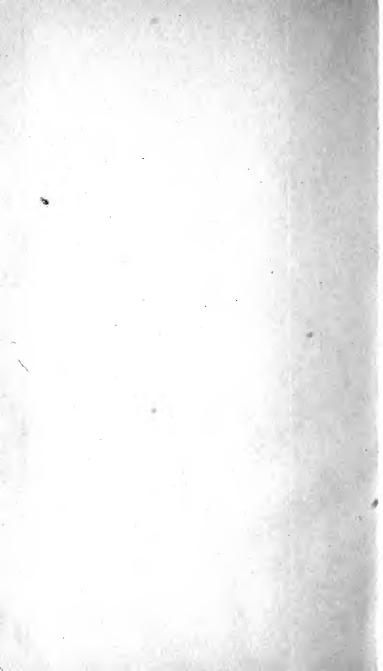
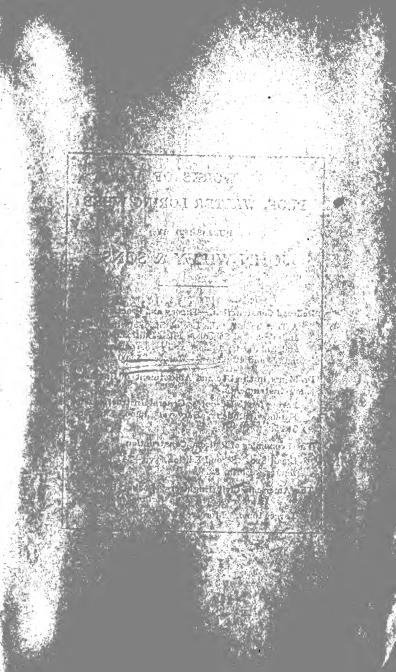


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## WORKS OF

## PROF. WALTER LORING WEBB

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# RAILROAD CONSTRUCTION.

## THEORY AND PRACTICE.

## A TEXT-BOOK FOR THE USE OF STUDENTS IN COLLEGES AND TECHNICAL SCHOOLS.

BY

## WALTER LORING WEBB, C.E.,

Member American Society of Civil Engineers; Member American Railway Engineering Association; Assistant Professor of Civil Engineering (Railroad Engineering) in the University of Pennsylvania, 1893–1901; etc.

## FIFTH EDITION, REVISED AND ENLARGED.

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## PREFACE TO FIRST EDITION.

The preparation of this book was begun several years ago, when much of the subject-matter treated was not to be found in print, or was scattered through many books and pamphlets, and was hence unavailable for student use. Portions of the book have already been printed by the mimeograph process or have been used as lecture-notes, and hence have been subjected to the refining process of class-room use.

The author would call special attention to the following features:

a. Transition curves; the multiform-compound-curve method is used, which has been followed by many railroads in this country; the particular curves here developed have the great advantage of being exceedingly simple, and although the method is not theoretically exact, it is demonstrable that the differences are so small that they may safely be neglected.

b. A system of earthwork computations which makes the multiplication and reduction in a single operation by means of a sliderule and which enables one to compute readily the volume of the most complicated earthwork forms with an accuracy which is only limited by the precision of the cross-sectioning.

c. The "mass curve" in earthwork; the theory and use of this very valuable process.

d. Tables I, II, III, and IV have been computed *ab novo*. Tables I and II were checked (after computation) with other tables, which are generally considered as standard, and all discrepancies were further examined. They are believed to be perfect.

e. Tables V, VI, VII, and IX have been borrowed, by permission, from "Ludlow's Mathematical Tables." It is believed that five-place tables give as accurate results as actual field

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practice requires. Tables VIII and X have been compiled to conform with Ludlow's system.

The author wishes to acknowledge his indebtedness to Mr. Chas. A. Sims, civil engineer and railroad contractor, for reading and revising the portions relating to the cost of earthwork.

Since the book is written primarily for students of railroad engineering in technical institutions, the author has assumed the usual previous preparation in algebra, geometry, and trigonometry.

WALTER LORING WEBB.

UNIVERSITY OF PENNSYLVANIA, PHILADELPHIA, Jan. 1, 1900.

## PREFACE TO SECOND EDITION.

SINCE the issue of the first edition the author has conferred with many noted educators in civil engineering, among them the late Professors E. A. Fuertes and J. B. Johnson, regarding the most desirable size of page for this book. The inconvenience of the octavo edition for field-work was found to be limiting its use. It was therefore decided to recast the whole work and reduce the page from "octavo" to "pocket-book" size. Advantage was then taken of the opportunity to revise freely and to add new matter. The original text has now been almost doubled by the addition of several chapters on structures, train resistance, rolling stock, etc., and also several chapters giving the fundamental principles of the economics of railroad location. Those who are familiar with the late Mr. Wellington's masterpiece, "The Eccnomic Theory of Railway Location," will readily appreciate the author's indebtedness to that work. But while the same general method has been followed, the author has taken advantage of the classification of operating expenses adopted by the Interstate Commerce Commission, has used the figures

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published by them (which were unavailable when Mr. Welling ton wrote), and has developed the theory on an independent basis, with the exception of a few minor details. Those who deny the utility of such methods of computation are referred to §§ 367, 426, and elsewhere for a practical discussion of that subject.

The author's primary aim has been to produce a "text-book for students," and the subject-matter has therefore been cut down to that which may properly be required of students in the time usually allotted to railroad work in a civil-engineering curriculum. On this account no extended discussion has been given to the multitudinous forms of various railroad devices in the chapters on structures. The aim has been to teach the principles and to guide the students into proper methods of investigation.

January, 1903.

## PREFACE TO THIRD EDITION.

In the present edition Tables IX and X have been entirely changed, the tables having been rewritten so that the values are given for single minutes rather than for each ten minutes. There has also been added a table of squares, cubes, square roots, cube roots, and reciprocals, which are frequently of so great service in computations. Advantage has also been taken of the opportunity to make numerous typographical and verbal changes.

February, 1905.

## PREFACE TO FOURTH EDITION.

In this edition a very extensive revision has been made in the chapter on Earthwork. Table XXXIII, giving the volume of level sections, has been added to the book, with a special demonstration of the method of utilizing this table for pre-

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liminary and approximate earthwork calculations. A demonstration, with table, for determining the economics of ties has also been added. In accordance with the suggestions of Prof. R. B. H. Begg, of Syracuse University, additions have been made to Table IV, which facilitate the solution of problems in transition curves. Very numerous and sometimes extensive alterations and additions, as well as mere verbal and typographical changes, have been made in various parts of the The chapters on Economics have been revised to make book. them conform to more recent estimates of cost of operation.

Julv. 1908.

## PREFACE TO FIFTH EDITION.

THE very radical changes made, during recent years, by the Interstate Commerce Commission, in the analysis of operating expenses of railroads, have required that all of the chapters on Economics should be almost entirely rewritten. The writer has also endeavored to make all recommendations as to construction work to conform with the most recent recommendations on those points by the American Railway Engineering Association, who granted the Author special permission to make such quotations. This gives all such statements the highest possible authority. Advantage was taken of the opportunity to correct minor typographical errors and blemishes which have been discovered since issuing the fourth edition.

March, 1913.

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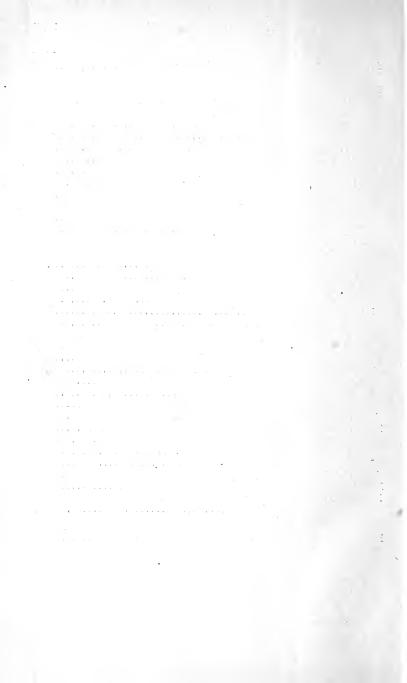
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## RAILROAD CONSTRUCTION.

## CHAPTER I.

## RAILROAD SURVEYS

THE proper conduct of railroad surveys presupposes an adequate knowledge of almost the whole subject of railroad engineering, and particularly of some of the complicated questions of Railroad Economics, which are not generally studied except at the latter part of a course in railroad engineering, if at all. This chapter will therefore be chiefly devoted to methods of instrumental work, and the problem of choosing a general route will be considered only as it is influenced by the topography or by the application of those elementary principles of Railroad Economics which are self-evident or which may be accepted by the student until he has had an opportunity of studying those principles in detail

## RECONNOISSANCE SURVEYS.

**I.** Character of a reconnoissance survey. A reconnoissance survey is a very hasty examination of a belt of country to determine which of all possible or suggested routes is the most promising and best worthy of a more detailed survey. It is essentially very rough and rapid. It aims to discover those salient features which instantly stamp one route as distinctly superior to another and so narrow the choice to routes which are so nearly equal in value that a more detailed survey is necessary to decide between them.

2. Selection of a general route. The general question of running a railroad between two towns is usually a financial rather

than an engineering question. Financial considerations usually determine that a road *must* pass through certain more or less important towns between its termini. When a railroad runs through a thickly settled and very flat country, where, from a topographical standpoint, the road may be run by any desired route, the "right-of-way agent" sometimes has a greater influence in locating the road than the engineer. But such modifications of alignment, on account of business considerations, are foreign to the engineer's side of the subject, and it will be hereafter assumed that topography alone determines the location of the line. The consideration of those larger questions combining finance and engineering (such as passing by a town on account of the necessary introduction of heavy grades in order to reach it) will be taken up in Chap. XIX, et seq.

3. Valley route. This is perhaps the simplest problem. If the two towns to be connected lie in the same valley, it is frequently only necessary to run a line which shall have a nearly uniform grade. The reconnoissance problem consists largely in determining the difference of elevation of the two termini of this division and the approximate horizontal distance so that the proper grade may be chosen. If there is a large river running through the valley, the road will probably remain on one side or the other throughout the whole distance, and both banks should be examined by the reconnoissance party to determine which is preferable. If the river may be easily bridged, both banks may be alternately used, especially when better alignment is thereby secured. A river valley has usually a steeper slope in the upper part than in the lower part. A uniform grade throughout the valley will therefore require that the road climbs up the side slopes in the lower part of the valley. In case the "ruling grade" \* for the whole road is as great as or greater than the steepest natural valley slope, more freedom may be used in adopting that alignment which has the least costregardless of grade. The natural slope of large rivers is almost invariably so low that grade has no influence in determining the choice of location. When bridging is necessary, the river banks should be examined for suitable locations for abutments

<sup>\*</sup> The *ruling grade* may here be loosely defined as the maximum grade which is permissible. This definition is not strictly true, as may be seen later when studying Railroad Economics, but it may here serve the purpose.

and piers. If the soil is soft and treacherous, much difficulty may be experienced and the choice of route may be largely determined by the difficulty of bridging the river except at certain favorable places.

4. Cross-country route. A cross-country route always has one or more summits to be crossed. The problem becomes more complex on account of the greater number of possible solutions and the difficulty of properly weighing the advantages and disadvantages of each. The general aim should be to choose the lowest summits and the highest stream crossings, provided that by so doing the grades between these determining points shall be as low as possible and shall not be greater than the ruling grade of the road. Nearly all railroads combine cross-country and valley routes to some extent. Usually the steepest natural slopes are to be found on the cross-country routes, and also the greatest difficulty in securing a low through grade. An approximate determination of the ruling grade is usually made during the reconnoissance. If the ruling grade has been previously decided on by other considerations, the leading feature of the reconnoissance survey will be the determination of a general route along which it will be possible to survey a line whose maximum grade shall not exceed the ruling grade.

5. Mountain route. The streams of a mountainous region frequently have a slope exceeding the desired ruling grade. In such cases there is no possibility of securing the desired grade by following the streams. The penetration of such a region may only be accomplished by "development"—accompanied perhaps by tunneling. "Development" consists in deliberately increasing the length of the road between two extremes of elevation so that the rate of grade shall be as low as desired. The usual method of accomplishing this is to take advantage of some convenient formation of the ground to introduce some lateral deviation. The methods may be somewhat classified as follows:

(a) Running the line up a convenient lateral valley, turning a sharp curve and working back up the opposite slope. As shown in Fig. 1, the considerable rise between A and B was surmounted by starting off in a very different direction from the general direction of the road; then, when about one-half of the desired rise had been obtained, the line crossed the valley and continued the climb along the opposite slope. (b) Switch-

back. On the steep side-hill BCD (Fig. 1) a very considerable gain in elevation was accomplished by the switchback CD. The gain in elevation from B to D is very great. On the other hand, the speed must always be slow; there are two complete stoppages of the train for each run; all trains must run backward from C to D. (c) *Bridge spiral*. When a valley is so narrow at some point that a bridge or viaduct of reasonable length can span the valley at a considerable elevation above the

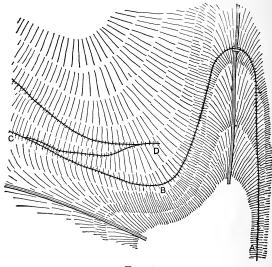


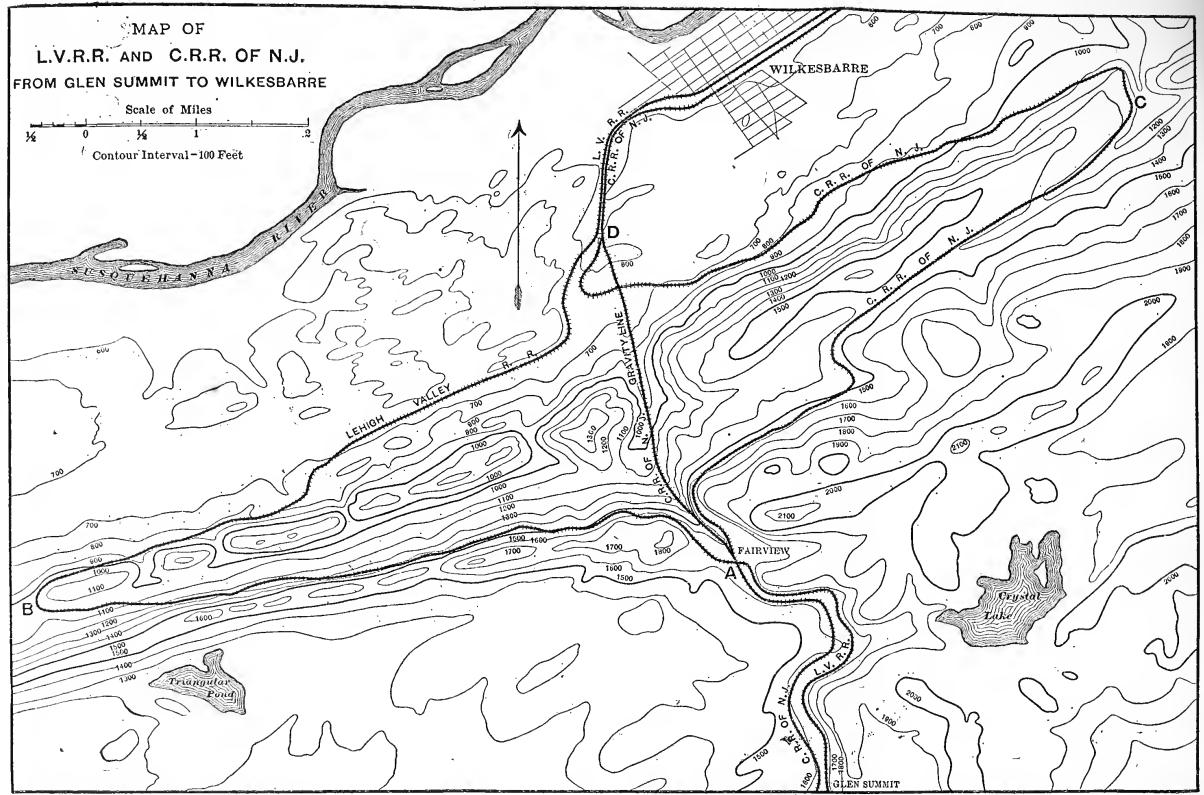
FIG. 1.

bottom of the valley, a bridge spiral may be desirable. In Fig. 2 the line ascends the stream valley past A, crosses the stream at B, works back to the narrow place at C, and there crosses itself, having gained perhaps 100 feet in elevation. (d) *Tunnel spiral* (Fig. 3). This is the reverse of the previous plan. It implies a thin steep ridge, so thin at some place that a tunnel through it will not be excessively long. Switchbacks and spirals are sometimes necessary in mountainous countries, but they should not be considered as normal types of construction. A region must be very difficult if these devices cannot be avoided.

On Plate I are shown three separate ways (as actually constructed) of running a railroad between two points a little over three miles apart and having a difference of elevation of nearly

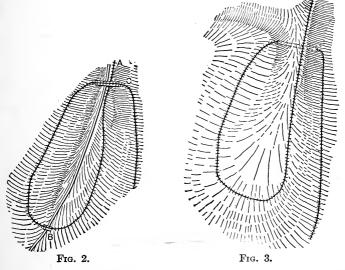
§ 5.

PLATE I.





1100 feet. At A the Central R. R. of New Jersey runs under the Lehigh Valley R. R. and soon turns off to the northeast for about six miles, then doubles back, reaching D, a fall of about 1050 feet with a track distance of about 12.7 miles. The L. V. R. R. at A runs to the westward for six to seven miles,



then turns back until the roads are again close together at D. The track distance is about 14 miles and the drop a little greater, since at A the L. V. R. R. crosses *over* the other, while at D they are at practically the same level. From B to C the distance is over eleven miles. From A directly down to D the C. R. R. of N. J. runs a "gravity" road, used exclusively for freight, on which cars alone are hauled by cable. The main-line routes are remarkable examples of sheer "development." Even as constructed the L. V. R. R. has a grade of about 95 feet per mile, and this grade has proved so excessive for freight work that the company has constructed a cut-off (not shown on the map) which leaves the main line at A, nearly parallels the C. R. R. to C, and then running in a northeasterly direction again joins the main line beyond Wilkesbarre. The grade is thereby cut down to 65<sup>\*</sup> feet per mile.

Rack railways and cable roads, although types of mountain railroad construction, will not be here considered.

6. Existing maps. The maps of the U.S. Geological Survey are exceedingly valuable as far as they have been completed. So far as topographical considerations are concerned, they almost dispense with the necessity for the reconnoissance and "first preliminary" surveys. Some of the State Survey maps will give practically the same information. County and township maps can often be used for considerable information as to the relative *horizontal* position of governing points, and even some approximate data regarding elevations may be obtained by a study of the streams. Of course such information will not dispense with surveys, but will assist in so planning them as to obtain the best information with the least work. When the relative horizontal positions of points are reliably indicated on a map, the reconnoissance may be reduced to the determination of the relative elevations of the governing points of the route.

7. Determination of relative elevations. A recent description of European methods includes spirit-leveling in the reconnoissance work. This may be due to the fact that, as indicated above, previous topographical surveys have rendered unnecessary the "exploratory" survey which is required in a new country, and that their reconnoissance really corresponds more nearly to our preliminary.

The perfection to which barometrical methods have been brought has rendered it possible to determine differences of elevation with sufficient accuracy for reconnoissance purposes by the combined use of a mercurial and an aneroid barometer. The mercurial barometer should be kept at "headquarters," and readings should be taken on it at such frequent intervals that any fluctuation is noted, and throughout the period that observations with the aneroid are taken in the field. At each observation there should also be recorded the time, the reading of the attached thermometer, and the temperature of the external air. For uniformity, the mercurial readings should then be "reduced to 32° F." The form of notes for the mercurial barometer readings should be as follows:

Time.	Merc. Barom.	Attached Therm.	Reduction to 32° F.	External Therm.	Corrected reading.
7:00 A.M. :15 :30 :45	$29.872 \\ .866 \\ .858 \\ .850$	72° 73.5 75 76	$117 \\ .121 \\ .125 \\ .127 $	73° 75 76 77	$29.755 \\ .745 \\ .733 \\ .723$

The corrections in column 4 are derived from Table XI by interpolation.

Before starting out, a reading of the aneroid should be taken at headquarters coincident with a reading of the mercurial. The difference is one value of the correction to the aneroid. As soon as the aneroid is brought back another comparison of readings should be made. Even though there has been considerable rise or fall of pressure in the interval, the difference in readings (the correction) should be substantially the same provided the aneroid is a good instrument. If the difference of elevation is excessive (as when climbing a high mountain) even the best aneroid will "lag" and not recover its normal reading for several hours, but this does not apply to such differences of elevation as are met with in railroad work. The best aneroids read directly to  $\frac{1}{100}$  of an inch of mercury and may be estimated to  $\frac{1}{1000}$  of an inch—which corresponds to about 0.9 foot difference of elevation. In the field there should be read, at each point whose elevation is desired, the aneroid, the time, and the temperature. These readings, corrected by the mean value of the correction between the aneroid and the mercurial, should then be combined with the reading of the mercurial (interpolated if necessary) for the times of the aneroid observations and the difference of elevation obtained. The field notes for the aneroid should be taken as shown in the first four columns of the tabular form. The "corrected aneroid" readings of column 5 are found by correcting the readings of column 3 by the mean difference between the mercurial and aneroid when compared at morning and night. Column 6 is a copy of the "corrected readings" from the office notes. interpolated when necessary for the proper time. Column 7 is similarly obtained. Col. 8 is obtained from cols. 4 and 5, and col. 9 from cols. 6 and 7, with the aid of Table XII. The correction for temperature (col. 11), which is generally small unless the difference of elevation is large, is obtained with the aid of Table XIII. The elevations in Table XII are elevations above an assumed datum plane, where under the given atmospheric conditions the mercurial reading would be 30". Of course the position of this assumed plane changes with varying atmospheric conditions and so the elevations are to be considered as *relative* and their difference taken. [See the author's "Problems in the Use and Adjustment of Engineering In-

§ 7.

(Left-hand	page of	Notes.)
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Time.	Place.	Aneroid.	Therm.	Corr. Aner.	Corr. Merc.
7:00 7:10 7:30 7:50	Office ⊿0 saddle-back river cross.	$29.628 \\ 29.662 \\ 29.374 \\ 29.548$	73° 72° 63° 70°	29.789 29.501 29.675	29.755 29.748 29.733 29.720

struments," Prob. 22.] Important points should be observed more than once if possible. Such duplicate observations will be found to give surprisingly concordant results even when a general fluctuation of atmospheric pressure so modifies the tabulated readings that an agreement is not at first apparent. Variations of pressure produced by high winds, thunder-storms, etc., will generally vitiate possible accuracy by this method. By "headquarters" is meant any place whose elevation above any given datum is known and where the mercurial may be placed and observed while observations within a range of several miles are made with the aneroid. If necessary, the elevation of a new headquarters may be determined by the above method, but there should be if possible several independent observations whose accordance will give a fair idea of their accuracy.

The above method should be neither slighted nor used for more than it is worth. When properly used, the errors are compensating rather than cumulative. When used, for example, to determine that a pass B is 260 feet higher than a determined bridge crossing at A which is six miles distant, and that another pass C is 310 feet higher than A and is ten miles distant, the figures, even with all necessary allowances for inaccuracy, will give an engineer a good idea as to the choice of route especially as affected by ruling grade. There is no comparison between the time and labor involved in obtaining the above information by barometric and by spirit-leveling methods, and *for reconnoissance purposes* the added accuracy of the spirit-leveling method is hardly worth its cost.

8. Horizontal measurements, bearings, etc. When there is no map which may be depended on, or when only a skeleton map is obtainable, a rapid survey, sufficiently accurate for the purpose, may be made by using a pocket compass for bearings and a telemeter, odometer, or pedometer for distances. The telemeter [stadia] is more accurate, but it requires a definite clear

Temp. at Approx. headqu. field read.		Approx. headq. read.	Diff.	Corr. for temp.	Diff. elev.
75° 76 77	192     457     297	$230 \\ 244 \\ 256$	-38 + 213 + 41	-(+2) + (+10) + (+2)	-40 + 223 + 43

(Right-hand page of Notes.)

sight from station to station, which may be difficult through a wooded country. The odometer, which records the revolutions of a wheel of known circumference, may be used even in rough and wooded country, and the results may be depended on to a small percentage. The pedometer (or pace-measurer) depends for its accuracy on the actual movement of the mechanism for each pace and on the uniformity of the pacing. Its results are necessarily rough and approximate, but it may be used to fill in some intermediate points in a large skeleton map. A handlevel is also useful in determining the relative elevation of various topographical features which may have some bearing on the proper location of the road.

9. Importance of a good reconnoissance. The foregoing instruments and methods should be considered only as aids in exercising an educated common sense, without which a proper location cannot be made. The reconnoissance survey should command the best talent and the greatest experience available. If the general route is properly chosen, a comparatively low order of engineering skill can fill in a location which will prove a paying railroad property; but if the general route is so chosen that the ruling grades are high and the business obtained is small and subject to competition, no amount of perfection in detailed alignment or roadbed construction can make the road a profitable investment.

### PRELIMINARY SURVEYS.

10. Character of survey. A preliminary railroad survey is properly a topographical survey of a belt of country which has been selected during the reconnoissance and within which it is estimated that the located line will lie. The width of this belt will depend on the character of the country. When a railroad is to follow a river having very steep banks the choice of location is sometimes limited at places to a very few feet of width and the belt to be surveyed may be correspondingly narrowed. In very flat country the desired width may be only limited by the ability to survey points with sufficient accuracy at a considerable distance from what may be called the "backbone line" of the survey.

11. Cross-section method. This is the only feasible method in a wooded country, and is employed by many for all kinds of country. The *backbone* line is surveyed either by observing magnetic bearings with a compass or by carrying forward

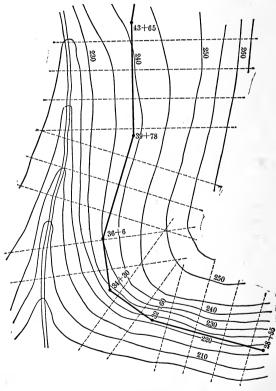


FIG. 4.

absolute azimuths with a transit. The compass method nas the disadvantages of limited accuracy and the possibility of considerable local error owing to local attraction. On the other hand there are the advantages of greater simplicity, no necessity

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for a back rodman, and the fact that the errors are purely local and not cumulative, and may be so limited, with care, that they will cause no vital error in the subsequent location survey. The transit method is essentially more accurate, but is liable to be more laborious and troublesome. If a large tree is encountered, either it must be cut down or a troublesome operation of offsetting must be used. If the compass is employed under these circumstances, it need only be set up on the far side of the tree and the former bearing produced. An error in reading a transit azimuth will be carried on throughout the survey. An error of only five minutes of arc will cause an offset of nearly eight feet in a mile. Large azimuth errors may, however, be avoided by immediately checking each new azimuth with a needle reading. It is advisable to obtain true azimuth at the beginning of the survey by an observation on the sun\* or Polaris, and to check the azimuths every few miles by azimuth observations. Distances along the backbone line should be measured with a chain or steel tape and stakes set every 100 feet. When a course ends at a substation, as is usually the case, the remaining portion of the 100 feet should be measured along the next course. The level party should immediately obtain the elevations (to the nearest tenth of a foot) of all stations, and also of the lowest points of all streams crossed and even of dry gullies which would require culverts.

12. Cross-sectioning. It is usually desirable to obtain contours at five-foot intervals This may readily be done by the use of a Locke level (which should be held on top of a simple five-foot stick), a tape, and a rod ten feet in length graduated to feet and tenths. The method of use may perhaps be best explained by an example. Let Fig. 5 represent a section perpendicular to the survey line—such a section as would be made by the dotted lines in Fig. 4. C represents the station point. Its elevation as determined by the level is, say, 158.3 above datum. When the Locke level on its five-foot rod is placed at C, the level has an elevation of 163.3. Therefore when a point is found (as at a) where the level will read 3.3 on the rod, that point has an elevation of 160.0 and its distance from the center gives the position of the 160-foot contour. Leaving the long rod at that point (a), carry the level to some point (b) such that the level will sight at the top of the rod. b is then on the 165-

\* For detailed methods of such determinations, see the author's "Problems in the Use and Adjustment of Engineering Instruments," Problems 35 and 36.

## RAILROAD CONSTRUCTION.

foot contour, and the *horizontal* distance ab added to the horizontal distance ac gives the position of that contour from the center. The contours on the lower side are found similarly. The first rod reading will be 8.3, giving the 155-foot contour.

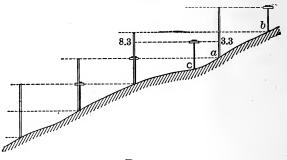
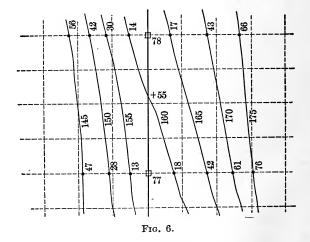


FIG. 5.

Plot the results in a note-book which is ruled in quarter-inch squares, using a scale of 100 feet per inch in both directions. Plot the work UP the page; then when looking ahead along the line, the work is properly oriented. When a contour crosses



the survey line, the place of crossing may be similarly determined. If the ground flattens out so that five-foot contours are very far apart, the absolute elevations of points at even fifty-

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foot distances from the center should be determined. The method is exceedingly rapid. Whatever error or inaccuracy occurs is confined in its effect to the one station where it occurs. The work being thus plotted in the field, unusually irregular topography may be plotted with greater certainty and no great error can occur without detection. It would even be possible by this method to detect a gross error that might have been made by the level party

13. Stadia method. This method is best adapted to fairly open country where a "shot" to any desired point may be taken without clearing. The backbone survey line is the same as in the previous method except that each course is limited to the practicable length of a stadia sight. The distance between stations should be checked by foresight and backsight-also the vertical angle. Azimuths should be checked by the needle. Considering the vital importance of leveling on a railroad survey it might be considered desirable to run a line of levels over the stadia stations in order that the leveling may be as precise as possible; but when it is considered that a preliminary survey is a somewhat hasty survey of a route that may be abandoned, and that the errors of leveling by the stadia method (which are conpensating) may be so minimized that no proposed route would be abandoned on account of such small error, and that the effect of such an error may be easily neutralized by a slight change in the location, it may be seen that excessive care in the leveling of the preliminary survey is hardly justifiable.

Since the students taking this work are assumed to be familiar with the methods of stadia topographical surveys, this part of the subject will not be further elaborated.

14. "First" and "Second" preliminary surveys. Some engineers advocate two preliminary surveys. When this is done, the first is a very rapid survey, made perhaps with a compass, and is only a better grade of reconnoissance. Its aim is to rapidly develop the facts which will decide for or against any proposed route, so that if a route is found to be unfavorable another more or less modified route may be adopted without having wasted considerable time in the survey of useless details. By this time the student should have grasped the fundamental idea that both the reconnoissance and preliminary surveys are not surveys of *lines* but of *areas*; that their aim is to survey only those topographical features which would have a deter-

mining influence on any railroad line which might be constructed through that particular territory, and that the value of a locating engineer is largely measured by his ability to recognize those determining influences with the least amount of work from his surveying corps. Frequently too little time is spent on the comparative study of preliminary lines. A line will be hastily decided on after very little study; it will then be surveyed with minute detail and estimates carefully worked up, and the claims of any other suggested route will then be handicapped, if not disregarded, owing to an unwillingness to discredit and throw away a large amount of detailed surveying. The cost of two or three extra preliminary surveys (*at critical sections* and not over the whole line) is utterly insignificant compared with the probable improvement in the "operating value" of a line located after such a comparative study of preliminary lines.

## LOCATION SURVEYS.

15. "Paper location." When the preliminary survey has been plotted to a scale of 200 feet per inch and the contours drawn in, a study may be made for the location survey. Disregarding for the present the effect on location of transition curves, the alignment may be said to consist of straight lines (or "tangents") and circular curves. The "paper location" therefore consists in plotting on the preliminary map a succession of straight lines which are tangent to the circular curves connecting them. The determining points should first be considered. Such points are the termini of the road, the lowest practicable point over a summit, a river-crossing, etc. So far as is possible, having due regard to other considerations, the road should be a "surface" road, i.e., the cut and fill should be made as small as possible. The maximum permissible grade must also have been determined and duly considered. The method of location differs radically according as the lines joining the determining points have a very low grade or have a grade that approaches the maximum permissible. With very low natural grades it is only necessary to strike a proper balance between the requirements for easy alignment and the avoidance of excessive earthwork. When the grade between two determined points approaches the maximum, a study of the location may be begun by finding a strictly surface line which will connect those

points with a line at the given grade. For example, suppose the required grade is 1.6% and that the contours are drawn at 5-foot intervals It will require 312 feet of 1.6% grade to rise 5 feet. Set a pair of dividers at 312 feet and step off this interval on successive contours. This line will in general be very irregular, but in an easy country it may lie fairly close to the proper location line, and even in difficult country such a surface line will assist greatly in selecting a suitable location. When the larger part of the line will evidently consist of tangents, the tangents should be first located and should then be connected by suitable curves. When the curves predominate, as they generally will in mountainous country, and particularly when the line is purposely lengthened in order to reduce the grade, the curves should be plotted first and the tangents may then be drawn connecting them. Considering the ease with which such lines may be drawn on the preliminary map, it is frequently advisable. after making such a paper location, to begin all over, draw a new line over some specially difficult section and compare results. Profiles of such lines may be readily drawn by noting their intersection with each contour crossed. Drawing on each profile the required grade line will furnish an approximate idea of the comparative amount of earthwork required. After deciding on the paper location, the length of each tangent, the central angle (see § 21), and the radius of each curve should be measured as accurately as possible. Since a slight error made in such measurements, taken from a map with a scale of 200 feet per inch, would by accumulation cause serious discrepancies between the plotted location and the location as afterward surveyed in the field, frequent tie lines and angles should be determined between the plotted location line and the preliminary line, and the location should be altered, as may prove necessary, by changing the length of a tangent or changing the central angle or radius of a curve, so that the agreement of the check-points will be sufficiently close. The errors of an inaccurate preliminary survey may thus be easily neutralized (see § 33). When the preliminary line has been properly run, its "backbone" line will lie very near the location line and will probably cross it at frequent intervals, thus rendering it easy to obtain short and numerous tie lines.

16. Surveying methods. A transit should be used for alignment, and only precise work is allowable. The transit stations

should be centered with tacks and should be tied to witnessstakes, which should be located outside of the range of the earthwork, so that they will neither be dug up nor covered up. All original property lines lying within the limits of the right of way should be surveyed with reference to the location line, so that the right-of-way agent may have a proper basis for settlement. When the property lines do not extend far outside of the required right of way they are frequently surveyed completely.

The leveler usually reads the target to the nearest thousandth of a foot on turning-points and bench-marks, but reads to the nearest tenth of a foot for the elevation of the ground at stations. Considering that  $\frac{1}{1000}$  of a foot has an angular value of about

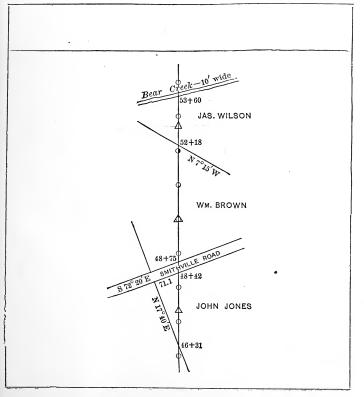
1.00	ett-nand p	,				
	Sta.	Align- ment.	Vernier.	Tangential Deflection.	Calculated Bearing.	Needle.
	54		1			
0	53 + 72.2	Р.Т.	9° 11′	18° 22′	N 54° 48′ E	N 62° 15' E
	52		7 57			
	51	zht for , 272.5	$6\ 15$			+
0	50	ve to rig ng. dist	4 33		+	
	49	24' curve to right for 22'; tang. dist., 272.5	$2\ 51$			
	48	[ 3°	1 09			
Э	$+32\\47$	P.C.	0°			
	46				N 36° 26' E	N 44° 0' E

[Left-hand page]

FORM OF NOTES.

one second at a distance of 200 feet, and that one division of a levelbubble is usually about 30 seconds, it may be seen that it is a useless refinement to read to thousandths unless corresponding care is taken in the use of the level. The leveler should also locate his bench-marks outside of the range of earthwork. A knob of rock protruding from the ground affords an excellent mark. A large nail, driven in the roots of a tree, which is not to be disturbed, is also a good mark. These marks should be clearly described in the note-book. The leveler should obtain the elevation of the ground at all station-points; also at all sudden breaks in the profile line, determining also the distance of these breaks from the previous even station. This will in-

[Right-hand page.]



§ 16.

clude the position and elevation of all streams, and even dry gullies, which are crossed

Measurements should preferably be made with a steel tape, care being taken on steep ground to insure horizontal measurements. Stakes are set each 100 feet, and also at the beginning and end of all curves. Transit-points (sometimes called "plugs" or "hubs") should be driven flush with the ground, and a "witness-stake," having the "number" of the station, should be set three feet to the right. For example, the witness-stake might have on one side "137+69.92," and on the other side "P C 4° R," which would signify that the transit hub is 69.92 feet beyond station 137, or 13769.92 feet from the beginning of the line, and also that it is the "point of curve" of a "4° curve" which turns to the *right*.

Alignment. The alignment is evidently a part of the location survey, but, on account of the magnitude and importance of the subject, it will be treated in a separate chapter.

17. Form of Notes. Although the Form of Notes cannot be thoroughly understood until after curves are studied, it is here introduced as being the most convenient place. The right-hand page should have a sketch showing all roads, streams, and property lines crossed with the bearings of those lines. This should be drawn to a scale of 100 feet per inch-the quarterinch squares which are usually ruled in note-books giving convenient 25-foot spaces. This sketch will always be more or less distorted on curves, since the center line is always shown as straight regardless of curves. The station points ("Sta." in first column, left-hand page) should be placed opposite to their sketched positions, which means that even stations will be recorded on every fourth line. This allows three intermediate lines for substations, which is ordinarily more than sufficient. The notes should read UP the page, so that the sketch will be properly oriented when looking ahead along the line The other columns on the left-hand page will be self-explanatory when the subject of curves is understood. If the "calculated bearings" are based on azimuthal observations, their agreement (or constant difference) with the needle readings will form a valuable check on the curve calculations and the instrumental work.

# CHAPTER II.

## ALIGNMENT.

In this chapter the alignment of the *center line* only of a pair of rails is considered. When a railroad is crossing a summit in the grade line, although the horizontal projection of the alignment may be straight, the vertical projection will consist of two sloping lines joined by a curve. When a curve is on a grade, the center line is really a spiral, a curve of double curvature, although its horizontal projection is a circle. The center line therefore consists of straight lines and curves of single and double curvature. The simplest method of treating them is to consider their horizontal and vertical projections separately. In treating simple, compound, and transition curves, only the horizontal projections of those curves will be considered.

### SIMPLE CURVES.

18. Designation of curves. A curve may be designated either by its radius or by the angle subtended by a chord of unit

length. Such an angle is known as the "degree of curve" and is indicated by D. Since the curves that are practically used have very long radii, it is generally impracticable to make any use of the actual center, and the curve is located without reference to it. If AB in Fig. 4 represents a unit chord (C) of a curve of radius R, then by the above definition the angle AOBequals D. Then

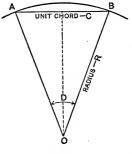


FIG. 7.

$$AO\sin\frac{1}{2}D = \frac{1}{2}AB = \frac{1}{2}C$$

$$R = \frac{\frac{2}{2}C}{\sin \frac{1}{2}D}$$

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(1)

or, by inversion,

$$\sin \frac{1}{2}D = \frac{C}{2R}.$$
 (2)

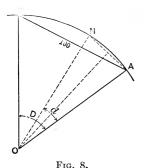
The unit chord is variously taken throughout the world as 100 feet, 66 feet, and 20 meters. In the United States 100 feet is invariably used as the unit chord length, and throughout this work it will be so considered. Table I has been computed on this basis. It gives the radius, with its logarithm, of all curves from a  $0^{\circ}$  01' curve up to a  $10^{\circ}$  curve, varying by single minutes. The sharper curves, which are seldom used, are given with larger intervals.

An approximate value of R may be readily found from the following simple rule, which should be memorized:

$$R = \frac{5730}{D}.$$

Although such values are not mathematically correct, since R does not strictly vary inversely as D, yet the resulting value is within a tenth of one per cent for all commonly used values of R, and is sufficiently close for many purposes, as will be shown later.

19. Length of a subchord. Since it is impracticable to measure along a curved arc, curves are always measured by



laying off 100-foot chord lengths. This means that the actual arc is always a little longer than the chord. It also means that a *subchord* (a chord shorter than the unit length) will be a little longer than the ratio of the angles subtended would call for. The truth of this may be seen without calculation by noting that two equal subchords, each subtending the angle  $\frac{1}{2}D$ , will evidently be slightly longer

than 50 feet each. If c be the length of a subchord subtending the angle d, then, as in Eq. 2,

$$\sin \frac{1}{2}d = \frac{c}{2R},$$

or, by inversion,

$$c = 2R \sin \frac{1}{2}d. \qquad (3)$$

The nominal length of a subchord =  $100\frac{d}{D}$  For example,

a nominal subchord of 40 feet will subtend an angle of  $\frac{40}{100}$  of  $D^{\circ}$ ; its true length will be slightly more than 40 feet, and may be computed by Eq. 3. The difference between the nominal and true lengths is maximum when the subchord is about 57 feet long, but with the low degrees of curvature ordinarily used the difference may be neglected. With a 10° curve and a nominal chord length of 60 feet, the true length is 60.049 feet. Very sharp curves should be laid off with 50-foot or even 25-foot chords (nominal length). In such cases especially the true lengths of these subchords should be computed and used instead of the nominal lengths.

20. Length of a curve. The length of a curve is always indicated by the quotient of  $100 \cancel{1} \div D$ . If the quotient of  $\cancel{1} \div D$  is a whole number, the length as thus indicated is the true length—measured in 100-foot chord lengths. If it is an odd number or if the curve begins and ends with a subchord (even though  $\cancel{1} \div D$  is a whole number), theoretical accuracy requires that the *true* subchord lengths shall be used, although the difference may prove insignificant. The length of the arc (or the mean length of the two rails) is therefore always in excess of the length as given above. Ordinarily the amount of this excess is of no practical importance. It simply adds an insignificant amount to the length of rail required.

*Example.* Required the nominal and true lengths of a 3° 45′ curve having a central angle of 17° 25′. First reduce the degrees and minutes to decimals of a degree.  $(100 \times 17^{\circ} 25')$  $\div 3^{\circ} 45' = 1741.667 \div 3.75 = 464.444$ . The curve has four 100-foot chords and a nominal chord of 64.444. The true chord should be 64 451. The actual arc is

$$17^{\circ}.4167 \times \frac{\pi}{180^{\circ}} \times R = 464.527$$

The excess is therefore 464.527 - 464.451 = 0.076 foot.

21. Elements of a curve. Considering the line as running from A toward B, the beginning of the curve, at A, is called the *point of curve* (PC). The other end of the curve, at B, is

§ 20.

The angle made by the tangents ities of the curve, is called the Т

FIG. 9.

the middle of the arc to the vertex is called the external distance (E). From the figure it is very easy to derive the following frequently used relations:

$T = R \tan \frac{1}{2} \Delta$					(4)
$LC = 2R \sin \frac{1}{2} \Delta$	٠,	•			(5)
$M = R \text{ vers } \frac{1}{2} \Delta$	•	•		•	(6)
$E = R \operatorname{exsec} \frac{1}{2} \Delta$	•	•			(7)

tangents is called the vertex (V).

at V, which equals the angle made by the radii to the extrem-

central angle (1). AV and BV, the two equal tangents from the

vertex to the PC and PT, are called the tangent distances (T). The chord AB is called the *long* chord (LC). The intercept HGfrom the middle of the long chord to the middle of the arc is called the middle ordinate (M).

That part of the secant GV from

22. Relation between T, E, and  $\Delta$ . Join A and G in Fig. 9. The angle  $VAG = \frac{1}{4}A$ , since it is measured by one half of the arc AG between the secant and tangent.  $AGO = 90^{\circ} - \frac{1}{4}$ .

$$AV: VG:: \sin AGV: \sin VAG;$$
  

$$\sin AGV = \sin AGO = \cos \frac{1}{4} d;$$
  

$$T: E: \cos \frac{1}{4} d: \sin \frac{1}{4} d;$$
  

$$T = E \cot \frac{1}{4} d. \ldots d.$$
(8)

The same relation may be obtained by dividing Eq. 4 by Eq. 7, since  $\tan a \div \operatorname{exsec} a = \cot \frac{1}{2}a$ .

23. Elements of a 1° curve. From Eqs. 1 to 8 it is seen that the elements of a curve vary directly as R. It is also seen to be very nearly true that R varies inversely as D. If the elements of a 1° curve for various central angles are calculated and tabulated, the elements of a curve of  $D^{\circ}$  curvature may be approximately found by dividing by D the corresponding elements of a 1° curve having the same central angle. For small

called the point of tangency (PT). The intersection of the

central angles and low degrees of curvature the errors involved by the approximation are insignificant, and even for larger angles the errors are so small that for many purposes they may be disregarded.

In Table II is given the value of the tangent distances. external distances, and long chords for a 1° curve for various central angles The student should familiarize himself with the degree of approximation involved by solving a large number of cases under various conditions by the exact and by the approximate methods, in order that he may know when the approximate method is sufficiently exact for the intended purpose. The approximate method also gives a ready check on the exact method.

24. Exercises. (a) What is the tangent distance of a 4° 20' curve having a central angle of 18° 24'?

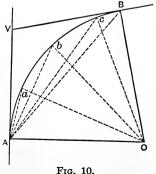
(b) Given a 3° 30' curve and a central angle of 16° 20', how far will the curve pass from the vertex? [Use Eq. 7.]

(c) An 18° curve is to be laid off using 25-foot (nominal) chord lengths. What is the true length of the subchords?

(d) Given two tangents making a central angle of 15° 24'. It is desired to connect these tangents by a curve which shall pass 16.2 feet from their intersection. How far down the tangent will the curve begin and what will be its radius? (Use Eq. 8 and then use Eq. 4 inverted.)

25. Curve location by deflections. The angle between a secant and a tangent (or between two secants intersecting on an arc) is measured by one half of the intercepted arc. Beginning

at the PC (A in Fig. 10), if the first chord is to be a full chord we may deflect an angle VAa v  $(=\frac{1}{2}D)$ , and the point *a*, which is 100 feet from A, is a point on the curve. For the next station. b. deflect an additional angle bAa $(=\frac{1}{2}D)$  and, with one end of the tape at a, swing the other end until the 100-foot point is on the line Ab. The point b is then on A the curve. If the final chord cBis a subchord, its additional deflection  $(\frac{1}{2}d)$  is something less than  $\frac{1}{2}D$ . The last deflection (BAV) is



of course  $\frac{1}{2}A$ . It is particularly important, when a curve begins or ends with a subchord and the deflections are odd quantities, that the last additional deflection should be carefully computed and added to the previous deflection, to check the mathematical work by the agreement of this last computed deflection with  $\frac{1}{2}A$ .

*Example.* Given a 3° 24' curve having a central angle of 18° 22' and beginning at sta. 47+32, to compute the deflections. The nominal length of curve is  $18^{\circ} 22' \div 3^{\circ} 24' = 18.367 \div 3.40 = 5.402$  stations or 540.2 feet. The curve there ends at sta. 52+72.2. The deflection for sta. 48 is  ${}_{106}^{68} \times \frac{1}{2}(3^{\circ} 24') = 0.68 \times 1^{\circ}.7 = 1^{\circ}.156 = 1^{\circ}.09'$  nearly. For each additional 100 feet it is 1° 42' additional. The final additional deflection for the final subchord of 72.2 feet is

$$\frac{72.2}{100} \times \frac{1}{2} (3^{\circ} 24') = 1^{\circ} .2274 = 1^{\circ} 14' \text{ nearly.}$$

The deflections are

$47 + 32 \dots \dots$	0°
480°	$+1^{\circ} 09' = 1^{\circ} 09'$
491° 09'	$+1^{\circ} 42' = 2^{\circ} 51'$
502° 51′	$+1^{\circ} 42' = 4^{\circ} 33'$
514° 33'	$+1^{\circ} 42' = 6^{\circ} 15'$
526° 15'	$+1^{\circ} 42' = 7^{\circ} 57'$
$.52 + 72.27^{\circ} 57'$	$+1^{\circ} 14' = 9^{\circ} 11'$
	491° 09' 502° 51' 514° 33'

As a check  $9^{\circ} 11' = \frac{1}{2}(18^{\circ} 22') = \frac{1}{2}\Delta$ . (See the Form of Notes in § 17.)

26. Instrumental work. It is generally impracticable to locate more than 500 to 600 feet of a curve from one station. Obstructions will sometimes require that the transit be moved up every 200 or 300 feet. There are two methods of setting off the angles when the transit has been moved up from the PC.

(a) The transit may be sighted at the previous transit station with a reading on the plates equal to the deflection angle from that station to the station occupied, but with the angle set off on the *other* side of  $0^{\circ}$ , so that when the telescope is turned to  $0^{\circ}$  it will sight along the tangent at the station occupied. Plunging the telescope, the forward stations may be set off by deflecting the proper deflections from the tangent at the station occupied This is a very common method and, when the degree of curvature is an even number of degrees and when the transit is only set at even stations, there is but little objection to it. But the degree of curvature is sometimes an odd quantity, and the exigencies of difficult location frequently require that substations be occupied as transit stations. Method (a) will then require the recalculation of all deflections for each new station occupied. The mathematical work is largely increased and the probability of error is very greatly increased and not so easily detected. Method (b) is just as simple as method (a) even for the most simple cases, and for the more difficult cases just referred to the superiority is very great.

(b) Calculate the deflection for each station and substation throughout the curve as though the whole curve were to be lo-

cated from the PC. The computations may thus be completed and checked (as above) before beginning the instrumental work. If it unexpectedly becomes necessary to introduce a substation at any point, its deflection from the PC may be readily interpolated. The stations actually set from the PC are located as usual. RULE. When the transit is set on any forward station, backsight to ANY previous station with the plates set at the deflection Plunge 3. angle for the station sighted at. the telescope and sight at any forward station with the deflection angle originally computed for that station. When the plates read the deflection angle for the station occupied, the telescope is sighting along the tangent at that station—which is the method of getting the forward tangent when occupying the PT. Even though the station occupied is an unexpected substation, when the instrument is properly oriented at that station, the angle reading

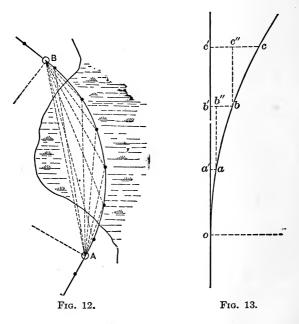


Fig. 11.

for any station, forward or back, is that originally computed for it from the PC. In difficult work, where there are obstructions, a valuable check on the accuracy may be found by sighting backward at any visible station and noting whether

§ 26.

its deflection agrees with that originally computed. As a numerical illustration, assume a 4° curve, with 28° curvature, with stations 0, 2, 4, and 7 occupied. After setting stations 1 and 2, set up the transit at sta. 2 and backsight to sta. 0 with the deflection for sta. 0, which is 0°. The reading on sta. 1 is 2°; when the reading is 4° the telescope is tangent to the curve, and when sighting at 3 and 4 the deflections will be 6° and 8°. Occupy 4; sight to 2 with a reading of 4°. When the reading is 8° the telescope is tangent to the curve and, by plunging the telescope, 5, 6, and 7 may be located with the originally computed deflections of 10°, 12°, and 14°. When occupying 7 a backsight may be taken to any visible station with the plates reading the deflection for that station; then when



the plates read 14° the telescope will point along the forward tangent.

The location of curves by deflection angles is the normal method. A few other methods, to be described, should be considered as exceptional.

27. Curve location by two transits. A curve might be located more or less on a swamp where accurate chaining would be exceedingly difficult if not impossible. The long chord AB (Fig. 12) may be determined by triangulation or otherwise, and the elements of the curve computed, including (possibly) subchords at each end. The deflection from A and B to each point may be computed. A rodman may then be sent (by whatever means) to locate long stakes at points determined by the simultaneous sightings of the two transits.

28. Curve location by tangential offsets. When a curve is very flat and no transit is at hand the following method may be used (see Fig. 13): Produce the back tangent as far forward as necessary. Compute the ordinates Oa', Ob', Oc', etc., and the abscissæ a'a, b'b, c'c, etc. If Oa is a full station (100 feet), then

$$\begin{array}{l}
Oa' = Oa' = 100 \cos \frac{1}{2}D, \ also = R \sin D; \\
Ob' = Oa' + a'b' = 100 \cos \frac{1}{2}D + 100 \cos \frac{3}{2}D, \\
also = R \sin 2D; \\
Oc' = Oa' + a'b' + b'c' = 100(\cos \frac{1}{2}D + \cos \frac{3}{2}D + \cos \frac{5}{2}D), \\
also = R \sin 3D;
\end{array}$$
(9)

etc.

$$\begin{array}{ll} a'a = & 100 \sin \frac{1}{2}D, \ \text{also} = R \ \text{vers} \ D; \\ b'b = a'a + b''b & = 100 \ \sin \frac{1}{2}D + 100 \ \sin \frac{3}{2}D, \\ also = R \ \text{vers} \ 2D; \\ c'c = b'b + c''c & = 100(\sin \frac{1}{2}D + \sin \frac{3}{2}D + \sin \frac{5}{2}D), \\ also = R \ \text{vers} \ 3D; \end{array} \right\}$$
(10)

etc.

The functions  $\frac{1}{2}D$ ,  $\frac{2}{3}D$ , etc., may be more conveniently used without logarithms, by adding the several natural trigonometrical functions and pointing off two decimal places. It may also be noted that Ob' (for example) is one half of the long chord for four stations; also that b'b is the middle ordinate for four stations. If the engineer is provided with tables giving the long chords and middle ordinates for various degrees of curvature, these quantities may be taken (perhaps by interpolation) from such tables.

If the curve begins or ends at a substation, the angles and terms will be correspondingly altered. The modifications may

§ 27.

be readily deduced on the same principles as above, and should be worked out as an exercise by the student.

In Table II are given the long chords for a 1° curve for various values of  $\Delta$ . Dividing the value as given by the degree of the curve, we have an approximate value which is amply close for low degrees of curvature, especially for laying out curves without a transit. For example, given a 4° 30' curve, required the ordinate Oc'. This is evidently one half of a chord of six stations, with  $\Delta = 27^{\circ}$ . Dividing 2675.1 (which is the long chord of a 1° curve with  $\Delta = 27^{\circ}$ ) by 4.5 we have 594.47; one half of this is the required ordinate, Oc' = 297.23. The exact value is 297.31, an excess of .08, or less than .03 of 1%. The true values are always slightly in excess of the value as computed from Table II.

*Exercise.* A 3° 40′ curve begins at sta. 18+70 and runs to sta. 23+60. Required the tangential offsets and their corresponding ordinates. The first ordinate =  $30 \cos \frac{1}{2} \left(\frac{30}{100} \times 3^{\circ} 40'\right) = 30 \times .99995 = 29.9985$ ; the offset =  $30 \sin 0^{\circ} 33' = 30 \times .0096 = 0.288$ . For the second full station (sta. 20) the ordinate =  $\frac{1}{2}$  long chord for  $\Delta = 2(1^{\circ} 06' + 3^{\circ} 40')$  with  $D = 3^{\circ} 40'$ . Dividing 476.12, from Table II, by  $3\frac{2}{3}$ , we have 129.85. Otherwise, by Eq. 9, the ordinate =  $30 \times \cos 0^{\circ} 33' + 100 \cos (1^{\circ} 06' + 1^{\circ} 50') = 0.288 + 5.12 = 5.41$ . Work out similarly the ordinates and offsets for sta. 21, 22, 23, and 23 + 60.

29. Curve location by middle ordinates. Take first the simpler case when the curve begins at an even station. If we consider (in Fig. 14) the curve produced back to z, the chord  $za = 2 \times 100 \cos \frac{1}{2}D$ ,  $A'a = 100 \cos \frac{1}{2}D$ , and  $A'A = am = zn = 100 \sin \frac{1}{2}D$ . Set off AA' perpendicular to the tangent and A'a parallel to the tangent. AA' = aa' = bb' = cc', etc. = 100 sin  $\frac{1}{2}D$ . Set off aa' perpendicular to a'A. Produce Aa' until a'b = A'a, thus determining b. Succeeding points of the curve may thus be determined indefinitely.

Suppose the curve begins with a subchord. As before  $ra = Am' = c' \cos \frac{1}{2}d'$ , and  $rA = am' = c' \sin \frac{1}{2}d'$ . Also  $sz = An' = c'' \cos \frac{1}{2}d''$ , and  $sA = zn' = c'' \sin \frac{1}{2}d''$ , in which (d' + d'') = D. The points z and a being determined on the ground, aa' may be computed and set off as before and the curve continued in

full stations. A subchord at the end of the curve may be located by a similar process.

30. Curve location by offsets from the long chord. (Fig. 16.) Consider at once the general case in which the curve commences with a subchord (curvature, d'), continues with one or more full

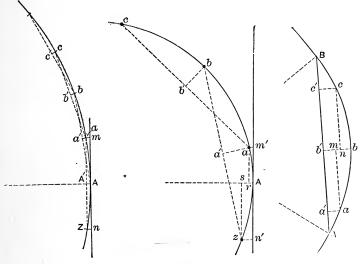


FIG. 14.



FIG. 16.

chords (curvature of each, D), and ends with a subchord with curvature d''. The numerical work consists in computing first AB, then the various abscissæ and ordinates.  $AB = 2R \sin \frac{1}{2}d$ .

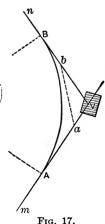
$$\begin{aligned} Aa' = Aa' &= e' \cos \frac{1}{2}(d - d'); \\ Ab' = Aa' + a'b' &= c' \cos \frac{1}{2}(d - d') + 100 \cos \frac{1}{2}(d - 2d' - D); \\ Ac' = Aa' + a'b' + b'c' = c' \cos \frac{1}{2}(d - d') + 100 \cos \frac{1}{2}(d - 2d' - D) \\ &+ 100 \cos \frac{1}{2}(d - 2d'' - D); \end{aligned}$$
(11)  
also  
$$= AB - Bc' = 2R \sin \frac{1}{2}d - c'' \cos \frac{1}{2}(d - d''). \\ a'a = a'a &= c' \sin \frac{1}{2}(d - d'); \\ b'b = a'a + mb = c' \sin \frac{1}{2}(d - d') + 100 \sin \frac{1}{2}(d - 2d' - D); \\ c'c = b'b - nb = c' \sin \frac{1}{2}(d - d') + 100 \sin \frac{1}{2}(d - 2d' - D); \\ -100 \sin \frac{1}{2}(d - 2d'' - D); \end{aligned}$$
(12)  
also  
$$= c'' \sin \frac{1}{2}(d - d''). \end{aligned}$$

The above formulæ are considerably simplified when the

curve begins and ends at even stations. When the curve is very long a regular law becomes very apparent in the formation of all terms between the first and last. There are too few terms in the above equations to show the law.

31. Use and value of the above methods. The chief value of the above methods lies in the possibility of doing the work without a transit. The same principles are sometimes employed, even when a transit is used, when obstacles prevent the use of the normal method (see § 32, c). If the terminal tangents have already been accurately determined, these methods are useful to locate points of the curve when rigid accuracy is not essential. Track foremen frequently use such methods to lay out unimportant sidings, especially when the engineer and his transit are not at hand. Location by tangential offsets (or by offsets from the long chord) is to be preferred when the curve is flat (i.e., has a small central angle 4) and there is no obstruction along the tangent, or long chord. Location by middle ordinates may be employed regardless of the length of the curve, and in cases when both the tangents and the long chord are obstructed. The above methods are but samples of a large number of similar methods which have been devised. The choice of the particular method to be adopted must be determined by the local conditions.

32. Obstacles to location. In this section will be given only



a few of the principles involved in this class of problems, with illustrations. The engineer must decide, in each case, which is the best method to use. It is frequently advisable to devise a special solution for some particular case.

a. When the vertex is inaccessible. As shown in § 26, it is not absolutely essential that the vertex of a curve should be located on the ground. But it is very evident that the angle between the terminal tangents is determined with far less probable error if it is measured by a single measurement at the vertex rather than as the result of numerous angle measurements along the curve, involving several posi-

tions of the transit and comparatively short sights. Some-

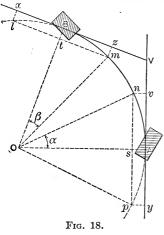
times the location of the tangents is already determined on the ground (as by bn and am, Fig. 17), and it is required to join the tangents by a curve of given radius. Method. Measure ab and the angles Vba and baV.  $\Delta$  is the sum of these angles. The distances bV and aV are computable from the above data. Given  $\Delta$  and R, the tangent distances are computable, and then Bb and aA are found by subtracting bV and aV from the tangent distances. The curve may then be run from A, and the work may be checked by noting whether the curve as run ends at B—previously located from b.

*Example.* Assume  $ab = 546\ 82$ ; angle  $a = 15^{\circ}\ 18'$ ; angle  $b = 18^{\circ}\ 22'$ ;  $D = 3^{\circ}\ 40'$ ; required aA and bB.  $d = 15^{\circ}\ 18' + 18^{\circ}\ 22' = 33^{\circ}\ 40'$ 

Eq. (4)	$\begin{array}{ccc} R & (3^{\circ}  40') \dots \\ \tan \frac{1}{2} \mathcal{A} = \tan  16^{\circ}  50' \dots \\ T = 472.85 \dots \end{array}$	$ \begin{array}{r} 3.1939\bar{2} \\ \underline{9.48080} \\ \underline{2.6747}\bar{2} \\ \hline \end{array} $
$aV = ab \frac{\sin 18^\circ 22'}{\sin 33^\circ 40'}$	ab log sin 18° 22' co-log sin 33° 40' aV = 310.81	$2.7378\bar{4} \\ 9.4984\bar{4} \\ 0.25621 \\ \hline 2.49250$
	AV = 472.85 aA = 162.04	
$bV = ab \frac{\sin 15^\circ 18'}{\sin 33^\circ 40'}$	ab log sin 15° 18' co-log sin 33° 40'	$2.7378ar{4}$ $9.4213ar{9}$ 0.25621
	bV = 260.29 BV = 472.85 bB = 212.56	2.41545
	010	

**b.** When the point of curve (or point of tangency) is inaccessible. At some distance (As, Fig. 18) an unobstructed line pn may be run parallel with AV. nv = py = As = R vers a.

• vers  $a = As \div R$ .  $ns = ps = R \sin c$ . At y, which is at a distance ps back from the *computed* position of A, make an offset sA



a chord may be run. a may equal any angle, but it is preferable that a should be a multiple of D, the degree of curve, and that the points m and n should be on even stations.  $mn = 2R \sin \frac{1}{2}a$ . А point s may be located by an offset ks from the chord mn by a similar method to that outlined in § 30.

The device of introducing the dotted curve mn having the same radius of curvature as the other, although neither necessary nor advisable in the case shown in Fig. 19, is sometimes the best method of surveying around an

curve at n makes an angle of awith np. From n the curve is run in as usual If the point of tangency is obstructed, a similar process, somewhat reversed, may be

to p. Run pn parallel to the tangent. A tangent to the

used.  $\beta$  is that portion of  $\Delta$  still to be laid off when m is reached.  $tm = tl = R \sin \beta$ . mz = tB = lx = Rvers  $\beta$ .

c. When the central part of the curve is obstructed. a is the central angle between two points of the curve between which

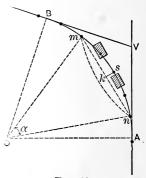


FIG. 19.

obstacle. The offset from any point on the dotted curve to the corresponding point on the true curve is twice the "ordinate to the long chord," as computed in § 30.

33. Modifications of location. The following methods may be used in allowing for the discrepancies between the "paper location" based on a more or less rough preliminary survey and the more accurate instrumental location. (See § 15.) They are

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#### ALIGNMENT.

also frequently used in locating new parallel tracks and modifying old tracks.

a. To move the forward tangent parallel to itself a distance x, the point of curve (A) remaining fixed. (Fig. 20.)

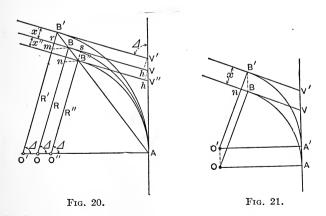
V'h = R'r = r'

$$AV' = AV + VV'$$
.

The triangle BmB' is isosceles and Bm = B'm.

$$R' - R = O'O = mB = \frac{B'r}{\operatorname{vers} B'mB} = \frac{x'}{\operatorname{vers} 4}.$$
  
$$\therefore R' = R + \frac{x'}{\operatorname{vers} 4}.$$
 (14)

The solution is very similar in case the tangent is moved inward to V''B''. Note that this method necessarily changes the



radius. If the radius is not to be changed, the point of curve must be altered as follows:

b. To move the forward tangent parallel to itself a distance x, the radius being unchanged. (Fig. 21.) In this case the whole

§ 33.

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curve is moved bodily a distance OO' = AA' = VV' = BB', and moved parallel to the first tangent AV

$$BB' = \frac{B'n}{\sin nBB'} = \frac{x}{\sin d} = AA'. \qquad (15)$$

c. To change the direction of the forward tangent at the point of tangency. (Fig. 22.) This problem involves a change (a) in

the central angle and also requires a new radius. An error in the determination of the central angle furnishes an occasion for its use.  $R, \Delta, a, AV$ , and BV are known.  $\Delta' = \Delta - a$ . Bs = R vers  $\Delta$ . Bs = R' vers  $\Delta'$ . Frg. 22.  $As = R \sin \Delta$ .  $A's = R' \sin \Delta'$ .

$$\therefore AA' = A's - As = R' \sin \Delta' - R \sin \Delta. \qquad (17)$$

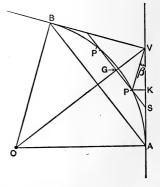
The above solutions are given to illustrate a large class of problems which are constantly arising. All of the ordinary problems can be solved by the application of elementary geometry and trigonometry.

34. Limitations in location. It may be required to run a curve that shall join two given tangents and also pass through a given point The point (P, Fig.

23) is assumed to be determined by its distance (VP) from the vertex and by the angle  $AVP = \beta$ .

It is required to determine the radius (R) and the tangent distance (AV).  $\varDelta$  is known.

$$PVG = \frac{1}{2}(180^{\circ} - 4) - \beta$$
  
= 90^{\circ} - ( $\frac{1}{2}4 + \beta$ ).  
$$PP' = 2VP \sin PVG$$
  
= 2VP cos ( $\frac{1}{2}4 + \beta$ ).  
$$PSV = \frac{1}{2}4.$$
  
$$\therefore SP = VP \frac{\sin \beta}{\sin \frac{1}{2}4}.$$





$$AS = \sqrt{SP \times SP'} = \sqrt{SP(SP + PP')}$$
$$= \sqrt{VP \frac{\sin \beta}{\sin \frac{1}{2}d}} \left[ VP \frac{\sin \beta}{\sin \frac{1}{2}d} + 2VP \cos \left(\frac{1}{2}d + \beta\right) \right]$$
$$= VP \sqrt{\frac{\sin^2 \beta}{\sin^2 \frac{1}{2}d} + \frac{2 \sin \beta \cos \left(\frac{1}{2}d + \beta\right)}{\sin \frac{1}{2}d}}.$$

$$SV = VP \frac{\sin\left(\frac{1}{2}d + p\right)}{\sin\left(\frac{1}{2}d\right)}$$

AV = AS + SV=  $\frac{VP}{\sin\frac{1}{2}d} [\sin(\frac{1}{2}d + \beta) + \sqrt{\sin^2\beta + 2\sin\beta\sin\frac{1}{2}d\cos(\frac{1}{2}d + \beta)}].$  (18)  $R = AV \cot \frac{1}{2}d.$ 

In the special case in which P is on the median line OV,  $\beta = 90^{\circ} - \frac{1}{2}A$ , and  $(\frac{1}{2}A + \beta) = 90^{\circ}$ . Eq. 18 then reduces to

$$AV = \frac{VP}{\sin \frac{1}{2}\mathcal{A}} (1 + \cos \frac{1}{2}\mathcal{A}) = VP \cot \frac{1}{4}\mathcal{A},$$

as might have been immediately derived from Eq. 8.

In case the point P is given by the offset PK and by the distance VK, the triangle PKV may be readily solved, giving the distance VP and the angle  $\beta$ , and the remainder of the solution will be as above.

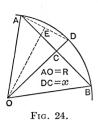
35. Determination of the curvature of existing track. (a) Using a transit. Set up the transit at any point in the center of the track. Measure in each direction 100 feet to points also in the center of the track. Sight on one point with the plates at  $0^{\circ}$ . Plunge the telescope and sight at the other point. The angle between the chords equals the degree of curvature.

(b) Using a tape and string. Stretch a string (say 50 feet long) between two points on the inside of the head of the outer rail. Measure the ordinate (x) between the *middle* of the string and the head of the rail. Then

$$R = \frac{\text{chord}^2}{8x} \text{(very nearly)}. \quad . \quad . \quad . \quad (19)$$

For, in Fig. 24, since the triangles AOE and ADC are similar.

AO: AE:: AD: DC or  $R = \frac{1}{2}\overline{AD^2} \div x$ . When, as is usual,



the arc is very short compared with the radius,  $AD = \frac{1}{2}AB$ , very nearly. Making this substitution we have Eq. 19. With a chord of 50 feet and a 10° curve, the resulting difference in x is .0025 of an inch—far within the possible accuracy of such a method. The above method gives the radius of the inner head of the outer rail. It should be diminished by  $\frac{1}{3}a$  for the radius

of the center of the track. With easy curvature, however, this will not affect the result by more than one or two tenths of one per cent.

The inversion of this formula gives the required middle ordinate for a rail on a given curve. For example, the middle ordinate of a 30-foot rail, bent for a  $6^{\circ}$  curve, is

 $x = 900 \div (8 \times 955) = .118$  foot = 1.4 inches.

Another much used rule is to require the foreman to have a string, knotted at the center, of such length that the middle ordinate, measured in inches, equals the degree of curve. To find that length, substitute (in Eq. 19)  $5730 \div D$  for R and  $D \div 12$  for x. Solving for *chord*, we obtain *chord*=61.8 feet. The rule is not theoretically exact, but, considering the uncertain stretching of the string, the error is insignificant. In fact, the distance usually given is 62 feet, which is close enough for all purposes for which such a method should be used.

36. Problems. A systematic method of setting down the solution of a problem simplifies the work. Logarithms should always be used, and *all* the work should be so set down that a revision of the work to find a supposed error may be readily done. The value of such systematic work will become more apparent as the problems become more complicated. The two solutions given below will illustrate such work.

a. Given a 3° curve beginning at Sta. 27+60 and running to Sta. 32+45. Compute the ordinates and offsets used in locating the curve by tangential offsets.

b. With the same data as above, compute the distances to locate the curve by offsets from the long chord.

c. Assume that in Fig. 17 ab is measured as 217.6 feet, the

#### ALIGNMENT.

angle  $abV = 17^{\circ} 42'$ , and the angle  $baV = 21^{\circ} 14'$ . Join the tangents by a 4° 30' curve. Determine bB and aA.

d. Assume that in a case similar to Fig. 18 it was noted that a distance (As) equal to 12 feet would clear the building. Assume that  $\Delta = 38^{\circ} 20'$  and that  $D = 4^{\circ} 40'$ . Required the value of a and the position of n. Solution:

vers 
$$a = As \div R$$
 $As = 12$  $\log = 1.07918$  $R$  (for 4° 40′ curve) $\log = 3.0892\bar{3}$  $a = 8° 01′$  $\log vers a = \overline{7.98994}$  $ns = R \sin a$  $\log \sin a = 9.1444\bar{5}$  $ns = 171.27$  $\log = 2.23369$ 

e. Assume that the forward tangent of a  $3^{\circ} 20'$  curve having a central angle of  $16^{\circ} 50'$  must be moved 3.62 feet *inward*, without altering the *P.C.* Required the change in radius.

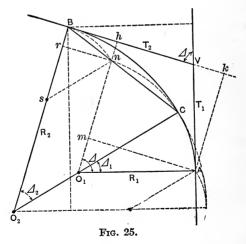
f. Given two tangents making an angle of  $36^{\circ} 18'$ . It is required to pass a curve through a point 93.2 feet from the vertex, the line from the vertex to the point making an angle of  $42^{\circ} 21'$  with the tangent. Required the radius and tangent distance. Solution: Applying Eq. 18, we have

2	$\log = 0.30103$
$\beta = 42^{\circ} 21'$	$\log \sin = 9.82844$
$\frac{1}{2}J = 18^{\circ} 09'$	$\log \sin = 9.4934\overline{6}$
$(\frac{1}{2}\Delta + \beta) = 60^{\circ} 30'$	$\log \cos = 9.69234$
.20667	$9.3152\overline{7}$
$\log \sin^2 \beta = 9.65688$	
29.81987	
$9.9099\bar{3}$	
nat. $\sin 60^{\circ} 30' \dots .870\bar{3}$	
$1.683\bar{0}$	$\dots \log = 0.22610$
- VP = 93.2	$\dots \log = 1.9694\bar{1}$
	$2.1955\bar{1}$
	$\log \sin \frac{1}{2} d = 9.4934 \bar{6}$
Tang. dist. $AV = 503.36$	
Contraction and an an	$\log \cot \frac{1}{2} d = 10.48437$
R = 1536.1	$\log \cos \frac{10}{22} = 10.10101$
$D = 3^{\circ} 44'$	

#### COMPOUND CURVES.

37. Nature and use. Compound curves are formed by a succession of two or more simple curves of different curvature. The curves must have a common tangent at the point of compound curvature (*P.C.C.*). In mountainous regions there is frequently a necessity for compound curves having several changes of curvature. Such curves may be located separately as a succession of simple curves, but a combination of two simple curves has special properties which are worth investigating and utilizing. In the following demonstrations  $R_2$  always represents the *longer* radius and  $R_1$  the *shorter*, no matter which succeeds the other.  $T_1$  is the tangent adjacent to the curve of shorter radius  $(R_1)$ , and is invariably the shorter tangent.  $\mathcal{L}_1$  is the central angle of the curve of radius  $R_1$ , but it may be greater or less than  $\mathcal{L}_2$ 

38. Mutual relations of the parts of a compound curve having two branches.' In Fig. 25, AC and CB are the two branches of



the compound curve having radii of  $R_1$  and  $R_2$  and central angles of  $\Delta_1$  and  $\Delta_2$ . Produce the arc AC to n so that  $AO_1n = \Delta$ . The chord Cn produced must intersect B. The line ns, parallel to  $CO_2$ , will intersect  $BO_2$  so that  $Bs = sn = O_2O_1 = R_2 - R_1$ . Draw Am perpendicular to  $O_1n$ . It will be parallel to hk.

$$Br = sn \text{ vers } Bsn = (R_2 - R_1) \text{ vers } d_2;$$
  

$$mn = AO_1 \text{ vers } AO_1n = R_1 \text{ vers } d;$$
  

$$Ak = AV \sin AVk = T_1 \sin d;$$
  

$$Ak = hm = mn + nh = mn + Br.$$
  

$$T_1 \sin d = R_1 \text{ vers } d + (R_2 - R_1) \text{ vers } d_2.$$
 (20)

Similarly it may be shown that

$$T_2 \sin \Delta = R_2 \text{ vers } \Delta - (R_2 - R_1) \text{ vers } \Delta_1. \quad . \quad (21)$$

The mutual relations of the elements of compound curves may be solved by these two equations. For example, assume the tangents as fixed ( $\Delta$  therefore known) and that a curve of given radius  $R_1$  shall start from a given point at a distance  $T_1$ from the vertex, and that the curve shall continue through a given angle  $\Delta_1$ . Required the other parts of the curve. From Eq. 20 we have

$$R_2 - R_1 = \frac{T_1 \sin \Delta - R_1 \operatorname{vers} \Delta}{\operatorname{vers} \Delta_2}.$$
  

$$\therefore R_2 = R_1 + \frac{T_1 \sin \Delta - R_1 \operatorname{vers} \Delta}{\operatorname{vers} (\Delta - \Delta_1)}. \quad (22)$$

 $T_2$  may then be obtained from Eq. 21.

As another problem, given the location of the two tangents, with the two tangent distances (thereby locating the PC and PT), and the central angle of each curve; required the two radii. Solving Eq. 20 for  $R_1$ , we have

$$R_1 = \frac{T_1 \sin \varDelta - R_2 \operatorname{vers} \varDelta_2}{\operatorname{vers} \varDelta - \operatorname{vers} \varDelta_2}.$$

Similarly from Eq. 21 we may derive

$$R_1 = \frac{T_2 \sin \varDelta - R_2 (\text{vers } \varDelta - \text{vers } \varDelta_1)}{\text{vers } \varDelta_1}.$$

Equating these, reducing, and solving for  $R_2$ , we have

$$R_2 = \frac{T_1 \sin \Delta \operatorname{vers} \Delta_1 - T_2 \sin \Delta \operatorname{(vers} \Delta - \operatorname{vers} \Delta_2)}{\operatorname{vers} \Delta_2 \operatorname{vers} \Delta_1 - (\operatorname{vers} \Delta - \operatorname{vers} \Delta_1) (\operatorname{vers} \Delta - \operatorname{vers} \Delta_2)}.$$
 (23)

Although the various elements may be chosen as above with considerable freedom, there are limitations. For example, in Eq. 22, since  $R_2$  is always greater than  $R_1$ , the term to be added to  $R_1$  must be essentially positive—i.e.,  $T_1 \sin A$  must be greater than  $R_1$  vers A. This means that  $T_1 > R_1 \frac{\text{vers } A}{\sin A}$ , or that

 $T_1 > R_1 \tan \frac{1}{2} d$ , or that  $T_1$  is greater than the corresponding tangent on a simple curve. Similarly it may be shown that  $T_2$  is less than  $R_2 \tan \frac{1}{2} d$  or less than the corresponding tangent on a simple curve. Nevertheless  $T_2$  is always greater than  $T_1$ . In the limiting case when  $R_2 = R_1$ ,  $T_2 = T_1$ , and  $d_2 = d_1$ .

**39.** Modifications of location. Some of these modifications may be solved by the methods used for simple curves. For example:

a. It is desired to move the tangent VB, Fig. 26, parallel to itself to V'B'. Run a new curve from the *P.C.C.* which shall reach the new tangent at B', where the chord of the old curve

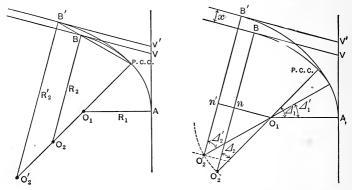


FIG. 26.

FIG. 27.

intersects the new tangent. The solution is almost identical with that in § 33, a.

b. Assume that it is desired to change the forward tangent (as above) but to retain the same radius. In Fig. 27

$$\begin{array}{l}
(R_2 - R_1) \cos \Delta_2 = O_2 n; \\
(R_2 - R_1) \cos \Delta_2' = O_2' n'. \\
x = O_2 n - O_2' n' = (R_2 - R_1)(\cos \Delta_2 - \cos \Delta_2'). \\
\cos \Delta_2' = \cos \Delta_2 - \frac{x}{R_2 - R_1}. \quad . \quad . \quad . \quad (24)
\end{array}$$

The *P.C.C.* is moved backward along the sharper curve an angular distance of  $d_2' - d_2 = d_1 - d_1'$ .

In case the tangent is moved inward rather than outward, the solution will apply by transposing  $\Delta_2$  and  $\Delta_2'$ . Then we shall have

$$\cos \Delta_2' = \cos \Delta_2 + \frac{x}{R_2 - R_1}$$
. . . . (25)

The P.C.C. is then moved forward.

c. Assume the same case as (b) except that the larger radius comes first and that the tangent adjacent to the smaller radius is moved. In Fig. 28

$$(R_2 - R_1) \cos \Delta_1 = O_1 n;$$
  

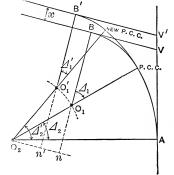
$$(R_2 - R_1) \cos \Delta_1' = O_1' n'.$$
  

$$x = O_1' n' - O_1 n$$
  

$$= (R_2 - R_1) (\cos \Delta_1' - \cos \Delta_1).$$

$$\cos \Delta_1' = \cos \Delta_1 + \frac{x}{R_2 - R_1}, \quad (26)$$

The P.C.C. is moved forward along the easier curve an angular distance of  $\Delta_1' - \Delta_1 = \Delta_2 - \Delta_2'$ .



F1G. 28.

In case the tangent is moved *inward*, transpose as before and we have

$$\cos \Delta_1' = \cos \Delta_1 - \frac{x}{R_2 - R_1} \dots \dots \dots (27)$$

The P.C.C. is moved backward.

**d.** Assume that the radius of one curve is to be altered without changing either tangent. Assume conditions as in Fig. 29.

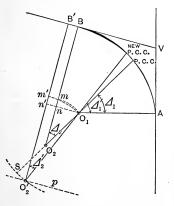


FIG. 29.

curve produced at NEW P.C.C.

For the diagrammatic solution assume that  $R_2$  is to be increased by  $O_2S$ . Then, since  $R_2'$  must pass through  $O_1$  and extend beyond  $O_1$  a distance  $O_1S$ , the locus of the new center must lie on the arc drawn about  $O_1$  as center and with OS as radius. The locus of  $O_2'$  is also given by a line  $O_2'p$  parallel to BVand at a distance of  $R_2'$  (equal to  $S \dots P.C.C.$ ) from it. The new center is therefore at the intersection  $O_2'$ . An arc with radius  $R_2'$  will therefore be tangent at B' and tangent to the old Draw  $O_1n'$  perpendicular to  $O_2B_1$ .

With  $O_2$  as center draw the arc  $O_1m$ , and with  $O_2'$  as center draw the arc  $O_1m'$ .  $mB = m'B' = R_1$ .

:. 
$$mn = m'n' = (R_2' - R_1)$$
 vers  $\Delta_2' = (R_2 - R_1)$  vers  $\Delta_2$ .

:. vers 
$$\Delta_2' = \frac{(R_2 - R_1)}{(R_2' - R_1)}$$
 vers  $\Delta_2$ . . . . (28)

$$O_1 n = (R_2 - R_1) \sin \Delta_2;$$

$$O_1 n' = (R_2' - R_1) \sin \Delta_2'.$$

$$BB' = O_1 n' - O_1 n = (R_2' - R_1) \sin \Delta_2' - (R_2 - R_1) \sin \Delta_2.$$
(29)

This problem may be further modified by assuming that the radius of the curve is decreased rather than increased, or that the smaller radius follows the larger. The solution is similar and is suggested as a profitable exercise.

It might also be assumed that, instead of making a given change in the radius  $R_2$ , a given change BB' is to be made.  $\mathcal{A}_2'$ and  $R_2'$  are required. Eliminate  $R_2'$  from Eqs. 28 and 29 and solve the resulting equation for  $\mathcal{A}_2'$ . Then determine  $R_2'$ by a suitable inversion of either Eq. 28 or 29.

As in §§ 32 and 33, the above problems are but a few, although perhaps the most common, of the problems the engineer may meet with in compound curves. All of the ordinary problems may be solved by these and similar methods.

40. Problems. *a.* Assume that the two tangents of a compound curve are to be 348 feet and 624 feet, and that  $d_1 = 22^{\circ} 16'$  and  $d_2 = 28^{\circ} 20'$ . Required the radii.

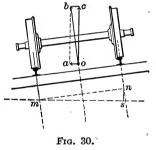
[Ans.  $R_1 = 326.92$ ;  $R_2 = 1574.85$ .]

b. A line crosses a valley by a compound curve which is first a 6° curve for 46° 30' and then a 9° 30' curve for 84° 16'. It is afterward decided that the last tangent should be 6 feet farther up the hill. What are the required changes? [Note. The second tangent is evidently moved outward. The solution corresponds to that in the first part of § 39, c. The P.C.C. is moved forward 16.39 feet. If it is desired to know how far the P.T. is moved in the direction of the tangent (i.e., the projection of BB', Fig. 28, on V'B'), it may be found by observing that it is equal to  $nn' = (R_2 - R_1)(\sin A_1 - \sin A_1')$ . In this case it equals 0.65 foot, which is very small because  $A_1$  is nearly 90°. The value of  $A_2$  (46° 30') is not used, since the solution is independent of the value of  $A_2$ . The student should learn to recognize which quantities are mutually related and therefore essential to a solution, and which are independent and non-essential.]

### TRANSITION CURVES.

41. Superelevation of the outer rail on curves. When a mass is moved in a circular path it requires a centripetal force to keep it moving in that path. By the principles of mechanics we know that this force equals  $Gv^2 \div gR$ , in which G is the weight, v the velocity in feet per second, g the acceleration of gravity in feet per second in a second, and R the radius of curvature. If the two rails of a curved track were laid on a level (transversely), this centripetal force could only be furnished by the pressure of the wheel-flanges against the rails. As this is very objectionable, the outer rail is elevated so that the reaction of

the rails against the wheels shall contain a horizontal component equal to the required centripetal force. In Fig. 30, if *ob* represents the reaction, *oc* will represent the weight *G*, and *ao* will represent the required centripetal force. From similar triangles we may—write sn : sm :: ao : oc. Call g = 32.17. Call  $R = 5730 \div D$ , which is sufficiently accurate for this purpose (see



§ 19). Call  $v = 5280V \div 3600$ , in which V is the velocity in miles per hour. mn is the distance between rail centers, which, for an 80-lb. rail and standard gauge, is 4.916 feet  $\cdot$  sm is slightly less than this. As an average value we may call it 4.900, which is its exact value when the superelevation is  $4\frac{3}{4}$  inches. Calling sn = e, measured in feet, we have

$$e = sm\frac{ao}{oc} = 4.9 \frac{Gv^2}{gR} \frac{1}{G} = \frac{4.9 \times 5280^2 V^2 D}{32.17 \times 3600^2 \times 5730}.$$

$$e = .0000572 V^2 D. \tag{30}$$

It should be noticed that, according to this formula, the required superelevation varies as the square of the velocity, which means that a change of velocity of only 10% would call for a change of superelevation of 21%. Since the velocities of trains over any road are extremely variable, it is impossible to adopt any superelevation which will fit all velocities even approximately. The above fact also shows why any over-refinement in the calculations is useless and why the above approximations, which are really small, are amply justifiable. For example, the above formula contains the approximation that  $R = 5730 \div D$ . In the extreme case of a 10° curve the error involved would be about 1%. A change of about  $\frac{1}{2}$  of 1% in the velocity, or say from 40 to 40.2 miles per hour, would mean as much. The error in *e* due to the assumed constant value of *sm* is never more than a very small fraction of 1%. The rail-laying is not done closer than this The following tabular form is based on Eq. (30):

SUPERELEVATION OF THE OUTER RAIL (IN FEET) FOR VARIOUS VELOCITIES AND DEGREES OF CURVATURE.

Velocity in Miles per		Degree of Curve.								
Hour.	1°	2°	3°	4°	5°	6°	7°	8°	9°	10°
30 40	.05 .09	.10 .18	.15 .27	.20 .37	.26 .46	.31 .55	.36 .64	.41 .73	.46	.51
50 60	.14 .20	$.29 \\ .41$	.43 1.62	.57 .82	.71	.86				

42. Practical rules for superelevation. A much used rule for superelevation is to "elevate one half an inch for each degree of curvature." The rule is rational in that e in Eq. 30 varies directly as D. The above rule therefore agrees with Eq. 30 when V is about 27 miles per hour. However applicable the rule may have been in the days of low velocities, the elevation thus computed is too small now. The rule to elevate one inch for each degree of curvature is also used and is precisely similar in its nature to the above rule. It agrees with Eq. 30 when the velocity is about 38 miles per hour, which is more nearly the average speed of trains.

Another (and better) rule is to "elevate for the speed of the fastest trains." This rule is further justified by the fact that a four-wheeled truck, having two parallel axles, will always tend to run to the outer rail and will require considerable flange pressure to guide it along the curve. The effect of an excess of superelevation on the slower trains will only be to relieve this flange pressure somewhat. This rule is coupled with the limitation that the elevation should never exceed a limit of six inches sometimes eight inches. This limitation implies that locomotive engineers must reduce the speed of fast trains around sharp curves until the speed does not exceed that for which the actual superelevation used is suitable. The heavy line in the tabular form (§ 41) shows the six-inch limitation.

Some roads furnish their track foremen with a list of the superelevations to be used on each curve in their sections. This method has the advantage that each location may be separately studied, and the proper velocity, as affected by local conditions (e.g., proximity to a stopping-place for all trains), may be determined and applied.

Another method is to allow the foremen to determine the superelevation for each curve by a simple measurement taken at the curve. The rule is developed as follows: By an inversion of Eq. 19 we have

$$x = chord^2 \div 8R. \qquad (31)$$

Putting x equal to e in Eq. 30 and solving for "chord," we have

$$chord^{2} = .0000572V^{2}D\otimes\mathbb{R}$$
  
=2.621V<sup>2</sup>.  
$$chord = 1.62V.$$
 (32)

To apply the rule, assume that 50 miles per hour is fixed as the velocity from which the superelevation is to be computed. Then  $1.62V=1.62\times50=81$  feet, which is the distance given to the trackmen. Stretch a tape (or even a string) with a length of 81 feet between two points on the concave side of the head of cither the inner or the outer rail. The ordinate at the middle point then equals the superelevation. The values of this chord length for varying velocities are given in the accompanying tabular form.

1		1		1				1	1
Velocity in miles per hour	20	25	30	35	40	45	50	55	60
Chord length in feet	32.4	40.5	48.6	56.7	64.8	72.9	81.0	89.1	97.2
				I .				]	

The following tabular form shows the standard (at one time) on the N. Y., N. H. & H. R. R. It should be noted that the elevations do not increase proportionately with the radius, and that they are higher for descending grades than for level or

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ascending grades. This is on the basis that the velocity on curves and on ascending grades will be less than on descending grades. For example, the superelevation for a  $0^{\circ} 30'$  curve on a descending grade corresponds to a velocity of about 54 miles per hour, while for a  $4^{\circ}$  curve on a level or ascending grade the superelevation corresponds to a velocity of only about 38 miles per hour.

TABLE OF THE	SUPERELEVATION	OF THE	OUTER	RAIL	ON	CURVES.
	N. Y., N. I	н. & н. в	. R.			

Degree of	Level or as-	Descending
curve.	cending grade.	grade.
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	inches. 03 15 15 2 2 2 2 2 2 2 2 2 3 3 5 3 5 5 3 5 5 5 5	inches. 1 1 2 2 2 2 4 2 2 4 3 3 4 3 4 3 4 4 4 4 4 4 4 2 2 4 4 4 4 4 4 4 4 4 4 4 4 4

43. Transition from level to inclined track. On curves the track is inclined transversely; on tangents it is level. The transition from one condition to the other must be made gradually. If there is no transition curve, there must be either inclined track on the tangent or insufficiently inclined track on the curve or both. Sometimes the full superelevation is continued through the total length of the curve and the "run-off" (having a length of 100 to 400 feet) is located entirely on the tangents at each In other practice it is located partly on the tangent and end. partly on the curve. Whatever the method, the superelevation is correct at only one point of the run-off. At all other points it is too great or too small. This (and other causes) produces objectionable lurches and resistances when entering and leaving curves. The object of transition curves is to obviate these resistances.

On the Lehigh Valley R. R. the run-off is made in the form of a reversed vertical curve, as shown in the accompanying figure. According to this system the length of run-off varies

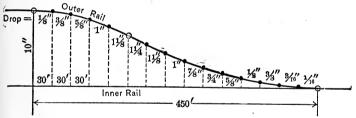
#### ALIGNMENT.

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from 120 feet, for a superelevation of one inch, to 450 feet, for a superelevation of ten inches. Such a superelevation as ten inches is very unusual practice, but is successfully operated on that road. The curve is concave upward for twothirds of its length and then reverses so that it is convex upward. TABLE FOR RUN-OFF OF ELEVATION OF OUTER RAIL OF CURVES.

Drop in inches for each 30-foot rail commencing at theoretical point of curve.

Eleva-	<del>1</del> ″	ŧ"	3"	<u>1</u> "	<del>§</del> ″	<u>3</u> ″	<del>7</del> ″	1″	1 <del>]</del> ″	1 <del>1</del> ″	1 <del>1</del> ″	1″	<del>7</del> ″	<u>3</u> ″	<u>5</u> ″	1 <u>2</u> "	<u>3</u> ″	ł″	13″ 13	<del>1</del> 8″	₽ <b>6</b> ″	Total.
				-									-									
1″	1	30	30		1		1	1				1		1				30		30		120
2″	1	30	1		Í	30		۱		1			1	1		30	30			30		150
3″		30				30					1	1	30	1	30		30			30		180
4″	1	30		30			30						30		30			30		30		240
1" 2" 3" 4" 5" 6" 7" 8" 9" 10"	1::	30		30				$\dot{30}$				$ \dot{30}$			30			30		30		270
6"	1	30		30		i	$\dot{30}$		30		i	30			30					30		300
7//	1	30		30			30		30		30	30			30			30		30		330
										·				100	30							
8″	1	30		30		30			30	30	30	30		30	30		30		30			360
9″	30		I	30	1	30	1	30	30		30	30	30	30	30	30	30				30	420
10″	30		30		30			30	30 30	30	30	30	130	30	30	30	30		30		30	450
	00	t	100	· · ·	100																	



The figure (and also the lower line of the tabulated form) shows the drop for each thirty-foot rail length. For shorter lengths of run-off, the drop for each 30 feet is shown by the corresponding lines in the tabular form. Note in each horizontal line that the sum of the drops, under which 30 is found, equals the total superelevation as found in the first column. For example, for 4 inches superelevation, length of curve 240 feet, the successive drops are  $\frac{1}{4}$ ,  $\frac{1}{2}$ ,  $\frac{7}{8}$ ,  $\frac{5}{8}$ ,  $\frac{1}{2}$ ,  $\frac{1}{4}$ , and  $\frac{1}{8}$ , whose sum is 4 inches. Possibly the more convenient form would be to indicate for each 30-foot point the actual superelevation of the outer rail, which would be for the above case (running from the tangent to the curve)  $\frac{1}{8}$ ,  $\frac{3}{8}$ ,  $\frac{7}{8}$ ,  $1\frac{12}{7}$ ,  $2\frac{3}{8}$ ,  $3\frac{1}{4}$ ,  $3\frac{3}{4}$ , 4.

44. Fundamental principle of transition curves. If a curve

has variable curvature, beginning at the tangent with a curve of infinite radius, and the curvature gradually sharpens until it equals the curvature of the required simple curve and there becomes tangent to it, the superelevation of such a transition curve may begin at zero at the tangent, gradually increase to the required superelevation for the simple curve, and yet have at every point the superelevation required by the curvature at that point. Since in Eq. (30) e is directly proportional to D, the required curve must be one in which the degree of curve increases directly as the distance along the curve. The mathematical development of such a curve is quite complicated. It has, however, been developed, and tables have been computed for its use, by Prof. C. L. Crandall. The following method has the advantage of great simplicity, while its agreement with the true transition curve is as close as need be, as will be shown.

45. Multiform compound curves. If the transition curve commences with a very flat curve and at regular even chord lengths compounds into a curve of sharper curvature until the desired curvature is reached, the increase in curvature at each chord point being uniform, it is plain that such a curve is a close approximation to the true spiral, especially since the rails as laid will gradually change their curvature rather than maintain a uniform curvature throughout each chord length and then abruptly change the curvature at the chord points. Such a curve, as actually laid, will be a much closer approximation to the true curve than the multiform compound curve by which it is set out. There will actually be a gradual increase in curvature which increases directly as the length of the curve.

46. Required length of spiral. The required length of spiral evidently depends on the amount of superelevation to be gained, and also depends somewhat on the speed. If the spiral is laid off in 25-foot chord lengths, with the first chord subtending a 1° curve, the second a 2° curve, etc., the fifth chord will subtend a 5° curve, and the increase from this last chord to a 6° curve is the same as the uniform increase of curvature between the chords. The same spiral extended would run on to a 12° curve in (12-1)25=275 feet. The last chord of a spiral should have a smaller degree of curvature than the simple curve to which it is joined. If the curves are very sharp, such as are used in street work and even in suburban trolley work, an increase in degree of curvature of 1° per 25 feet will not be sufficiently rapid, as

such a rate would require too long curves. 2°, 10°, or even 20° increase per 25 feet may be necessary, but then the chords

should be reduced to 5 feet. Such a rapid rate of increase is justified by the necessary reduction in speed. On the other hand, very high speed will make a lower rate of increase desirable, and therefore a spiral whose degree of curvature increases only 0° 30' per 25 feet may be used. Such a spiral would require a length of 375 feet to run on to an 8° curve, which is inconveniently long, but it might be used to run on to a 4° curve, where its length would be only 175 feet. Three spirals have been developed in Table IV, each with chords of 25 feet, the rate of increase in the degree of curvature being 0° 30', 1° and 2° per chord. One of these will be suitable for any curvature found on ordinary steam-railroads.

47. To find the ordinates of a  $1^{\circ}$ -per-25-feet spiral. Since the

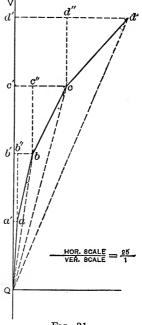


FIG. 31.

first chord subtends a 1° curve, its central angle is 0° 15' and the angle aQV (Fig. 31) is 7' 30". The tangent at a makes an angle of 15' with VQ. The angle between the chord ba and the tangent at a is  $\frac{1}{2}(30')=15'$ , and the angle  $bab''=\frac{1}{2}(30')+15'=30'$ . Similarly

the angle  $cbc'' = \frac{1}{2}(45') + 30' + 15' = 67' 30'' = 1^{\circ} 07' 30''$ , and the angle  $dcd'' = 2^{\circ} 0'$ .

The ordinate 
$$aa' = 25 \sin 7' 30''$$
, and  
 $Qa' = 25 \cos 7' 30''$ .  
 $Qb' = Qa' + a'b'$   
 $= Qa' + ab''$   
 $= 25 (\cos 7' 30'' + \cos 30')$ .  
 $bb' = b'b'' + bb''$   
 $= 25 (\sin 7' 30'' + \sin 30')$ .

Similarly the ordinates of c, d, etc., may be obtained.

48. To find the deflections from any point of the spiral. aQV=7'30''. Tan  $bQV=bb'\div Qb'$ ; tan  $cQV=cc'\div Qc'$ ; etc. Thus we are enabled to find the deflection angles from the tangent at Q to any point of the spiral.

The tangent to the curve at c (Fig. 32) makes an angle of

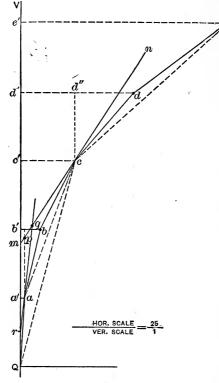


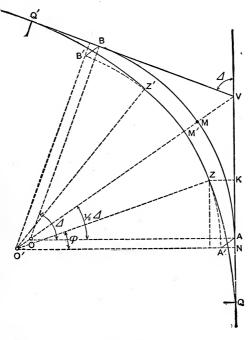
Fig. 32.

1° 30' with QV, or  $cmV=1^{\circ}30'$ . Qcm=cmV-cQm. The value of cQm is known from previous work. The deflection from c to Q then becomes known.

acm = cmV - cap = cmV - caq - qap. caq is the deflection angle to c from the tangent at a and will have been previously computed numerically. qap = 15'. acm therefore becomes known.

 $bcm = \frac{1}{2}$  of  $45' = 22' \ 30''$ ;  $dcn = \frac{1}{2}$  of 60' = 30'. ecn = ecd'' - ncd'', ncd'' = cmV, tan  $ecd'' = (ee' - d''d') \div c'e'$ , all cf which are known from the previous work.

By this method the deflections from the tangent at any point





of the curve to any other point are determinable. These values are compiled in Table IV. The corresponding values of these angles when the increase in the degree of curvature per chord length is 30', and when it is  $2^\circ$ , are also given in Table IV.

49. Connection of spiral with circular curve and with tangent. See Fig. 33.\* Let AV and BV be the tangents to be connected

<sup>\*</sup> The student should at once appreciate the fact of the necessary distortion of the figure. The distance MM' in Fig. 33 is perhaps 100 times its real proportional value.

by a  $D^{\circ}$  curve, having a suitable spiral at each end. If no spirals were to be used, the problem would be solved as in simple curves giving the curve AMB Introducing the spiral has the effect of throwing the curve away from the vertex a distance MM' and reducing the central angle of the  $D^{\circ}$  curve by  $2\phi$ . Continuing the curve beyond Z and Z' to A' and B', we will have AA'=BB'=MM'. ZK=the x ordinate and is therefore known. Call MM'=m. A'N=x-R vers  $\phi$ . Then

$$m = MM' = AA' = \frac{A'N}{\cos\frac{1}{2}d} = \frac{x - R \operatorname{vers} \phi}{\cos\frac{1}{2}d}.$$
 (33)

$$NA = AA' \sin \frac{1}{2} d = (x - R \operatorname{vers} \phi) \tan \frac{1}{2} d.$$
  

$$VQ = QK - KN + NA + AV$$
  

$$= y - R \sin \phi + (x - R \operatorname{vers} \phi) \tan \frac{1}{2} d + R \tan \frac{1}{2} d$$
  

$$= y - R \sin \phi + x \tan \frac{1}{2} d + R \cos \phi \tan \frac{1}{2} d. \quad . \quad . \quad . \quad (34)$$

When A'N has already been computed, it may be more convenient to write

$$VQ = y + R (\tan \frac{1}{2}A - \sin \phi) + A'N \tan \frac{1}{2}A.$$
 (35)

$$VM' = VM + MM'$$

$$=R \operatorname{exsec} \frac{1}{2} d + \frac{x}{\cos \frac{1}{2} d} - \frac{R \operatorname{vers} \phi}{\cos \frac{1}{2} d}. \quad . \quad . \quad . \quad (36)$$

$$AQ = VQ - AV$$
  
=  $y - R \sin \phi + (x - R \operatorname{vers} \phi) \tan \frac{1}{2}A$ . . . . (37)

A method of obtaining the necessary dimensions using tables, is given in § 53a.

*Example.* To join two tangents making an angle of 34° 20' by a 5° 40' curve and suitable spirals. Use 1°-per-25-feet spirals with five chords. Then  $\phi=3^{\circ}$  45', x=2.999,  $\frac{1}{2}A=17^{\circ}$  10', and y=124.942.

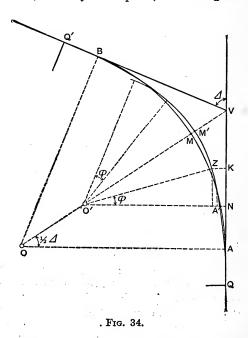
§ 50.

[Eq. 33]		R	3.00497
		vers $\phi$	7.33063
	2.166		0.33560
	x = 2.999		
	A'N = 0.833		$9.9206ar{4}$
		$\cos \frac{1}{2} d$	9.98021
	m = MM' = AA' = 0.872		$9.9404\overline{3}$
[Eq. 36]		R	3.00497
	e	$x \sec \frac{1}{2} d$	$8.6686\bar{3}$
	VM = 47.164		$\overline{1.67360}$
	m = 0.872		
	$VM' = \overline{48.036}$		
[Eq. 35]	$y = 124.942$ nat. $\overline{\tan \frac{1}{2}d} =$	.30891	
	nat. sin $\phi =$	.06540	
		.24351	$9.3865\bar{1}$
		R	3.00497
	246.314		$2.3914\overline{8}$
	[See above]	A'N	9.92064
		tan <u></u> ₄₄	9.48984
	0.257	АN	9.41048
	$VQ = \overline{371.513}$		a han make the shirts
[Eq. 37]	•	$\vec{R}$	3.00497
		$tan \frac{1}{2} I$	9.48984
	312 471	Ÿ	$\overline{2.49481}$
	AQ = 59.042		

50: Field-work. When the spiral is designed during the original location, the tangent distance VQ should be computed and the point Q located. It is hardly necessary to locate all of the points of the spiral until the track is to be laid. The extremities should be located, and as there will usually be one and perhaps two full station points on the spiral, these should also be located. Z may be located by setting off QK = y and KZ = x, or else by the tabular deflection for Z from Q and the distance ZQ, which is the long chord. Setting up the instrument at Z and sighting back at Q with the proper deflection, the tangent at Z may be found and the circular curve located as usual, its central angle being  $4-2\phi$ . A similar operation will locate Q' from Z'.

To locate points on the spiral. Set up at Q, with the plates

reading 0° when the telescope sights along VQ. Set off from Q the deflections given in Table IV for the instrument at Q, using a chord length of 25 feet, the process being like the method for simple curves except that the deflections are irregular. If a full station-point occurs within the spiral, interpolate between the deflections for the adjacent spiral-points. For example, a spiral begins at Sta. 56+15. Sta. 57 comes 10 feet beyond the third spiral point. The deflection for the third point is 35' 0''; for the fourth it is 56' 15''.  $\frac{1}{25}$  of the difference (21' 15'') is 8' 30''; the deflection for Sta. 57 is therefore 43' 30''. This method is not theoretically accurate, but the error is small. Arriving at Z, the forward alignment may be obtained by sighting back at Q (or at any other point) with the given deflection



for that point from the station occupied. Then when the plates read 0° the telescope will be tangent to the spiral and to the succeeding curve. All rear points should be checked from Z. If it is necessary to occupy an intermediate station, use the deflections given for that station, orienting as just explained for Z,

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checking the back points and locating all forward points up to Z if possible.

After the center curve has been located and Z' is reached, the other spiral must be located but *in reverse order*, i.e., the sharp curvature of the spiral is at Z' and the curvature decreases toward Q'.

51. To replace a simple curve by a curve with spirals. This may be done by the method of § 49, but it involves shifting the whole track a distance m, which in the given example equals 0.87 foot. Besides this the track is appreciably shortened, which would require rail-cutting. But the track may be kept at practically the same length and the lateral deviation from the old track may be made very small by slightly sharpening the curvature of the old track, moving the new curve so that it is wholly or partially *outside* of the old curve, the remainder of it with the spirals being *inside* of the old curve. It is found by experience that a decrease in radius of from 1% to 5% will answer the purpose. The larger the central angle the less the change. The solution is as indicated in Fig. 34.

$$O'N = R' \cos \phi + x.$$
  

$$O'V = O'N \sec \frac{1}{2}A$$
  

$$= R' \cos \phi \sec \frac{1}{2}A + x \sec \frac{1}{2}A.$$
  

$$m = MM' = MV - M'V$$
  

$$= R \operatorname{exsec} \frac{1}{2}A - (O'V - R')$$
  

$$= R \operatorname{exsec} \frac{1}{2}A - R' \cos \phi \sec \frac{1}{2}A - x \sec \frac{1}{2}A + R'... (38)$$
  

$$AQ = QK - KN + NV - VA$$
  

$$= y - R' \sin \phi + (R' \cos \phi + x) \tan \frac{1}{2}A - R \tan \frac{1}{2}A$$
  

$$= y - R' \sin \phi + R' \cos \phi \tan \frac{1}{2}A - (R - x) \tan \frac{1}{2}A... (39)$$

The length of the old curve from Q to  $Q' = 2AQ + 100\frac{\Delta}{D}$ .

The length of the new curve from Q to  $Q'=2L+100\frac{d-2\phi}{D'}$ , in which L is the length of each spiral.

**Example.** Suppose the old curve is a 7° 30' curve with a central angle of 38° 40'. As a trial, compute the relative length of a new 8° curve with spirals of seven chords.  $\phi = 7^{\circ} 0'$ ;  $\frac{1}{2}d = 19^{\circ} 20'$ ; R (for the 7° 30' curve) = 764.489; R' (for the 8° curve) = 716.779; x = 7.628.

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§ 51.

#### RAILROAD CONSTRUCTION.

§ 52.

[Eq. 38]		· R 2.88337
	$45.687 \\ R' = 716.779$	$\frac{\text{exsec } \frac{1}{2}4}{1.65979}$
	762.466	$\begin{array}{ccc} R' & 2.8553\overline{8} \\ \cos \phi & 9.99675 \\ \sec \frac{1}{2} \varDelta & 0.02521 \end{array}$
		753.953 2.87734
		x = 0.88241 = 0.02521
	$m = \frac{762.037}{0.429}$	$\frac{8.084}{762.037} \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \cdot \frac{0.90762}{200000000000000000000000000000000000$
[Eq. 39]	$y = \frac{0.423}{174.722}$	R' 2.85538
		$\sin \varphi$ 9.08589 87.353 • • • • • • 1.94128
		$\begin{array}{ccc} R' & 2.8553\bar{8} \\ \cos \varphi & 9.99675 \\ \tan \frac{1}{2} & 9.54512 \end{array}$
	249.606 .	$\ldots \ldots \ldots \ldots \ldots 2.39725$
		R = 764.489 x = 7.628
		$\begin{array}{rrrr} 756.861 & 2.8790\overline{1} \\ tan \frac{1}{2}4 & 9.54512 \end{array}$
	$\overline{424.328}_{352.896}$	$\frac{265.543}{352.896}$ 2.42413
	AQ = 71.432	
		0 ·

The length of the old curve from Q to Q' is

$100 \frac{d}{D} = 100 \frac{38.667}{7.5} = \dots \dots$	515.556
$2AQ = 2 \times 71.432 = \ldots \ldots$	$\frac{142.864}{658.420}$
New curve: $100 \frac{A - 2\phi}{D'} = 100 \frac{38.667 - 14.000}{8.0} = 308.333$	
$2L = 2 \times 175 = 350.000$	
658.333	658.333
Difference in length $=$	0.087

Considering that this difference may be divided among 22 joints (using 30-foot rails) no rail-cutting would be necessary. If the difference is too large, a slight variation in the value of the new radius R' will reduce the difference as much as necessary. A truer comparison of the lengths would be found by comparing the lengths of the arcs.

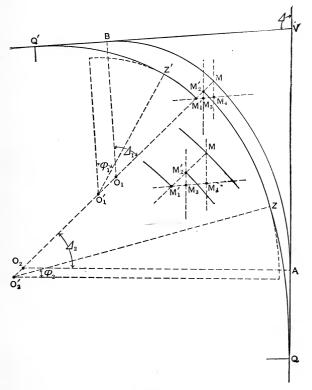
52. Application of transition curves to compound curves. Since compound curves are only employed when the location is limited by local conditions, the elements of the compound curve should be determined (as in §§ 38 and 39) regardless of the

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#### ALIGNMENT.

transition curves, depending on the fact that the lateral shifting of the curve when transition curves are introduced is very small. If the limitations are very close, an estimated allowance may be made for them.

Methods have been devised for inserting transition curves between the branches of a compound curve, but the device is



## FIG. 35.

complicated and usually needless, since when the train is once on a curve the wheels press against the outer rail steadily and a change in curvature will not produce a serious jar even though the superelevation is temporarily a little more or less than it should be.

§ 52.

curves are used at both ends or at one end only.

If the easier curve of the compound curve is less than 3° or 4°, there may be no need for a transition curve off from that branch. This problem then has two cases according as transition

a. With transition curves at both ends. Adopting the method of § 49, calling  $d_1 = \frac{1}{2}d$ , we may compute  $m_1 = MM_1'$ . Similarly, calling  $d_2 = \frac{1}{2}d$ , we may compute  $m_2 = MM_2'$ . But  $M_1'$  and  $M_2'$ must be made to coincide. This may be done by moving the curve  $Z'M_1'$  and its transition curve parallel to Q'V a distance  $M_1'M_3$ , and the other curve parallel to QV a distance  $M_2'M_3$ . In the triangle  $M_1'M_3M_2'$ , the angle at  $M_1'=90^\circ - d_1$ , the angle at  $M_2'=90^\circ - d_2$ , and the angle at  $M_3 = d$ .

Then 
$$M_1'M_3 = M_1'M_2' \frac{\sin(90^\circ - \mathcal{A}_2)}{\sin \mathcal{A}} = (m_1 - m_2) \frac{\cos \mathcal{A}_2}{\sin \mathcal{A}}.$$
  
Similarly  $M_2'M_3 = M_1'M_2' \frac{\sin(90^\circ - \mathcal{A}_1)}{\sin \mathcal{A}} = (m_1 - m_2) \frac{\cos \mathcal{A}_1}{\sin \mathcal{A}}.$  (40)

**b.** With a transition curve on the sharper curve only. Compute  $m_1 = MM_1'$  as before; then move the curve  $Z_1M_1'$  parallel to Q'V a distance of

The simple curve MA is moved parallel to VA a distance of

$$MM_4 = m_1 \frac{\cos d_1}{\sin d}.$$
 (42)

If  $d_1$  and  $d_2$  are both small,  $M_1'M_4$  and  $MM_4$  may be more than  $m_1$ , but the lateral deviation of the new curve from the old will always be less than  $m_1$ .

53. To replace a compound curve by a curve with spirals. The numerical illustration given below employs another method. We first solve for  $m_1$  for the sharper branch of the curve, placing  $d_1 = \frac{1}{2}d$  in Eq. 38. A value for  $R_2'$  may be found whose corresponding value of  $m_2$  will equal  $m_1$ . Solving Eq. 38 for R', we obtain

Substituting in this equation the known value of  $m_1 (=m_2)$ and calling  $R' = R_2'$ ,  $R = R_2$ , and  $\Delta_2 = \frac{1}{2}\Delta$ , solve for  $R_2'$ . Obtain the value of AQ for each branch of the curve separately by Eq. 39, and compare the lengths of the old and new lines.

*Example.* Assume a compound curve with  $D_1=8^\circ$ ,  $D_2=4^\circ$ ,  $d_1 = 36^\circ$ , and  $d_2 = 32^\circ$ . Use 1°-per-25-feet spirals;  $\phi_1 = 7^\circ 0'$ ;  $\phi_2 = 1^{\circ} 30'$ . Assume that the sharper curve is sharpened from 8° 0' to 8° 12'.

 $R_1$ 

[Eq. 38]

[14:00]							101		2.00000
						e	exsec 36°	<b>)</b>	9.37303
	169.209								2.22842
	$R_1' = 699.326$			•	•	•••	• • •	•	
	868.535						$R_1'$		2.84468
	000.000						$\cos \phi_1$	•	9.99675
							sec 4		0.09204
		857.970		•	•	• •	• •	•	2.93347
									0.88241
							$x_1$		0.88241 0.09204
		0 400					sec 4	1	
		9.429	•	• •	•	•	• • •	•	0.97445
	867.399	867.399							
	$m_1 = 1.136$								
	-								
[Eq. 43]							$R_2$		3.15615
							vers 32°	>	$9.1817\overline{0}$
	015 500								
	217.700		•	•	•	• •	• • •	•	$2.3378\overline{5}$
							1 100		0.05538
						m	1 = 1.136 $\cos 32^{\circ}$		9.92842
		0.963 .					COS 34		9.98380
		$x_2 = 0.763$	•	•	•	•••	• • •	•	9.90000
	1 796	$\frac{1.726}{1.726}$							
	1.726	1.720							
	215.974		•	•	•	• •	• • •	•	2.33440
				+			99966	,	
							=.99900 =.84805		
			1	iau.	00	5 42			
							.15161	• .	9.18073
	$R_2' = 1424.54$	[4° 1′ 22″]	•	•	•	• •	• • •	•	3.15367
[Eq. 39]	$y_1 = 174.722$						$R_{1}'$		$\overline{2.84468}$
							$\sin \phi_1$		$9.0858\overline{9}$
1 A.		85.226 .							$1.9305\overline{7}$
			•	•	•			•	
							$R_{1'}$		2.84468
	1.1					1 /	$\cos \phi_1$	07	9.99675
					T.	an $\frac{1}{2}$	$[4_1 = 36]$	-1	9.86126
	504.302		•	•	•	• •		•	2.70269
						$R_1 =$	716.779	)	
						$x_1 =$		\$	
•	,						709.151		$2.8507\overline{4}$
							tan 1		9.86126
	679.024						0 and 2	-	
	600.461	515.235	•	•	•	• •		•	$2.7120\overline{0}$
	$AQ_1 = 78.563$	600.461							

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2.85538

#### RAILROAD CONSTRUCTION.

[Eq. 39]	<sub>2</sub> = 74.994						$R_{2^{\prime}} \sin \phi_{2}$		$3.1536\overline{7}$ 8.41792
		37.290	• •	•	•	• •	• • •	•	1.57159
					ta	n <u></u> 1∕1(	$\begin{array}{c} R_2'\\\cos\phi_2\\ \Delta_2=32^\circ\end{array}$		$3.15367 \\ 9.99985 \\ 9.79579$
	889.843; .	• • •	٠	•••	•	• •		•	2.9+931
						$R_2 = x_2 $	1432.69 0.76		
							1431.93 tan ½4		$3.15592 \\ 9.79579$
		894.770	• •	•	•	• •	• • •	•	2.95171
	$964.837 \\ 932.060$	932.060							

$$AQ_2 = 32.777$$

For the length of the old track we have :

$$100\frac{d_{1}}{D_{1}} = 100 \frac{36^{\circ}}{8^{\circ}} = 450.$$
  

$$100\frac{d_{2}}{D_{2}} = 100 \frac{32^{\circ}}{4^{\circ}} = 800.$$
  

$$AQ_{1} = 78.563$$
  

$$AQ_{2} = 32.777$$
  

$$1361.340$$

For the length of the new track we have:

$100\frac{d_1 - \phi_1}{D_1'} = 100\frac{29^\circ}{8^\circ.20} = 353.659$	
$100\frac{d_2 - \phi_2}{D_2'} = 100 \frac{30^\circ.5}{4^\circ.023} = 758.140$	
Spiral on 8° 12′ curve 175.000 " 4° 01′ 22″ " 75.	
Length of new track $=$ 1361.799 " old " $=$ 1361.340	
Excess in length of new track $=$ 0.459	feet.

Since the new track is slightly longer than the old, it shows that the new track runs too far *outside* the old track at the *P.C.C.* On the other hand the offset m is only 1.136. The maximum amount by which the new track comes *inside* of the 'old track at two points, presumably not far from Z' and Z, is very difficult to determine exactly. Since it is desirable that the maximum offsets (inside and outside) should be made as nearly equal as possible, this feature should not be sacrificed to an effort to make the two lines of precisely equal length so that the rails need not be cut. Therefore, if it is found that the offsets inside the old track are nearly equal to m (1.136), the above figures should stand. Otherwise m may be diminished (and the above excess in length of track diminished) by *increasing*  $R_1'$ very slightly and making the necessary consequent changes.

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**53a.** Use of Table IV. Prof. R. B. H. Begg, of Syracuse University, has submitted to the author a series of tables which will materially simplify the work of solving Equations (33) to (37), and which have been added to Table IV of previous editions. Since these equations involve R and  $\Delta$  (which may each have any values) in combination with several values of  $\phi$ , it would require impracticably extensive tables to give precise values of the required dimensions for any possible combination of R,  $\Delta$ , and  $\phi$ . But the tables may be utilized by interpolation with all necessary accuracy within their range. Rules for the use of the tables and for the field work are as follows:

- 1. Find P. C. (point A) as if no transition curve were to be used.
- 2. Lay off the distance AN (part C of table) to N; then offset the distance A'N (part B) to A', the new P. C.; from N measure a distance NQ (part B) to Q.
- 3. Set transit on A'; sight parallel to tangent and run in circular curve, setting Z from deflection and distance (part B); or Z can be set by measuring ZK and QK (part B) from Q.
- 4. Set transit on Q, sight along tangent and turn the deflection (part A) for each 25-foot station, for as many chord lengths as required; or the points may be located by measuring distances y along the tangent from Q and offsetting the corresponding distances x

# VERTICAL CURVES:

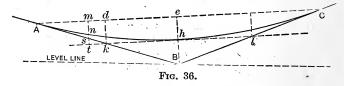
54. Necessity for their use. Whenever there is a change in the rate of grade, it is necessary to eliminate the angle that would be formed at the point of change and to connect the two grades by a curve. This is especially necessary at a sag between two grades, since the shock caused by abruptly forcing an upward motion to a rapidly moving heavy train is very severe both to the track and to the rolling stock. The necessity for vertical curves was even greater in the days when link couplers were in universal use and the "slack" in a long train was very great. Under such circumstances, when a train was moving down a heavy grade the cars would crowd ahead against the engine. Reaching the sag, the engine would begin to pull out, rapidly taking out the slack. Six inches of slack on each car would amount to several feet on a long train, and the resulting jerk on

§ 53a.

the couplers, especially those near the rear of the train, has frequently resulted in broken couplers or even derailments. A vertical curve will practically eliminate this danger if the curve is made long enough, but the rapidly increasing adoption of close spring couplers and air-brakes, even for freight trains, is obviating the necessity for such very long curves.

55. Required length. Theoretically the length should depend on the change in the rate of grade and on the length of the longest train on the road. A sharp change in the rate of grade requires a long curve; a long train requires a long curve; but since the longest trains are found on roads with light grades and small changes of grade, the required length is thus somewhat The A.R.E.A. rule is: "On class A roads (see § 198) equalized. rates of change of 0.1 per cent per station on summits and 0.05 per cent per station in sags should not be exceeded. On minor roads 0.2 per cent per station on summits and 0.1 per cent per station in sags may be used." When changing from a down grade to an up grade (or vice versa) the change of grade equals the numerical sum of the two rates of grade. For example, if a 0.5 per cent down grade is followed by a 0.7 per cent up grade, the road being a "minor" road, then, by the above rule the length of the curve should be at least  $[0.5 - (-0.7)] \div 0.1 = 12$  stations or 1200 feet. Added length increases the amount of earthwork required both in cuts and fills, but the resulting saving in operating expenses will always justify a considerable increase.

56. Form of curve. In Fig. 36 assume that A and C, equi-



distant from B, are the extremities of the vertical curve. Bisect AC at e; draw Be and bisect it at h. Bisect AB and BC at k and l. The line kl will pass through h. A parabola may be drawn with its vertex at h which will be tangent to AB and BC at A and C. It may readily be shown \* from the properties of a parabola that if an ordinate be drawn at any point (as at n) we will have

\* See note\_at\_foot of p. 64.

## ALIGNMENT.

$$sn : eh \text{ (or } hB\text{)} :: \overline{Am^2} : \overline{Ae},^2$$
$$sn = eh \frac{\overline{Am^2}}{\overline{Ae^2}} \quad \dots \quad \dots \quad (44)$$

or

§ 57.

In Fig. 36 the grades are necessarily exaggerated enormously. With the proportions found in practice we may assume that ordinates (such as mt, eB, etc.) are perpendicular to either grade, as may suit our convenience, without any appreciable error. In the numerical case given below, the variation of these ordinates from the vertical is 0° 07', while the effect of this variation on the calculations in this case (as in the most extreme cases) is absolutely inappreciable. It may easily be shown that the angle CAB = half the *algebraic difference* of the rates of grade. Call the difference, expressed in per cent of grade, r; then  $CAB = \frac{1}{2}r$ . Let l = length (in "stations" of 100 feet) of the line AC, which is practically equal to the horizontal measurement. Since the angle CAB is one-half the total change of grade at B, it follows that  $Be = \frac{1}{2}l \times \frac{1}{2}r$  Therefore

Since Bh (or eh) are constant for any one curve, the correction sn at any point (see Eq. 44) equals a constant times  $Am^2$ .

57. Numerical example. Assume that B is located at Sta. 16+20; that the grade of AB is -0.5%, and of BC +0.7%; also that the elevation of B above the datum plane is 162.6. Then the algebraic difference of the grades, r, =0.7-(-0.5) = 1.2; l=12.  $Bh=\frac{1}{8}lr=\frac{1}{8}\times12\times1.2=1.8$ . A is at Sta. 10+20 and its elevation is  $162.6+(6\times0.5)=165.6$ ; C is at Sta. 22+20 and its elevation is  $162.6+(6\times0.7)=166.8$ . The elevation of Sta. 11 is found by adding sn to the elevation of s on the straight grade line. The constant  $(eh \div Ae^2)$  equals in this case  $1.8\div600^2 = \frac{1}{200000}$ . Therefore the curve elevations are

A,	Sta.	10 + 20,	$162.6 + (6.00 \times 0.5)$	= 165.60
		11	$165.6 - (0.80 \times 0.5) + \frac{1}{200000} 80$	$0^2 = 165.23$
		12	$165.6 - (1.80 \times 0.5) + \frac{1}{200000} 180$	$D^2 = 164.86$
		13	$165.6 - (2.80 \times 0.5) + \frac{1}{200000} 280$	$0^2 = 164.59$
		14 ′	$165.6 - (3.80 \times 0.5) + \frac{1}{200000} 38$	$0^2 = 164.42$
		15	$165.6 - (4.80 \times 0.5) + \frac{1}{200000} 48$	$0^2 = 164.35$
		16	$165.6 - (5.80 \times 0.5) + \frac{1}{200000} 58$	$0^2 = 164.38$

В,	16 + 20,	$162.6 \pm 1.80$	=164.40
	17	$166.8 - (5.20 \times 0.7) + \frac{1}{200000} 520^{2}$	=164.51
	18	$166.8 - (4.20 \times 0.7) + \frac{1}{200000} 420^{2}$	=164.74
	19	$166.8 - (3.20 \times 0.7) + \frac{1}{200000} 320^2$	=165.07
	20	$166.8 - (2.20 \times 0.7) + \frac{1}{200000} 220^{2}$	=165.50
	21	$166.8 - (1.20 \times 0.7) + \frac{1}{200000} 120^{2}$	=166.03
	22	$166.8 - (0.20 \times 0.7) + \frac{1}{200000} 20^{2}$	=166.66
С,	22+20,	$162.6 + (6.00 \times 0.7)$	=166.80

#### DEMONSTRATION OF EQ. 44.

The general equation of a parabola passing through the point n (Fig. 36) may be written

$$y^{2} + y_{n}^{2} = 2p(x + x_{n})_{1}$$
$$s_{n} = \frac{y^{2}}{2p} + \frac{y_{n}^{2}}{2p} - x.$$

from which

from which

When  $x = x_A, y = y_A$ , and we have

$$x_n = \frac{y_A^2}{2p} + \frac{y_n^2}{2p} - x_A$$

 $x_{A}$ 

The general equation of a tangent passing through the point A may be written

$$yy_A = p(x + x_A),$$
$$x = \frac{yy_A}{p} - x_A.$$

÷

When  $x = x_s$ ,  $y = y_s [= y_n]$ , and we have

$$x_{s} = \frac{y_{n}y_{A}}{p} - x_{A},$$

$$\overline{sn} = x_{n} - x_{s} = \frac{y_{A}^{2} + y_{n}^{2} - 2y_{n}y_{A}}{2p}$$

$$= \frac{(y_{A} - y_{n})^{2}}{2p} = \frac{\overline{Am}^{2}}{2p},$$

$$2p = \frac{y_{A}^{2}}{x_{A}} = \frac{\overline{Ae}^{2}}{\overline{eh}}.$$

$$\therefore \quad \overline{sn} = \overline{eh}\frac{\overline{Am}^{2}}{\overline{Ae}^{2}}.$$

This proves the general proposition that if secants are drawn parallel to the axis of x, intersecting a parabola and a tangent to it, the intercepts between the tangent and the parabola are proportional to the square of the distances (measured parallel to y) from the tangent point.

# CHAPTER III.

## EARTHWORK.

### FORM OF EXCAVATIONS AND EMBANKMENTS.

58. Usual form of cross-section in cut or fill. The normal form of cross-section in cut is as shown in Fig. 37, in which  $g \dots g$  represents the natural surface of the ground, no matter

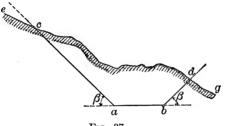


FIG. 37.

how irregular; ab represents the position and width of the required roadbed; ac and bd represent the "side slopes" which begin at a and b and which intersect the natural surface at such

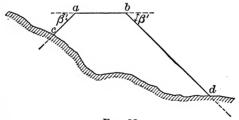


FIG. 38.

points (c and d) as will be determined by the required slope angle  $(\beta)$ .

The normal section in fill is as shown in Fig. 38. The points c and d are likewise determined by the intersection of the re-

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quired side slopes with the natural surface. In case the required roadbed (ab in Fig. 39) intersects the natural surface, both cut

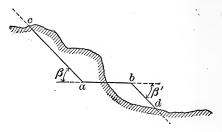


FIG. 39.

and fill are required, and the points c and d are determined as before. Note that  $\beta$  and  $\beta'$  are not necessarily equal. Their proper values will be discussed later.

59. Terminal pyramids and wedges. Fig. 40 illustrates the general form of cross-sections when there is a transition from cut to fill.  $a \dots g$  represents the grade line of the road which

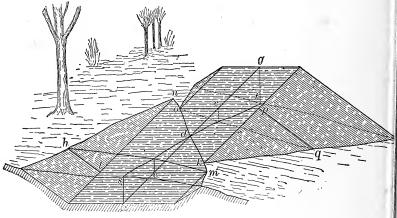


Fig. 40.

passes from cut to fill at d. sdt represents the surface profile. A cross-section taken at the point where either side of the roadbed *first* cuts the surface (the point m in this case) will usually be triangular if the ground is regular. A similar cross-section should be taken at o, where the other side of the roadbed cuts the surface. In general the earthwork of cut and fill terminates in two pyramids. In Fig. 40 the pyramid vertices are at n and k, and the bases are lhm and opq. The roadbed is generally wider in cut than in fill, and therefore the section lhm and the altitude ln are generally greater than the section opq and the altitude pk. When the line of intersection of the roadbed and natural surface (nodkm) becomes perpendicular to the axis of the roadbed (ag) the pyramids become wedges whose bases are the nearest convenient cross-sections.

60. Slopes. a. Cuttings. The required slopes for cuttings vary from perpendicular cuts, which may be used in hard rock which will not disintegrate by exposure, to a slope of perhaps 4 horizontal to 1 vertical in a soft material like quicksand or in a clayey soil which flows easily when saturated. For earthy materials a slope of 1:1 is the maximum allowable, and even this should only be used for firm material not easily affected by saturation. A slope of  $1\frac{1}{2}$  horizontal to 1 vertical is a safer slope for average earthwork. It is a frequent blunder that slopes in cuts are made too steep, and it results in excessive work in clearing out from the ditches the material that slides down, at a much higher cost per yard than it would have cost to take it out at first, to say nothing of the danger of accidents from possible landslides.

**b.** Embankments. The slopes of an embankment vary from 1:1 to 1.5:1. A rock fill will stand at 1:1, and if some care is taken to form the larger pieces on the outside into a rough dry wall, a much steeper slope can be allowed. This method is sometimes a necessity in steep side-hill work. Earthwork embankments generally require a slope of  $1\frac{1}{2}$  to 1. If made steeper at first, it generally results in the edges giving way, requiring repairs until the ultimate slope is nearly or quite  $1\frac{1}{2}:1$ . The difficulty of incorporating the added material with the old embankment and preventing its sliding off frequently makes these repairs disproportionately costly.

61. Compound sections. When the cut consists partly of earth and partly of rock, a compound cross-section must be made. If borings have been made so that the contour of the rock surface is accurately known, then the true cross-section may be determined. The rock and earth should be calculated separately, and this will require an accurate knowledge of where the rock "runs out"—a difficult matter when it must be determined by boring. During construction the center part of the earth cut would be taken out first and the cut widened until a sufficient width of rock surface had been exposed so that the rock cut would have its proper width and side slopes. Then the earth slopes could be cut down at the proper angle. A"berm" of about three feet is usually left on the edges of the rock cut as

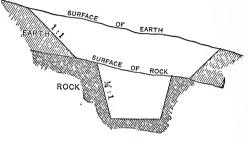


FIG. 41.

a margin of safety against a possible sliding of the earth slopes. After the work is done, the amount of excavation that has been made is readily computable, but accurate preliminary estimates are difficult. The area of the cross-section of earth in the figure must be determined by a method similar to that developed for borrow-pits (see § 89).

62. Width of roadbed. Owing to the large and often disproportionate addition to volume of cut or fill caused by the addition of even one foot to the width of roadbed, there is a natural tendency to reduce the width until embankments become unsafe and cuts are too narrow for proper drainage. The cost of maintenance of roadbed is so largely dependent on the drainage of the roadbed that there is true economy in making an ample allowance for it. The practice of some of the leading railroads of the country in this respect is given in the following table, in which are also given some data belonging more properly to the subject of superstructure.

It may be noted from the table that the average width for an *earthwork* cut, single track, is about 24.7 feet, with a minimum of 19 feet 2 inches. The widths of fills, single track, average over 18 feet, with numerous minimums of 16 feet. The widths for double track may be found by adding the distance between track centers, which is usually 13 feet.

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Cut.
$\left\{\begin{array}{l} 28' \operatorname{earth} \\ 22' \operatorname{rock} \\ 14+(2\times5)* \\ 18+(2\times6)* \\ 20+(2\times4)* \\ 20,84'' \\ 20'84'' \\ 14+(2\times3.5) \\ 13+(2\times4.5) \\ 13+(2\times4.5) \\ 13+(2\times4.5) \\ 13+(2\times3.5) \\ 16' \operatorname{rock} \\ 19' 2' \operatorname{light} \operatorname{traffle} \\ 27' 2'' \operatorname{heavy} \\ 14+(2\times3.5) \end{array}\right.$

§ 62.

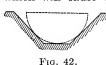
EARTHWORK.

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63. Form of subgrade. Specifications (or the cross-section drawings) formerly required that the subgrade should have a curved form, convex upward, or that it should slope outward from a slight ridge in the center, with the evident purpose of draining to the sides all water which might percolate through the ballast. If the subsoil were hard and impenetrable by the ballast, the method might answer, but experience has shown that, with ordinary subsoils, the ballast immediately under each rail is forced a little deeper into the subsoil by the passage of each train. Periodical retamping of ballast under the ends of the ties, and little or no tamping under the center, only adds to the accumulation under each rail. A cross-section of a very old roadbed will frequently show twice as much depth of ballast under the rails as there is under the center. This method of tamping quickly obliterates the original line of demarcation between ballast and subsoil and any expected improvement in drainage due to sloping subsoil is not realized. Therefore the A.R.E.A. specifications call for *flat* subgrades.

64. Ditches. "The stability of the track depends upon the strength and permanence of the roadbed and structures upon which it rests; whatever will protect them from damage or prevent premature decay should be carefully observed. The worst enemy is WATER, and the further it can be kept away from the track, or the sooner it can be diverted from it, the better the track will be protected. Cold is damaging only by reason of the water which it freezes; therefore the first and most important provision for good track is drainage." (Rules of the Road Department, Illinois Central R. R.)

The form of ditch generally prescribed has a flat bottom 12'' to 24'' wide and with sides having a minimum slope, except in rock-work, of 1:1, more generally 1.5:1 and sometimes 2:1. Sometimes the ditches are made V-shaped, which is objectionable unless the slopes are low The best form is evidently that which will cause the greatest flow for a given slope, and this



will evidently be the form in which the ratio of area to wetted perimeter is the largest. The semicircle fulfills this condition better than any other form, but the nearly vertical sides would be difficult to

maintain. (See Fig. 42.) A ditch, with a flat bottom and such

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slopes as the soil requires, which approximates to the circular form will therefore be the best.

When the flow will probably be large and at times rapid it will be advisable to pave the ditches with stone, especially if the soil is easily washed away. Six-inch tile drains, placed 2' under the ditches, are prescribed on some roads. (See Fig. 43.) No better method could be devised to insure a dry subsoil. The ditches through cuts should be led off at the end of the cut so that the adjacent embankment will not be injured.

Wherever there is danger that the drainage from the land above a cut will drain down into the cut, a ditch should be made near the edge of the cut to intercept this drainage, and this ditch should be continued, and paved if necessary, to a point where the outflow will be harmless. Neglect of these simple and inexpensive precautions frequently causes the soil to be loosened on the shoulders of the slopes during the progress of a heavy rain, and results in a landslide which will cost more to repair than the ditches which would have prevented it for all time.

Ditches should be formed along the bases of embankments; they facilitate the drainage of water from the embankment, and may prevent a costly slip and disintegration of the embankment.

65. Effect of sodding the slopes, etc. Engineers are unanimously in favor of rounding off the shoulders and toes of embankments and slopes, sodding the slopes, paving the ditches, and providing tile drains for subsurface drainage, all to be put in during original construction. (See Fig. 43.) Some of the highest grade specifications call for the removal of the top layer of vegetable soil from cuts and from under proposed fills to some convenient place, from which it may be afterwards spread on the slopes, thus facilitating the formation of sod from grassseed. But while engineers favor these measures and their economic value may be readily demonstrated, it is generally impossible to obtain the authorization of such specifications from railroad directors and promoters. The addition to the original cost of the roadbed is considerable, but is by no means as great as the capitalized value of the extra cost of maintenance resulting from the usual practice. Fig. 43 is a copy of

designs \* presented at a convention of the American Society of Civil Engineers by Mr. D. J. Whittemore, Past President of the Society and Chief Engineer of the Chi., Mil. & St. Paul

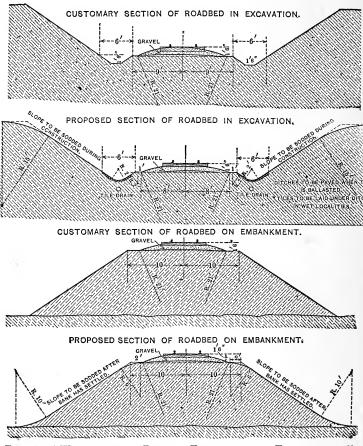


FIG. 43.—" WHITTEMORE ON RAILWAY EXCAVATION AND EMBANKMENTS" Trads. Am. Soc. C. E., Sept. 1894.

R. R. The "customary sections" represent what is, with some variations of detail, the practice of many railroads. The "pro-

\* Trans. Am. Soc. Civil Eng., Sept. 1894.

posed sections" elicited unanimous approval. They should be adopted when not prohibited by financial considerations.

### EARTHWORK SURVEYS.

66. Relation of actual volume to the numerical result. It should be realized at the outset that the accuracy of the result of computations of the volume of any given mass of earthwork has but little relation to the accuracy of the mere numerical work. The process of obtaining the volume consists of two distinct parts. In the first place it is assumed that the volume of the earthwork may be represented by a more or less complicated geometrical form, and then, secondly, the volume of such a geometrical form is computed. A desire for simplicity (or a frank willingness to accept approximate results) will often cause the cross-section men to assume that the volume may be represented by a very simple geometrical form which is really only a very rough approximation to the true volume. In such a case, it is only a waste of time to compute the volume with minute numerical accuracy. One of the first lessons to be learned is that economy of time and effort requires that the accuracy of the numerical work should be kept proportional to the accuracy of the cross-sectioning work, and also that the accuracy of both should be proportional to the use to be made of the results. The subject is discussed further in § 94.

67. Prismoids. To compute the volume of earthwork, it is necessary to assume that it has some geometric form whose volume is readily determinable. The general method is to consider the volume as consisting of a series of prismoids, which are solids having parallel plane ends and bounded by surfaces which may be formed by lines moving continuously along the edges of the bases These surfaces may also be considered as the surfaces generated by lines moving along the edges joining the corresponding points of the bases, these edges being the directrices. and the lines being always parallel to either base, which is a plane director. The surfaces thus developed may or may not be planes. The volume of such a prismoid is readily determinable (as explained in § 70 et seq.), while its definition is so very general that it may be applied to very rough ground. The "two plane ends" are sections perpendicular to the axis of the road. The roadbed and side slopes (also plane) form three of

the side surfaces. The only approximation lies in the degree of accuracy with which the plane (or warped) surfaces coincide with the actual surface of the ground between these two sections. This accuracy will depend (a) on the number of points which are taken in each cross-section and the accuracy with which the lines joining these points coincide with the actual cross-sections; (b) on the skill shown in selecting places for the cross-sections so that the warped surfaces shall coincide as nearly as possible with the surface of the ground. In fairly smooth country, crosssections every 100 feet, placed at the even stations, are sufficiently accurate, and such a method simplifies the computations greatly; but in rough country cross-sections must be interpolated as the surface demands. As will be explained later. carelessness or lack of judgment in cross-sectioning will introduce errors of such magnitude that all refinements in the computations are utterly wasted.

68. Cross-sectioning. The process of cross-sectioning consists in determining at any place the intersection by a vertical plane of the prism of earth lying between the roadbed, the side slopes, and the natural surface. The intersection with the road-

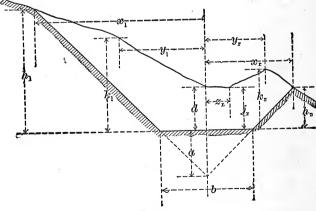


FIG. 44.

bed and side slopes gives three straight lines. The intersection with the natural surface is in general an irregular line. On smooth regular ground or when approximate results are acceptable this line is assumed to be straight. According to the irregularity of the ground and the accuracy desired more and more "intermediate points" are taken.

The distance (d in Fig. 44) of the roadbed below (or above) the natural surface at the center is known or determined from the profile or by the computed establishment of the grade line. The distances out from the center of all "breaks" are determined with a tape. To determine the elevations for a cut, set. up a level at any convenient point so that the line of sight is higher than any point of the cross-section, and take a rod reading on the center point. This rod reading added to d gives the height of the instrument (H. I.) above the roadbed. Subtracting from H. I. the rod reading at any "break" gives the height of that point above the roadbed  $(h_l, k_l, h_r, \text{ etc.})$ . This is true for all cases in excavation. For fill, the rod reading at center minus d equals the H. I., which may be positive or negative. When negative, add to the "H. I." the rod readings of the intermediate points to get their depths below "grade"; when positive, subtract the "H. I." from the rod readings.

The heights or depths of these intermediate points above or below grade need only be taken to the nearest tenth of a foot, and the distances out from the center will frequently be sufficiently exact when taken to the nearest foot. The roughness of the surface of farming land or woodland generally renders useless any attempt to compute the volume with any greater accuracy than these figures would imply unless the form of the ridges and hollows is especially well defined. The position of the slopestake points is considered in the next section. Additional discussion regarding cross-sectioning is found in § S2.

69. Position of slope-stakes. The slope-stakes are set at the intersection of the required side slopes with the natural surface, which depends on the center cut or fill (d). The distance of the slope-stake from the center for the lower side is  $x=\frac{1}{2}b$  +s(d+y); for the up-hill side it is  $x'=\frac{1}{2}b+s(d-y')$ . s is the "slope ratio" for the slopes, the ratio of horizontal to ver tical. In the above equation both x and y are unknown. Therefore some position must be found by trial which will satisfy the equation. As a preliminary, the value of x for the point  $a=\frac{1}{2}b$  +sd, which is the value of x for level cross-sections. In the case of fills on sloping ground the value of x on the down-hill side is greater than this; on the up-hill side it is less. The difference in distance is s times the difference of elevation. Take a

numerical case corresponding with Fig. 45. The rod reading on c is 2.9; d=4.2; therefore the telescope is 4.2-2.9=1.3below grade. s=1.5:1, b=16. Hence for the point a (or for level ground)  $x=\frac{1}{2}\times16+1.5\times4.2=14.3$ . At a distance out of 14.3 the ground is seen to be about 3 feet lower, which will not only require  $1.5\times3=4.5$  more, but enough additional distance so that the added distance shall be 1.5 times the additional drop. As a first trial the rod may be held at 24 feet out and a reading of, say, 8.3 is obtained. 8.3+1.3=9.6, the depth of the point below grade. The point on the slope line (n) which has this depth below grade is at a distance from the center

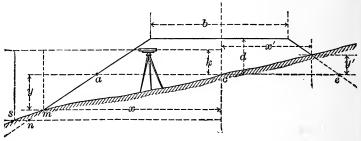


Fig. 45.

 $x=8+1.5\times9.6=22.4$ . The point on the surface (s) having that depth is 24 feet out. Therefore the true point (m) is nearer the center. A second trial at 20.5 feet out gives a rod reading of, say, 7.1 or a depth of 8.4 below grade. This corresponds to a distance out of 20.6. Since the natural soil (especially in farming lands or woods) is generally so rough that a difference of elevation of a tenth or so may be readily found by slightly varying the location of the rod (even though the distance from the center is the same), it is useless to attempt too much refinement, and so in a case like the above the combination of 8.4 below grade and 20.6 out from center may be taken to indicate the proper position of the slope-stake. This is usually indicated in the form of a fraction, the distance out being the denominator and the height above (or below) grade being the numerator; the fact of cut or fill may be indicated by C or  $F_{\bullet}$ Ordinarily a second trial will be sufficient to determine with sufficient accuracy the true position of the slope-stake. Experienced men will frequently estimate the required distance out to within a few tenths at the first trial. The left-hand pages of the note-book should have the station number, surface elevation, grade elevation, center cut or fill, and rate of grade. The right-hand pages should be divided in the center and show the distances out and heights above grade of all points, as is illustrated in § 84. The notes should read UP the page, so that when looking ahead along the line the figures are in their proper relative position. The "fractions" farthest from the center line represent the slope-stake points.

70. Setting slope-stakes by means of "automatic" slope-stake rods. The equipment consists of a specially graduated tape and a specially constructed rod. The tape may readily be prepared by marking on the *back* side of an ordinary 50-foot tape which is graduated to feet and tenths. Mark "0" at " $\frac{1}{2}b$ " from the tapering. Then graduate from the zero backward, at true scale, to the ring. Mark off "feet" and "tenths" on a scale proportionate to the slope ratio. For example, with the usual slope ratio of 1.5:1 each "foot" would measure 18 inches and each "tenth" in proportion.

The rod, 10 feet long, is shod at each end and has an endless tape passing within the shoes at each end and over pulleys—to reduce friction. The tape should be graduated in feet and tenths, from 0 to 20 feet—the 0 and 20 coinciding. By moving the tape so that 0 is at the bottom of the rod—or (practically) so that the 1-foot mark on the tape is one foot above the bottom of the shoe, an index mark may be placed on the back of the rod (say at 15—on the tape) and this readily indicates when the tape is "set at zero."

The method of use may best be explained from the figure and from the explicit rules as stated. The proof is given for two assumed positions of the level.

(1) Set up the level so that it is higher than the "center" and (if possible) higher than both slope-stakes, but not more than a rod-length higher. On very steep ground this may be impossible and each slope-stake must be set by separate positions of the level.

(2) Set the rod-tape at zero (i.e., so that the 15-foot mark on the *back* is at the index mark).

(3) Hold the rod at the center-stake (B) and note the reading  $(n_1 \text{ or } n_2)$ . Consider n to be always plus; consider d to be plus for cut and minus for fill.

(4) Raise the tape on the face side of the rod (n+d). Applied literally (and algebraically), when the level is below the roadbed (only possible for fill),  $(n+d) = (n_2 + (-d_f)) = n_2 - d_f$ . This being numerically negative, the tape is lowered  $(d_f - n_2)$ . With level at (1), for fill,  $(n+d) = (n_1 + (-d_f)) = (n_1 - d_f)$ ; this being positive, the tape is raised. With level at (1), for cut, the tape is raised  $(n_1+d_c)$ . In every case the effect is the same as if the telescope were set at the elevation of the roadbed.

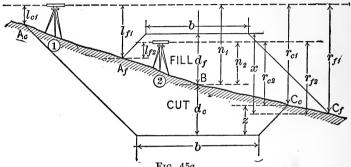


FIG. 45a.

(5) With the special distance-tape, so held that its zero is  $\frac{1}{2}b$ from the center, carry the rod out until the rod reading equals the reading indicated by the tape. Since in cut the tape is raised (n+d), the zero of the rod-tape is always higher than the level (unless the rod is held at or below the elevation of the roadbed-which is only possible on side-hill work), and the reading at either slope-stake is necessarily negative. The reading for slope-stakes in fill is always positive.

(6) Record the rod-tape reading as the numerator of a fraction and the actual distance out (read directly from the other side of the distance-tape) as the denominator of the fraction.

**Proof.** Fill. Level at (1). Tape is raised  $(n_1 - d_f)$ . When rod is held at  $C_f$ , the rod reading is +x, which  $=r_{f_1}-(n_1-d_f)$ . But the reading on the back side of the distance-tape is also x.

Fill. Level at (2). Tape is raised  $(n_2-d_f)$ , i.e., it is lowered  $(d_f - n_2).$ When rod is held at  $C_f$ , the rod reading is +x, which similarly  $= r_{f_2} - (n_2 - d_f) = r_{f_2} + (d_f - n_2)$ . Distance-tape as before.

Cut Level at (1). Tape is raised  $(n_1+d_c)$ . When rod is held at  $C_c$  the rod reading is -z, which  $= r_{c_1} - (n_1 + d_c)$ , i.e.,  $z = (n_1 + d_c) - r_{c_1}$ . The distance-tape will read z.

Side-hill work. It is easily demonstrated that the method, when followed literally, may be applied to side-hill work. although there is considerable chance for confusion and error, when, as is usual,  $\frac{1}{2}b$  and the slope ratio are different for cut and for fill.

The method appears complicated at first, but it becomes mechanical and a time-saver when thoroughly learned. The advantages are especially great when the ground is fairly level transversely, but decrease when the difference of elevation of the center and the slope-stake is more than the rod length. By setting the rod-tape "at zero," the rod may always be used as an ordinary level rod and the regular method adopted, as in § 69. Many engineers who have thoroughly tested these rods are enthusiastic in their praise as a time-saver.

## COMPUTATION OF VOLUME.

71. Prismoidal formula. Let Fig. 46 represent a triangular prismoid. The two triangles forming the ends lie in *parallel* planes, but since the angles of one triangle are not equal to the corresponding angles of the other triangle, at least two of the surfaces must be *warped*. If a section, parallel to the bases, is

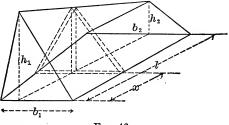


Fig. 46.

made at any point at a distance x from one end, the area of the section will evidently be

$$A_{x} = \frac{1}{2}b_{x}h_{x} = \frac{1}{2}\left[b_{1} + (b_{2} - b_{1})\frac{x}{l}\right]\left[h_{1} + (h_{2} - h_{1})\frac{x}{l}\right]$$

§ 71.

The volume of a section of infinitesimal length will be  $A_x dx_y$ and the total volume of the prismoid will be \*

$$\int_{0}^{l} A_{x} dx = \frac{1}{2} \int_{0}^{l} \left[ b_{1} + (b_{2} - b_{1}) \frac{x}{l} \right] \left[ h_{1} + (h_{2} - h_{1}) \frac{x}{l} \right] dx$$

$$= \frac{1}{2} \left[ b_{1} h_{1} x + (b_{2} - b_{1}) h_{1} \frac{x^{2}}{2l} + b_{1} (h_{2} - h_{1}) \frac{x^{2}}{2l} + (b_{2} - b_{1}) (h_{2} - h_{1}) \frac{x^{3}}{3l^{2}} \right]_{0}^{l}$$

$$= \frac{1}{2} \left\{ b_{1} h_{1} l + \left[ (b_{2} - b_{1}) h_{1} + b_{1} (h_{2} - h_{1}) \right] \frac{l}{2} + (b_{2} - b_{1}) (h_{2} - h_{1}) \frac{l}{3} \right\}$$

$$= \frac{l}{2} \left[ \frac{1}{3} b_{1} h_{1} + \frac{1}{6} b_{1} h_{2} + \frac{1}{6} b_{2} h_{1} + \frac{1}{3} b_{2} h_{2} \right]$$

$$= \frac{l}{6} \left[ \frac{1}{2} b_{1} h_{1} + \frac{1}{2} b_{1} (h_{1} + h_{2}) + \frac{1}{2} b_{2} (h_{1} + h_{2}) + \frac{1}{2} b_{2} h_{2} \right]$$

$$= \frac{l}{6} \left[ \frac{1}{2} b_{1} h_{1} + 4 \left( \frac{1}{2} \cdot \frac{b_{1} + b_{2}}{2} \cdot \frac{b_{1} + h_{2}}{2} \right) + \frac{1}{2} b_{2} h_{2} \right]$$

$$= \frac{l}{6} \left[ A_{1} + 4A_{m} + A_{2} \right], \qquad (45)$$

in which  $A_1$ ,  $A_2$ , and  $A_m$  are the areas respectively of the two bases and of the middle section. Note that  $A_m$  is not the mean of  $A_1$  and  $A_2$ , although it does not necessarily differ very greatly from it.

The above proof is absolutely independent of the values, absolute or relative, of  $b_1$ ,  $b_2$ ,  $h_1$ , or  $h_2$ . For example,  $h_2$  may be zero and the second base reduces to a line and the prismoid becomes wedge-shaped; or  $b_2$  and  $h_2$  may both vanish, the second base becoming z point and the prismoid reduces to a pyramid. Since every prismoid (as defined in § 67) may be reduced to a combination of triangular prismoids, wedges, and pyramids, and

\* Students unfamiliar with the Integral Calculus may take for granted the fundamental formulæ that  $\int dx = x$ , that  $\int x dx = \frac{1}{2}x^2$ , and that  $\int x^2 dx = \frac{1}{2}x^3$ ; also that in integrating between the Einits of *l* and 0 (zero), the value of the integral may be found by simply substituting *l* for *x* after integration.

since the formula is true for any one of them individually, it is true for all collectively; therefore it may be stated that \*

The volume of a prismoid equals one sixth of the perpendicular distance between the bases multiplied by the sum of the areas of the two bases plus four times the area of the middle section.

While it is always possible to compute the volume of any prismoid by the above method, it becomes an extremely complicated and tedious operation to compute the true value of the middle section if the end sections are complicated in form. It therefore becomes a simpler operation to compute volumes by approximate formulæ and apply, if necessary, a correction. The most common methods are as follows:

72. Averaging end areas. The volume of the triangular prismoid (Fig. 46), computed by averaging end areas, is  $\frac{l}{2}[\frac{1}{2}b_1h_1+\frac{1}{2}b_2h_2]$ . Subtracting this from the true volume (as given in the equation above Eq. 45), we obtain the correction

$$\frac{l}{12}[(b_1-b_2)(h_2-h_1)].$$
 (46)

This shows that if either the h's or b's are equal, the correction vanishes; it also shows that if the bases are roughly similar and b varies roughly with h (which usually occurs, as will be seen later), the correction will be *negative*, which means that the method of averaging end areas usually gives too large results.

73. Middle areas. Sometimes the middle area is computed and the volume is assumed to be equal to the length times the middle area. This will equal  $\frac{l}{2} \times \frac{b_1 + b_2}{2} \times \frac{h_1 + h_2}{2}$ . Subtracting this from the true volume, we obtain the correction

As before, the form of the correction shows that if either the h's or b's are equal, the correction vanishes; also under the *usual* conditions, as before, the correction is *positive* and only one-half as large as by averaging end areas. Ordinarily the labor involved in the above method is no less than that of applying the exact prismoidal formula.

§ 72.

<sup>\*</sup> The student should note that the derivation of equation (45) does not complete the proof, but that the statements in the following paragraph are logically necessary for a general proof.

74. Two-level ground. When approximate computations of earthwork are sufficiently exact the field-work may be materially reduced by observing simply the center cut (or fill) and the natural slope a, measured with a clinometer. The area of such a section (see Fig. 48) equals

$$\frac{1}{2}(a+d)(x_l+x_r)-\frac{ab}{2}.$$

But

$$x_l \tan \beta = a + d + x_l \tan a$$

from which

$$x_l = \frac{a+d}{\tan\beta - \tan a}.$$

Similarly,

$$x_r = \frac{a+a}{\tan\beta + \tan a}.$$

Substituting,

Area = 
$$(a+d)^2 \frac{\tan\beta}{\tan^2\beta - \tan^2\alpha} - \frac{ab}{2}$$
. (48)

The values a,  $\tan \beta$ ,  $\tan^2 \beta$  are constant for all sections, so that it requires but little work to find the area of any section.

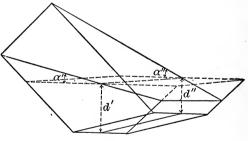


FIG. 47.

As this method of cross-sectioning implies considerable approximation, it is generally a useless refinement to attempt to com-

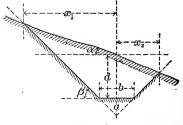


FIG. 48.

EARTHWORK.

pute the volume with any greater accuracy than that obtained by averaging end areas. It may be noted that it may be easily proved that the correction to be applied is of the same form as that found in § 72 and equals

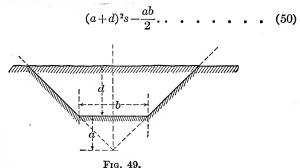
 $\frac{l}{12}[(x_{l}'+x_{r}')-(x_{l}''+x_{r}'')][(d''+a)-(d'+a)],$ 

which reduces to

$$\operatorname{Corr.} = \frac{l}{6} \left\{ \left[ (a+d') \frac{\tan\beta}{\tan^2\beta - \tan^2\alpha'} - (a+d'') \frac{\tan\beta}{\tan^2\beta - \tan^2\alpha''} \right] [d''-d'] \right\}.$$
(49)

When d''=d' the correction vanishes. This shows that when the center heights are equal there is no correction—regardless of the slope. If the slope is uniform throughout, the form of the correction is simplified and is invariably *negative*. Under the usual conditions the correction is *negative*, i.e., the method generally gives too large results.

75. Level sections. When the country is very level or when only approximate preliminary results are required, it is sometimes assumed that the cross-sections are level. The method of level sections is capable of easy and rapid computation. The area may be written as



This also follows from Eq. 48 when  $\alpha = 0$  and  $\tan \beta = \frac{1}{s}$ . s here represents the "slope ratio," i.e., the ratio of the horizontal projection of the slope to the vertical. A table is very readily formed giving the area in square feet of a section of given depth and for any given width of roadbed and ratio of side-slopes. The area may also be readily determined (as illustrated in the following example) without the use of such a table; a table of squares will facilitate the work. Assuming the cross-sections at equal distances (=l) apart, the total approximate volume for any distance will be

$$\frac{l}{2}[A_0+2(A_1+A_2+\ldots,A_{n-1})+A_n].$$
 (51)

The prismoidal correction may be directly derived from Eq. 46 as  $\frac{l}{12}[2(a+d')s-2(a+d'')s][(a+d'')-(a+d')]$ , which reduces to

$$-\frac{ls}{6}(d'-d'')^2$$
 or  $-\frac{b}{12}\frac{b}{a}(d'-d'')^2$ . (52)

This may also be derived from Eq. 49, since a=0, tan a=0, and tan  $\beta=2a \div b$  This correction is always negative, showing that the method of averaging end areas, when the sections are level, always gives too large results. The prismoidal correction for any one prismoid is therefore a constant times the square of a difference. The squares are always positive whether the differences are positive or negative. The correction therefore becomes

$$-\frac{l}{12}\frac{b}{a}\Sigma(d'\sim d'')^2.$$
 (53)

76. Numerical example: level sections. Given the following center heights for the same number of consecutive stations 106 feet apart; width of roadbed 18 feet; slope  $1\frac{1}{2}$  to 1.

The products in the fifth column may be obtained very readily and with sufficient accuracy by the use of the slide-rule described in §79. The products should be considered as  $(a+d)(a+d) \div \frac{1}{s}$ . In this problem  $s=1\frac{1}{2}, \frac{1}{s}=.6667$ . To apply the rule to the first case above, place 6667 on scale *B* over 89 on scale *A*, then opposite 89 on scale *B* will be found 118.8 on scale *A*. The position of the decimal point will be evident from an approximate mental solution of the problem.

§ 76.

Sta.	Center Height.	a+d	$(a+d)^2$	$(a+d)^2s$	Areas.	$d' \sim d''$	$(d' \sim d'')^2$
$     \begin{array}{r}       17 \\       18 \\       19 \\       20 \\       21 \\       22     \end{array} $	$     \begin{array}{r}       2.9 \\       4.7 \\       6.8 \\       11.7 \\       4.2 \\       1.6     \end{array} $	$\begin{array}{r} 8.9 \\ 10.7 \\ 12.8 \\ 17.7 \\ 10.2 \\ 7.6 \end{array}$	$\begin{array}{r} 79.21 \\ 114.49 \\ 163.84 \\ 313.29 \\ 104.04 \\ 57.76 \end{array}$	$\begin{array}{c}118.81\\171.74\\245.76\\469.93\\156.06\\86.64\end{array}$	$\times 2 = \begin{cases} 118.81\\ 343.48\\ 491.52\\ 939.86\\ 312.12\\ 86.64 \end{cases}$	$2.1 \\ 4.9 \\ 7.5$	$\begin{array}{r} 3.24 \\ 4.41 \\ 24.01 \\ 56.25 \\ 6.76 \end{array}$
$\frac{ab}{2} =$	$\frac{6 \times 18}{2} = 54$			10	$2292.43 \\ 0 \times 54 = \frac{540}{1752.43}$		94.67

- 54	1752.43
$\frac{1752.43 \times 100}{2 \times 27} = 3245 \text{ cub. yards}$	=approx.vol.
$\operatorname{Corr.} = -\frac{100 \times 18}{12 \times 6 \times 27} \times 94.67$	= -91 cub. yds.
3245 - 91 = 3154 cub. yds.	= exact volume.

The above demonstration of the correction to be applied to the approximate volume, found by averaging end areas, is introduced mainly to give an idea of the amount of that correction. Absolutely level sections are practically unknown, and the error involved in assuming any given sections as truly level will ordinarily be greater than the computed correction. If greater accuracy is required, more points should be obtained in the cross-sectioning, which will generally show that the sections are not truly level.

77. Equivalent sections. When sections are very irregular the following method may be used, especially if great accuracy is not required. The sections are plotted to scale and then a uniform slope line is obtained by stretching a thread so that the undulations are averaged and an *equivalent section* is obtained. The *center depth* (d) and the *slope angle* (a) of this line *can* be obtained from the drawing, but it is more convenient to measure the distances  $(x_l \text{ and } x_r)$  from the center. The area may then be obtained independent of the center depth as follows: Let  $s = \text{the slope ratio of the side slopes} = \cot \beta = \frac{b}{2a}$ . (See Fig. 50.) Then the

The true volume, according to the prismoidal formula, of a length of the road measured in this way will be

$$\frac{l}{6} \left[ \frac{x_{l}'x_{r}'}{s} - \frac{ab}{2} + 4\left( \frac{x_{l}' + x_{l}''}{2} \frac{x_{r}' + x_{r}''}{2} \frac{1}{s} - \frac{ab}{2} \right) + \frac{x_{l}''x_{r}''}{s} - \frac{ab}{2} \right].$$

If computed by averaging end areas, the approximate volume will be

$$\frac{l}{2}\left[\frac{x_l'x_r'}{s} - \frac{ab}{2} + \frac{x_l''x_r''}{s} - \frac{ab}{2}\right].$$

Subtracting this result from the true volume, we obtain as the correction

Correction = 
$$\frac{l}{6s}(x_{l}''-x_{l}')(x_{r}'-x_{r}'')$$
. (55)

This shows that if the side distances to either the right or left are equal at adjacent stations the correction is *zero*, and also that if the difference is small the correction is also small and very probably within the limit of accuracy obtainable by that method of cross-sectioning. In fact, as has already been shown in the latter part of § 75, it will usually be a useless

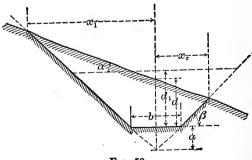


FIG. 50.

refinement to compute the prismoidal correction when the method of cross-sectioning is as rough and approximate as this method generally is.

78. Equivalent level sections. These sloping "two-level" sections are sometimes transformed into "level sections of equal

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area," and the volume computed by the method of level sections (§ 75). But the true volume of a prismoid with sloping ends does not agree with that of a prismoid with equivalent bases and level ends except under special conditions, and when this method is used a correction must be applied if accuracy is desired, although, as intimated before, the assumption that the sections have uniform slopes will frequently introduce greater inaccuracies than that of this method of computation. The following demonstration is therefore given to show the scope and limitations of the errors involved in this much used method.

To obtain  $d_1$  directly from notes, given in terms of d and  $\alpha$ , we may substitute the values of  $x_l$  and  $x_r$  given in §74, which gives

$$a+d_1=(a+d)\frac{\tan\beta}{\sqrt{\tan^2\beta-\tan^2 a}}=\frac{a+d}{\sqrt{1-s^2\tan^2 a}}$$
. (57)

The true volume of the equivalent section may be represented by

$$\frac{ls}{6} \left[ (a+d_1')^2 + 4\left(\frac{a+d_1'}{2} + \frac{a+d_1''}{2}\right)^2 + (a+d_1'')^2 \right].$$

From this there should be subtracted the volume of the "grade prism" under the roadbed to obtain the volume of the cut that would be actually excavated, but in the following comparison, as well as in other similar comparisons elsewhere made, the volume of the grade prism invariably cancels out, and so for the sake of simplicity it will be disregarded. This expression for volume may be transposed to

$$\frac{ls}{6} \left[ \frac{x_{l}'x_{r}'}{s^{2}} + 4\left( \frac{\sqrt{x_{l}'x_{r}'}}{2s} + \frac{\sqrt{x_{l}''x_{r}''}}{2s} \right)^{2} + \frac{x_{l}''x_{r}''}{s^{2}} \right].$$

§ 78.

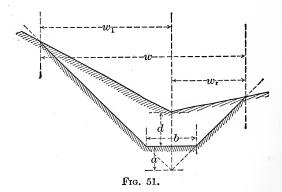
The true volume of the prismoid with sloping ends is (see § 77)

$$\frac{l}{6}\left[\frac{x_{l}'x_{r}'}{s}+4\left(\left(\frac{x_{l}'+x_{l}''}{2}\right)\left(\frac{x_{r}'+x_{r}''}{2}\right)\frac{1}{s}\right)+\frac{x_{l}''x_{r}''}{s}\right].$$

The difference of the two volumes

This shows that "equivalent level sections" do not in general give the true volume, there being an exception when  $xt'x_{r}''=xt''x_{r}'$ . This condition is fulfilled when the slope is uniform, i.e., when a'=a''. When this is nearly so the error is evidently not large. On the other hand, if the slopes are inclined in opposite directions the error may be very considerable, particularly if the angles of slope are also large.

79. Three-level sections. The next method of cross-sectioning in the order of complexity, and therefore in the order of



accuracy, is the method of three-level sections. The area of the section is  $\frac{1}{2}(a+d)(w_r+w_l)-\frac{ab}{2}$ , which may be written

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 $\frac{1}{2}(a+d)w - \frac{ab}{2}$ , in which  $w = w_r + w_l$  If the volume is computed by averaging end areas, it will equal

$$\frac{l}{4}[(a+d')w'-ab+(a+d'')w''-ab].$$
 (59)

If we divide by 27 to reduce to cubic yards, we have, when l=100,

Vol  $(,...,) = \frac{25}{27}(a+d')w' - \frac{25}{27}ab + \frac{25}{27}(a+d'')w'' - \frac{25}{27}ab$ For the next section

Vol  $(\dots, \dots) = \frac{25}{27}(a+d'')w'' - \frac{25}{27}ab + \frac{25}{27}(a+d''')w''' - \frac{25}{27}ab$ 

For a partial station length compute as usual and multiply result by  $\frac{\text{length in feet}}{100}$  The prismoidal correction may be obtained by applying Eq. 46 to each side in turn For the left side we have

$$\frac{l}{12}[(a+d')-(a+d'')](wl''-wl'), \text{ which equals},\\ \frac{l}{12}(d'-d'')(wl''-wl').$$

For the right side we have, similarly,

$$\frac{l}{12}(d'-d'')(wr''-wr').$$

The total correction therefore equals

$$\frac{l}{12}(d'-d'')[(wl''+wr'')-(wl'+wr')]$$
  
=  $\frac{l}{12}(d'-d'')(w''-w').$ 

Reduced to cubic yards, and with l=100,

Pris. Corr. 
$$=\frac{25}{81}(d'-d'')(w''-w')$$
. . . . (60)

When this result is compared with that given in Eq. 55 there is an apparent inconsistency. If two-level ground is considered as but a special case of three-level ground, it would seem as if

the same laws should apply. If, in Eq. 55,  $x_r' = x_r''$ , and  $x_l''$ is different from  $x_{i'}$ , the equation reduces to zero; but in this case d' would also be different from d''; and since  $x_l' + x_r'$ would =w', and  $x_{l}'' + x_{r}'' = w''$  in Eq. 60, w'' - w' would not equal zero and the correction would be some finite quantity and not zero. The explanation lies in the difference in the form and volume of the prismoids, according to the method of the formation of the warped surfaces. If the surface is supposed to be generated by the locus of a line moving parallel to the ends as plane directors and along two straight lines lying in the side slopes, then  $x_l^{\text{mid.}}$  will equal  $\frac{1}{2}(x_l'+x_l'')$ , and  $x_r^{\text{mid.}}$  will equal  $\frac{1}{2}(x_r'+x_r'')$ , but the profile of the center line will not be straight and  $d^{\text{mid.}}$  will not equal  $\frac{1}{2}(d'+d'')$ . On the other hand, if the surfaces be generated by two lines moving parallel to the ends as plane directors and along a straight center line and straight side lines lying in the slopes, a warped surface will be generated each side of the center line, which will have uniform slopes on each side of the center at the two ends and nowhere else. This shows that when the upper surface of earthwork is warped (as it generally is), two-level ground should not be considered as a special case of three-level ground. This discussion, however, is only valuable to explain an apparent inconsistency and error. The method of two-level ground should only be used when such refinements as are here discussed are of no importance as affecting the accuracy.

An example is given on the opposite page to illustrate the method of three-level sections.

In the first column of yards

 $210 = \frac{25}{27}(a+d)w = \frac{25}{27} \times 7.3 \times 31.1;$ 507, 734, etc., are found similarly; 595 = 210 - 61 + 507 - 61;  $448 = \frac{40}{100}(507 - 61 + 734 - 61);$  $602 = \frac{60}{100}(734 - 61 + 392 - 61);$ 449 = 392 - 61 + 179 - 61.

For the prismoidal correction,

$$-20 = \frac{25}{81} (d' - d'') (w'' - w') = \frac{25}{81} (2.6 - 8.1) (42.8 - 31.1)$$
$$= \frac{25}{81} (-5.5) (+11.7).$$

For the next line,  $-3 = \frac{40}{100} \int_{10}^{10} \frac{1}{81} (-2.6)(+8.7)$ ], and similarly for the rest. The "F" in the columns of center heights, as well

Station.	Station. Center.	Left.	Right.	a+d	m	Yaı	Yards.	ď' – ď"	w" – w'	Pris. Corr.	$x_l \sim x_r$	$\frac{V(x_l \sim x_r)}{3R} \begin{array}{ c } Curv. \\ Corr. * \end{array}$	Curv. Corr.*
17	2.6F	<u>10.6F</u> 22.9	$\frac{0.8F}{8.2}$	7.3	31.1	210		×			14.7	+1	
18	8.1F	15.8F 30.7	$\frac{3.4F}{12.1}$	12.8	42.8	507	595	-5.5	+11.7	-20	18.6	+	+4
+ 40	10.7F	$\frac{20.2F}{37.3}$	$\frac{4.8F}{14.2}$	15.4	51.5	734	448	-2.6	+ 8.7	00 	23.1	+6	+
19	6.4F	$\frac{14.0F}{28.0}$	$\frac{2.1F}{10.1}$	11.1	38.1	392	602	+4.3	-13.4	-11	17.9	+	+5
20	3.7F	$\frac{5.8F}{15.7}$	$\frac{0.2F}{7.3}$	8.4	23.0	179	449	+2.7	-15.1	-13	8.4	+1	+3
Roadbed, 14' Slope 14 to 1.	Roadbed, 14' wide in fill Slope 1 <del>}</del> to 1.	in fill.	_	Pri	$\frac{1}{\text{Approx. Vol.} = 2094}$ Pris. corr. = 47	ol. =	2094 47			2F-	_		+16
$a = \frac{b}{28} = \frac{14}{3} = 4.7;$	$\frac{14}{3} = \frac{4}{4}$			Tr	True Vol.	11	2047 (d	2047 (disregarding curv. corr.)*	curv. corr.)*	×			

\*For the derivation of the curvation correction, see § 93.

 $\frac{25}{27}ab = 61.$ 

§ 79.

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as in the columns of "right" and "left," are inserted to indicate fill for all those points. Cut would be indicated by "C."

80. Computation of products. The quantities  $\frac{25}{27}(a+d)w$ and  $\frac{25}{27}ab$  represent in each case the product of two variable terms and a constant. These products are sometimes obtained from tables which are calculated for all ordinary ranges of the variable terms as arguments. A similar table computed for  $\frac{25}{81}(d'-d'')(w''-w')$  will assist similarly in computing the prismoidal correction. Prof. Charles L. Crandall, of Cornell University, is believed to be the first to prepare such a set of tables, which were first published in 1886 in "Tables for the Computation of Railway and Other Earthwork." Another easy method of obtaining these products is by the use of a sliderule. A slide-rule has been designed by the author to accompany this volume.\* It is designed particularly for this special work, although it may be utilized for many other purposes for which slide-rules are valuable. To illustrate its use, suppose (a+d) = 28.2, and w = 62.4; then

$$\frac{25}{27}(a+d)w = \frac{28.2 \times 62.4}{1.08}$$
.

Set 108 (which, being a constant of frequent use, is specially marked) on the sliding scale (B) opposite 282 on the other scale (A), and then opposite 624 on scale B will be found 1629 on scale A, the 162 being read directly and the 9 read by estimation. Although strict rules may be followed for pointing off the final result, it only requires a very simple mental calculation to know that the result must be 1629 rather than 162.9 or 16290. For products less than 1000 cubic yards the result may be read directly from the scale; for products between 1000 and 5000 the result may be read directly to the nearest 10

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<sup>\*</sup> The first edition of this book was octavo, and a pasteboard slide-rule, especially marked, accompanied each volume. Cutting down the size of the pages to "pocket size" prevents the incorporation of the rule with the present edition. Any slide-rule with a logarithmic unit 22<sup>1</sup>/<sub>2</sub> inches long will do equally well provided that the ro8 mark is specially distinguished for ready use in computing the volume and that the 324 mark is similarly distinguished for use in **computing** the prismoidal correction.

yards, and the tenths of a division estimated. Between 5000 and 10000 yards the result may be read directly to the nearest 20 yards, and the fraction estimated; but prisms of such volume will never be found as simple triangular prisms—at least, an assumption that any mass of ground was as regular as this would probably involve more error than would occur from faulty estimation of fractional parts. Facilities for reading as high as 10000 cubic yards would not have been put on the scale except for the necessity of finding such products as  $\frac{2}{27}(9.1 \times 9.5)$ , for example. This product would be read off from the same part of the rule as  $\frac{2}{27}(91 \times 95)$ . In the first case the product (80.0) could be read directly to the nearest .2 of a cubic yard, which is unnecessarily accurate. In the other case, the product (8004) could only be obtained by estimating  $\frac{4}{20}$  of a division.

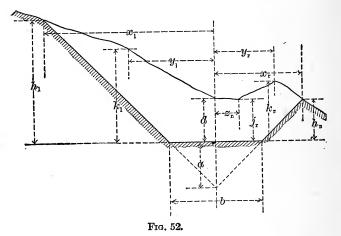
The computation for the prismoidal correction may be made similarly except that the divisor is 3.24 instead of 1.08. For example,  $\frac{25}{81}(5.5\times11.7) = \frac{5.5\times11.7}{3.24}$ . Set the 324 on scale *B* (also specially marked like 108) opposite 55 on scale *A*, and proceed as before.

81. Five-level sections. Sometimes the elevations over each edge of the roadbed are observed when cross-sectioning. These are distinctively termed "five-level sections." If the center, the slope-stakes, and one intermediate point on each side (not necessarily over the edge of the roadbed) are observed, it is termed an "irregular section." The field-work of cross-sectioning five-level sections is no less than for irregular sections with one intermediate point; the computations, although capable of peculiar treatment on account of the location of the intermediate point, are no easier, and in some respects more laborious; the cross-sections obtained will not in general represent the actual cross-sections as truly as when there is perfect freedom in locating the intermediate point; as it is generally inadvisable or unnecessary to employ five-level sections throughout the length of a road, the change from one method to another adds a possible element of inaccuracy and loses the advantage of uniformity of method, particularly in the notes and form of computations. On these accounts the method will not be further developed, except to note that this case, as well as any other, may be solved by dividing the whole prismoid into triangular prismoids, computing the volume by averaging end areas, and computing

the prismoidal correction by adding the computed corrections for each elementary triangular prismoid.

82. Irregular sections. In cross-sectioning irregular sections, the distance from the center and the elevation above "grade" of every "break" in the cross-section must be observed. The area of the irregular section may be obtained by computing the area of the trapezoids (*five*, in Fig. 52 and subtracting the two external triangles. For Fig. 52 the area would be

$$\frac{h_{l}+k_{l}}{2}(x_{l}-y_{l})+\frac{k_{l}+d}{2}y_{l}+\frac{d+j_{r}}{2}z_{r}+\frac{j_{r}+k_{r}}{2}(y_{r}-z_{r})$$
$$+\frac{k_{r}+h_{r}}{2}(x_{r}-y_{r})-\frac{h_{l}}{2}\left(x_{l}-\frac{b}{2}\right)-\frac{h_{r}}{2}\left(x_{r}-\frac{b}{2}\right).$$



Expanding this and collecting terms, of which many will cancel, we obtain

$$AREA = \frac{1}{2} \left[ x_l k_l + y_l (d - h_l) + x_r k_r + y_r (j_r - h_r) + z_r (d - k_r) + \frac{b}{2} (h_l + h_r) \right].$$
 (61)

An examination of this formula will show a perfect regularity in its formation which will enable one to write out a similar formula for any section, no matter how irregular or how many points there are, without any of the preliminary work. The formula may be expressed in words as follows:

AREA equals one-half the sum of products obtained as follows :

the distance to each slope-stake times the height above grade of the point next inside the slope-stake;

the distance to each intermediate point in turn times the height of the point just inside minus the height of the point just outside;

finally, one-half the width of the roadbed times the sum of the slope-stake heights.

If one of the sides is perfectly regular from center to slopestake, it is easy to show that the rule holds literally good. The "point next inside the slope-stake" in this case is the center; the intermediate terms for that side vanish. The *last term* must always be used. The rule holds good for three-level sections, in which case there are three terms, which may be reduced to two. Since these two terms are both variable quantities for each cross-section, the special method, given in § 78, in which one term  $\left(\frac{ab}{2}\right)$  is a constant for all sections, is preferable. In the general method, each intermediate "break" adds another term.

83. Volume of an irregular prismoid. This is obtained by computing first the approximate volume by "averaging end areas" or by multiplying the length by the half sum of the end areas, as computed from Eq. (61). In other words, the Approx. volume  $=\frac{100}{27} \times \frac{1}{2}$  (area'+area"). But since each area equals one-half the sum of products of width times height (see Eq. (61)) we may say that

Approx. volume =  $\frac{25}{27}$  (summation of *width* times *height*) . (62) the terms of width times height being like those found within the bracket of Eq. (61).

As before, for partial station lengths, multiply the result by (length in feet  $\div$  100). There will be no constant subtractive term,  $\frac{25}{27}ab$ , as in § 79.

The correction to this approximate volume is found by considering that for the purpose of this correction .nly the end sections are considered as "three-level" sections and the correction is computed by applying Eq. (60).

§ 83.

84. Numerical example; irregular sections; volume with approximate prismoidal correction. Assume the earthwork notes as given below, where the roadbed is 18 feet wide in cut and the slope is  $1\frac{1}{2}$  to 1. Note that the stations read UP the page and that when the surveyor is looking ahead along the line the several combinations of heights and distances out have approximately the same relative position on the note book as they have on the ground. For example, beginning at the bottom line (Sta. 16) the combination  $\frac{8.9c}{22.4}$  means that the extreme left-hand point of that section (the "slope stake") is 22.4 feet horizontally from the center and that it is 8.9 feet above the required roadbed. The cut (c) would be 8.9 feet to reach the roadbed, but of course the actual cutting is zero at the slope stake. The next point is 12.0 feet horizontally from the center and 7.6 feet above the roadbed. The cut at the center is 6.8 feet. The combinations of dimensions on the right-hand side are to be interpreted similarly.

Sta.	$Center \begin{cases} cut \\ or \\ fill. \end{cases}$		Left.		Rig	ht.
19	0.60	$\frac{3.6c}{14.4}$			$\frac{0.1c}{4.2}$	0.4c 9.6
18	2.30	$\frac{4.2c}{15.3}$	$\frac{6.8c}{8.4}$	$\frac{3.2c}{5.2}$		$\frac{1.2c}{10.8}$
17	7.60	8.2c 21.3	$\frac{10.2c}{17.4}$	$\frac{8.0c}{6.1}$		$\frac{4.2c}{15.3}$
+42	10.2c	$\frac{12.2c}{27.3}$		$\frac{12 \ 6c}{8.2}$	$\frac{6.2c}{7.5}$	$\frac{8.4c}{21.6}$
16	6.8c	$\frac{8.9c}{22.4}$		$\frac{7.6c}{12.0}$	$\frac{3.2c}{4.1}$	$\frac{2.6c}{12.9}$

The numerical computation is greatly facilitated by a systematic form as given below. For Sta. 16, the first term is "the distance to the left slope stake" (22.4) times "the height above grade of the point next inside" (the height being 7.6), and we place this pair of figures in the columns of "width" and "height." The "distance to the point next inside" is 12.0 and the "height of the point just inside (6.8) minus the

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height of the point just outside" (8.9) equals (-2.1) and these are the next pair of widths and heights. Taking  $\frac{25}{27}$  of the product of each pair of numbers we have the numbers in the first column of "yards." The sum of all these numbers in the first and second groups multiplied by  $\frac{42}{100}$  (that section being only 42 feet long) equals 378 cubic yards, the volume by averaging end areas. The determination of center heights and total widths and the application of Eq. (60), to obtain the approximate prismoidal correction, is self-evident.

VOLUME OF IRREGULAR PRISMOID, WITH APPROXIMATE PRISMOIDAL CORRECTION.

Sta.	W'th	H'ght	Ya	rds.	Cen. Height	Total width	d'-d''	w''-w'	Approx. pris.corr.	
16	$22.4 \\ 12.0 \\ 12.9 \\ 4.1 \\ 9.0$	$7.6 \\ -2.1 \\ 3.2 \\ 4.2 \\ 11.5$	$158 \\ -23 \\ 40 \\ 16 \\ 96$		+6.8	35.3				
+42	$27.3 \\ 8.2 \\ 21.6 \\ 7.5 \\ 9.0$	$ \begin{array}{r} 12.6 \\ -2.0 \\ 6.2 \\ 1.8 \\ 20.6 \end{array} $	$     \begin{array}{r}       319 \\       -15 \\       124 \\       13 \\       172     \end{array} $	378	+10.2	48.9	-3.4	+13.6	-14 (-6)	
17	$21.3 \\ 17.4 \\ 6.1 \\ 15.3 \\ 9.0$	$ \begin{array}{r} 10.2 \\ -0.2 \\ -2.6 \\ 7.6 \\ 12.4 \end{array} $	$ \begin{array}{r} 201 \\ - 3 \\ -14 \\ 107 \\ 103 \end{array} $	584	+ 7.6	36.6	+2.6	-12.3	-10 (-6)	
18	$15.3 \\ 8.4 \\ 5.2 \\ 10.8 \\ 9.0$	$ \begin{array}{r}     6.8 \\     -1.0 \\     -4.5 \\     2.3 \\     5.4 \end{array} $	95 - 7 - 22 - 23 - 45	528	+ 2.3	26.1	+5.3	-10.5	-17 (-17)	
19	$     \begin{array}{r}       14.4 \\       9.6 \\       4.2 \\       9.0 \\       9.0 \\       \end{array} $	$0.6 \\ 0.1 \\ 0.2 \\ 4.0$	$\begin{array}{c} 8\\1\\1\\33\end{array}$	177	+ 0.6	24.0	+1.7	-2.1	-1 (-1)	
	Approx. volume = $1667$ -30 Approx. pris. corr = $-30$									

Approx. pris. corr. = -30

Corrected volume = 1637 cubic yards

85. Magnitude of the probable error of this method. In previous editions of this work, methods were given for computing the mathematically exact volume of a prismoid whose ends coincide with the "irregular sections" as measured, and

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whose upper surfaces are assumed to coincide with the actual surface of the ground. As in the previous methods, the "approximate volume" is computed by averaging end areas and then a correction is applied. If the end sections have the same number of intermediate points on each side, and if it can be assumed that the corresponding lines in each section are connected by plane or warped surfaces, which coincide with the surface of the ground, then the mathematically exact or "true" correction may be obtained by dividing the volume into elementary triangular prismoids, finding the correction for each and adding the results. Although such a method appears very complicated, it is readily possible to develop a law by means of which the true prismoidal correction may be written out (similarly to writing out the formula for the area, Eq. (61)) without any preliminary calculation. Such a law has a mathematical fascination, but it should be remembered that when the ground surface is so broken up that the cross-sections are "irregular" it is in general correspondingly rough and irregular between the cross-sections, especially when those sections are 100 feet apart. It is also true that the cross-sections do not usually have the same number of intermediate points on corresponding sides of the center. In such a case, unless the actual form of the ground between the cross-sections is observed and measured, the exact method cannot be used. An extra point in one crosssection implies an extra ridge (or hollow) which "runs out" or disappears by the time the adjoining section is reached. Theoretically a cross-section should be taken at the point where such a ridge or hollow runs out. In general this point will not be at an even 100-foot station. The attempt to compute the exact prismoidal correction usually gives merely a false appearance of extreme accuracy to the work which is not justified by the results. It should not be forgotten that it is readily possible to spend an amount of time on the surveying and computing which is worth more than the few cubic yards of earth which represents the additional accuracy of the more precise method. The accuracy of the office computation should be kept proportionate to the accuracy of the cross-sectioning in the field. The discussion of the magnitude of the prismoidal correction in §§ 72-79 shows that it is small except when the two ends of the prismoid are very dissimilar. The dissimiliarity between the two ends of a prismoid would be substantially the same whether the ends were actually "irregular" or had "threelevel" sections, which for each end had the same slope stakes and center heights as the irregular sections. Experience proves that the approximate prismoidal correction, computed by considering the ground as three-level, is so nearly equal to the true prismoidal correction that the difference is perhaps no greater than the *probable* difference between the true volume of earth and the volume of the geometrical prismoid which is assumed to represent that volume. The experienced surveyor will take his cross-sections at such places and so close together that the warped surfaces joining the sections will lie very nearly in the surface or at least will so average the errors that they will substantially neutralize each other.

86. Numerical illustration of the accuracy of the approximate rule. The "true" prismoidal correction for the numerical case given in § 84 was computed by the method outlined above, and on the basis of certain figures as to the vanishing of the ridges and valleys found in one section and not found in the adjacent sections. The various quantities for the volumes between the cross-sections have been tabulated as shown.

	1	2	3	4	5	6	7
Sections.	Approx, vol. by averaging end areas.	True pris- moidal correction.	True volume.	Approx. pris. corr. on basis of three-level ground.	Error; Col.4 – col. 2.	Approx. vol. computed from center and side heights <i>only</i> .	Error; Col. 6 – col. 3
$\begin{array}{c} 16 \dots 16 + 42 \\ 16 + 42 \dots 17 \\ 17 \dots 18 \\ 18 \dots 19 \end{array}$	$     \begin{array}{r}       378 \\       584 \\       528 \\       177 \\       1667     \end{array} $	$ \begin{array}{r} - 5 \\ - 3 \\ - 16 \\ - 3 \\ - 27 \end{array} $	$     \begin{array}{r}       373 \\       581 \\       512 \\       174 \\       1649     \end{array} $	$ \begin{array}{r} - & 6 \\ - & 6 \\ - & 17 \\ - & 1 \\ - & 30 \\ \end{array} $	$     \begin{array}{r}       -1 \\       -3 \\       -1 \\       +2 \\       -3     \end{array}   $	396     577     463     147     1583	$     \begin{array}{r}       -23 \\       +4 \\       +49 \\       +27 \\       +57 \\       +57     \end{array} $

There has also been shown in the last two columns the error involved if the "intermediate points" had been ignored in the cross-sectioning. From the tabular form we may learn that 1. The *differences* between the "true" and approximate corrections is so small that it is *probably* swallowed up by errors

resulting from inaccurate cross-sectioning.2. The error which would have been involved in ignoring the intermediate points is so very large in comparison with

the other corresponding errors that (although it proves nothing absolutely definite, being an individual case) the *probabilities* of the relative error from these sources are clearly indicated.

87. Cross-sectioning irregular sections. The slope stake should preferably be determined first, and then the "breaks" between the slope stake and the center. When, as is usual, the ground is not even between the cross-section just taken and the section at the next 100-foot station, a point should be selected for a cross-section such that the lines to the previous section should coincide with the actual surface of the ground as closely as the accuracy of the work demands. § 94 gives a numerical illustration of the magnitude of some of these errors. Although it is possible for a skillful surveyor to so choose his cross-sections in rough and irregular ground that the positive and negative errors will nearly balance, it requires exceptional skill. Frequently the work may be simplified by computing separately the volume of a mound or pit, the existence of which has been ignored in the regular crosssectioning.

88. Side-hill work. When the natural slope cuts the roadbed there is a necessity for both cut and fill at the same cross-section.

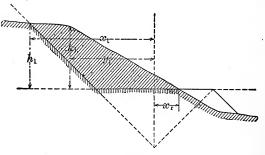


FIG. 53.

When this occurs the cross-sections of both cut and fill are often so nearly triangular that they may be considered as such without great error, and the volumes may be computed separately as triangular prismoids without adopting the more elaborate form of computation so necessary for complicated irregular sections. When the ground is too irregular for this the best plan is to

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follow the uniform system. In computing the cut, as in Fig. 53, the left side would be as usual; there would be a small center cut and an ordinate of zero at a short distance to the right of the center. Then, *ignoring the fill*, and applying Eq. 61 strictly, we have two terms for the left side, one for the right, and the term involving  $\frac{1}{2}b$ , which will be  $\frac{1}{2}bh_l$  in this case, since  $h_r=0$ , and the equation becomes

Area = 
$$\frac{1}{2} [x_l k_l + y_l (d - h_l) + x_r d + \frac{1}{2} b h_l].$$

The area for fill may also be computed by a strict application of Eq. 61, but for Fig. 54 all distances for the left side are zero and the elevation for the first point out is zero. d also must be

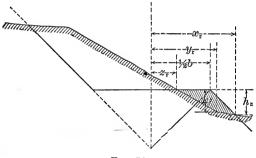


Fig. 54.

considered as zero. Following the rule, § 81, literally, the equation becomes

$$Area_{(Fill)} = \frac{1}{2} [x_r k_r + y_r (o - h_r) + z_r (o - k_r) + \frac{1}{2} b(o + h_r)],$$

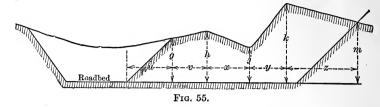
which reduces to

$$\frac{1}{2}[x_rk_r-y_rh_r-z_rk_r+\frac{1}{2}bh_r].$$

(Note that  $x_r$ ,  $h_r$ , etc., have different significations and values in this and in the preceding paragraphs.) The "terminal pyramids" illustrated in Fig. 40 are instances of side-hill work for very short distances. Since side-hill work always implies both cut and fill at the same cross-section, whenever either the cut or fill disappears and the earthwork becomes wholly cut or wholly fill, that point marks the end of the "side-hill work," and a cross-section should be taken at this point.

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89. Borrow-pits. The cross-sections of borrow-pits will vary not only on account of the undulations of the surface of the



ground. but also on the sides, according to whether they are made by widening a convenient cut (as illustrated in Fig. 55) or simply by digging a pit. The sides should always be propvrly sloped and the cutting made cleanly, so as to avoid unsightly roughness. If the slope ratio on the right-hand side (Fig. 55) is s, the area of the triangle is  $\frac{1}{2}sm^2$ . The area of the section is  $\frac{1}{2}[ug+(g+h)v+(h+j)x+(j+k)y+(k+m)z-sm^2]$ . If all the horizontal measurements were referred to one side as an origin, a formula similar to Eq. 61 could readily be developed, but little or no advantage would be gained on account of any simplicity of computation. Since the exact volume of the earth borrowed is frequently necessary, the prismoidal correction should be computed; and since such a section as Fig. 55 does not even approximate to a three-level section, the method suggested in § 83 cannot be employed. It will then be necessary to employ the more exact method of dividing the volume into triangular prismoids and taking the summation of their corrections, found according to the general method of § 72.

**go.** Correction for curvature. The volume of a solid, generated by revolving a plane area about an axis lying in the plane but outside of the area, equals the product of the given area times the length of the path of the center of gravity of the area. If the centers of gravity of all cross-sections lie in the center of the road, where the length of the road is measured, there is absolutely no necessary correction for curvature. If all the cross-sections in any given length were exactly the same and therefore had the same eccentricity, the correction for curvature would be very readily computed according to the above principle. But when both the areas and the eccentricities vary from point to point, as is generally the case, a theoretically exact

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solution is quite complex, both in its derivation and application. Suppose, for simplicity, a curved section of the road, of uniform cross-sections and with the center of gravity of every crosssection at the same distance e from the center line of the road The length of the path of the center of gravity will be to the length of the center line as  $R \pm e : R$ . Therefore we have True vol.: nominal vol. ::  $R \pm e : R$ .  $\therefore$  True vol. =  $lA \frac{R \pm e}{R}$  for a volume of uniform area and eccentricity. For any other area and eccentricity we have, similarly, True vol.' =  $lA' \frac{R \pm e'}{R}$ . This shows that the effect of curvature is the same as increasing (or diminishing) the area by a quantity depending on the area and eccentricity, the increased (or diminished) area being found by multiplying the actual area by the ratio  $\frac{R \pm e}{R}$ . This being independent of the value of l, it is true for infinitesimal lengths. If the eccentricity is assumed to vary uniformly between two sections, the equivalent area of a cross-section located midway between the two end cross-sections would be  $A_m \frac{\left(R \pm \frac{e' + e''}{2}\right)}{P}$  . Therefore the volume of a solid which, when straight, would be  $\frac{l}{6}(A'+4A_m+A'')$ , would then become

True vol. = 
$$\frac{l}{6R} \left[ A'(R \pm e') + 4 A_m \left( R \pm \frac{e' + e''}{2} \right) + A''(R \pm e'') \right].$$

Subtracting the nominal volume (the true volume when the prismoid is straight), the

$$Correction = \pm \frac{l}{6R} \left[ (A' + 2A_m)e' + (2A_m + A'')e'' \right].$$
(63)

Another demonstration of the same result is given by Prof. C. L. Crandall in his "Tables for the Computation of Railway and other Earthwork," in which is obtained by calculus methods the summation of elementary volumes having variable areas with variable eccentricities. The exact application of Eq. 63 requires that  $A_m$  be known, which requires laborious computa-

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tions, but no error worth considering is involved if the equation is written approximately

Curv. corr. = 
$$\frac{l}{2R}(A'e' + A''e'')$$
, . . . (64)

which is the equation generally used. The approximation consists in assuming that the difference between A' and  $A_m$  equals the difference between  $A_m$  and A'' but with opposite sign. The error due to the approximation is always utterly insignificant.

**91.** Eccentricity of the center of gravity. The determination of the true positions of the centers of gravity of a long series of irregular cross-sections would be a very laborious operation, but fortunately it is generally sufficiently accurate to consider the cross-sections as three-level ground, or, for side-bill work, to

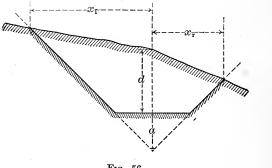


Fig. 56.

be triangular, for the purpose of this correction. The eccentricity of the cross-section of Fig. 56 (including the grade triangle) may be written

$$e^{\frac{(a+d)x_{l}x_{l}}{2} - \frac{(a+d)x_{r}}{\frac{(a+d)x_{l}}{2} + \frac{(a+d)x_{r}}{2} - \frac{x_{r}}{3}} = \frac{1}{3} \frac{x_{l}^{2} - x_{r}^{2}}{x_{l} + x_{r}} = \frac{1}{3} (x_{l} - x_{r}). \quad (65)$$

The side toward  $x_l$  being considered positive in the above demonstration, if  $x_r > x_l$ , *e* would be negative, i.e., the center of gravity would be on the right side. Therefore, for three-level ground, the correction for curvature (see Eq. 64) may be written

$$Correction = \frac{l}{6R} [A'(x_{l}' - x_{r}') + A''(x_{l}'' - x_{r}'')].$$

Since the approximate volume of the prismoid is

$$\frac{l}{2}(A + A') = \frac{l}{2}A' + \frac{l}{2}A'' = V' + V'',$$

in which V' and V'' represent the number of cubic yards corresponding to the area at each station, we may write

Corr. in cub. yds. = 
$$\frac{1}{3R} [V'(x_l' - x_r') + V''(x_l'' - x_r'')].$$
 (66)

It should be noted that the value of e, derived in Eq. 65, is the eccentricity of the whole area including the triangle under the roadbed. The eccentricity of the true area is greater than this and equals

$$e \times \frac{\text{true area} + \frac{1}{2}ab}{\text{true area}} = e_1.$$

The required quantity  $(\underline{A'e'}$  of Eq. 64) equals *true* area  $\times e_1$ which equals (*true* area  $+\frac{1}{2}ab$ )  $\times e$ . Since the value of e is very simple, while the value of  $e_1$  would, in general, be a complex quantity, it is easier to use the simple value of Eq. 65 and add  $\frac{1}{2}ab$  to the area. Therefore, in the case of three-level ground the subtractive term  $\frac{25}{27}ab$  (§ 79) should not be subtracted in computing this correction. For irregular ground, when computed by the method given in §§ 82 and 83, which does not involve the grade triangle, a term  $\frac{25}{27}ab$  must be added at every station when computing the quantities V' and V'' for Eq. 66.

It should be noted that the factor  $1 \div 3R$ , which is constant for the length of the curve, may be computed with all necessary accuracy and without resorting to tables by remembering that

$$R = \frac{5730}{\text{degree of curve}}.$$

Since it is useless to attempt the computation of railroad earthwork closer than the nearest cubic yard, it will frequently 106

be possible to write out all curvature corrections by a simple mental process upon a mere inspection of the computation sheet. Eq. 66 shows that the correction for each station is of the form  $\frac{V(x_l-x_r)}{3R}$ . 3*R* is generally a large quantity—for a 6° curve it is 2865.  $(x_l-x_r)$  is generally small. It may frequently be seen by inspection that the product  $V(x_l-x_r)$  is roughly twice or three times 3*R*, or perhaps less than half of 3*R*, so that the corrective term for that station may be written 2, 3, or 0 cubic yards, the fraction being disregarded. For much larger absolute amounts the correction must be computed with a correspondingly closer percentage of accuracy.

The algebraic sign of the curvature correction is best determined by noting that the center of gravity of the cross-section is on the right or left side of the center according as  $x_r$  is greater or less than  $x_i$ , and that the correction is *positive* if the center of gravity is on the *outside* of the curve, and *negative* if on the *inside*.

It is frequently found that  $x_l$  is uniformly greater (or uniformly less) than  $x_r$  throughout the length of the curve. Then the curvature correction for each station is uniformly positive or negative. But in irregular ground the center of gravity is apt

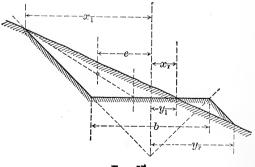


FIG. 57.

to be irregularly on the outside or on the inside of the curve, and the curvature correction will be correspondingly positive or negative. If the curve is to the *right*, the correction will be positive or negative according as  $(x_l - x_r)$  is positive or negative; if the curve is to the *left*, the correction will be positive or negative according as  $(x_r-x_l)$  is positive or negative. Therefore when computing curves to the *right* use the form  $(x_l-x_r)$  in Eqs. 66 and 68; when computing curves to the *left* use the form  $(x_r-x_l)$  in these equations; the algebraic sign of the correction will then be strictly in accordance with the results thus obtained.

92. Center of gravity of side-hill sections. In computing the correction for side-hill work the cross-section would be treated as triangular unless the error involved would evidently be tool great to be disregarded. The center of gravity of the triangle lies on the line joining the vertex with the middle of the base and at  $\frac{1}{3}$  of the length of this line from the base. It is therefore equal to the distance from the center to the foot of this line plus  $\frac{1}{3}$  of its horizontal projection. Therefore

By the same process as that used in § 91 the correction equation may be written

Corr. in cub. yds. = 
$$\frac{1}{3R} \left[ V' \left( \frac{b}{2} + (x_l' - x_r') \right) + V'' \left( \frac{b}{2} + (x_l'' - x_r'') \right) \right].$$
 (68)

It should be noted that since the grade triangle is not used in this computation the volume of the grade prism is *not* involved in computing the quantities V' and V''.

The eccentricities of cross-sections in side-hill work are *never* zero, and are frequently quite large. The total volume is generally quite small. It follows that the correction for curvature is generally a vastly larger proportion of the total volume than in ordinary three-level or irregular sections.

If the triangle is wholly to one side of the center, Eq. 67 can still be used. For example, to compute the eccentricity of the triangle of fill, Fig. 57, denote the two distances to the slopestakes by  $y_r$  and  $-y_l$  (note the minus sign). Applying Eq. 67 literally (noting that  $\frac{b}{2}$  must here be considered as negative in order to make the notation consistent) we obtain

$$e = \frac{1}{3} \left[ -\frac{b}{2} + (-y_l - y_r) \right],$$

which reduces to

$$e = -\frac{1}{3} \left[ \frac{b}{2} + y_l + y_r \right]. \qquad (69)$$

As the algebraic signs tend to create confusion in these formule, it is more simple to remember that for a triangle lying on both sides of the center e is always numerically equal to  $\frac{1}{3}\left[\frac{b}{2}+(x_l\sim x_r)\right]$ , and for a triangle entirely on one side, e is numerically equal to  $\frac{1}{3}\left[\frac{b}{2}+\text{the numerical sum of the two dis$  $tances out]}$ . The algebraic sign of e is readily determinable as in § 91. 93. Example of curvature correction. Assume that the fill in § 79 occurred on a 6° curve to the rtght.  $\frac{1}{3R} = \frac{1}{2865}$ . The quantities 210, 507, etc., represent the quantities V', V'', etc., since they include in each case the 61 cubic yards due to the grade prism. Then

$$\frac{V(x_l \sim x_r)}{3R} = \frac{210(22.9 - 8.2)}{2865} = \frac{3101.7}{2865} = +1.$$

The sign is plus, since the center of gravity of the cross-section is on the left side of the center and the road curves to the right, thus making the true volume larger. For Sta. 18 the correction, computed similarly, is +3, and the correction for the whole section is 1+3=4. For Sta. 18+40 the correction is computed as 6 yards. Therefore, for the 40 feet, the correction is  $\frac{400}{100}(3+6)=3.6$ , which is called 4. Computing the others similarly we obtain a total correction of +16 cubic yards.

§ 93.

94. Accuracy of earthwork computations. The preceding methods give the precise volume (except where approximations are distinctly admitted) of the prismoids which are supposed to represent the volume of the earthwork. To appreciate the accuracy necessary in cross-sectioning to obtain a given accuracy in volume, consider that a fifteen-foot length of the cross-section, which is assumed to be straight, really sags 0.1 foot, so that the cross-section is in error by a triangle 15 feet wide and 0.1 foot high. This sag 0.1 foot high would hardly be detected by the eye, but in a length of 100 feet in each direction it would make an error of volume of 1.4 cubic vards in each of the two prismoids, assuming that the sections at the other ends were perfect. If the cross-sections at both ends of a prismoid were in error by this same amount, the volume of that prismoid would be in error by 2.8 cubic yards if the errors of area were both plus or both minus. If one were plus and one minus, the errors would neutralize each other, and it is the compensating character of these errors which permits any confidence in the results as obtained by the usual methods of cross-sectioning. It demonstrates the utter futility of attempting any closer accuracy than the nearest cubic yard. It will thus be seen that if an error really exists at any cross-section it involves the prismoids on both sides of the section, even though all the other cross-sections are perfect. As a further illustration, suppose that cross-sections were taken by the method of slope angle and center depth (§ 74), and that a cross-section, assumed as uniform, sags 0.4 foot in a width of 20 feet. Assume an equal error (of same sign) at the other end of a 100-foot section. The error of volume for that one prismoid is 38 cubic yards.

The computations further assume that the warped surface, passing through the end sections, coincides with the surface of the ground. Suppose that the cross-sectioning had been done with mathematical perfection; and, to assume a simple case, suppose a sag of 0.5 foot between the sections, which causes an error equal to the volume of a pyramid having a base of 20 feet (in each cross-section) times 100 feet (between the cross-sections) and a height of 0.5 foot. The volume of this pyramid is  $\frac{1}{2}(20 \times 100) \times 0.5 = 333$  cub. ft. = 12 cub. yds. And yet this sag or hump of 6 inches would generally be utterly unnoticed, or at least disregarded.

When the ground is very rough and broken it is sometimes

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practically impossible, even with frequent cross-sections, to locate warped surfaces which will closely coincide with all the sudden irregularities of the ground. In such cases the computations are necessarily more or less approximate and dependence must be placed on the compensating character of the errors.

95. Approximate computations from profiles. When a "paper location" has been laid out on a topographical map having contours, it is possible to compute approximately the amount of earthwork required by some very simple and rapid calculations. A profile may be readily drawn by noting the intersections of the proposed center line with the various contours and plotting the surface line on profile paper. Drawing the grade-line on the profile, the depth of cut or fill may be scaled off at any point. When it is only desired to obtain

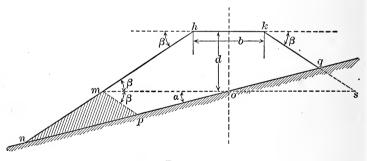


FIG. 58.

very quickly an approximate estimate of the amount of earthwork required on a suggested line, it may be done by the method described in § 75, or by the use of Table XXXIII. But the assumption that the surface of the ground at each cross-section is level invariably has the effect that the estimated volumes are not as large as those actually required. The difference between the "level section" hkms and the actual slope section hknq equals the difference between the triangles mon and oqs, and this difference equals the shaded area mpn. The excess volume is proportional to the area of the triangle mpn. This area may be expressed by the formula,

Area  $mpn = 2(\frac{1}{2}b + d \cot \beta)^2 \frac{\sin^2 \alpha \sin \beta \cos \beta}{\cos 2\alpha - \cos 2\beta}$ .

The percentage of this excess area to the nominal area hkmstherefore depends on the dimensions b and d and the angles  $\alpha$ and  $\beta$ . A solution of this equation for ninety different combinations of various numerical values for these four variables is included in Table XXXIII for the purpose of making corrections. A study of this correction table points conclusively to the following laws, a thorough understanding of which will enable an engineer to appreciate the degree of accuracy which is attainable by this approximate method:

(a) Increasing the *width* of the roadbed (b), the other three factors remaining constant, *increases* the percentage of error, but the increase is comparatively small.

(b) Increasing the *depth* of cut or fill (d), *decreases* the percentage of error, but the decrease is almost insignificant.

(c) Increasing the angle of the side slopes  $(\beta)$  decreases the percentage of error, the decrease being very considerable.

(d) Increasing the angle of the slope of the ground  $(\alpha)$ , increases the percentage of error, the percentage rapidly increasing to infinity as the value of  $\alpha$  approaches that of  $\beta$ . This is another method of stating the fact that  $\alpha$  must always be less than  $\beta$  and, practically, must be considerably less, so that the slope stake shall be within a reasonable distance from the center.

Since the above value for the corrective area is a function of the angle  $\alpha$ , which is usually variable and whose value is frequently known only approximately, it is useless to attempt to apply the correction with great precision, and the following rules will usually be found amply accurate, considering the probable lack of precision in the data used.

1. For embankments or cuts, having a slope of 1.5:1, and with a surface slope of 5° (nearly 9%) the excess of true area over nominal area is *about* 2%. There is only a slight variation from this value for all ordinary depths (d) and widths (b) of roadbed. Therefore the nominal volume would be about 2% too *small*. On the other hand, the effect of the prismoidal correction is such that, even with truly level sections, the nominal volume is too *large*. See §§ 75 and 76. The amount of the prismoidal correction depends on the differences between successive center depths. In the very ordinary numerical case given in § 76, the correction was nearly 3%, which more than neutralizes the error due to surface slope. Therefore in many cases on slightly sloping ground the error due to the surface slope will so nearly neutralize the prismoidal correction that the quantities taken directly from the tables (without correction for either cause) will equal the true volume with as close an approach to accuracy as the precision of the surveying will permit.

2. For a cut with a slope of 1:1, and with a surface slope of  $5^{\circ}$  the error is about 1%. This will be neutralized by still smaller prismoidal corrections. Therefore, for surface slopes of  $5^{\circ}$  or less, no allowance should be made for this error unless the prismoidal correction is also considered.

3. When the surface slope is  $10^{\circ}$  (nearly 18%) the error for a 1.5:1 slope is from 7% to 10% and for a 1:1 slope from 3% to 5%.

4. For a 30° surface slope and 1.5:1 side slopes the excess volume is three or four times the nominal volume. Such a steep surface slope implies the probability of "side-hill work" to which the above corrective rules are not applicable. When the surface slopes are very steep careful work must be done to avoid excessive error. For a 1:1 side slope, the errors are from 50% to 80%.

A still closer approximation, especially for the steeper surface slopes, may be obtained by using, directly or by interpolation, figures from the corrective tabular form which forms part of Table XXXIII. Unless the surface slope angle is known accurately (especially when large) no great accuracy in the final result is possible. Close accuracy would also require the determination of the prismoidal correction. But if such close accuracy is deemed essential, it can be most easily obtained by accurate cross-sectioning at each station and the adoption of other methods of computation—such as are given in §§ 83 and 84.

When the contours have been drawn in for a sufficient distance on either side to include the position of both slope stakes at every station, as will usually be the case, cross-sections may be obtained by drawing lines on the map at each station perpendicular to the center line—see Fig. 4. The intersection of these lines with the contours will furnish the distances for drawing on cross-section paper the transverse profile at each station. Drawing on the same cross-section the lines representing the roadbed and the side slopes, the cross-section of cut (or fill) is complete and its area may be obtained by scaling from the cross-section paper. If the contours have been located on the map with sufficient accuracy, such a method will determine the cross-sectional area very closely. When cross-sections have been taken with a wye- or hand-level, as described in § 12, the cross-sections as plotted will probably be more accurate than when the contours are run in from points determined by the stadia method. In fact this semigraphical method is frequently used, in place of the purely numerical methods described in previous sections, to make final estimates of the volume of earthwork.

As a numerical example, an assumed location line was laid out on the contours given in Fig. 4. The volume of cut, as determined by Table XXXIII for a roadbed 20 feet wide, with side slopes of 1:1, was 5746 cubic yards. The surface slope varied from 3° to 11°. Computing the corrections by a careful interpolation from the corrective table, the total correction was found to be 128 cubic yards, or an average of a little over 2%. On the other hand the negative prismoidal correction amounts to 72 cubic yards, which leaves a net correction of 56 cubic yards—about 1%. It so happens that in this case a correction. These figures merely verify numerically the general conclusions stated above, although it should not be forgotten that in individual cases the figures taken from Table XXXIII require ample correction.

The following approximate rule, for which the author is indebted to Mr. W. H. Edinger, is exceedingly useful when it is desired to rapidly determine the approximate volume of earthwork between two points along the road. Its great merit lies in the fact that it only means the memorizing of a comparatively simple rule which will make it possible to make such computations in the field, without the use of tables. The rule is based on the fact that the area of any level section equals  $bd + sd^2$ ; and therefore,

$$\Sigma(\text{vol.}) = (b \Sigma d + s \Sigma d^2) \frac{L}{27},$$

in which L is usually 100 feet. For strict accuracy this would only be the volume provided the total length was an even number of hundred feet, and the various values of d represented the depths which were uniform for hundred foot sections. It makes no allowance for the comparatively large prismoidal error of the pyramidal and wedge-shaped sections usually found at each end of a cut or fill, but where an approximate estimate is desired, in which this inaccuracy may be neglected, the method is very useful. The method of applying this rule without tables may best be illustrated by a simple numerical example. Assume that the levels on a stretch of fairly level ground, which is about 500 feet long, have been taken, the depths being taken at points 100 feet apart, the first and last points being about 40 or 50 feet from the ends of the cut, or fill. The depths are as given in the first column in the tabular form below; the slope is 1.5:1, and the breadth (b) is 14 feet.

d	$d^{i}$
1.6	2.56
2.8	7.84
4.5	20.25
3.1	9.61
0.9	.81
$\Sigma d = 12.9$	$\Sigma d^2 = 41.07$
14	20.53
$b\Sigma d = 180.6$	$s\Sigma d^2 = 61.60$
61.60	
242.2	
$24220 \div 27 = 897$	cubic yards.

The 180.6 is the  $b\Sigma d$  and the 61.6 is  $s\Sigma d^2$ ; adding these and moving the decimal point two places to multiply by 100, we only have to divide by 27 to obtain the value in cubic yards. Although the above rule requires more work than the employment of earthwork tables, yet it is a very convenient method of estimating the approximate volume of a short section of earthwork when no tables are at hand.

96. Shrinkage of earthwork. The statistical data indicating the amount of shrinkage is very conflicting, a fact which is probably due to the following causes:

1. The various kinds of earthy material act very differently as respects shrinkage. There is a great lack of uniformity in the *classification of earths* in the tests and experiments which have been made.

2. Very much depends on the *method* of forming an embankment (as will be shown later). Different reports have been based on different methods—often without mention of the method.

3. An embankment requires considerable *time* to shrink to its final volume, and therefore much depends on the time elapsed between construction and the measurement of what is supposed to be the settled volume.

4. A soft subsoil will frequently settle under the weight of a high embankment and apparently indicate a far greater shrinkage than the actual reduction in volume.

5. An embankment of very soft material will sometimes "mush" or widen at the sides, with a consequent settling of the top, due to this cause alone.

This subject has called forth much discussion in the technical press and literature. Quotations can be made of figures covering a large range of values, but space will only permit the statement of the conclusions which may be drawn from the large mass of testimony which has been presented.

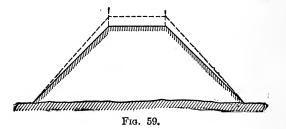
1. Volume of loose material. When material of any character is excavated and deposited loosely in a pile, its volume is always largely in excess of the volume of the excavation. Solid rock will occupy from 60% to 80% more space when broken up than when solid. A soft earth will have an excess volume of about 20% to 25%.

2. Effect of method of depositing. When material is deposited loosely, as from a trestle, the excess of volume when the embankment is just completed is very large. The time required for final settlement is also very great. When an embankment is formed by the wheelbarrow method, the initial expansion is about as great as when the material is merely dumped from cars. When the material is deposited in small increments from wagons and each layer is subjected to compression from horses' hoofs and from wheels, the contraction during construction is far greater and the additional shrinkage is comparatively small. Wheeled scrapers and drag scrapers will produce even more initial compression.

3. Time required for final settlement. This depends partly on the method of formation and also on the character of the material. When a soft loamy soil is deposited loosely, the drying out of the soil during the first long dry season will develop large cracks. Subsequent rains will close these cracks by a general contraction of the whole mass. When the embankment is loosely formed it may take two years before additional settlement becomes inappreciable, but when the method of deposition ensures compression during construction the *subsequent* shrinkage is less in time as well as amount.

4. Classification of soils with respect to shrinkage. Loose vegetable surface soil will expand very greatly when excavated and first deposited, but will subsequently shrink to considerably less than its original volume. Clay soils are next in order and the sandy and gravelly soils come at the other end of the list of earthy materials. Rock expands very greatly when first broken up and deposited and there is no appreciable subsequent shrinkage.

97. Proper allowance for shrinkage. Specifications for the Mississippi River levees require that there shall be a 10% shrinkage allowance for embankments formed by team work and 25% allowance for wheelbarrow work. It is contended



that such figures are only justified because the subsoil settles or because the embankments mush out at the sides, and that if these effects do not occur the levees are permanently higher than designed.

It is usual to require that embankments shall be constructed higher than their desired ultimate, as shown in Fig. 59. Since the base does not contract, the contraction may be said to be all vertical. Since a high embankment will unquestionably shrink a greater total amount than a low embankment (whatever the percentage), it follows that an embankment having variable heights (as usual) should have an initial grade-line somewhat like the dotted line *adc* in Fig. 60. Although some such method is essential if there is to be no ultimate sag below the desired grade-line, the policy is sharply criticized. The grade *ad*, even though temporary, may prove objectionable from an operating standpoint. Frequently the allowance is made too great or the shrinkage is not as much as anticipated, and it becomes necessary to cut off the top of the bank. On the other hand, the expense of raising the track after the road is in operation and the inevitable loss of ballast is so great that the danger of being required to fill up a sag should be avoided if possible.

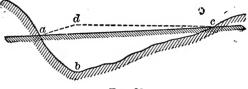


FIG. 60.

A sharp and clear distinction should be made between the *coefficient of extra height* of an embankment and the *coefficient* of shrinkage which determines how many cubic yards of settled embankment may be made from a definite volume of earth or rock measured in the excavation. The values quoted above for the Mississippi levees (from 10% to 25%) refers usually to a very soft soil and includes the effects other than actual contraction of volume. From 8% to 15% is usually quoted as the required extra height of embankments, although it is strenuously claimed by many that 3% or 2% is sufficient, or even that *no* allowance should be made.

The coefficients to determine the amount of settled embankment which may be made from a given volume of earth or rock measured in the excavation, are necessarily subject to variation on account of the method employed and the amount of compression and settlement which will take place during the progress of the work. The following figures have the weight of considerable authority but, if in error, the coefficients are probably high rather than low:

Gravel or sand	about	8%
Clay	"	10%
Loam	"	12%
Loose vegetable surface soil	"	15%

It may be noticed from the above table that the harder and cleaner the material the less is the contraction. Perfectly clean gravel or sand would not probably change volume appreciably. The above coefficients of shrinkage and expansion may be used to form the following convenient table:

Material.	To make 1000 cubic yards of embankment will require	1000 cubic yards measured in exca- vation will make
Gravel or sand Clay Loam Loose vegetable soil Rock, large pieces small ''	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	920 cubic yards 900 ** ** 880 ** ** 1400 ** ** 1600 ** ** of embankment.

Since writing the above the following values have been adopted by the American Railway Engineering and Maintenance of Way Association as representing standard practice:

COEFFICIENTS OF SHRINKAGE ALLOWANCE FOR DEPOSITING EARTHWORK.

	Trestle filling.	Raising under traffic.
Black dirt Clay Sand	$15\% \\ 10\% \\ 6\%$	5% 5% 5%

98. Methods of forming embankments. Embankments of moderate height are sometimes formed by scraping material with drag scrapers from ditches at the sides, especially if there is little or no cutting to be done in the immediate vicinity. Over a low level swampy stretch this method has the double advantage of building an embankment which is well above the general level and also provides generous drainage ditches which keep the embankment dry. Wheeled scrapers may be used economically up to a distance of 400 feet to excavate cuts and deposit the material on low embankments. Such methods have the advantage of compacting the embankments during construction and reducing future shrinkage.

When carts are used, an embankment of any height may be formed by "dumping over the end" and building to the full height (or even higher to allow for shrinkage) as the embankment proceeds. The method is especially applicable when the material comes from a place as high as or higher than the grade-line, so that no up-hill hauling is necessary. Only a small contractor's plant is required for all of these methods.

Trestles capable of carrying carts, or even cars and locomotives, from which excavated material may be dropped, are found to be economical in spite of the fact that their cost is a construction expense. There is the disadvantage that such embankments require a long time to settle, but there are the advantages that the earth may be hauled by the train load from a distance of perhaps several miles, dumped from the

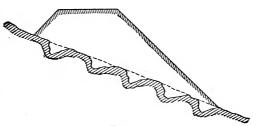


FIG. 61.

cars by train ploughs, or automatically dumped when the material is carried in patent dumping-cars, and all at a comparatively small cost per cubic yard. The disadvantages of slow settlement may be obviated, although at some additional cost, by making the trestle sufficiently strong to support regular traffic until the settlement is complete.

During recent years cableways have been utilized to fill comparatively narrow but deep ravines from material obtainable on either side of the ravine. This method obviates the construction of an excessively high trestle which might otherwise be considered necessary.

When an embankment is to be placed on a steep side hill which has a slippery clay surface, the embankment will sometimes slide down the hill, unless means are taken to prevent it. Some sort of bond between the old surface and the new material becomes necessary. This has sometimes been provided by cutting out steps somewhat as is illustrated in Fig. 61. It is possible that a deep ploughing of the surface would accomplish the result just as effectively and much cheaper. The tendency to slip is generally due not only to the nature of the soil but also to the usual accompanying characteristic that the soil is wet and springy. The sub-surface drainage of such a place with tile drains will still further prevent such slipping, which often proves very troublesome and costly.

### COMPUTATION OF HAUL.

99. Nature of subject. As will be shown later when analyzing the cost of earthwork, the most variable item of cost is that depending on the distance hauled. As it is manifestly impracticable to calculate the exact distance to which every individual cartload of earth has been moved, it becomes necessary to devise a means which will give at least an equivalent of the haulage of all the earth moved. Evidently the average haul for any mass of earth moved is equal to the distance from the center of gravity of the excavation to the center of gravity of the embankment formed by the excavated material. As a rough approximation the center of gravity of a cut (or fill) may sometimes be considered to coincide with the center of gravity of that part of the profile representing it, but the error is frequently very large. The center of gravity may be determined by various methods. but the method of the "mass diagram" accomplishes the same ultimate purpose (the determination of the haul) with all-sufficient accuracy and also furnishes other valuable information.

100. Mass diagram. In Fig. 62 let  $A'B' \ldots G'$  represent a profile and grade line drawn to the usual scales. Assume A'to be a point past which no earthwork will be hauled. Such a point is determined by natural conditions, as, for example, a river crossing, or one end of a long level stretch along which no grading is to be done except the formation of a low embankment from the material excavated from ample drainage ditches on each side. Above the profile draw an indefinite horizontal line (ACn in Fig. 62), which may be called the "zero line." Above every station point in the profile draw an ordinate (above or be-

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low the zero line) which will represent the algebraic sum of

the cubic vards of cut and fill (calling cut + and fill -) from the point A' to the point considered. The computations of these ordinates should first be made in tabular form as shown below. In doing this shrinkage must be allowed for by considering how much embankment would actually be made by so many cubic yards of excavation of such material. For example, it will be found that 1000 cubic yards of sand or gravel, measured in place (see § 97), will make about 920 cubic yards of embankment; therefore all cuttings in sand or gravel should be discounted in about this proportion. Excavations in rock should be increased in the proper ratio. In short, all excavations should be valued according to the amount of settled embankment that could be made from them. Place in the first column a list of the stations: in the second column, the number of cubic yards of cut or fill between each station and the preceding station; in

ROFIL MASS CURVI Fig. 62.—Mass Diagram

the third and fourth columns, the kind of material and the proper shrinkage factor; in the fifth column, a repetition of the quantities in cubic yards, except that the excavations are diminished (or increased, in the case of rock) to the number of cubic yards of settled embankment which may be made from them. In the sixth column place the *algebraic sum* of the quantities in the fifth column (calling cuts + and fills -) from the startingpoint to the station considered. These algebraic sums at each station will be the ordinates, drawn to some scale, of the mass curve. The scale to be used will depend somewhat on whether

### RAILROAD CONSTRUCTION.

the work is heavy or light, but for ordinary cases a scale of 5000 cubic yards per inch may be used. Drawing these ordinates to scale, a curve  $A, B, \ldots G$  may be obtained by joining the extremities of the ordinates.

Sta.	$\left  \text{Yards} \left\{ \begin{array}{l} \text{cut} + \\ \text{fill} - \end{array} \right. \right.  ight.$	Material.	Shrinkage factor.	Yards, reduced for shrinkage.	Ordinate in mass curve.
$\begin{array}{r}$	$\begin{array}{c} & & + & 195 \\ & + & 1792 \\ & + & 614 \\ & - & 143 \\ & - & 906 \\ & - & 1985 \\ & - & 1721 \\ & - & 112 \\ & + & 177 \\ & + & 180 \\ & - & 52 \\ & - & 71 \\ & + & 276 \\ & + & 1242 \\ & + & 1302 \end{array}$	Clayey soil """" Hard rock Clayey soil """	- 10 per cent - 10 " - 10 " - 10 " - 10 " - 10 per cent + 60 per cent - 10 per cent - 10 per cent - 10 "	$\begin{array}{c}$	$\begin{array}{c} 0\\ + 175\\ + 1788\\ + 2341\\ + 2198\\ + 1292\\ - 693\\ - 2414\\ - 2526\\ - 2243\\ - 1954\\ - 2006\\ - 2077\\ - 1828\\ - 710\\ + 462\\ \end{array}$

## 101. Properties of the mass curve.

1. The curve will be rising while over cuts and falling while over fills.

2. A tangent to the curve will be horizontal (as at B, D, E, F, and G) when passing from cut to fill or from fill to cut.

3. When the curve is *below* the "zero line" it shows that material must be drawn *backward* (to the left); and *vice versa*, when the curve is *above* the zero line it shows that material must be drawn *jorward* (to the right).

4. When the curve crosses the zero line (as at A and C) it shows (in this instance) that the cut between A' and B' will just provide the material required for the fill between B' and C', and that no material should be hauled past C', or, in general, past any intersection of the mass curve and the zero line.

5. If any horizontal line be drawn (as ab), it indicates that the cut and fill between a' and b' will just balance.

6. When the center of gravity of a given volume of material is to be moved a given distance, it makes no difference (at least theoretically) how far each individual load may be hauled or how any individual load may be disposed of. The summation of the products of each load times the distance hauled will be a constant, whatever the method, and will equal the total volume times the movement of the center of gravity. The average haul, which is the movement of the center of gravity, will therefore equal the summation of these products divided by the total volume. If we draw two horizontal parallel lines at an infinitesimal distance dx apart, as at ab, the small increment of cut dx at a' will fill the corresponding increment of fill at b', and this material must be hauled the distance ab. Therefore the product of ab and dx, which is the product of distance times volume, is represented by the area of the infinitesimal rectangle at ab, and the total area ABC represents the summation of volume times distance for all the earth movement between A' and C'. This summation of products divided by the total volume gives the average haul.

7. The horizontal line, tangent at E and cutting the curve at e, f, and g, shows that the cut and fill between e' and E' will just balance, and that a *possible* method of hauling (whether desirable or not) would be to "borrow" earth for the fill between C' and e', use the material between D' and E' for the fill between e' and D', and similarly balance cut and fill between E' and f'and also between f' and g'.

8. Similarly the horizontal line hklm may be drawn cutting the curve, which will show another possible method of hauling. According to this plan, the fill between C' and h' would be made by borrowing; the cut and fill between h' and k' would balance: also that between k' and l' and between l' and m'. Since the area ehDkE represents the measure of haul for the earth between e' and E', and the other areas measure the corresponding hauls similarly, it is evident that the sum of the areas ehDkE and ElFmf, which is the measure of haul of all the material between e' and f', is largely in excess of the sum of the areas hDk, kEl, and lFm, plus the somewhat uncertain measures of haul due to borrowing material for e'h' and wasting the material between m' and f'. Therefore to make the measure of haul a minimum a line should be drawn which will make the sum of the areas between it and the mass curve a minimum. Of course this is not necessarily the cheapest plan, as it implies more or less borrowing and wasting of material, which may cost more than the amount saved in haul. The comparison of the two methods is quite simple, however. Since the amount

of fill between e' and h' is represented by the *difference* of the ordinates at e and h, and similarly for m' and f', it follows that the amount to be borrowed between e' and h' will exactly equal the amount wasted between m' and f'. By the first of the above methods the haul is excessive, but is definitely known from the mass diagram, and all of the material is utilized; by the second method the haul is reduced to about one-half, but there is a known quantity in cubic yards wasted at one place and the same quantity borrowed at another. The length of haul necessary for the borrowed material would need to be ascertained; also the haul necessary to waste the other material at a place where it would be unobjectionable. Frequently this is best done by widening an embankment beyond its necessary width. The computation of the relative cost of the above methods will be discussed later (§ 116).

9. Suppose that it were deemed best, after drawing the mass curve, to introduce a trestle between s' and v', thus saving an amount in fill equal to tv. If such had been the original design, the mass curve would have been a straight horizontal line between s and t and would continue as a curve which would be at all points a distance tv above the curve vFmzfGg. If the line Ef is to be used as a zero line, its intersection with the new curve at xwill show that the material between E' and z' will just balance if the trestle is used, and that the amount of haul will be measured by the area between the line Ex and the broken line Estx. The same computed result may be obtained without drawing the auxiliary curve  $txn \dots$  by drawing the horizontal line zyat a distance xz(=tv) below Ex. The amount of the haul can then be obtained by adding the triangular area between Es and the horizontal line Ex, the rectangle between st and Ex, and the irregular area between vFz and  $y \dots z$  (which last is evidently equal to the area between tx and  $E \dots x$ ). The disposal of the material at the right of z' would then be governed by the indications of the profile and mass diagram which would be found at the right of q'. In fact it is difficult to decide with the best of judgment as to the proper disposal of material without having a mass diagram extending to a considerable distance each side of that part of the road under immediate consideration.

102. Area of the mass curve. The area may be computed most readily by means of a planimeter, which is capable with reasonable care of measuring such areas with as great accuracy as is necessary for this work. If no such instrument is obtainable, the area may be obtained by an application of "Simpson's rule." The ordinates will usually be spaced 100 feet apart. Select an *even* number of such spaces, leaving, if necessary, one or more triangles or trapezoids at the ends for separate and independent computation. Let  $y_0 \ldots y_n$  be the ordinates, i.e., the number of cubic yards at each station of the mass curve, or the figures of "column six" referred to in § 100. Let the uniform distance between ordinates (=100 feet) be called 1, i.e., one *station*. Then the units of the resulting area will be cubic yards hauled one station. Then the

Area = 
$$\frac{1}{3}[y_0 + 4(y_1 + y_3 + \dots + y_{(n-1)} + 2(y_2 + y_4 + \dots + y_{(n-2)} + y_n]].$$
 (70)

When an ordinate occurs at a substation, the best plan is to ignore it at first and calculate the area as above. Then, if the difference involved is too great to be neglected, calculate the area of the triangle having the extremity of the ordinate at the substation as an apex, and the extremities of the ordinates at the adjacent stations as the ends of the base. This may be done by finding the ordinate at the substation that would be a proportional between the ordinates at the adjacent full stations. Subtract this from the real ordinate (or vice versa) and multiply the difference by  $\frac{1}{2} \times 1$ . An inspection will often show that the correction thus obtained would be too small to be worthy of consideration. If there is more than one substation between two full stations, the corrective area will consist of two triangles and one or more trapezoids which may be similarly computed, if necessary.

When the zero line (Fig. 62) is shifted to eE, the drop from AC (produced) to E is known in the same units, cubic yards. This constant may be subtracted from the numbers ("column 6," § 100) representing the ordinates, and will thus give, without any scaling from the diagram, the exact value of the modified ordinates.

**103.** Value of the mass diagram. The great value of the mass diagram lies in the readiness with which different plans for the disposal of material may be examined and compared. When the mass curve is once drawn, it will generally require only a shifting of the horizontal line to show the disposal of the material by any proposed method. The mass diagram also shows the

extreme length of haul that will be required by any proposed method of disposal of material. This brings into consideration the "limit of profitable haul," which will be fully discussed in § 116. For the present it may be said that with each method of carrying material there is some limit beyond which the expense of hauling will exceed the loss resulting from borrowing and wasting. With wheelbarrows and scrapers the limit of profitable haul is comparatively short, with carts and tram-cars it is much longer, while with locomotives and cars it may be several miles. If, in Fig. 62, eE or Ej exceeds the limit of profitable haul, it shows at once that some such line as *hklm* should be drawn and the material disposed of accordingly.

104. Changing the grade line. The formation of the mass curve and the resulting plans as to the disposal of material are based on the mutual relations of the grade line and the surface profile and the amounts of cut and fill which are thereby implied. If the grade line is altered, every cross-section is altered. the amount of cut and fill is altered, and the mass curve is also changed. At the farther limit of the actual change of the grade line the revised mass curve will have (in general) a different ordinate from the previous ordinate at that point. From that point on, the revised mass curve will be parallel to its former position, and the revised curve may be treated similarly to the case previously mentioned in which a trestle was introduced. Since it involves tedious calculations to determine accurately how much the volume of earthwork is altered by a change in grade line, especially through irregular country, the effect on the mass curve of a change in the grade line cannot therefore be readily determined except in an approximate way. Raising the grade line will evidently increase the fills and diminish the cuts, and vice versa, Therefore if the mass curve indicated, for example, either an excessively long haul or the necessity for borrowing material (implying a fill) and wasting material farther on (implying a cut), it would be possible to diminish the fill (and hence the amount of material to be borrowed) by lowering the grade line near that place, and diminish the cut (and hence the amount of material to be wasted) by raising the grade line at or near the place farther on. Whether the advantage thus gained would compensate for the possibly injurious effect of these changes on the grade line would require patient investigation. But the method outlined shows how the mass

curve might be used to indicate a possible change in grade line which might be demonstrated to be profitable.

105. Limit of free haul. It is sometimes specified in contracts for earthwork that all material shall be entitled to free haul up to some specified limit, say 500 or 1000 feet, and that all material drawn farther than that shall be entitled to an allowance on the excess of distance. It is manifestly impracticable to measure the excess for each load, as much so as to measure the actual haul of each load. The mass diagram also solves this problem very readily. Let Fig. 63 represent a pro-

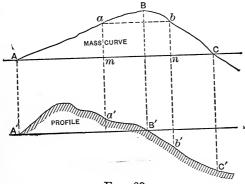


Fig. 63.

file and mass diagram of about 2000 feet of road, and suppose that 800 feet is taken as the limit of free haul. Find two points, a and b, in the mass curve which are on the same horizontal line and which are 800 feet apart. Project these points down to a'and b'. Then the cut and fill between a' and b' will just balance, and the cut between A' and a' will be needed for the fill between b' and C'. In the mass curve, the area between the horizontal line ab and the curve aBb represents the haulage of the material between a' and b', which is all free. The rectangle abmn represents the haulage of the material in the cut A'a' across the 800 feet from a' to b'. This is also free. The sum of the two areas Aam and bnC represents the haulage entitled to an allowance, since it is the summation of the products of cubic yards times the *excess* of distance hauled.

If the amount of cut and fill was symmetrical about the point

B', the mass curve would be a symmetrical curve about the vertical line through B, and the two limiting lines of free haul would be placed symmetrically about B and B'. In general there is no such symmetry, and frequently the difference is considerable The area aBbnm will be materially changed accord. ing as the two vertical lines am and bn, always 800 feet apart. are shifted to the right or left. It is easy to show that the area *aBbnm* is a *maximum* when *ab* is horizontal. The minimum value would be obtained either when m reached A or n reached C, depending on the exact form of the curve. Since the position for the minimum value is manifestly unfair, the best definite value obtainable is the maximum, which must be obtained as above described. Since *aBbnm* is made maximum, the remainder of the area, which is the allowance for overhaul, becomes a minimum. The areas Aam and bCn may be obtained as in § 102. If the whole area AaBbCA has been previously computed, it may be more convenient to compute the area aBbnm and subtract it from the total area.

Since the intersections of the mass curve and the "zero line" mark limits past which no material is drawn, it follows that there will be no allowance for overhaul except where the distance between consecutive intersections of the zero line and mass curve exceeds the limit of free haul.

Frequently all allowances for overhaul are disregarded; the profiles, estimates of quantities, and the required disposal of material are shown to bidding contractors, and they must then make their own allowances and bid accordingly. This method has the advantage of avoiding possible disputes as to the amount of the overhaul allowance, and is popular with railroad companies on this account. On the other hand the facility with which different plans for the disposal of material may be studied and compared by the mass-curve method facilitates the adoption of the most economical plan, and the elimination of uncertainty will frequently lead to a safe reduction of the bid, and so the method is valuable to both the railroad company and the contractor.

## ELEMENTS OF THE COST OF EARTHWORK.

106. Analysis of the total cost into items. The variation in the total cost of excavating earthwork, hauling it a greater or less distance, and forming with it an embankment of definite

form or wasting it on a spoil bank, is so great that the only possible method of estimating the cost under certain assumed conditions is to separate the total cost into elementary items. Ellwood Morris was perhaps the first to develop such a method -see Journal of the Franklin Institute, September and October. 1841. Trautwine used the same general method with some modifications. The following analysis will follow the same general plan, will quote some of the figures given by Morris and by Trautwine, but will also include facts and figures better adapted to modern conditions. Since every item of cost (except interest on cost of plant and its depreciation) is a direct function of the current price of common labor, all calculations will be based on the simple unit of \$1 per day. Then the actual cost may be obtained by multiplying the calculated cost under the given conditions by the current price of day labor. When possible, figures will be quoted giving the cost of all items of work on a loose sandy soil which is the easiest to work and also for the cost of the heaviest soils, such as stiff clay and hard pan. These represent the extremes, excluding rock, which will be treated separately. The cost of intermediate grades may be interpolated between the extreme values according to the judgment of the engineer as to the character of the soil.

The possible division into items varies greatly according to the method adopted, but the differentiation into items given below (which is strictly applicable to the old fashioned simpler methods of work) can usually be applied to any other method by merely combining or eliminating some of the items. The items are

- 1. Loosening the natural soil.
- 2. Loading the soil into whatever carrier may be used.
- 3. Hauling excavated material from excavation to embankment or spoil bank.
- 4. Spreading or distributing the soil on the embankment.
- 5. Keeping roadways or tracks in good running order.
- 6. Trimming cuts to their proper cross-section (sometimes called "sandpapering").
- 7. Repairs, wear, depreciation, and interest on cost of plant.
- 8. Superintendence and incidentals.

107. Item 1. Loosening. (a) Ploughs. Very light sandy soils can frequently be shovelled without any previous loosening, but it is generally economical, even with very light material, to use a plough. Morris quotes, as the results of experiments, that a three-horse plough would loosen from 250 to 800 cubic yards of earth per day, which at a valuation of \$5 per day would make the cost per yard vary from 2 cents to 0.6 cent. Trautwine estimates the cost on the basis of two men handling a two-horse plough at a total cost of \$3.87 per day, being \$1 each for the men, 75 c. for each horse, and an allowance of 37 c. for the plough, harness, etc. From 200 to 600 cubic yards is estimated as a fair day's work, which makes a cost of 1.9 c. to 0.65 c. per yard, which is substantially the same estimate as above. Extremely heavy soils have sometimes been loosened by means of special ploughs operated by traction-engines.

Gillette estimates that "a two-horse team with a driver and a man holding the plough will loosen 25 cubic yards of fairly tough clay, or 35 cubic yards of gravel and loam per hour." For ten hours per day this would be 250 to 350 cubic yards per day. These values are neither as high nor as low as the extremes above noted. It is probably very seldom that a soil will be so light that a two-horse (or three-horse) plough can loosen as much as 600 (or 800) cubic yards per day.

It is sometimes necessary to plough up a macadamized street. This may be done by using as a plough a pointed steel bar which is fastened to a very strong plough frame. A preliminary hole must be made which will start the bar under the macadam shell. Then, as the plough is drawn ahead, the shell is ripped up. Four or six horses, or even a traction-engine, are used for such work. Gillette quotes two such cases where the cost of such loosening was 2 c. and 6 c. per cubic yard, with common labor at 15 c. per hour. Two-thirds of such figures will reduce them to the \$1 per day basis. The cost for ploughing on the \$1 per day basis may therefore be summarized as follows:

For	very	loose sandy soils	0.6 c.	$\mathbf{per}$	cubic ;	yard
"	"	heavy clay "	2.0 c.	"	"	"
"	hard	pan and macadam, up to	4.0 c.	"	**	"

(b) Picks. When picks are used for loosening the earth, as is frequently necessary and as is often done when ploughing would perhaps be really cheaper, an estimate \* for a fair day's work is from 14 to 60 cubic yards, the 14 yards being the estimate for stiff clay or cemented gravel, and the 60 yards the estimate for the lightest soil that would require loosening. At 1 per day this means about 7 c. to 1.7 c. per cubic yard, which is about three times the cost of ploughing. Five feet of the face is estimated \* as the least width along the face of a bank that should be allowed to enable each laborer to work with freedom and hence economically.

(c) Blasting. Although some of the softer shaly rocks may be loosened with a pick for about 15 to 20 c. per yard, yet rock in general, frozen earth, and sometimes even compact clay are most economically loosened by blasting. The subject of blasting will be taken up later, §§ 117-123.

(d) Steam-shovels. The items of loosening and loading merge together with this method, which will therefore be treated in the next section.

108. Item 2. LOADING. (a) Hand-shovelling. Much depends on proper management, so that the shovellers need not wait unduly either for material or carts. With the best of management considerable time is thus lost, and yet the intervals of rest need not be considered as entirely lost, as it enables the men to work, while actually loading, at a rate which it would be physically impossible for them to-maintain for ten hours. Seven shovellers are sometimes allowed for each cart: otherwise there should be five, two on each side and one in the rear. Economy requires that the number of loads per cart per day should be made as large as possible, and it is therefore wise to employ as many shovellers as can work without mutual interference and without wasting time in waiting for material or carts. The figures obtainable for the cost of this item are unsatisfactory on account of their large disagreements. The following are quoted as the number of cubic yards that can be loaded into a cart by an average laborer in a working day of ten hours, the lower estimate referring to heavy soils, and the higher to light sandy soils: 10 to 14 cubic yards (Morris), 12 to 17 cubic yards (Haskoll), 18 to 22 cubic yards (Hurst), 17 to 24 cubic yards (Trautwine), 16 to 48 cubic yards (Ancelin). As these estimates are generally claimed to be based on actual experience, the discrepancies are probably due to differences of management. If the

average of 15 to 25 cubic yards be accepted, it means, on the basis of \$1 per day, 6.7 c. to 4 c. per cubic yard. These estimates apply only to earth. Rockwork costs more, not only because it is harder to handle, but because a cubic yard of solid rock, measured in place, occupies about 1.8 cubic yards when broken up, while a cubic yard of earth will occupy about 1.2 cubic yards. Rockwork will therefore require about 50% more loads to haul a given volume, measured in place, than will the same nominal volume of earthwork. The above authorities give estimates for loading rock varying from 6.9 c. to 10 c. per cubic vard. The above estimates apply only to the loading of carts or cars with shovels or by hand (loading masses of rock). The cost of loading wheelbarrows and the cost of scraper work will be treated under the item of hauling.

(b) Steam-shovels.\* Whenever the magnitude of the work will warrant it there is great economy in the use of steam-shovels. These have a "bucket" or "dipper" on the end of a long beam, the bucket having a capacity varying from  $\frac{1}{2}$  to  $2\frac{1}{2}$  cubic vards. Steam-shovels handle all kinds of material from the softest earth to shale rock, earthy material containing large boulders. tree-stumps, etc. The record of work done varies from 200 to 1000 cubic yards in 10 hours. They perform all the work of loosening and loading. Their economical working requires that the material shall be hauled away as fast as it can be loaded, which usually means that cars on a track, hauled by horses or mules, or still better by a locomotive, shall be used. The expenses for a steam-shovel, costing about \$5000, will average about \$1000 per month. Of this the engineer may get \$100; the fireman \$50; the cranesman \$90; repairs perhaps \$250 to \$300; coal, from 15 to 25 tons, cost very variable on account of expensive hauling; water, a very uncertain amount, sometimes costing \$100 per month; about five laborers and a foreman, the laborers getting \$1.25 per day and the foreman \$2.50 per day, which will amount to \$227.50 per month. This gang of laborers is employed in shifting the shovel when necessary, taking up and relaying

<sup>\*</sup> For a thorough treatment of the capabilities, cost, and management of steam-snovels the reader is referred to "Steam-shovels and Steam-shovel Work," by E. A. Hermann. D. Van Nostrand Co., New York. This book is now out of print. "Earthwork and its Cost," by H. P. Gil-lette, to which the student is referred for a more elaborate exposition of the subject, has used many of Hermann's cuts.

tracks for the cars, shifting loaded and unloaded cars, etc. In shovelling through a deep cut, the shovel is operated so as to undermine the upper parts of the cut, which then fall down within reach of the shovel, thus increasing the amount of material handled for each new position of the shovel. If the material is too tough to fall down by its own weight, it is sometimes found economical to employ a gang of men to loosen it or even blast it rather than shift the shovel so frequently. Non-condensing engines of 50 horse-power use so much water that the cost of water-supply becomes a serious matter if water is not readily obtainable. The lack of water facilities will often justify the construction of a pipe line from some distant source and the installation of a steam-pump. Hence the seemingly large estimate of \$100 per month for water-supply, although under favorable circumstances the cost may almost vanish. The larger steam-shovels will consume nearly a ton of coal per day of 10 hours. The expense of hauling this coal from the nearest railroad or canal to the location of the cut is often a very serious item of expense and may easily double the cost per ton. Some steam-shovels have been constructed to be operated by electricity obtained from a plant perhaps several miles away. Such a method is especially advantageous when fuel and water are difficult to obtain.

The following general requirements and specifications were recommended in 1907 by the American Railway Engineering and Maintenance of Way Association:

Three important cardinal points should be given careful attention in the selection of a steam-shovel. These are in their order

(1) Care in the selection, inspection and acceptance of all material that enters into every part of the machine.

(2) Design for strength.

(3) Design for production.

### GENERAL SPECIFICATIONS.

Weight of shovel: Seventy (70) tons.

Capacity of dipper: Two and one-half  $(2\frac{1}{2})$  yards.

Steam pressure: One hundred and twenty (120) pounds.

Clear height above rail of shovel track at which dipper should unload: Sixteen (16) feet. Depth below rail of shovel track at which dipper should dig Four (4) feet.

Number of movements of dipper per minute from time of entering bank to entering bank: Three (3).

Character of hoist: Cable.

Character of swing: Cable.

Character of housing: Permanent for all employes.

Capacity of tank: Two thousand (2000) gallons.

Capacity of coal-bunker: Four (4) tons.

Spread of jack arm: Eighteen (18) feet. A special short arm should be provided.

Form of steam-shovel track: "T" rails on ties.

Length of rails for ordinary work: Six (6) feet.

Form of rail joint: Strap.

Manufacturers of steam-shovels will cometimes "guarantee" that certain of their shovels will excavate, say 3000 cubic yards of earth per day of ten hours. Even if it were possible for a shovel to fill a car at the rate of 5 cubic yards per minute, it is always impracticable to maintain such a speed, since a shovel must always wait for the shifting of cars and for the frequent shifting of the shovel itself. There are also delays due to adjustments and minor breakdowns. The best shovel records are made when the cars are large-other things being equal. The item of interest and depreciation of the plant is very large in steam-shovel work. This will be discussed further later. The cost of loading alone will usually come to between 3 and 4 c. per cubic yard. The cost of shifting the cars so as to place them successively under the shovel, haul them to the dumping place, dump them and haul them back, will generally be as much more. Gillette quotes five jobs on one railroad where the total cost for loading and hauling varied from 5.9 c. to 11.4 c. per cubic yard. But as these figures are based on car measurement, the cost per cubic yard in place measurement must be increased about one-fourth, or from 7.4 c. to 14.2 c.

109. Item 3. Hauling. The cost of hauling depends on the number of round trips per day that can be made by each vehicle employed. As the cost of each vehicle is practically the same whether it makes many trips or few, it becomes important that the number of trips should be made a maximum, and to that end there should be as little delay as possible in loading and § 109

unloading. Therefore devices for facilitating the passage of the vehicles have a real money value.

(a) Carts. The average speed of a horse hauling a twowheeled cart has been found to be 200 feet per minute, a little slower when hauling a load and a little faster when returning empty. This figure has been repeatedly verified. It means an allowance of one minute for each 100 feet (or "station") of "lead—the lead being the distance the earth is hauled." The time lost in loading, dumping, waiting to load, etc., has been found to average 4 minutes per load. Representing the number of stations (100 feet) of lead by s, the number of loads handled in 10 hours (600 minutes) would be  $600 \div (s+4)$ . The number of loads per cubic yard, measured in the bank, is differentiated by Morris into three classes, viz.:

> 3 loads per cubic yard in descending hauling;  $3\frac{1}{2}$  '' '' '' level hauling; and 4 '' '' ascending hauling.

Attempts have been made to estimate the effect of the grade of the roadway by a theoretical consideration of its rate, and of the comparative strength of a horse on a level and on various While such computations are always practicable on a grades. railway (even on a temporary construction track), the traction on a temporary earth roadway is always very large and so very variable that any refinements are useless. On railroad earthwork the hauling is generally nearly level or it is descendingforming embankments on low ground with material from cuts in high ground. The only common exception occurs when an embankment is formed from borrow-pits on low ground. One method of allowing for ascending grade is to add to the horizontal distance 14 times the difference of elevation for work with carts and 24 times the difference of elevation for work with wheelbarrows, and use that as the lead. For example, using carts, if the lead is 300 feet and there is a difference of elevation of 20 feet, the lead would be considered equivalent to  $300 + (14 \times 20) = 580$  feet on a level.

Trautwine assumes the average load for all classes of work to be  $\frac{1}{3}$  cubic yard, which figure is justified by large experience. Using one figure for all classes of work simplifies the calculations and gives the number of cubic yards carried per day of 10 hours

equal to  $\frac{600}{3(s+4)}$ . Dividing the cost of a cart per day by the

number of cubic yards carried gives the cost of hauling per yard. In computing the cost of a cart per day, Trautwine refers to the practice of having one driver manage four carts, thus making a charge of 25 c. per day for each cart for the driver. Although this might be an economical method when the haul is very long, it is not economical for short hauls. A safer estimate is to allow not more than two carts per driver and in many cases a driver for each cart. Some contractors employ a driver for each cart and then require that the drivers shall assist in loading. The policy to be adopted is sometimes dependent on labor union conditions, which may demand that drivers must not assist in loading. The supply of labor and the amount of work on hand have a great influence on the methods of work which a contractor may adopt, for a strike will often disarrange all plans.

The cost of a horse and cart must practically include a charge for the time of the horse on Sundays, rainy days and holidays. The cost of repairs of cart and harness is generally included in this item for simplicity, but, under a strict application of the analysis suggested in § 106, it should properly be included under Item 7, Repairs, etc.

Since the time required for loading loose rock is greater than for earthwork, less loads will be hauled per day. The time allowance for loading, etc., is estimated by Trautwine as 6 minutes instead of 4 as for earth. Considering the great expansion of rock when broken up (see § 97), one cubic yard of solid rock, measured in place, would furnish the equivalent of five loads of earthwork of  $\frac{1}{3}$  cubic yard. Therefore, on the basis of five loads per cubic yard, the number of cubic yards handled per day per cart would be  $\frac{600}{5(s+6)}$ .

Let C represent the daily cost of a horse and cart and of the proportional cost of the driver (according to the number of carts handled by one driver), then the cost per cubic yard, *measured in the cut*, for hauling may be given by the formula:

Cost per cu. yd. of hauling earth in carts 
$$=\frac{C \times 3(s+4)}{600}$$
  
" " " " " " rock " "  $=\frac{C \times 5(s+6)}{600}$  } . (71)

(b) Wagons. For longer leads (i.e., from  $\frac{1}{3}$  to  $\frac{2}{3}$  of a mile) wagons drawn by two horses have been found most economical. The wagons have bottoms of loose thick narrow boards and are unloaded very easily and quickly by lifting the individual boards and breaking up the continuity of the bottom, thus depositing the load directly underneath the wagon. The capacity is about one cubic yard. The cost may be estimated on the same principle as that for carts.

The number of wagon trips per 10 hours will depend somewhat on the management of the shovellers. Too many shovellers per wagon is not economical, measured in yards shovelled per man, although it may reduce the time consumed in loading any one wagon. At an average figure of 20 cubic yards, measured in place, per shoveller per 10 hours, seven shovellers would load 14 cubic yards per hour or one cubic yard in 4.3 minutes. This would be the allowance for a wagon with a capacity of about  $1\frac{1}{3}$  yards of loose earth. Adding time for unloading, waiting to load and other possible "lost time," there is probably a total of six minutes. This figure will vary very considerably according to the number of shovellers per wagon, the capacity of the wagon, the type of wagon (whether selfdumping) and other details in the method of management. Adopting six minutes as the time used for loading, unloading, and other "lost time," the formula becomes.

Cost per cubic yard of hauling in wagons 
$$=\frac{C(s+6)}{600c}$$
, ... (71a)

in which C is the cost of the wagon, team and driver per day of 10 hours; s is the distance hauled in stations of 100 feet, and c is the capacity of the wagon in cubic yards, *place measurement*, which should be about three fourths of the nominal capacity of the wagon for earth and about sixty per cent when handling rock.

(c) Wheelbarrows. Gillette has computed from observations that a man will trundle a wheelbarrow at the rate of 250 feet per minute or 1.25 stations of lead per minute for the round trip. The time required for loading is estimated at  $2\frac{1}{4}$  minutes and for unloading, adjusting wheeling planks, short rests, etc.,  $\frac{3}{4}$  minute, or a total of three minutes per trip for all purposes except hauling. Gillette allows for a load only 1/15 cubic yard, measured in place, or about 1/11 yard, 2.5 cubic feet, on the wheelbarrow. With notation as before

Cost per cubic yard of loading and hauling earth in wheelbarrows - =  $\frac{C \times 15(1.25s+3)}{600}$ . (72)

In this equation C is the cost of both loading and hauling, and usually includes the allowance (Item 7) for the cost, repairs and depreciation of the wheelbarrows, whose service is very short lived. Trautwine estimates this at five cents per day or a total of \$1.05 for labor and wheelbarrow.

The number of wheelbarrow loads required for a cubic yard of rock, measured in place, is about twenty-four. The time required for loading should also be increased about one fourth; the time required for all purposes except hauling is therefore about 3.75 minutes, and the corresponding equation becomes

 $\frac{\text{Cost per cubic yard of loading and}}{\text{hauling rock in wheelbarrows}} = \frac{C \times 24(1.25s + 3.75)}{600}.$  (72a)

(d) Scrapers. These are made in three general ways, "buck" scrapers, "drag" scrapers and "wheeled" scrapers. The buck scraper in its original form consisted merely of a wide plank, shod with an iron strap on the lower edge and provided with a pole and a small platform on which the driver may stand to weight it down. The earth is not loaded on to any receptacle and carried, but is merely pushed over the ground. Notwithstanding the apparent inefficiency of the method, its extreme simplicity has caused its occasional adoption for the construction of canal embankments out of material from the bed of the canal. The occasions are rare when their use for railroad work would be practicable, and even then drag scrapers would probably be preferable.

A drag scraper is an immense "scoop shovel" about three feet long and three feet wide. There are usually two handles and a bail in front by which it is dragged by a team of horses. The nominal capacity varies from 7.5 cubic feet for the largest sizes, down to 3 cubic feet for the "one-horse" size, but these figures must be discounted by perhaps 40 or 50% for the actual average volume (as measured in the cut) loaded on during one scoop. The expansion of the earth during loosening is alone respons-

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ible for a discount of 25%. These scrapers cost from \$10 to \$18.

A wheeled scraper is essentially an extra-large drag scraper which may be raised by a lever and carried on a pair of large wheels. Their nominal capacity ranges from 10 to 17 cubic feet, which should usually be liberally discounted when estimating output. They are loaded by dropping the scoop so that it scrapes up its load. The lever raises the scoop so that the load is carried on wheels instead of being dragged. At the dump the scoop is tipped so as to unload it. The movement of the scraper is practically continuous. They cost from \$40 to \$75. Their advantages over drag scrapers consist (1) in their greater capacity, (2) in the economy of transporting the load on wheels instead of by dragging, and (3) in the far greater length of haul over which the earth may be economically handled.

Morris estimated the speed of drag scrapers to be 140 feet per minute, or 70 feet of lead per minute. The "lead" should be here interpreted as the average distance from the center of the pit to the center of the dump. Gillette declares the speed to be 220 feet per minute. Some of this variation may be due to differences in the method of measuring the distance actually travelled, especially when the lead is very short, since the scraper teams must always travel a considerable extra distance at each end in order to turn around most easily. This extra distance is practically constant whether the lead is long or short. Gillette quotes an instance where the length of lead was actually about 20 feet, but the scraper teams travelled about 150 feet for each load carried. On this account Gillette adopts a minimum of 75 feet of lead no matter how short the lead actually may be. Of course the speed depends considerably on how strictly the men are kept to their work and also on the care which may be taken to obtain a full load for each scraper. As a compromise between Morris's and Gillette's estimates we may adopt the convenient rate of speed of 200 feet per minute, or 100 feet of lead per minute. There should also be allowed for the time lost in loading and unloading and for travelling the extra distance travelled by the teams in making the circuit, 1<sup>2</sup>/<sub>3</sub> minutes. Allowing the average value of seven loads per cubic yard and letting C represent the cost of scraper team and driver per day, we have for the cost as follows:

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In this formula C should include the cost of not only the driver, team, and scraper, but also the proper proportion of the wages of an extra man, who assists each driver in loading his scraper, and whose wages should be divided among the two (or three) scrapers to which he is assigned. Scraper work nearly always implies ploughing, the cost of which should be computed as under Item 1.

When a low embankment is formed from borrow-pits on each side of the road, it may be done with scrapers, which move from one borrow-pit to the other, taking a load alternately from each side to the center and making but one half turn for each load carried. This reduces the time lost in turning by one third of a minute and reduces the constant in the numerator in Eq. (73) from  $1\frac{1}{3}$  to 1. In this case the lead will usually be not greater than 75 feet, and therefore, if we consider this as a minimum value, *s* will ordinarily equal .75 and the quantity in the parenthesis will equal 1.75.

When using wheeled scrapers the catalogue capacity, which varies from 9 or 10 feet for a No. 1 scraper to 16 or 17 feet for a No. 3 scraper, must be reduced to 5 loads per cubic yard (place measurement) for a No. 1 scraper and to 2<sup>1</sup>/<sub>2</sub> loads per cubic vard for a No. 3, not only on account of the expansion of the earth during loosening, but also on account of the impracticability of loading these scrapers to their maximum nominal capacity. When the haul or lead for wheeled scrapers is 300 feet or over, it will be justifiable to employ shovellers to fill up the bowl of the shovel, especially when the soil is tough and when it is impracticable to fill the shovel even approximately full by the ordinary method. A snatch team to assist in loading the scrapers it also economical, especially with the larger scrapers. The proportionate number of snatch teams to the total number of scrapers of course depends on the length of haul. The cost of these extra shovellers and extra snatch teams must be divided proportionally among the number of scrapers assisted, in determining the value C in the formula given below. The extra time to be allowed on account of turning, loading, and dumping is about  $1\frac{1}{2}$  minutes. The speed is considered one station of lead per minute as before. If we call C the average

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daily cost of one scraper and n the capacity of the scraper, or the number of loads per cubic yard, we may write the following formula:

Cost per cubic yard of loading and hauling earth in wheeled scrapers  $= \frac{C \times n(s+1\frac{1}{2})}{600}$ . (73a)

(e) Cars and horses. The items of cost by this method are (a) charge for horses employed, (b) charge for men employed strictly in hauling, (c) charge for shifting rails when necessary, (d) repairs, depreciation, and interest on cost of cars and track. Part of this cost should strictly be classified under items 5 and 7, mentioned in § 106, but it is perhaps more convenient to estimate them as follows:

The traction of a car on rails is so very small that grade resistance constitutes a very large part of the total resistance if the grade is 1% or more. For all ordinary grades it is sufficiently accurate to say that the grade resistance is to the gross weight as the rise is to the distance. If the distance is supposed to be measured along the slope, the proportion is strictly true; i.e., on a 1% grade the grade resistance is 1 lb. per 100 of weight or 20 lbs. per ton. If the resistance on a level at the usual velocity is  $\frac{1}{120}$ , a grade of 1:120 (0.83%) will exactly double it. If the material is hauled down a grade of 1:120, the cars will run by gravity after being started. The work of hauling will then consist practically of hauling the empty cars up the grade. The grade resistance depends only on the rate of grade and the weight, but the tractive resistance will be greater per ton of weight for the unloaded than for the loaded cars. The tractive power of a horse is less on a grade than on a level, not only because the horse raises his own weight in addition to the load, but is anatomically less capable of pulling on a grade than on a level. In general it will be possible to plan the work so that loaded cars need not be hauled upa grade, unless an embankment is to be formed from a low borrow-pit, in which case another method would probably be advisable. These computations are chiefly utilized in designing the method of work—the proportion of horses to cars. An example may be quoted from English practice (Hurst), in which the cars had a capacity of  $3\frac{1}{3}$  cubic yards, weighing 30 cwt. empty. Two horses took five "wagons"  $\frac{3}{4}$  of a mile on a level

railroad and made 15 journeys per day of 10 hours, i.e., they handled 250 yards per day. In addition to those on the "straight road," another horse was employed to make up the train of loaded wagons. With a short lead the straightroad horses were employed for this purpose. In the above example the number of men required to handle these cars. shift the tracks, etc., is not given, and so the exact cost of the above work cannot be analyzed. It may be noticed that the two horses travelled  $22\frac{1}{2}$  miles per day, drawing in one direction a load, including the weight of the cars, of about 57,300 lbs., or 28.65 net tons. Allowing  $\frac{1}{120}$  as the necessary tractive force, it would require a pull of 477.5 lbs., or 239 lbs. for each horse. With a velocity of 220 feet per minute this would amount to 11 horse-power per horse, exerted for only a short time, however, and allowing considerable time for rest and for drawing only the empty cars. Gillette claims that the rolling resistance for such cars on a contractor's track should be considered as 40 lbs. per ton (the equivalent of a 2% grade) and quotes many figures to support the assertion. Unquestionably the resistance on tracks with very light rails, light ties with wide spacing and no tamping, would be very great and might readily amount to 40 lbs. per ton. In the above case, the resistance could not have been much if any over  $\frac{1}{120}$ . A resistance of 40 lbs. per ton would have required each horse to pull about 573 lbs. for nearly five hours per day, beside pulling the empty cars the rest of the time. This is far greater exertion than any ordinary horse can maintain. The cars generally used in this country have a capacity of  $1\frac{1}{2}$  cubic yards and cost about \$65 apiece. Besides the shovellers and dumping-gang, several men and a foreman will be required to keep the track in order and to make the constant shifts that are necessary. Two trains are generally used, one of which is loaded while the other is run to the dump. Some passing-place is necessary, but this is generally provided by having a switch at the cut and running the trains on each track alternately. This insures a train of cars always at the cut to keep the shovellers employed. The cost of hauling per cubic yard can only be computed when the number of laborers, cars, and horses employed are known, and these will depend on the lead, on the character of the excavation, on the grade, if any, etc., and must be so proportioned that the shovellers need not wait for cars to fill, nor the dumping-gang for material to handle, nor the horses and drivers for cars to haul. Much skill is necessary to keep a large force in smooth running order.

(f) Cars and locomotives. 30-lb. rails are the lightest that should be used for this work, and 35- or 40-lb. rails are better. One or two narrow-gauge locomotives (depending on the length of haul), costing about \$2500 each, will be necessary to handle two trains of about 15 cars each, the cars having a capacity of about 2 cubic yards and costing about \$100 each. Some cars can be obtained as low as \$70. A force of about five men and a foreman will be required to shift the tracks. The trackshifters, except the foreman, may be common laborers. The dumping-gang will require about seven men. Even when the material is all taken down grade the grades may be too steep for the safe hauling of loaded cars down the grade, or for hauling empty cars up the grade. Under such circumstances temporary trestles are necessary to reduce the grade. When these are used, the uprights and bracing are left in the embankmentonly the stringers being removed. This is largely a necessity, but is partially compensated by the fact that the trestle forms a core to the embankment which prevents lateral shifting during settlement. The average speed of the trains may be taken as 10 miles per hour or 5 miles of lead per hour. The time lost in loading and unloading is estimated (Trautwine) as 9 minutes or .15 of an hour. The number of trips per day of 10 hours 10 50 will equal  $\frac{10}{\frac{1}{16}}$  or (miles of lead) + .15 or (miles of lead) + .75Of course this quotient must be a whole number. Knowing the number of trains and their capacity, the total number of cubic yards handled is known, which, divided into the total daily cost of the trains, will give the cost of hauling per yard. The daily cost of a train will include

(a) Wages of engineer, who frequently fires his own engine;
(b) Fuel, about ¼ to 1 ton of bituminous coal, depending on work done;

(c) Water, a very variable item, frequently costing \$3 to \$5 per day;

(d) Repairs, variable, frequently at rate of 50 to 60% per year;
(e) Interest on cost and depreciation, 16 to 40%.

To these must be added, to obtain the total cost of haul,

(f) Wages of the gang employed in shifting track.

The above calculation for the number of train loads depends on the assumption that 9 minutes is total time lost by a locomotive for each round trip. If the haul is very short it may readily happen that a steam-shovel cannot fill one train of cars before the locomotive has returned with a load of empties and is ready to haul a loaded train away. The estimation of the number of train loads is chiefly useful in planning the work so as to have every tool working at its highest efficiency. Usually the capacity of the steam-shovel or the ability to promptly "spot" the cars under the shovel is the real limiting agent which determines the daily output.

110. Choice of method of haul dependent on distance. In light side-hill work in which material need not be moved more than 12 or 15 feet, i.e., moved *laterally* across the roadbed. the earth may be moved most cheaply by mere shovelling. Beyond 12 feet scrapers are more economical. At about 100 feet drag-scrapers and wheelbarrows are equally economical. Between 100 and 200 feet wheelbarrows are generally cheaper than either carts or drag-scrapers, but wheeled scrapers are always cheaper than wheelbarrows. Beyond 500 feet twowheeled carts become the most economical up to about 1700 feet: then four-wheeled wagons become more economical up to 3500 feet. Beyond this cars on rails, drawn by horses or by locomotives, become cheaper. The economy of cars on rails becomes evident for distances as small as 300 feet provided the volume of the excavation will justify the outlay. Locomotives will always be cheaper than horses and mules, providing the work to be done is of sufficient magnitude to justify the purchase of the necessary plant and risk the loss in selling the plant ultimately as second-hand equipment, or keeping the plant on hand and idle for an indefinite period waiting for other work. Horses will not be economical for distances much over a mile. For greater distances locomotives are more economical, but the question of "limit of profitable haul" (§ 116) must be closely studied, as the circumstances are certainly not common when it is advisable to haul material much over a mile.

111. Item 4. SPREADING. The cost of spreading varies with the method employed in dumping the load. When the earth is tipped over the edge of an embankment there is little if any necessary work. Trautwine allows about  $\frac{1}{4}$  c. per cubic yard for keeping the dumping-places clear and in order. This would. represent the wages of one man at \$1 per day attending to the unloading of 1200 two-wheeled carts each carrying  $\frac{1}{3}$  cubic yard. 1200 carts in 10 hours would mean an average of two per minute. which implies more rapid and efficient work than may be depended on. The allowance is probably too small. When the material is dumped in layers some levelling is required, for which Trautwine allows 50 to 100 cubic yards as a fair day's work, costing from 1 to 2 cents per cubic yard. The cost of spreading will not ordinarily exceed this and is frequently nothing-all depending on the method of unloading. It should be noted that Mr. Morris's examples and computations (Jour. Franklin Inst., Sept. 1841) disregard altogether any special charge for this item.

112. Item 5. KEEPING ROADWAYS IN ORDER. This feature is important as a measure of true economy, whatever the system of transportation, but it is often neglected. A petty saving in such matters will cost many times as much in increased labor in hauling and loss of time. With some methods of haul the cost is best combined with that of other items.

(a) Wheelbarrows. Wheelbarrows should generally be run on planks laid on the ground. The adjusting and shifting of these planks is done by the wheelers, and the time for it is allowed for in the " $\frac{3}{4}$  minute for short rests, adjusting the wheeling plank, etc." The actual cost of the planks must be added, but it would evidently be a very small addition per cubic yard in a large contract. When the wheelbarrows are run on planks placed on "horses" or on trestles the cost is very appreciable; but the method is frequently used with great economy. The variations in the requirements render any general estimate of such cost impracticable.

(b) Carts and wagons. The cost of keeping roadways in order for carts and wagons is sometimes estimated merely as so much per cubic yard, but it is evidently a function of the *lead*. The work consists in draining off puddles, filling up ruts, picking up loose stones that may have fallen off the loads, and in general doing everything that will reduce the traction as much as possible. Temporary inclines, built to avoid excessive grade at some one point, are often measures of true economy. Trautwine suggests  $\frac{1}{10}$  c. per cubic yard per 100 feet of lead for earthwork and  $\frac{2}{10}$  c. for rockwork, as an estimate for this item when carts are used.

(c) Cars. When cars are used a shifting-gang, consisting of a foreman and several men (say five), are constantly employed in shifting the track so that the material may be loaded and unloaded where it is desired. The average cost of this item may be estimated by dividing the total daily cost of this gang by the number of cubic yards handled in one day.

1122. Item 6. TRIMMING CUTS TO THEIR PROPER CROSS-SECTION. This process, often called "sand-papering," must be treated as an expense, since the payment received for the very few cubic yards of earth excavated is wholly inadequate to pay for the work involved. Gillette quotes bids of 2 cents per square yard of surface trimmed, and from this argues that, for average excavations, it adds to the cost four cents per cubic yard of the total excavation. The shallower the cut the greater is the proportionate cost. Of course the actual cost to the contractor will depend largely on the accuracy of outline demanded by the engineer or inspector.

113. Item 7. REPAIRS, WEAR, DEPRECIATION, AND INTEREST ON COST OF PLANT. The amount of this item evidently depends upon the character of the soil—the harder the soil the worse the wear and depreciation. The *interest on cost* depends on the current borrowing value of money. The estimate for this item has already been included in the allowances for horses, carts, ploughs, harness, wheelbarrows, steam-shovels, etc. Trautwine estimates  $\frac{1}{4}$  c. per cubic yard for picks and shovels. Depreciation is generally a large percentage of the cost of earth-working tools, the life of all being limited to a few years, and of many tools to a few months.

114. Item 8. SUPERINTENDENCE AND INCIDENTALS. The incidentals include the cost of water-boys, timekeepers, watchmen, blacksmiths, fences, and other precautions to protect the public from possible injury, cost of casualty insurance for workmen, etc. Although the cost of some of these sub-items may be definitely estimated, others are so uncertain that it is only possible to make a lump estimate and add say 5 to 7% of the sum of the previous items for this item.

115. Contractor's profit and contingencies. The word "contingencies" here refers to the abnormal expenses caused by freshets, continued wet weather, and "hard luck," as distinguished from mere incidentals which are really normal expenses. They are the expenses which literally cannot be foreseen, and on which the contractor must "take chances." They are therefore included with the expected profit. The allowance for these two elements combined is variously estimated up to 25% of the previously estimated cost of the work, according to the sharpness of the competition, the contractor's confidence in the accuracy of his estimates, and the possible uncertainty as to true cost owing to unfavorable circumstances. The contractor's real profit may vary considerably from this. He often pays clerks, boards and lodges the laborers in shanties built for the purpose, or keeps a supply-store, and has various other items both of profit and expense. His profit is largely dependent on skill in so handling the men that all can work effectively without interference or delays in waiting for others. An unusual season of bad weather will often affect the cost very seriously. It is a common occurrence to find that two contractors may be working on the same kind of material and under precisely similar conditions and at the same price, and yet one may be making money and the other losing it-all on account of difference of management.

116. Limit of profitable haul. As intimated in §§ 103 and 110, there is with every method of haul a limit of distance beyond which the expense for excessive hauling will exceed the loss resulting from borrowing and wasting. This distance is somewhat dependent on local conditions, thus requiring an independent solution for each particular case, but the general principles involved will be about as follows: Assume that it has been determined, as in Fig. 62, that the cut and fill will exactly balance between two points, as between e and x, assuming that, as indicated in § 101 (9), a trestle has been introduced between sand t, thus altering the mass curve to  $Estan \ldots$  Since there is a balance between A' and C', the material for the fill between C' and e' must be obtained either by "borrowing" in the immediate neighborhood or by transportation from the excavation

between z' and n'. If cut and fill have been approximately balanced in the selection of grade line, as is ordinarily done, borrowing material for the fill C'e' implies a wastage of material at the cut z'n'. To compare the two methods, we may place against the plan of borrowing and wasting, (a) cost, if any, of extra right of way that may be needed from which to obtain earth for the fill C'e'; (b) cost of loosening, loading, hauling a distance equal to that between the centers of gravity of the borrow-pit and of the fill, and the other expenses incidental to borrowing M cubic yards for the fill C'e'; (c) cost of loosening, loading, hauling a distance equal to that between the centers of gravity of the cut z'n' and of the spoil-bank, and the other expenses incidental to wasting M cubic yards at the cut z'n': (d) cost, if any, of land needed for the spoil-bank. The cost of the other plan will be the cost of loosening, loading, hauling (the hauling being represented by the trapezoidal figure Cexn), and the other expenses incidental to making the fill C'e' with the material from the cut z'n', the amount of material being M cubic yards, which is represented in the figure by the vertical ordinate from e to the line Cn. The difference between these costs will be the cost, if any, of land for borrow-pit and spoil-bank plus the cost of loosening, loading, etc. (except hauling and roadways) of M cubic yards, minus the difference in cost of the excessive haul from Ce to xn and the comparatively short hauls from borrow-pit and to spoil-bank.

As an illustration, taking some of the estimates previously given for operating with average material, the cost of all items, except hauling and roadways, would be about as follows: loosening, with plough, 1.2 c., loading 5.0 c., spreading 1.5 c., wear, depreciation, etc., .25 c., superintendence, etc., 1.5 c.; total 8.95 c. Suppose that the haul for both borrowing and wasting averages 100 feet or 1 station. Then the cost of haul per vard, using carts, would be (§ 109, a)  $[125 \times 3(1+4)] \div 600$ =3.125 c. The cost of roadways would be about 0.1 c. per yard, making a total of 3.225 c. per cubic yard. Assume M = 10000cubic yards and the area Cexn = 180000 yards-stations or the equivalent of 10000 yards hauled 1800 feet. This haul would  $\cos [125 \times 3(18+4)] \div 600 = 13.75$  c. per cubic yard. The cost of roadways will be  $18 \times .1$  or 1.8 c., making a total of 15.55 c. for hauling and roadways. The difference of cost of hauling and roadways will be  $15.55 - (2 \times 3.225) = 9.10$  c. per yard or \$910

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for the 10000 yards. Offsetting this is the cost of loosening, etc., 10000 yards, at 8.95 c., costing \$895. These figures may be better compared as follows:

LONG HAUL.	Loosening, etc. Hauling, "	, 10000 yard 10000 "	s, @ 8.95 c. @ 15.55 c.	\$ 895. 1555.
	l			\$2450.
	[Loosening, etc.	, 10000 yard	s (borrowed), @ 8.9	5 c. \$895.
	** **	10000 "	(wasted), @ 8.9	5 c. 895.
Borrowing	Hauling, etc.,	10000 "	(borrowed), @ 3.2	25 c. 322.50
WASTING.	{	10000 "	(wasted), @ 3.2	25 c. 322.50
WASTING.			•	\$2435.00

These costs are practically balanced, but no allowance has been made for right of way. If any considerable amount had to be paid for that, it would decide this particular case in favor of the long haul. This shows that *under these conditions* 1800 feet is *about* the limit of profitable haul, the land costing nothing extra.

#### BLASTING.

117. Explosives. The effect of blasting is due to the extremely rapid expansion of a gas which is developed by the decomposition of a very small amount of solid matter. Blasting compounds may be divided into two general classes, (a) slowburning and (b) detonating. Gunpowder is a type of the slowburning compounds. These are generally ignited by heat; the ignition proceeds from grain to grain; the heat and pressure produced are comparatively low. Nitro-glycerine is a type of the detonating compounds. They are exploded by a shock which instantaneously explodes the whole mass. The heat and pressure developed are far in excess of that produced by the explosion of powder. Nitro-glycerine is so easily exploded that it is very dangerous to handle. It was discovered that if the nitro-glycerine was absorbed by a spongy material like infusorial earth, it was much less liable to explode, while its power when actually exploded was practically equal to that of the amount of pure nitro-glycerine contained in the dynamite, which is the name given to the mixture of nitro-glycerine and infusorial earth. Nitro-glycerine is expensive; many other explosive chemical compounds which properly belong to the slow-burning class are comparatively cheap. It has been conclusively demonstrated that a mixture of nitro-glycerine and some of the cheaper chemicals has a greater explosive force than the sum of the strengths of the component parts when exploded separately. Whatever the reason, the fact seems established. The reason is possibly that the explosion of the nitro-glycerine is sufficiently powerful to produce a *detonation* of the other chemicals, which is impossible to produce by ordinary means, and that this explosion caused by detonation is more powerful than an ordinary explosion. The majority of the explosive compounds and "powders" on the market are of this character—a mixture of 20 to 60 per cent. of nitro-glycerine with variable proportions of one or more of a great variety of explosive chemicals.

The choice of the explosive depends on the character of the A hard brittle rock is most effectively blasted by a rock. detonating compound. The rapidity with which the full force of the explosive is developed has a shattering effect on a brittle substance. On the contrary, some of the softer tougher rocks and indurated clays are but little affected by dynamite. The result is but little more than an enlargement of the blast-hole. Quarrying must generally be done with blasting-powder, as the quicker explosives are too shattering. Although the results obtained by various experimenters are very variable, it may be said that pure nitro-glycerine is eight times as powerful as black powder, dynamite (75% nitro-glycerine) six times, and guncotton four to six times as powerful. For open work where time is not particularly valuable, black powder is by far the cheapest, but in tunnel-headings, whose progress determines the progress of the whole work, dynamite is so much more effective and so expedites the work that its use becomes economical.

**118.** Drilling. Although many very complicated forms of drill-bars have been devised, the best form (with slight modifications to suit circumstances) is as shown in Fig. 64, (a) and (b). The width should flare at the bottom (a) about 15 to 30%. For hard rock the curve of the edge should be somewhat flatter and for soft rock somewhat more curved than shown, Fig. 64, (a). Sometimes the angle of the two faces is varied from that given, Fig. 64, (b), and occasionally the edge is purposely blunted so as to give a crushing rather than a cutting effect. The drills will require sharpening for each 6 to 18 inches depth of hole, and will require a new edge to be worked every 2 to 4 days.

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For drilling vertical holes the *churn-drill* is the most economical. The drill-bar is of iron, about 6 to 8 feet long,  $1\frac{1}{4}''$  in diameter, weighs about 25 to 30 lbs., and is shod with a piece of steel welded on. The bar is lifted a few inches between each blow, turned partially around, and allowed to fall, the impact doing the work. From 5 to 15 feet of holes, depending on the character of the rock, is a fair day's work—10 hours. In very soft rocks even more than this may be done. This method is

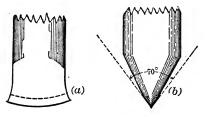


Fig. 64.

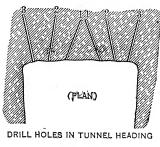
inapplicable for inclined holes or even for vertical holes in confined places, such as tunnel-headings. For such places the only practical *hand* method is to use hammers. This may be done by light drills and light hammers (one-man work), or by heavier drills held by one man and struck by one or two men with heavy hammers. The conclusion of an exhaustive investigation as to the relative economy of light or heavy hammers is that the lighthammer method is more economical for the softer rocks, the heavy-hammer method is more economical for the harder rocks, but that the light-hammer method is always more expeditious and hence to be preferred when time is important.

The subject of machine rock-drills is too vast to be treated here. The method is only practicable when the amount of work to be done is large, and especially when time is valuable. The machines are generally operated by compressed air for tunnel-work, thus doing the additional service of supplying fresh air to the tunnel-headings where it is most needed. The cost per foot of hole drilled is quite variable, but is usually somewhat less than that of hand-drilling—sometimes but a small fraction of it.

119. Position and direction of drill-holes. As the cost of drilling holes is the largest single item in the total cost of blasting, it is necessary that skill and judgment should be used in so

# § 119.

locating the holes that the blasts will be most effective. The greatest effect of a blast will evidently be in the direction of the "line of least resistance." In a strictly homogeneous material this will be the shortest line from the center of the explosive to the surface. The variations in homogeneity on account of laminations and seams require that each case shall be judged according to experience. In open-pit blasting it is generally easy to obtain two and sometimes three exposed faces to the



### FIG. 65.

rock, making it a simple matter to drill holes so that a blast will do effective work. When a solid face of rock must be broken into, as in a tunnel-heading, the work is necessarily ineffectual and expensive. A conical or wedgeshaped mass will first be blown out by simultaneous blasts in the holes marked 1, Fig. 65; blasts in the holes marked 2 and 3 will then complete the cross-

section of the heading. A great saving in cost may often be secured by skilfully taking advantage of seams, breaks, and irregularities. When the work is economically done there is but little noise or throwing of rock, a covering of old timbers and branches of trees generally sufficing to confine the smaller pieces which would otherwise fly up.

120. Amount of explosive. The amount of explosive required varies as the cube of the line of least resistance. The best results are obtained when the line of least resistance is  $\frac{3}{4}$  of the depth of the hole; also when the powder fills about  $\frac{1}{3}$  of the hole. For average rock the amount of powder required is as follows:

Strict compliance with all of the above conditions would require that the diameter of the hole should vary for every case. While this is impracticable, there should evidently be some variation in the size of the hole, depending on the work to be done. For example, a 1" hole, drilled 2' 8" deep, with its line of least resistance 2'. and loaded with  $\frac{1}{4}$  lb. of powder, would be filled to a depth of  $9\frac{1}{2}''$ , which is nearly  $\frac{1}{3}$  of the depth. A 3" hole, drilled 8' deep, with its line of least resistance 6', and loaded with  $6\frac{3}{4}$  lbs. of powder, would be filled to a depth of over 28", which is also nearly  $\frac{1}{3}$  of the depth. One pound of blastingpowder will occupy about 28 cubic inches. Quarrying necessitates the use of numerous and sometimes repeated light charges of powder, as a heavy blast or a powerful explosive like dynamite is apt to shatter the rock. This requires more powder to the cubic yard than blasting for mere excavation, which may usually be done by the use of  $\frac{1}{4}$  to  $\frac{1}{3}$  lb. of powder per cubic yard of easy open blasting. On account of the great resistance offered by rock when blasted in headings in tunnels, the powder used per cubic yard will run up to 2, 4, and even 6 lbs. per cubic yard. As before stated, nitro-glycerine is about eight times (and dynamite about six times) as powerful as the same *weight* of powder.

121. Tamping. Blasting-powder and the slow-burning explosives require thorough tamping. Clay is probably the best, but sand and fine powdered rock are also used. Wooden plugs, inverted expansive cones, etc., are periodically reinvented by enthusiastic inventors, only to be discarded for the simpler methods. Owing to the extreme rapidity of the development of the force of a nitro-glycerine or dynamite explosion, tamping is not so essential with these explosives, although it unquestionably adds to their effectiveness. Blasting under water has been effectively accomplished by merely pouring nitro-glycerine into the drilled holes through a tube and then exploding the charge without any tamping except that furnished by the superincumbent water. It has been found that air-spaces about a charge make a material reduction in the effectiveness of the explosion. It is therefore necessary to carefully ram the explosive into a solid mass. Of course the liquid nitro-glycerine needs no ramming, but dynamite should be rammed with a wooden rammer. Iron should be carefully avoided in ramming gunpowder. A copper bar is generally used.

122. Exploding the charge. Black powder is generally exploded by means of a fuse which is essentially a cord in which there is a thin vein of gunpowder, the cord being protected by tar, extra linings of hemp, cotton, or even gutta-percha. The fuse is inserted into the middle of the charge, and the tamping carefully packed around it so that it will not be injured. To

produce the detonation required to explode nitro-glycerine and dynamite, there must be an initial explosion of some easily ignited explosive. This is generally accomplished by means of caps containing fulminating-powder which are exploded by electricity. The electricity (in one class of caps) heats a very fine platinum wire to redness, thereby igniting the sensitive powder, or (in another class) a spark is caused to jump through the powder between the ends of two wires suitably separated. Dynamite can also be exploded by using a small cartridge of gunpowder which is itself exploded by an ordinary fuse.

123. Cost. Trautwine estimates the cost of blasting (for mere excavation) as averaging 45 cents per cubic yard, falling as low as 30 cents for easy but *brittle* rock, and running up to 60 cents and even \$1 when the cutting is shallow, the rock especially tough, and the strata unfavorably placed. Soft tough rock frequently requires more powder than harder brittle rock.

124. Classification of excavated material. The classification of excavated material is a fruitful source of dispute between contractors and railroad companies, owing mainly to the fact that the variation between the softest earth and the hardest rock is so gradual that it is very difficult to describe distinctions between different classifications which are unmistakable and indisputable. The classification frequently used is (a) earth, (b) loose rock, and (c) solid rock. As blasting is frequently used to loosen "loose rock" and even "earth" (if it is frozen), the fact that blasting is employed cannot be used as a criterion, especially as this would (if allowed) lead to unnecessary blasting for the sake of classifying material as rock.

Earth. This includes clay, sand, gravel, loam, decomposed rock and slate, boulders or loose stones not greater than 1 cubic foot (3 cubic feet, P. R. R.), and sometimes even "hard-pan." In general it will signify material which *can* be loosened by a plough with two horses, or with which one picker can keep one shoveller busy.

Loose rock. This includes boulders and loose stones of more than one cubic foot and less than one cubic yard; stratified rock, not more than six inches thick, separated by a stratum of clay; also all material (not classified as earth) which may be loosened by pick or bar and which "can be quarried without blasting, although blasting may occasionally be resorted to," Solid rock includes all rock found in masses of over one cubic yard which cannot be removed except by blasting.

It is generally specified that the engineer of the railroad company shall be the judge of the classification of the material, but frequently an appeal is taken from his decisions to the courts.

125. Specifications for earthwork. The following specifications, issued by the Norfolk and Western R. R., represent the average requirements. It should be remembered that very strict specifications invariably increase the cost of the work, and frequently add to the cost more than is gained by improved quality of work.

1. The grading will be estimated and paid for by the cubic yard, and will include clearing and grubbing, and all open excavations, channels, and embankments required for the formation of the roadbed, and for turnouts and sidings; cutting all ditches or drains about or contiguous to the road; digging the foundation-pits of all culverts, bridges, or walls; reconstructing turnpikes or common roads in cases where they are destroyed or interfered with; changing the course or channel of streams; and all other excavations or embankments connected with or incident to the construction of said Railroad.

2. All grading, except where otherwise specified, whether for cuts or fills, will be measured in the excavations and will be classified under the following heads, viz.: Solid Rock, Loose Rock, Hard-pan, and Earth.

SOLID ROCK shall include all rock occurring in masses which, in the judgment of the said Engineer Maintenance of Way, may be best removed by blasting.

LOOSE ROCK shall include all kinds of shale, soapstone, and other rock which, in the judgment of the said Engineer Maintenance of Way, can be removed by pick and bar, and is soft and loose enough to be removed without blasting, although blasting may be occasionally resorted to; also, detached stone of less than one (1) cubic yard and more than one (1) cubic foot.

HARD-PAN shall consist of tough indurated clay or cemented gravel, which requires blasting or other equally expensive means for its removal, or which cannot be ploughed with less than four horses and a railroad plough, or which requires two pickers to a shoveller, the said Engineer Maintenance of Way to be the judge of these conditions.

§ 125.

EARTH shall include all material of an earthy nature, of whatever name or character, not unquestionably loose rock or hardpan as above defined.

POWDER. The use of powder in cuts will not be considered as a reason for any other classification than earth, unless the material in the cut is clearly other than earth under the above specifications.

3. Earth, gravel, and other materials taken from the excavations, except when otherwise directed by the said Engineer Maintenance of Way or his assistant, shall be deposited in the adjacent embankment; the cost of removing and depositing which, when the distance necessary to be hauled is not more than sixteen hundred (1600) feet, shall be included in the price paid for the excavation.

4. EXTRA HAUL will be estimated and paid for as follows: whenever material from excavations is necessarily hauled a greater distance than sixteen hundred (1600) feet, there shall be paid in addition to the price of excavation the price of extra haul per 100 feet, or part thereof, after the first 1600 feet; the necessary haul to be determined in each case by the said Engineer Maintenance of Way or his assistant, from the profile and cross-sections, and the estimates to be in accordance therewith.

5. All embankments shall be made in layers of such thickness and carried on in such manner as the said Engineer Maintenance of Way or his assistant may prescribe, the stone and heavy materials being placed in slopes and top. And in completing the fills to the proper grade such additional heights and fulness of slope shall be given them, to provide for their settlement, as the said Engineer Maintenance of Way, or his assistant, may direct. Embankments about masonry shall be built at such times and in such manner and of such materials as the said Engineer Maintenance of Way or his assistant may direct.

6. In procuring materials for embankments from without the line of the road, and in wasting materials from cuttings, the place and manner of doing it shall in each case be indicated by the Engineer Maintenance of Way or his assistant; and care must be taken to injure or disfigure the land as little as possible. Borrow-pits and spoil-banks must be left by the Contractor in regular and sightly shape.

7. The lands of the said Railroad Company shall be cleared to the extent required by the said Engineer Maintenance of Way, or his assistant, of all trees, brushes, logs, and other perishable materials, which shall be destroyed by burning or deposited in heaps as the said Engineer Maintenance of Way, or his assistant, may direct. Large trees must be cut not more than two and one-half  $(2\frac{1}{2})$  feet from the ground, and under embankments less than four (4) feet high they shall be cut close to the ground. All small trees and bushes shall be cut close to the ground.

8. Clearing shall be estimated and paid for by the acre or fraction of an acre.

9. All stumps, roots, logs, and other obstructions shall be grubbed out, and removed from all places where embankments occur less than two (2) feet in height; also, from all places where excavations occur and from such other places as the said Engineer Maintenance of Way or his assistant may direct.

10. Grubbing shall be estimated and paid for by the acre or fraction of an acre.

11. Contractors, when directed by the said Engineer Maintenance of Way or his assistant in charge of the work, will deposit on the side of the road, or at such convenient points as may be designated, any stone, rock, or other materials that they may excavate; and all materials excavated and deposited as above, together with all timber removed from the line of the road, will be considered the property of the Railroad Company, and the Contractors upon the respective sections will be responsible for its safe-keeping until removed by said Railroad Company, or until their work is finished.

12. Contractors will be accountable for the maintenance of safe and convenient places wherever public or private roads are in any way interfered with by them during the progress of the work. They will also be responsible for fences thrown down, and for gates and bars left open, and for all damages occasioned thereby.

13. Temporary bridges and trestles, erected to facilitate the progress of the work, in case of delays at masonry structures from any cause, or for other reasons, will be at the expense of the Contractor.

14. The line of road or the gradients may be changed in any manner, and at any time, if the said Engineer Maintenance of Way or his assistant shall consider such a change necessary or expedient; but no claim for an increase in prices of excavation or embankment on the part of the Contractor will be allowed or considered unless made in writing before the work on that part of the section where the alteration has been made shall have been commenced. The said Engineer Maintenance of Way or his assistant may also, on the conditions last recited, increase or diminish the length of any section for the purpose of more nearly equalizing or balancing the excavations and embankments, or for any other reason.

15. The roadbed will be graded as directed by the said Engineer Maintenance of Way or his assistant, and in conformity with such breadths, depths, and slopes of cutting and filling as he may prescribe from time to time, and no part of the work will be finally accepted until it is properly completed and dressed off at the required grade.

# CHAPTER IV.

#### TRESTLES.

126. Extent of use. Trestles constitute from 1 to 3% of the length of the average railroad. It was estimated in 1889 that there was then about 2400 miles of single-track railway trestle in the United States, divided among 150,000 structures and estimated to cost about \$75,000,000. The annual charge for maintenance, estimated at  $\frac{1}{5}$  of the cost, therefore amounted to about \$9,500,000 and necessitated the annual use of perhaps 300,000,000 ft. B. M. of timber. The corresponding figures at the present time must be somewhat in excess of this. The magnitude of this use, which is causing the rapid disappearance of forests, has resulted in endeavors to limit the use of timber for this purpose. Trestles may be considered as justifiable under the following conditions:

a. Permanent trestles.

1. Those of *extreme* height—then called viaducts and frequently constructed of iron or steel, as the Kinzua viaduct, 302 ft. high.

2. Those across waterways—e.g., that across Lake Pontchartrain, near New Orleans, 22 miles long.

3. Those across swamps of soft deep mud, or across a riverbottom, liable to occasional overflow.

b. Temporary trestles.

1. To open the road for traffic as quickly as possible—often a reason of great financial importance.

2. To quickly replace a more elaborate structure, destroyed by accident, on a road already in operation, so that the interruption to traffic shall be a minimum.

3. To form an earth embankment with earth brought from a distant point by the train-load, when such a measure would cost less than to borrow earth in the immediate neighborhood.

4. To bridge an opening temporarily and thus allow time to learn the regimen of a stream in order to better proportion the

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size of the waterway and also to facilitate bringing *suitable* stone for masonry from a distance. In a new country there is always the double danger of either building a culvert too small, requiring expensive reconstruction, perhaps after a disastrous washout, or else wasting money by constructing the culvert unnecessarily large. Much masonry has been built of a very poor quality of stone because it could be conveniently obtained and because good stone was unobtainable except at a prohibitive cost for transportation. Opening the road for traffic by the use of temporary trestles obviates both of these difficulties.

127. Trestles vs. embankments. Low embankments are very much cheaper than low trestles both in first cost and maintenance. Very high embankments are very expensive to construct, but cost comparatively little to maintain. A trestle of equal height may cost much less to construct, but will be expensive to maintain—perhaps  $\frac{1}{8}$  of its cost per year. To determine the height beyond which it will be cheaper to maintain a trestle rather than build an embankment, it will be necessary to allow for the cost of maintenance. The height will also depend on the relative cost of timber, labor, and earthwork. At the present average values, it will be found that for less heights than 25 feet the first cost of an embankment will generally be less than that of a trestle; this implies that a permanent trestle should never be constructed with a height less than 25 feet except for the reasons given in § 126. The height at which a permanent trestle is certainly cheaper than earthwork is more uncertain. A high grade line joining two hills will invariably imply at least a culvert if an embankment is used. If the culvert is built of masonry, the cost of the embankment will be so increased that the height at which a trestle becomes economical will be materially reduced. The cost of an embankment increases much more rapidly than the height-with very high embankments more nearly as the square of the height-while the cost of trestles does not increase as rapidly as the height. Although local circumstances may modify the application of any set rules, it is probably seldom that it will be cheaper to build an embankment 40 or 50 feet high than to permanently maintain a wooden trestle of that height. A steel viaduct would probably be the best solution of such a case. These are frequently used for permanent structures, especially when very high. The cost of maintenance is much less than that of wood, which makes the

use of iron or steel preferable for permanent trestles unless wood is abnormally cheap. Neither the cost nor the construction of iron or steel trestles will be considered in this chapter.

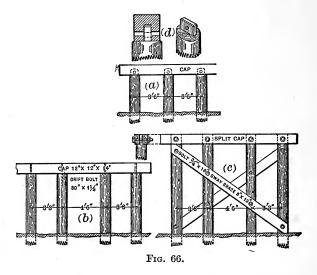
128. Two principal types. There are two principal types of wooden trestles—pile trestles and framed trestles. The great objection to pile trestles is the rapid rotting of the portion of the pile which is underground, and the difficulty of renewal. The maximum height of pile trestles is about 30 feet, and even this height is seldom reached. Framed trestles have been constructed to a height of considerably over 100 feet They are frequently built in such a manner that any injured piece may be readily taken out and renewed without interfering with traffic. Trestles consist of two parts—the supports called "bents," and the stringers and floor system. As the stringers and floor system are the same for both pile and framed trestles, the "bents" are all that need be considered separately.

### PILE TRESTLES.

129. Pile bents. A pile bent consists generally of four piles driven into the ground deep enough to afford not only sufficient vertical resistance but also lateral resistance. On top of these piles is placed a horizontal "cap." The caps are fastened to the tops of the piles by methods illustrated in Fig. 66. The method of fastening shown in each case should not be considered as applicable only to the particular type of pile bent used to illustrate it. Fig. 66 (a and d) illustrates a mortise-joint with a hardwood pin about  $1\frac{1}{4}$ " in diameter. The hole for the pin should be bored separately through the cap and the mortise, and the hole through the cap should be at a slightly higher level than that through the mortise, so that the cap will be drawn down tight when the pin is driven. Occasionally an iron dowel (an iron pin about  $1\frac{1}{2}$  in diameter and about 6" long) is inserted partly in the cap and partly in the pile. The use of drift-bolts, shown in Fig. 66 (b), is cheaper in first cost, but renders repairs and renewals very troublesome and expensive. "Split caps," shown in Fig. 66 (c), are formed by bolting two half-size strips on each side of a tenon on top of the pile. Repairs are very easily and cheaply made without interference with the traffic and without injuring other pieces of the bent. The smaller pieces are more easily obtainable in a sound condition; the

decay of one does not affect the other, and the first cost is but little if any greater than the method of using a single piece. For further discussion, see § 136.

For very light traffic and for a height of about 5 feet three vertical piles will suffice, as shown in Fig. 66 (a). Up to a height



of 8 or 10 feet four piles may be used without sway-bracing, as in Fig 66 (b), if the piles have a good bearing. For heights greater than 10 feet sway-bracing is generally necessary. The outside piles are frequently driven with a batter varying from 1:12 to 1:4.

Piles are made, if possible, from timber obtained in the vicinity of the work. Durability is the great requisite rather than strength, for almost any timber is strong enough (except as noted below) and will be suitable if it will resist rapid decay. The following list is quoted as being in the order of preference on account of durability:

1. Red cedar5. White pine2. Red cypress6. Redwood3. Pitch-pine7. Elm4. Yellow pine8. Spruce	10. Post-oak	12. Black oak 13. Hemlock 14. Tamarac
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Red-cedar piles are said to have an average life of 27 years with a possible maximum of 50 years, but the timber is rather weak, and if exposed in a river to flowing ice or driftwood is apt to be injured. Under these circumstances oak is preferable, although its life may be only 13 to 18 years.

130. Methods of driving piles. The following are the principal methods of driving piles:

a. A hammer weighing 2000 to 3000 lbs. or more, sliding in guides, is drawn up by horse-power or a portable engine, and allowed to fall *freely*.

b. The same as above except that the hammer does not fall freely, but drags the rope and revolving drum as it falls and is thus quite materially retarded. The mechanism is a little more simple, but is less effective, and is sometimes made deliberately deceptive by a contractor by retarding the blow, in order to apparently indicate the requisite resistance on the part of the pile.

The above methods have the advantage that the mechanism is cheap and can be transported into a new country with comparative ease, but the work done is somewhat ineffective and costly compared with some of the more elaborate methods given below.

c. Gunpowder pile-drivers, which automatically explode a cartridge every time the hammer falls. The explosion not only forces the pile down, but throws up the hammer for the next blow. For a given height of fall the effect is therefore doubled. It has been shown by experience, however, that when it is attempted to use such a pile-driver rapidly the mechanism becomes so heated that the cartridges explode prematurely, and the method has therefore been abandoned.

d. Steam pile-drivers, in which the hammer is operated directly by steam. The hammer falls freely a height of about 40 inches and is raised again by steam. The effectiveness is largely due to the rapidity of the blows, which does not allow time between the blows for the ground to settle around the pile and increase the resistance, which does happen when the blows are infrequent. "The hammer-cylinder weighs 5500 lbs., and with 60 to 75 lbs. of steam gives 75 to 80 blows per minute. With 41 blows a large unpointed pile was driven 35 feet into a hard clay bottom in half a minute." Such a driver would cost about \$800.

The above four methods are those usual for dry earth. In very soft wet or sandy soils, where an unlimited supply of water is available, the *water-jet* is sometimes employed. A pipe is fastened along the side of the pile and extends to the pile-point. If water is forced through the pipe, it loosens the sand around the point and, rising along the sides, decreases the side resistance so that the pile sinks by its own weight, aided perhaps by extra weights loaded on. This loading may be accomplished by connecting the top of the pile and the pile-driver by a block and tackle so that a portion of the weight of the pile-driver is continually thrown on the pile.

Excessive driving frequently fractures the pile below the surface and thereby greatly weakens its bearing power. To



prevent excessive "brooming" of the top of the pile, owing to the action of the hammer, the top should be protected by an iron ring fitted to the top of the pile. The "brooming" not only renders the driving ineffective and hence uneconomical, but vitiates the value of any test of the bearing power of the pile by noting the sinking due to a given weight falling a given distance. If the pile is so soft that brooming is unavoidable, the top

Fig. 67. should be adzed off frequently, and especially should it be done just before the final blows which are to test its bearing-power.

In a new country judgment and experience will be required to decide intelligently whether to employ a simple drop-hammer machine, operated by horse-power and easily transported but uneconomical in operation, or a more complicated machine working cheaply and effectively after being transported at greater expense.

131. Pile-driving formulæ. If R=the resistance of a pile, and s the set of the pile during the last blow, w the weight of the pile-hammer, and h the fall during the last blow, then we may state the approximate relation that Rs=wh, or  $R=\frac{wh}{s}$ . This is the basic principle of all rational formulæ, but the maximum weight which a pile will sustain after it has been driven some time is by no means equal to the resistance of the pile during the last blow. There are also many other modifying elements which have been variously allowed for in the many proposed formulæ. The formulæ range from the extreme of empirical simplicity to very complicated attempts to allow properly for all modifying causes. As the simplest rule, specifications sometimes require that the piles shall be driven until the pile will not sink more than 5 inches under five consecutive blows of a 2000-lb. hammer falling 25 feet. The "Engineering News formula" \* gives the safe load as  $\frac{2wh}{s+1}$ , in which w =weight of hammer, h = fall in feet, s = set of pile in inches underThis formula is derived from the above basic the last blow. formula by calling the safe load  $\frac{1}{6}$  of the final resistance, and by adding (arbitrarily) 1 to the final set (s) as a compensation for the extra resistance caused by the settling of earth around the pile between each blow. This formula is used only for ordinary hammer-driving. When the piles are driven by a steam pile-driver the formula becomes safe load  $=\frac{2wh}{s+0.1}$ . For the "gunpowder pile-driver," since the explosion of the cartridge drives the pile in with the same force with which it throws the hammer upward, the effect is *twice* that of the fall of the hammer, and the formula becomes safe load  $=\frac{4wh}{s+0.1}$ . In these last two formulæ the constant in the denominator is changed from s+1to s+0.1. The constant (1.0 or 0.1) is supposed to allow, as before stated, for the effect of the extra resistance caused by the earth settling around the pile between each blow. The more rapid the blows the less the opportunity to settle and the less the proper value of the constant. The above formulæ have been given on account of their simplicity and their practical agreement with experience. Many

simplicity and their practical agreement with experience. Many other formulæ have been proposed, the majority of which are more complicated and attempt to take into account the weight of the pile, resistance of the guides, etc. While these elements, as well as many others, have their influence, their effect is so overshadowed by the indeterminable effect of other elements as, for example, the effect of the settlement of earth around the pile between blows—that it is useless to attempt to employ anything but a purely empirical formula.

*Examples.* 1. A pile was driven with an ordinary hammer weighing 2500 pounds until the sinking under five consecutive blows was  $15\frac{1}{2}$  inches. The fall of the hammer during the last

<sup>\*</sup> Engineering News, Nov. 17, 1892.

blows was 24 feet. What was the safe bearing power of the pile?

$$\frac{2wh}{s+1} = \frac{2 \times 2500 \times 24}{(\frac{1}{s} \times 15.5) + 1} = \frac{120000}{4.1} = 29300 \text{ pounds.}$$

2. Piles are being driven into a firm soil with a steam piledriver until they show a *safe* bearing power of 20 tons. The hammer weighs 5500 pounds and its fall is 40 inches. What should be the sinking under the final blow?

$$40000 = \frac{2wh}{s+0.1} = \frac{2 \times 5500 \times 3.33}{s+0.1},$$
$$s = \frac{36667}{40000} - 0.1 = .81 \text{ inch.}$$

132. Pile-points and pile-shoes. Piles are generally sharpened to a blunt point. If the pile is liable to strike boulders, sunken

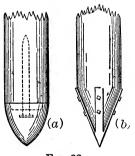


FIG. 68.

logs, or other obstructions which are liable to turn the point, it is necessary to protect the point by some form of shoe. Several forms in cast iron have been used, also a wrought-iron shoe, having four "straps" radiating from the apex, the straps being nailed on to the pile, as shown in Fig. 68 (b). The cast-iron form shown in Fig. 68 (a) has a base cast around a drift-bolt. The recess on the top of the base receives the bottom of the pile and pre-

vents a tendency to split the bottom of the pile or to force the shoe off laterally.

**133.** Details of design. No theoretical calculations of the strength of pile bents need be attempted on account of the extreme complication of the theoretical strains, the uncertainty as to the real strength of the timber used, the variability of that strength with time, and the insignificance of the economy that would be possible even if exact sizes could be computed. The piles are generally required to be not less than 10" or 12" in diameter at the large end. The P. R. R. requires that they shall

#### TRESTLES

be "not less than 14 and 7 inches in diameter at butt and small end respectively, exclusive of bark, which must be removed." The removal of the bark is generally required in good work. Soft *durable* woods, such as are mentioned in § 129, are best for the piles, but the caps are generally made of oak or yellow pine. The caps are generally 14 feet long (for single track) with a cross-section  $12'' \times 12''$  or  $12'' \times 14''$ . "Split caps" would consist of two pieces  $6'' \times 12''$ . The sway-braces, never used for less heights than 6', are made of  $3'' \times 12''$  timber, and are spiked on with  $\frac{2}{3}''$  spikes 8'' long. The floor system will be the same as that described later for framed trestles.

134. Cost of pile trestles. The cost, per linear foot, of piling depends on the method of driving, the scarcity of suitable timber, the price of labor, the length of the piles, and the amount of shifting of the pile-driver required. The cost of soft-wood piles varies from 8 to 15 c. per lineal foot, and the cost of oak piles varies from 10 to 30 c. per foot according to the length, the longer piles costing more per foot. The cost of driving will average about \$2.50 per pile, or 7.5 to 10 c. per lineal foot. Since the cost of shifting the pile-driver is quite an item in the total cost, the cost of driving a long pile would be *less* per foot than for a short pile, but on the other hand the cost of the pile is *greater* per foot, which tends to make the total cost per foot constant. Specifications generally say that the piling will be paid for per lineal foot of piling *left in the work*. The wastage of the tops of piles sawed off is always something, and is frequently very large. Sometimes a small amount per foot of piling sawed off is allowed the contractor as compensation for his loss. This reduces the contractor's risk and possibly reduces his bid by an equal or greater amount than the extra amount actually paid him.

#### FRAMED TRESTLES.

135. Typical design. A typical design for a framed trestle bent is given in Fig. 69. This represents, with slight variations of detail, the plan according to which a large part of the framed trestle bents of the country have been built—i.e., of those less than 20 or 30 feet in height, not requiring multiple story construction.

136. Joints. (a) The mortise-and-tenon joint is illustrated in

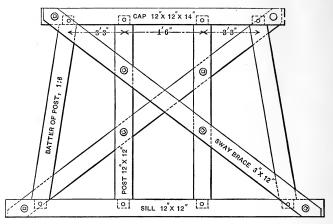
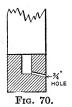


Fig. 69 and also in Fig. 66 (a). The tenon should be about

FIG. 69.

3" thick, 8" wide, and  $5\frac{1}{2}$ " long. The mortise should be cut

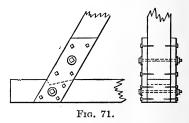


a little deeper than the tenon. "Drip-holes" from the mortise to the outside will assist in draining off water that may accumulate in the joint and thus prevent the rapid decay that would otherwise ensue. These joints are very troublesome if a single post decays and requires renewal. It is generally required that the mortise and tenon should be thoroughly daubed

with paint before putting them together. This will tend to make the joint water-tight and prevent decay from the accumulation and retention of water in the joint.

(b) The plaster joint. This joint is made by bolting and

spiking a  $3'' \times 12''$  plank on both sides of the joint. The cap and sill should be notched to receive the posts. Repairs are greatly facilitated by the use of these joints. This method has been used by the Delaware and Hudson Canal Co. [R. R.].



(c) Iron plates. An iron plate of the form shown in Fig. 72

(b) is bent and used as shown in Fig. 72 (a). Bolts passing

through the bolt-holes shown secure the plates to the timbers and make a strong joint which may be readily loosened for repairs. By slight modifications in the design the method may be used for inclined posts and complicated joints.

(d) Split caps and sills. These are described in

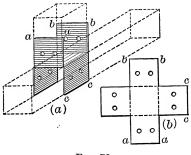


FIG. 72.

§ 129. Their advantages apply with even greater force to framed trestles.

(e) Dowels and drift-bolts. These joints facilitate cheap and rapid construction, but renewals and repairs are very difficult, it being almost impossible to extract a drift-bolt, which has been driven its full length, without splitting open the pieces containing it. Notwithstanding this objection they are extensively used, especially for temporary work which is not expected to be used long enough to need repairs.

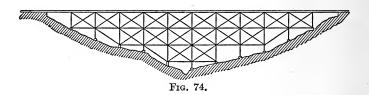
Fra. 73.

Multiple-story construc-137. tion. Single-story framed trestle bents are used for heights up to 18 or 20 feet and exceptionally up to 30 feet. For greater heights some such construction as is illustrated in a skeleton design in Fig. 73 is used. By using split sills between each story and separate vertical and batter posts in each story, any piece may readily be removed and renewed if necessary. The height of these stories varies, in different designs, from 15 to 25 and even 30 feet. Tn some designs the structure of each story is independent of the stories above and below. This greatly

facilitates both the original construction and subsequent repairs.

In other designs the verticals and batter-posts are made continuous through two consecutive stories. The structure is somewhat stiffer, but is much more difficult to repair.

Since the bents of any trestle are usually of variable height and those heights are not always an even multiple of the uniform height desired for the stories, it becomes necessary to make the



upper stories of uniform height and let the odd amount go to the lowest story, as shown in Figs. 73 and 74.

138. Span. The shorter the span the greater the number of trestle bents; the longer the span the greater the required strength of the stringers supporting the floor. Economy demands the adoption of a span that shall make the sum of these require-

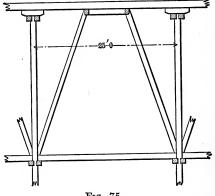


FIG. 75.

ments a minimum. The higher the trestle the greater the cost of each bent, and the greater the span that would be justifiable. Nearly all trestles have bents of variable height, but the advantage of employing uniform standard sizes is so grea<sup>+</sup> that many

 $170^{\circ}$ 

#### TRESTLES.

roads use the same span and sizes of timber not only for the panels of any given trestle, but also for all trestles regardless of height. The spans generally used vary from 10 to 16 feet. The Norfolk and Western R. R. uses a span of 12' 6" for all singlestory trestles, and a span of 25' for all multiple-story trestles. The stringers are the same in both cases, but when the span is 25 feet, knee-braces are run from the sill of the first story below to near the middle of each set of stringers. These knee-braces are connected at the top by a "straining-beam" on which the stringers rest, thus supporting the stringer in the center and virtually reducing the span about one-half.

139. Foundations. (a) Piles. Piles are frequently used as a foundation, as in Fig. 76, particularly in soft ground, and also

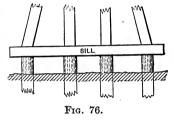
for temporary structures. These foundations are cheap, quickly constructed, and are particularly valuable when it is financially necessary to open the road for traffic as soon as possible and with the least expenditure of money; but there is the disadvantage of inevitable decay

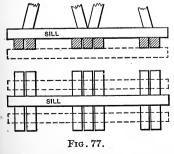
within a few years unless the piles are chemically treated, as will be discussed later. Chemical treatment, however, increases the cost so that such a foundation would often cost more than a foundation of stone. A pile should be driven under each post as shown in Fig. 76.

(b) Mud-sills. Fig. 77 illustrates the use of mud-sills as

built by the Louisville and Nashville R. R. Eight blocks  $12'' \times 12'' \times 6'$  are used under each bent. When the ground is very soft, two additional timbers  $(12'' \times 12'' \times \text{length of}$ bent-sill), as shown by the dotted lines, are placed underneath. The number required evidently depends on the nature of the ground.

(c) Stone foundations. Stone foundations are the best and the most expensive. For very high trestles the Norfolk and





Western R. R. employs foundations as shown in Fig. 78, the walls being 4 feet thick. When the height of the trestle is 72 feet or less (the plans requiring for 72' in height a foundation-wall 39' 6'' long) the foundation is made continuous. The sill



of the trestle should rest on several short lengths of  $3'' \times 12''$  plank, laid transverse to the sill on top of the wall.

140. Longitudinal bracing. This is required to give the structure longitudinal stiffness and also to reduce the columnar length of the posts. This bracing generally consists of horizontal "waling-strips" and diagonal braces. Sometimes the braces are placed wholly on the outside posts unless the trestle is very high. For single-story trestles the P. R. R. employs the "laced" system, i.e., a line of posts joining the cap of one bent with the sill of the next, and the sill of that bent with the cap of the next. Some plans employ braces forming an  $\times$  in alternate panels. Connecting these braces in the center more than doubles their columnar strength. Diagonal braces, when bolted to posts, should be fastened to them as near the ends of the posts as possible. The sizes employed vary largely, depending on the clear length and on whether they are expected to act by tension or compression.  $3'' \times 12''$  planks are often used when the design would require tensile strength only, and  $8'' \times 8''$ posts are often used when compression may be expected.

141. Lateral bracing. Several of the more recent designs of trestles employ diagonal lateral bracing between the caps of adjacent bents. It adds greatly to the stiffness of the trestle and better maintains its alignment.  $6'' \times 6''$  posts, forming an  $\times$  and connected at the center, will answer the purpose.

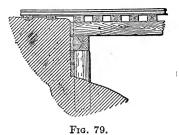
142. Abutments. When suitable stone for masonry is at hand and a suitable subsoil for a foundation is obtainable without too much excavation, a masonry abutment will be the best. Such an abutment would probably be used when masonry footings for trestle bents were employed (§ 139, c).

Another method is to construct a "crib" of 10"×12" timber,

laid horizontally, drift-bolted together, securely braced and embedded into the ground. Except for temporary construction

such a method is generally objectionable on account of rapid decay.

Another method, used most commonly for pile trestles, and for framed trestles having pile foundations (§ 139, a), is to use a pile bent at such a place that the natural surface on the uphill side is not far below the



cap, and the thrust of the material, filled in to bring the surface to grade, is insignificant.  $3'' \times 12''$  planks are placed behind the piles, cap, and stringers to retain the filled material.

#### FLOOR SYSTEMS.

143. Stringers. The general practice is to use two, three, and even four stringers under each rail. Sometimes a stringer is placed under each guard-rail. Generally the stringers are made of two panel lengths and laid so that the joints alternate. A few roads use stringers of only one panel length, but this practice is strongly condemned by many engineers. The stringers should be separated to allow a circulation of air around them and prevent the decay which would occur if they were placed close together. This is sometimes done by means of 2" planks. 6' to 8' long, which are placed over each trestle bent. Several bolts, passing through all the stringers forming a group and through the separators, bind them all into one solid construction. Cast-iron "spools" or washers, varying from 4" to  $\frac{3}{4}$ " in length (or thickness), are sometimes strung on each bolt so as to separate the stringers. Sometimes washers are used between the separating planks and the stringers, the object of the separating planks then being to bind the stringers, especially abutting stringers, and increase their stiffness.

The most common size for stringers is  $8'' \times 16''$ . The Pennsylvania Railroad varies the width, depth, and number of stringers under each rail according to the clear span. It may be noticed that, assuming a uniform load per running foot, both the pressure per square inch at the ends of the stringers (the caps having a width of 12") and also the stress due to transverse strain are kept *approximately* constant for the variable gross load on these varying spans.

\$ 144.

Clear span.	No. of pieces under each rail.	Width.	Depth.
10 feet	2	8 inches	16 inches
12 ''	2	10 ''	16 ''
14 ''	3	10 ''	16 ''

144. Corbels. A corbel (in trestle-work) is a stick of timber (perhaps two placed side by side), about 3' to 6' long, placed underneath and along the stringers and resting on the cap. There are strong prejudices for and against their use, and a corresponding diversity in practice. They are bolted to the stringers and thus stiffen the joint. They certainly reduce the objectionable crushing of the fibers at each end of the stringer, but if the corbel is no wider than the stringers, as is generally the case, the area of pressure between the corbels and the cap is



FIG. 80.

no greater and the pressure per square inch on the cap is no less than the pressure on the cap if no corbels were used. If the corbels and cap are made of hard wood, as is recommended by some, the danger of crushing is lessened, but the extra cost and the frequent scarcity of hard wood, and also the extra cost and labor of using corbels, may often neutralize the advantages obtained by their use.

145. Guard-rails. These are frequently made of  $5'' \times 8''$  stuff, notched 1" for each tie. The sizes vary up to  $8'' \times 8''$ , and the depth of notch from  $\frac{3}{4}$ " to  $1\frac{1}{2}$ ". They are generally bolted to every third or fourth tie. It is frequently specified that they shall be made of oak, white pine, or yellow pine. The joints are made over a tie, by halving each piece, as illustrated in Fig. 81. The joints on opposite sides of the trestle should be "stag-

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gered." Some roads fasten every tie to the guard-rail, using a bolt, a spike, or a lag-screw.

Guard-rails were originally used with the idea of preventing the wheels of a derailed truck from running off the ends of the ties. But it has been found that an outer guard-rail alone (without an inner guard-rail) becomes an actual element of danger, since it has frequently happened that a derailed wheel has caught on the outer guard-rail, thus causing the truck to slew around



and so produce a dangerous accident. The true function of the *outside* guard-rail is thus changed to that of a tie-spacer, which keeps the ties from spreading when a derailment occurs. The inside guard-rail generally consists of an ordinary steel rail spiked about 10 inches inside of the running rail. These inner guard-rails should be bent inward to a point in the center of the track about 50 feet beyond the end of the bridge or trestle. If the inner guard-rails are placed with a clear space of 10 inches inside the running rail, the outer guard-rails should be *at least* 6' 10" apart. They are generally much farther apart than this.

146. Ties on trestles. If a car is derailed on a bridge or trestle, the heavily loaded wheels are apt to force their way between the ties by displacing them unless the ties are closely spaced and fastened. The clear space between ties is generally equal to or less than their width. Occasionally it is a little more than their width.  $6'' \times 8''$  ties, spaced 14'' to 16'' from center to center, are most frequently used. The length varies from 9' to 12' for single track. They are generally notched  $\frac{1}{2}$ " deep on the under side where they rest on the stringers. Oak ties are generally required even when cheaper ties are used on the other sections of the road. Usually every third or fourth tie is bolted to the stringers. When stringers are placed underneath the guard-rails, bolts are run from the top of the guard-rail to the under side of the stringer. The guard-rails thus hold down the whole system of ties, and no direct fastening of the ties to the stringers is needed.

147. Superelevation of the outer rail on curves. The location of curves on trestles should be avoided if possible, especially when the trestle is high. Serious additional strains are intro-

§ 146.

duced especially when the curvature is sharp or the speed high. Since such curves are sometimes practically unavoidable, it is necessary to design the trestle accordingly. If a train is stopped on a curved trestle, the action of the train on the trestle is evidently vertical. If the train is moving with a considerable velocity, the resultant of the weight and the centrifugal action is a force somewhat inclined from the vertical. Both of these conditions may be expected to exist at times. If the axis of the system of posts is vertical (as illustrated in methods a, b, c, d, and e). any lateral force, such as would be produced by a moving train, will tend to rack the trestle bent. If the stringers are set vertically, a centrifugal force likewise tends to tip them sidewise. If the axis of the system of posts (or of the stringers) is inclined so as to coincide with the pressure of the train on the trestle when the train is moving at its normal velocity, there is no tendency to rack the trestle when the train is moving at that velocity, but there will be a tendency to rack the trestle or twist the stringers when the train is stationary. Since a moving train is usually the normal condition of affairs, as well as the condition which produces the maximum stress, an inclined axis is evidently preferable from a theoretical standpoint; but whatever design is adopted, the trestle should evidently be sufficiently cross-braced for either a moving or a stationary load, and any proposed design must be studied as to the effect of both of these conditions. Some of the various methods of securing the requisite superelevation may be described as follows:

(a) Framing the outer posts longer than the inner posts, so

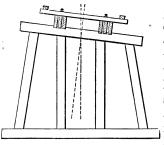


FIG. 82.

that the cap is inclined at the proper angle; axis of posts vertical. (Fig. 82.) The method requires more work in framing the trestle, but simplifies subsequent track-laying and maintenance, unless it should be found that the superelevation adopted is unsuitable, in which case it could be corrected by one of the other methods given below. The stringers tend to twist when the train is sta-

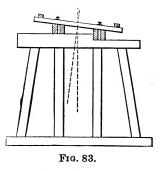
tionary.

(b) Notching the cap so that the stringers are at a different

elevation. (Fig. 83.) This weakens the cap and requires that

all ties shall be notched to a bevelled surface to fit the stringers, which also weakens the ties. A centrifugal force will tend to twist the stringers and rack the trestle.

(c) Placing wedges underneath the ties at each stringer. These wedges are fastened with two bolts. Two or more wedges will be required for each tie. The additional number of pieces required



for a long curve will be immense, and the work of inspection and keeping the nuts tight will greatly increase the cost of maintenance.

(d) Placing a wedge under the outer rail at each tie. This requires but one extra piece per tie. There is no need of a wedge under the inner tie in order to make the rail normal to the tread. The resulting inward inclination is substantially that produced by some forms of rail-chairs or tie-plates. The spikes (a little longer than usual) are driven through the wedge into the tie. Sometimes "lag-screws" are used instead of spikes. If experience proves that the superelevation is too much or too little, it may be changed by this method with less work than by any other.

(e) Corbels of different heights.

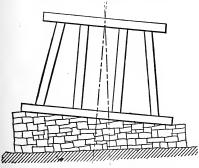


FIG. 84.

When corbels are used (see § 144) the required inclination of the floor sys\_ tem may be obtained by varying the depth of the corbels.

(f) Tipping the whole trestle. This is done by placing the trestle on an inclined foundation. If very much inclined, the trestle bent must be secured against the possibility of slipping sidewise.

for the slope would be considerable with a sharp curve, and the

vibration of a moving train would reduce the coefficient of friction to a comparatively small quantity.

(g) Framing the outer posts longer. This case is identical with case (a) except that the axis of the system of posts is inclined, as in case (f), but the sill is horizontal.

The above-described plans will suggest a great variety of methods which are possible and which differ from the above only in minor details.

148. Protection from fire. Trestles are peculiarly subject to fire, from passing locomotives, which may not only destroy the trestle, but perhaps cause a terrible disaster. This danger is sometimes reduced by placing a strip of galvanized iron along the top of each set of stringers and also along the tops of the caps. Still greater protection was given on a long trestle on the Louisville and Nashville R. R. by making a solid flooring of timber, covered with a layer of ballast on which the ties and rails were laid as usual.

Barrels of water should be provided and kept near all trestles, and on very long trestles barrels of water should be placed every two or three hundred feet along its length. A place for the barrels may be provided by using a few ties which have an extra length of about four feet, thus forming a small platform, which should be surrounded by a railing. The track-walker should be held accountable for the maintenance of a supply of water in these barrels, renewals being frequently necessary on account of evaporation. Such platforms should also be provided as REFUGE-BAYS for track-walkers and trackmen working on the trestle. On very long trestles such a platform is sometimes provided with sufficient capacity for a hand-car.

149. Timber. Any strong durable timber may be used when the choice is limited, but oak, pine, or cypress are preferred when obtainable. When all of these are readily obtainable, the various parts of the trestle will be constructed of different kinds of wood—the stringers of long-leaf pine, the posts and braces of pine or red cypress, and the caps, sills, and corbels (if used) of white oak. The use of oak (or a similar hard wood) for caps, sills, and corbels is desirable because of its greater strength in resisting crushing across the grain, which is the critical test for these parts. There is no physiological basis to the objection, sometimes made, that different species of timber, in contact with each other, will rot quicker than if only one

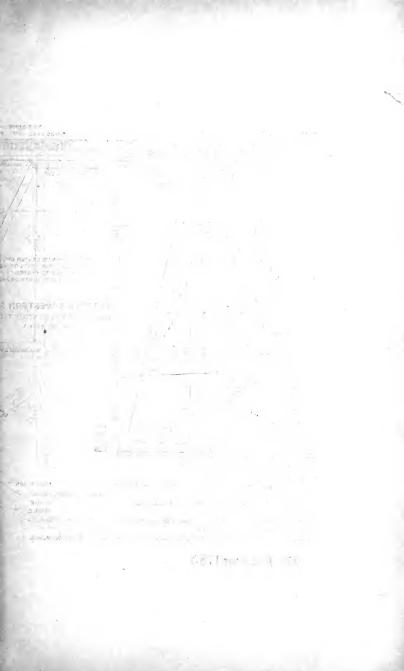
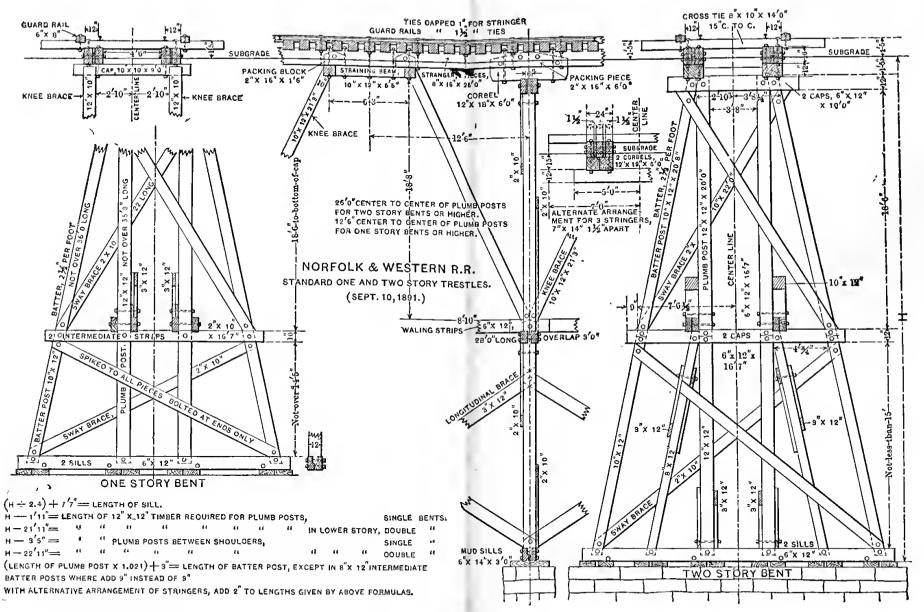
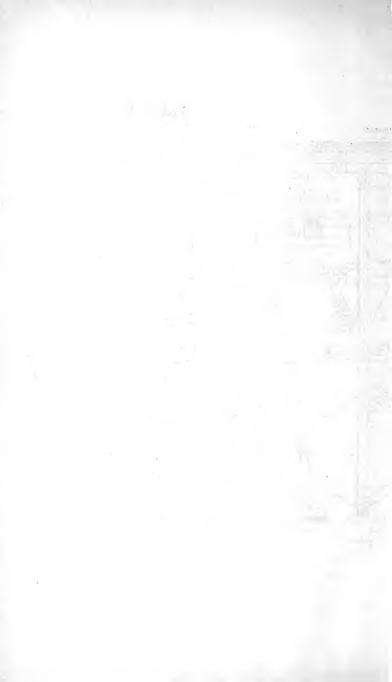




PLATE 11.



(To face page 178.)



kind of timber is used. When a very extensive trestle is to be built at a place where suitable growing timber is at hand but there is no convenient sawmill, it will pay to transport a portable sawmill and engine and cut up the timber as desired.

150. Cost of framed timber trestles. The cost varies widely on account of the great variation in the cost of timber. When a railroad is first penetrating a new and undeveloped region, the cost of timber is frequently small, and when it is obtainable from the company's right-of-way the only expense is felling and The work per M, B. M., is small, considering that a sawing. single stick  $12'' \times 12'' \times 25'$  contains 300 feet, B. M., and that sometimes a few hours' work, worth less than \$1, will finish all the work required on it. Smaller pieces will of course require more work per foot, B. M. Long-leaf pine can be purchased from the mills at from \$8 to \$12 per M feet, B. M., according to the dimensions. To this must be added the freight and labor of erection. The cartage from the nearest railroad to the trestle may often be a considerable item. Wrought iron will cost about 3 c. per pound and cast iron 2 c., although the prices are often lower than these. The amount of iron used depends on the detailed design, but, as an average, will amount to \$1.50 to \$2 per 1000 feet, B. M., of timber. A large part of the trestling of the country has been built at a contract price of about \$30 per 1000 feet, B. M., erected. While the cost will frequently rise to \$40 and even \$50 when timber is scarce, it will drop to \$13 (cost quoted) when timber is cheap.

## DESIGN OF WOODEN TRESTLES.

151. Common practice. A great deal of trestling has been constructed without any rational design except that custom and experience have shown that certain sizes and designs are *probably* safe. This method has resulted occasionally in failures but more frequently in a very large waste of timber. Many railroads employ a uniform size for all posts, caps, and sills, and a uniform size for stringers, all regardless of the height or span of the trestle. For repair work there are practical reasons favoring this. "To attempt to run a large lot of sizes would be more wasteful in the end than to maintain a few stock sizes only. Lumber can be bought more cheaply by giving a general order for 'the run of the mill for the season,' or 'a cargo lot,' specify ing approximate percentages of standard stringer size, of  $12 \times 12$ -inch stuff,  $10 \times 10$ -inch stuff, etc., and a liberal proportion of 3- or 4-inch plank, all lengths thrown in. The  $12 \times 12$ inch stuff, etc., is ordered all lengths, from a certain specified length up. In case of a wreck, washout, burn-out, or sudden call for a trestle to be completed in a stated time, it is much more economical and practical to order a certain number of carloads of 'trestle stuff' to the ground and there to select piece after piece as fast as needed, dependent only upon the length of stick required. When there is time to make the necessary survevs of the ground and calculations of strength, and to wait for a special bill of timber to be cut and delivered, the use of different sizes for posts in a structure would be warranted to a certain extent." \* For new construction, when there is generally sufficient time to design and order the proper sizes, such wastefulness is less excusable, and under any conditions it is both safer and more economical to prepare standard designs which can be made applicable to varying conditions and which will at the same time utilize as much of the strength of the timber as can be depended on. In the following sections will be given the elements of the preparation of such standard designs, which will utilize uniform sizes with as little waste of timber as possible. It is not to be understood that special designs should be made for each individual trestle.

152. Required elements of strength. The stringers of trestles are subject to transverse strains, to crushing across the grain at the ends, and to shearing along the neutral axis. The strength of the timber must therefore be computed for all these kinds of stress. Caps and sills will fail, if at all, by crushing across the grain; although subject to other forms of stress, these could hardly cause failure in the sizes usually employed. There is an apparent exception to this: if piles are improperly driven and an uneven settlement subsequently occurs, it may have the effect of transferring practically all of the weight to two or three piles, while the cap is subjected to a severe transverse strain which may cause its failure. Since such action is caused generally by avoidable errors of construction it may be considered as abnormal, and since such a failure will generally occur by a gradual settlement, all danger may be avoided by reasonable

<sup>\*</sup> From "Economical Designing of Timber Trestle Bridges."

#### TRESTLES.

care in inspection. *Posts* must be tested for their columnar strength. These parts form the bulk of the trestle and are the parts which can be definitely designed from known stresses. The stresses in the bracing are more indefinite, depending on indeterminate forces, since the inclined posts take up an unknown proportion of the lateral stresses, and the design of the bracing may be left to what experience has shown to be safe, without involving any large waste of timber.

153. Strength of timber. Until recently tests of the strength of timber have generally been made by testing small, selected, well-seasoned sticks of "clear stuff," free from knots or imperfections. Such tests would give results so much higher than the vaguely known strength of large unseasoned "commercial" timber that very large factors of safety were recommended factors so large as to detract from any confidence in the whole theoretical design. Recently the U. S. Government has been making a thoroughly scientific test of the strength of full-size timber under various conditions as to seasoning, etc. The work has been so extensive and thorough as to render possible the economical designing of timber structures.

One important result of the investigation is the determination of the great influence of the moisture in the timber and the law of its effect on the strength. It has been also shown that timber soaked with water has substantially the same strength as green timber, even though the timber had once been thoroughly seasoned. Since trestles are exposed to the weather they should be designed on the basis of using green timber. It has been shown that the strength of green timber is very regularly about 55 to 60% of the strength of timber in which the moisture is 12% of the dry weight, 12% being the proportion of moisture usually found in timber that is protected from the weather but not heated, as, e.g., the timber in a barn. Since the moduli of rupture have all been reduced to this standard of moisture (12%), if we take *one-eighth* of the rupture values, it still allows a factor of safety of about five, even on green timber. On page 182 there are quoted the values taken from the U.S. Government reports on the strength of timber, the tests probably being the most thorough and reliable that were ever made.

On page 183 are given the "working unit stresses for structural timber, expressed in pounds per square inch," as recommended by the committee on "Wooden Bridges and Trestles," of the American Railway Engineering Association. The report was presented at their tenth annual convention, held in Chicago, in March. 1909.

Moduli of rupture for various timbe	ers. [12% moisture.]
(Condensed from U.S. Forestry (	Circular, No. 15.)

			Cross	-bending.		across in.	along in.
No.	Species.	Weight per cubic foot.	Ultimate Strength.	Modulus of Elasticity.	Crush- ing end- wise.	Crushing aci the grain.	Shearing alc the grain.
$     \begin{array}{c}       1 \\       2 \\       3 \\       4 \\       5 \\       6 \\       7     \end{array} $	Long-leaf pine Cuban " Short-leaf " Loblolly " White " Red " Spruce "	$38 \\ 39 \\ 32 \\ 33 \\ 24 \\ 31 \\ 39$	$\begin{array}{c} 12\ 600\\ 13\ 600\\ 10\ 100\\ 11\ 300\\ 7\ 900\\ 9\ 100\\ 10\ 000\\ \end{array}$	$\begin{array}{c} 2 \ 070 \ 000 \\ 2 \ 370 \ 000 \\ 1 \ 680 \ 000 \\ 2 \ 050 \ 000 \\ 1 \ 390 \ 000 \\ 1 \ 620 \ 000 \\ 1 \ 640 \ 000 \end{array}$	$\begin{array}{r} 8000 \\ 8700 \\ 6500 \\ 7400 \\ 5400 \\ 6700 \\ 7300 \end{array}$	$1180 \\ 1220 \\ 960 \\ 1150 \\ 700 \\ 1000 \\ 1200$	700 700 700 400 500 800
8 9 10	Bald cypress White cedar Douglas spruce	29 23 32	7 900 6 300 7 900	${\begin{array}{c}1&290&000\\&910&000\\1&680&000\end{array}}$	6000 5200 5700	800 700 800	$500 \\ 400 \\ 500$
$     \begin{array}{r}       11 \\       12 \\       13 \\       14 \\       15 \\       16 \\       19 \\       20 \\       20 \\       \end{array} $	White oak.         Overcup "           Post         "         "           Cow         "         "           Red         "         "           Texan         "         "           Willow         "         Spanish "	$50 \\ 46 \\ 50 \\ 46 \\ 45 \\ 46 \\ 45 \\ 46 \\ 46$	$\begin{array}{c} 13 \ 100 \\ 11 \ 300 \\ 12 \ 300 \\ 11 \ 500 \\ 11 \ 500 \\ 11 \ 400 \\ 13 \ 100 \\ 10 \ 400 \\ 12 \ 000 \end{array}$	$\begin{array}{c} 2 \ 090 \ 000 \\ 1 \ 620 \ 000 \\ 2 \ 030 \ 000 \\ 1 \ 610 \ 000 \\ 1 \ 970 \ 000 \\ 1 \ 860 \ 000 \\ 1 \ 750 \ 000 \\ 1 \ 930 \ 000 \end{array}$	$\begin{array}{r} 8500 \\ 7300 \\ 7100 \\ 7400 \\ 7200 \\ 8100 \\ 7200 \\ 7700 \end{array}$	$\begin{array}{c} 2200\\ 1900\\ 3000\\ 1900\\ 2300\\ 2000\\ 1600\\ 1800\\ \end{array}$	$     \begin{array}{r}       1000 \\       1000 \\       1100 \\       900 \\       1100 \\       900 \\   $
21 27 28 29 30	Shagbark hickory Pignut " White elm Cedar " White ash	$51 \\ 56 \\ 34 \\ 46 \\ 39$	16 000 18 700 10 300 13 500 10 800	$\begin{array}{c} 2 \ 390 \ 000 \\ 2 \ 730 \ 000 \\ 1 \ 540 \ 000 \\ 1 \ 700 \ 000 \\ 1 \ 640 \ 000 \end{array}$	9500 10900 6500 8000 7200	$\begin{array}{c} 2700 \\ 3200 \\ 1200 \\ 2100 \\ 1900 \end{array}$	$1100 \\ 1200 \\ 800 \\ 1300 \\ 1100$

154. Loading. As shown in § 138, the span of trestles is always small, is generally 14 feet, and is never greater than 18 feet except when supported by knee-braces. The greatest load that will ever come on any one span will be the concentrated loading of the drivers of a consolidation locomotive. With spans of 14 feet or less it is impossible for even the four pairs of drivers to be on the same span at once. The weight of the rails, ties, and guard-rails should be added to obtain the total load on the stringers, and the weight of these, plus the weight of the stringers, should be added to obtain the pressure on the caps or corbels.

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RECOMMENDED I		
. PER SQ. IN. I ENGINEERING	Compression.	F
IN LBS		
EXPRESSED		
UCTURAL TIMBER 3 AND TRESTLES.	Shearing.	Modulus
WORKING UNIT STRESSES FOR STRUCTURAL TIMBER EXPRESSED IN LBS. PER SQ. IN. RECOMMENDED BY THE COMMITTEE ON WOODEN BRIDGES AND TRESTLES. AMERICAN RAILWAY ENGINEERING ASSOCIATION, 1909.	Bending.	aulubold 1
WORKING UNIT COMMITTEE O		

§ 154.

		Bending.	ng.		Shea	Shearing.				Co	Compression.	on.		Dotio
Kind of Timber.	Extreme fiber stress.	eme stress.	Modulus of elas- ticity.	Parallel to grain.		Longitudinal shear in beams	udinal beams	Perp to	endicular grain.	Parallel grain.	lel to in.	For colmns under	Formulas for	r of of of of of
	Aver. W'rk- ulti- mate. stress	W'rk- ing stress	Average.	Aver. ulti- mate.	W'rk- ing stress	Aver. ulti- mate.	Work- ing stress.	Elastic limit.	Work- ing stress.	Aver. ulti- mate.	Work- ing stress.	Work- diams. ing safe stress. stress.	working stress string. in long column er to over 15 diams. depth	an er to se depth.
:	6100		1200 1,510,000	690	170	270	110	630	310	3600	1200	006	$1200\left(1-\frac{L}{60D}\right)$	10
:	6500		1300 1,610,000	720	180	300	120	520	260	3800	1300	980	$1300(1 - \frac{L}{60D})$	10
Short-leaf pine	5600		1100 1,480,000	710	170	330	130	340	170	3400	1100	830	$1100(1-\frac{L}{60D})$	10
•	4400	006	900 1,130,000	400	100	180	20	290	150	3000	1000	750	$1000(1 - \frac{L}{60D})$	10
•	4800	1000	1000 1,310,000	600	150	170	70	370	180	3200	1100	830	$1100(1-\frac{L}{60D})$	
•	4200	800	800 1,190,000	590	130	250	100	:	150	2600*	800	600	$800\left(1-\frac{L}{60D}\right)$	
	4600	006	900 1,220,000	670	170	260	100	:	220	3200*	1000	750	$1000(1-\frac{L}{60D})$	(
Western hemlock	5800	1100	1100 1,480,000	630	160	270*	100	440	220	3500	1200	006	$1200(1 - \frac{L}{60D})$	()
•	5000	006	800,000	300	80	:	:	400	150	3300	006	680	$900(1 - \frac{L}{60D})$	()
•	4800	006	900 1,150,000	500	120	:		340	170	3900	1100	830	$1100(1-\frac{L}{60D})$	(
•	4200	800	860,000			:		470	230	2800	006	680	$900(1 - \frac{L}{60D})$	<u>[]</u>
	5700	1100	1100 1,150,000	840	210	270	110	920	450	3500	1300	980	$1300(1-\frac{1L}{60D})$	$\frac{1}{5}$ 12
fo	Note.—These unit stress live load stresses for impact. These working stresses eent. For buildings, etc., w nnder long-continued loadin	resses tet. ses are , when ding, t	Note.—These unit stresses are for a green condition of timber and are to be used, without increasing the live load atresses for impact. * Partially air-dry. These working stresses are for railroad bridges and trestles. For highway bridges and trestles increase eent. For buildings, etc., when protected from weakher and free from impact, increase them 50 per cent. Inder long-continued loading, use 50 per cent of modulus of elasticity.	reen co * Pa ad brid <sub>i</sub> l from cent of	ndition rtially ges and weather modul	in condition of timb * Partially air-dry. bridges and trestles om weather and fre nt of modulus of ele	oer and s. For ee from lasticity	are to b highwa, impact,	e usedar y bridge increas	vithout es and t e them	increasi restles i 50 per e	ng the ncrease sent. 7	and are to be used available increasing the $\left  \begin{array}{c} L = \text{length in inches} \\ D = \text{length in inches} \end{array} \right _{D}$ For highway bridges and trestles increase the figures by 25 per rom impact, increase them 50 per cent. To compute deflection, icity.	in inches. de in ins. y 25 per effection,

TRESTLES.

This dead load is almost insignificant compared with the live load and may be included with it. The weight of rails, ties, etc., may be estimated at 240 pounds per foot. To obtain the weight on the caps the weight of the stringers must be added. which depends on the design and on the weight per cubic foot of the wood employed. But as the weight of the stringers is comparatively small, a considerable percentage of variation in weight will have but an insignificant effect on the result. Disregarding all refinements as to actual dimensions, the ordinary maximum loading for standard-gauge railroads may be taken as that due to four driving-axles, spaced 5' 0" apart and giving a pressure of 40000 pounds per axle. This should be increased to 54000 pounds per axle (same spacing) for the heaviest traffic. On the basis of 40000 pounds per axle or 20000 pounds per wheel the following results have been computed: This loading is assumed to allow for impact.

STRESSES ON VARIOUS SPANS DUE TO MOVING LOADS OF 20000 POUNDS, SPACED 5' 0" APART, WITH 120 POUNDS PER FOOT OF LIVE LOAD.

Span in feet.	Max. moment, ft. lbs.	Max. shear.	Max. load on one cap under one rail.
$     \begin{array}{c}       10 \\       12 \\       14 \\       16 \\       18     \end{array} $	$\begin{array}{c} 51 \ 500 \\ 82 \ 160 \\ 112 \ 940 \\ 123 \ 840 \\ 164 \ 860 \end{array}$	$\begin{array}{r} 30 \ 600 \\ 35 \ 720 \\ 39 \ 410 \\ 43 \ 460 \\ 47 \ 747 \end{array}$	41 200 49 440 57 680 65 920 75 160

Although the dead load does not vary in proportion to the live load, yet, considering the very small influence of the dead load, there will be no appreciable error in assuming the corresponding values, for a load of 54000 lbs. per axle, to be  $\frac{54}{40}$  of those given in the above tabulation.

155. Factors of safety. The most valuable result of the government tests is the knowledge that under given moisture conditions the strength of various species of sound timber is not the variable uncertain quantity it was once supposed to be, but that its strength can be relied on to a comparatively close percentage. This confidence in values permits the employment of lower factors of safety than have heretofore been permissible. Stresses, which when excessive would result in immediate destruction, such as cross-breaking and columnar stresses, should be allowed a higher factor of safety—say 6 or 8 for green timber. Other stresses, such as crushing across the grain and shearing along the neutral axis, which will be apparent to inspection before it is dangerous, may be allowed lower factors—say 3 to 5.

156. Design of stringers. The strength of rectangular beams of equal width varies as the square of the depth; therefore deep beams are the strongest. On the other hand, when any crosssectional dimension of timber much exceeds 12" the cost is much higher per M, B. M., and it is correspondingly difficult to obtain thoroughly sound sticks, free from wind-shakes, etc. Wind-shakes especially affect the shearing strength. Also, if the required transverse strength is obtained by using high narrow stringers, the area of pressure between the stringers and the cap may become so small as to induce crushing across the grain. This is a very common defect in trestle design. As already indicated in § 138, the span should vary roughly with the average height of the trestle, the longer spans being employed when the trestle bents are very high, although it is usual to employ the same span throughout any one trestle.

To illustrate, if we select a span of 14 feet, the load on one cap will be 57680 lbs. If the stringers and cap are made of long-leaf yellow pine, the allowable value, according to the table on page 183 for "compression across the grain" is 260 pounds per square inch; this will require 222 square inches of surface. If the cap is 12" wide, this will require a width of 18.5 inches, or say 2 stringers under each rail, each 9 inches wide. For rectangular beams

Moment = 
$$\frac{1}{6}R'bh^2$$
.

Using for R' the safe value 1300 lbs. per square inch, we have

$$112940 \times 12 = \frac{1}{6} \times 1300 \times 18 \times h^2$$
,

from which h=18''.7. If desired, the width may be increased to 10" and the depth correspondingly reduced, which will give similarly h=17''.7 or say 18". This shows that two beams,  $10'' \times 18''$ , under each rail will stand the transverse bending and have more than enough area for crushing.

The shear per square inch will equal

 $\frac{3}{2} \frac{\text{total shear}}{\text{cross-section}} = \frac{3}{2} \frac{39410}{2 \times 10 \times 18} = 164 \text{ lbs. per sq. inch.}$ 

This is higher than the recommended working value. The combination suggested on page 174, viz., 3 beams  $10'' \times 16''$  for 14 feet span, gives a far safer value. Considering that wooden beams. tested to destruction, usually fail by shearing, the three-beam combination is safer.

The deflection should be computed to see if it exceeds the somewhat arbitrary standard of  $\frac{1}{200}$  of the span. The deflection for *uniform loading* is

$$\Delta = \frac{5Wl^3}{32bh^3E},$$

in which l =length in inches;

W =total load, assumed as uniform; E =modulus of elasticity, given as 850,000 lbs.

per sq. in. for long-leaf pine, according to the table on p. 183. Then

$$\Delta = \frac{5 \times 57680 \times 168^3}{32 \times 20 \times 18^3 \times 850000} = 0^{\prime\prime}.431$$

$$\overline{200} \times 168^{\prime\prime} = 0^{\prime\prime}.84,$$

so that the calculated deflection is well within the limit. Of course the loading is not strictly uniform, but even with a liberal allowance the deflection is still safe.

For the heaviest practice (54000 lbs. per axle) these stringer dimensions must be correspondingly increased.

157. Design of posts. Four posts are generally used for single-track work. The inner posts are usually braced by the cross-braces, so that their columnar strength is largely increased; but as they are apt to get more than their share of work, the advantage is compensated and they should be treated as unsupported columns for the total distance between cap and sill in simple bents, or for the height of stories in multiple-story construction. The caps and sills are assumed to have a width of 12". It facilitates the application of bracing to have the columns of the same width and vary the other dimension as required.

Unfortunately the experimental work of the U. S. Government on timber testing has not yet progressed far enough to establish unquestionably a general relation between the strength of long columns and the crushing strength of short blocks. The following formula has been suggested, but it cannot be considered as established:

$$f = F \times \frac{700 + 15c}{700 + 15c + c^2}$$
, in which

f=allowable working stress per sq. in for long columns; F= '' '' '' '' '' short blocks;  $c=\frac{l}{d}$ ; l=length of column in inches; d=least cross-sectional dimensions in inches.

Enough work has been done to give great reliability to the two following formulæ for white pine and yellow pine, quoted from Johnson's "Materials of Construction," p. 684:

Working load per sq. in. 
$$= p = 1000 - \frac{1}{4} \left(\frac{l}{h}\right)^2$$
, long-leaf pine;  
"""""""" "  $= p = 600 - \frac{1}{8} \left(\frac{l}{h}\right)^2$ , white pine;

in which l =length of column in inches, and

h =least cross-sectional dimension in inches.

The frequent practice is to use  $12'' \times 12''$  posts for all trestles. If we substitute in the above formula l=20'=240'' and h=12'' we have  $p=1000-\frac{1}{4}(\frac{240}{12})^2=900$  lbs.

 $900 \times 144 = 129600$  lbs., the working load for each post. This is more than the total load on one trestle bent and illustrates the usual great waste of timber. Making the post  $8'' \times 12''$  and calculating similarly, we have p = 775, and the working load per column is  $775 \times 96 = 74400$  lbs. As considerable must be allowed for "weathering," which destroys the strength of the outer layers of the wood, and also for the dynamic effect of the live load,  $8'' \times 12''$  may not be too great, but it is certainly a safe dimension.  $12'' \times 6''$  would possibly prove amply safe in practice. One method of allowing for weathering is to disregard the outer half-inch on all sides of the post, i.e., to calculate the strength of a post one inch smaller in each dimension than the post actually employed. On this basis an  $8'' \times 12'' \times 20'$  post, computed as a  $7'' \times 11'$  post, would have a safe columnar strength of 706 lbs. per square inch. With an area of 77 square inches, this gives a working load of 54362 lbs. for each post, or 217448 lbs. for the four posts. Considering that 74200 lbs. is the maximum load on one cap (14 feet span), the great excess of strength is apparent.

Utilizing the formula given on page 183 for long-leaf pine, we have safe stress =  $1300 \left(1 - \frac{L}{60D}\right)$ , in which L = 20 ft. = 240 in., and D = 12 ins. Then safe stress =  $1300(1 - \frac{1}{3}) = 867$  lbs. per square inch. This is practically a check on the above calculations.

**158.** Design of caps and sills. The stresses in caps and sills are very indefinite, except as to crushing across the grain. As the stringers are placed almost directly over the inner posts, and as the sills are supported just under the posts, the transverse stresses are almost insignificant. In the above case four posts have an area of  $4 \times 12'' \times 8'' = 384$  sq. in. The total load, 74200 lbs., will then give a pressure of 193 pounds per square inch, which is within the allowable limit. This one feature might require the use of  $8'' \times 12''$  posts rather than  $6'' \times 12''$  posts, for the smaller posts, although probably strong enough as posts, would produce an objectionably high pressure.

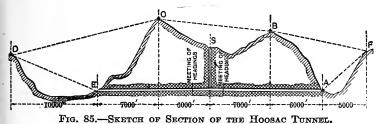
159. Bracing. Although some idea of the stresses in the bracing could be found from certain assumptions as to windpressure, etc., yet it would probably not be found wise to decrease, for the sake of economy, the dimensions which practice has shown to be sufficient for the work. The economy that would be possible would be too insignificant to justify any risk. Therefore the usual dimensions, given in §§ 139 and 140, should be employed.

## CHAPTER V.

## TUNNELS.

#### SURVEYING.

160. Surface surveys. As tunnels are always dug from each end and frequently from one or more intermediate shafts, it is necessary that an accurate surface survey should be made between the two ends. As the natural surface in a locality where a tunnel is necessary is almost invariably very steep and rough, it requires the employment of unusually refined methods of work to avoid inaccuracies. It is usual to run a line on the surface that will be at every point vertically over the center line of the tunnel. Tunnels are generally made straight unless curves are absolutely necessary, as curves add greatly to the cost. Fig. 85 represents roughly a longitudinal section of the



Hoosac Tunnel. Permanent stations were located at A, B, C, D, E, and F, and stone houses were built at A, B, C, and D. These were located with ordinary field transits at first, and then all the points were placed as nearly as possible in one vertical plane by repeated trials and minute corrections, using a very large specially constructed transit. The stations D and F were necessary because E and A were invisible from C and B. The alignment at A and E having been determined with great accuracy, the true alignment was easily carried into the tunnel.

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The relative elevations of A and E were determined with great accuracy. Steep slopes render necessary many settings of the level per unit of horizontal distance and require that the work be unusually accurate to obtain even fair accuracy per unit of distance. The levels are usually re-run many times until the probable error is a very small quantity.

The exact horizontal distance between the two ends of the tunnel must also be known, especially if the tunnel is on a grade. The usual steep slopes and rough topography likewise render accurate horizontal measurements very difficult. Frequently when the slope is steep the measurement is best obtained by measuring along the slope and allowing for grade. This may be very accurately done by employing two tripods (level or transit tripods serve the purpose very well), setting them up slightly less than one tape-length apart and measuring between horizontal needles set in wooden blocks inserted in the top of each tripod. The elevation of each needle is also observed. The true horizontal distance between two successive positions of the needles then equals the square root of the difference of the squares of the inclined distance and the difference of elevation. Such measurements will probably be more accurate than those made by attempting to hold the tape horizontal and plumbing down with plumb-bobs, because (1) it is practically difficult to hold both ends of the tape truly horizontal; (2) on steep slopes it is impossible to hold the down-hill end of a 100foot tape (or even a 25-foot length) on a level with the other end, and the great increase in the number of applications of the unit of measurement very greatly increases the probable error of the whole measurement; (3) the vibrations of a plumb-bob introduce a large probability of error in transferring the measurement from the elevated end of the tape to the ground, and the increased number of such applications of the unit of measurement still further increases the probable error.

161. Surveying down a shaft. If a shaft is sunk, as at S, Fig. 85, and it is desired to dig out the tunnel in both directions from the foot of the shaft so as to meet the headings from the outside, it is necessary to know, when at the bottom of the shaft, the elevation, alignment, and horizontal distance from each end of the tunnel.

The *elevation* is generally carried down a shaft by means of a steel tape. This method involves the least number of appli-

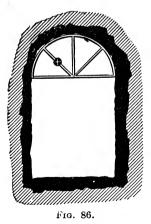
cations of the unit of measurement and greatly increases the accuracy of the final result.

The horizontal distance from each end may be easily transferred down the shaft by means of a plumb-bob, using some of the precautions described in the next paragraph.

To transfer the *alignment* from the surface to the bottom of a shaft requires the highest skill because the shaft is always small, and to produce a line perhaps several thousand feet long in a direction given by two points 6 or 8 feet apart requires that the two points must be determined with extreme accuracy. The eminently successful method adopted in the Hoosac Tunnel will be briefly described: Two beams were securely fastened across the top of the shaft (1030 feet deep), the beams being placed transversely to the direction of the tunnel and as far apart as possible and yet allow plumb-lines, hung from the intersection of each beam with the tunnel center line, to swing freely at the bottom of the shaft. These intersections of the beams with the center line were determined by averaging the results of a large number of careful observations for alignment. Two fine parallel wires, spaced about  $\frac{1}{16}$  apart, were then stretched between the beams so that the center line of the tunnel bisected at all points the space between the wires. Plumb-bobs, weighing 15 pounds, were suspended by fine wires beside each cross-beam, the wires passing between the two parallel alignment wires and bisecting the space. The plumbbobs were allowed to swing in pails of water at the bottom. Drafts of air up the shaft required the construction of boxes surrounding the wires. Even these precautions did not suffice to absolutely prevent vibration of the wire at the bottom through a very small arc. The mean point of these vibrations in each case was then located on a rigid cross-beam suitably placed at the bottom of the shaft and at about the level of the roof of the tunnel. Short plumb-lines were then suspended from these points whenever desired; a transit was set (by trial) so that its line of collimation passed through both plumb-lines and the line at the bottom could thus be prolonged.

Some recent experience in the "Tamarack" shaft, 4250 feet deep, shows that the accuracy of the results may be affected by air-currents to an unsuspected extent. Two 50-lb. cast-iron plumb-bobs were suspended with No. 24 piano-wire in this shaft. The carefully measured distances between the wires at top and bottom were 16.32 and 16.43 feet respectively. After considerable experimenting to determine the cause of the variation, it was finally concluded that air-currents were alone responsible. The variation of the bobs from a true vertical plane passing through the wires at the top was of course an unknown quantity, but since the variation in *one* direction amounted to 0.11 foot, the accuracy in other directions was very questionable. This shows that a careful comparative measurement between the wires at top and bottom should always be made as a test of their parallelism.

162. Underground surveys. Survey marks are frequently placed on the timbering, but they are apt to prove unreliable on account of the shifting of the timbering due to settlement of the surrounding material. They should never be placed at the bottom of the tunnel on account of the danger of being disturbed or covered up. Frequently holes are drilled in the roof and filled with wooden plugs in which a hook is screwed exactly on line. Although this is probably the safest method, even these plugs are not always undisturbed, as the material, unless very hard, will often settle slightly as the excavation proceeds. When a tunnel is perfectly straight and not too long, alignment-points may be given as frequently as desired from



permanent stations located outside the tunnel where they are not liable to disturbance. This has been accomplished by running the alignment through the upper part of the cross-section, at one side of the center, where it is out of the way of the piles of masonry material, débris, etc., which are so apt to choke up the lower part of the cross-section. The position of this line relative to the cross-section being fixed, the alignment of any required point of the cross-section is readily found by means of a light frame or template with a fixed tar-

get located where this line would intersect the frame when properly placed. A level-bubble on the frame will assist in setting the frame in its proper position. In all tunnel surveying the cross-wires must be illuminated by a lantern, and the object sighted at must also be illuminated. A powerful dark-lantern with the opening covered with *ground glass* has been found useful. This may be used to illuminate a plumb-bob string or a very fine rod, or to place behind a brass plate having a narrow slit in it, the axis of the slit and plate being coincident with the plumb-bob string by which it is hung.

On account of the interference to the surveying caused by the work of construction and also by the smoke and dust in the air resulting from the blasting, it is generally necessary to make the surveys at times when construction is temporarily suspended.

163. Accuracy of tunnel surveying. Apart from the very natural desire to do surveying which shall check well, there is an important financial side to accurate tunnel surveying. If the survey lines do not meet as desired when the headings come together, it may be found necessary, if the error is of appreciable size, to introduce a slight curve, perhaps even a reversed curve, into the alignment, and it is even conceivable that the tunnel section would need to be enlarged somewhat to allow for these curves. The cost of these changes and the perpetual annovance due to an enforced and undesirable alteration of the original design will justify a considerable increase in the expenses of the survey. Considering that the cost of surveys is usually but a small fraction of the total cost of the work, an increase of 10 or even 20% in the cost of the surveys will mean an insignificant addition to the total cost and frequent's, if not generally, it will result in a saving of many times the increased cost. The accuracy actually attained in two noted American tunnels is given as follows: The Musconetcong tunnel is about 5000 feet long, bored through a mountain 400 feet high. The error of alignment at the meeting of the headings was 0'.04, error of levels 0'.015, error of distance 0'.52. The Hoosac tunnel is over 25000 feet long. The heading from the east end met the heading from the central shaft at a point 11274 feet from the east end and 1563 feet from the shaft. The error in alignment was  $\frac{5}{16}$  of an inch, that of levels "a few hundredths," error of distance "trifling." The alignment, corrected at the shaft, was carried on through and met the heading from the west end at a point 10138 feet from the west end and 2056 feet from

the shaft. Here the error of alignment was  $\frac{9}{16}''$  and that of levels 0.134 ft.

#### DESIGN.

164. Cross-sections. Nearly all tunnels have cross-sections peculiar to themselves-all varying at least in the details. The general form of a great many tunnels is that of a rectangle surmounted by a semi-circle or semi-ellipse. In very soft material an inverted arch is necessary along the bottom. In such cases the sides will generally be arched instead of vertical. The sides are frequently battered. With very long tunnels, several forms of cross-section will often be used in the same tunnel, owing to differences in the material encountered. In solid rock, which will not disintegrate upon exposure, no lining is required, and the cross-section will be the irregular section left by the blasting. the only requirement being that no rock shall be left within the required cross-sectional figure. Farther on, in the same tunnel, when passing through some very soft treacherous material, it may be necessary to put in a full arch lining-top, sides, and bottom-which will be nearly circular in cross-section. For an illustration of this see Figs. 87 and 88.

The width of tunnels varies as greatly as the designs. Singletrack tunnels generally have a width of 15 to 16 feet. Occasionally they have been built 14 feet wide, and even less, and also up to 18 feet, especially when on curves. 24 to 26 feet is the most common width for double track. Many double-track tunnels are only 22 feet wide, and some are 28 feet wide. The heights are generally 19 feet for single track and 20 to 22 feet for double track. The variations from these figures are considerable. The lower limits depend on the cross-section of the rolling stock, with an indefinite allowance for clearance and ventilation. Cross-sections which coincide too closely with what is absolutely required for clearance are objectionable, because any slight settlement of the lining which would otherwise be harmless would then become troublesome and even dangerous. Figs. 87, 88, and 89 \* show some typical cross-sections.

165. Grade. A grade of at least 0.2% is needed for drainage. If the tunnel is at the summit of two grades, the tunnel grade should be practically level, with an allowance for drainage, the

\* Drinker's "Tunneling."

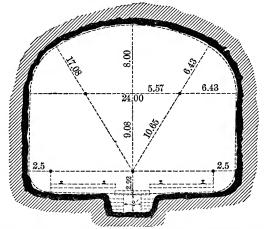


FIG. 87.-HOOSAC TUNNEL. SECTION THROUGH SOLID ROCK.

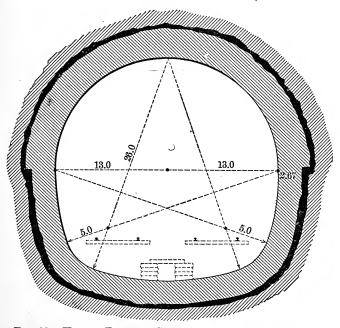


FIG. 88.-HOOSAC TUNNEL. SECTION THROUGH SOFT GROUND.

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actual summit being perhaps in the center so as to drain both ways. When the tunnel forms part of a long ascending grade, it is advisable to reduce the grade through the tunnel unless the tunnel is very short. The additional atmospheric resistance and the decreased adhesion of the driver wheels on the damp rails in a tunnel will cause an engine to work very hard and still more rapidly vitiate the atmosphere until the accumulation of poisonous gases becomes a source of actual danger to the engineer and

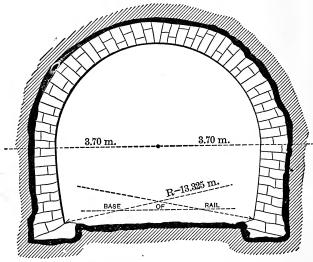


FIG. 89.-ST. CLOUD TUNNEL.

fireman of the locomotive and of extreme discomfort to the passengers. If the nominal ruling grade of the road were maintained through a tunnel, the maximum resistance would be found in the tunner. This would probably cause trains to stall there, which would be objectionable and perhaps dangerous.

166. Lining. It is a characteristic of many kinds of rock and of all earthy material that, although they may be selfsustaining when first exposed to the atmosphere, they rapidly disintegrate and require that the top and perhaps the sides and even the bottom shall be lined to prevent caving in. In this country, when timber is cheap, it is occasionally framed as an arch and used as the *permanent* lining, but masonry is always to be preferred. Frequently the cross-section is made extra

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large so that a masonry lining may subsequently be placed inside the wooden lining and thus postpone a large expense until the road is better able to pay for the work. In very soft unstable material, like quicksand, an arch of cut stone voussoirs may be necessary to withstand the pressure. A good quality of brick is occasionally used for lining, as they are easily handled and make good masonry if the pressure is not excessive. Only the best of cement mortar should be used, economy in this feature being the worst of folly. Of course the excavation must include the outside line of the lining. Any excavation which is made outside of this line (by the fall of earth or loose rock or by excessive blasting) must be refilled with stone well packed in. Occasionally it is necessary to fill these spaces with concrete. Of course it is not necessary that the lining be uniform throughout the tunnel.

167. Shafts. Shafts are variously made with square, rectangular, elliptical, and circular cross-sections. The rectangular

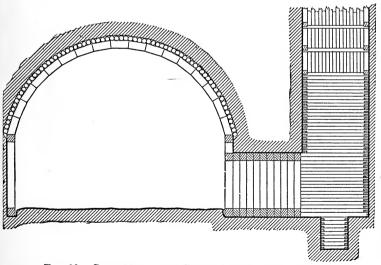


FIG. 90.-CONNECTION WITH SHAFT, CHURCH HILL TUNNEL.

cross-section, with the longer axis parallel with the tunnel, is most usually employed. Generally the shaft is directly over the center of the tunnel, but that always implies a complicated connection between the linings of the tunnel and shaft, provided

### RAILROAD CONSTRUCTION.

such linings are necessary. It is easier to sink a shaft near to one side of the tunnel and make an opening through the nearly vertical side of the tunnel. Such a method was employed in the Church Hill Tunnel, illustrated in Fig. 90.\* Fig. 91 † shows a cross-section for a large main shaft. Many shafts have been built with the idea of being left open permanently for ventilation and have therefore been elaborately lined with masonry.

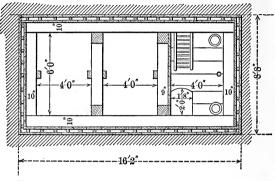


FIG. 91.-CROSS-SECTION. LARGE MAIN SHAFT.

The general consensus of opinion now appears to be that shafts are worse than useless for ventilation; that the quick passage of a train through the tunnel is the most effective ventilator; and that shafts only tend to produce cross-currents and are ineffective to clear the air. In consequence, many of these elaborately lined shafts have been permanently closed, and the more recent practice is to close up a shaft as soon as the tunnel is completed. Shafts always form drainage-wells for the material they pass through, and sometimes to such an extent that it is a serious matter to dispose of the water that collects at the bottom, requiring the construction of large and expensive drains.

168. Drains. A tunnel will almost invariably strike veins of water which will promptly begin to drain into the tunnel and not only cause considerable trouble and expense during construction, but necessitate the provision of permanent drains for its perpetual disposal. These drains must frequently be so large as

<sup>\*</sup> Drinker's "Tunneling."

<sup>†</sup> Rziha, "Lehrbuch der Gesammten Tunnelbaukunst."

to appreciably increase the required cross-section of the tunnel. Generally a small open gutter on each side will suffice for this purpose, but in double-track tunnels a large covered drain is often built between the tracks. It is sometimes necessary to thoroughly grout the outside of the lining so that water will not force its way through the masonry and perhaps injure it, but may freely drain down the sides and pass through openings in the side walls near their base into the gutters.

#### CONSTRUCTION.

169. Headings. The methods of all tunnel excavation depend on the general principle that all earthy material, except the softest of liquid mud and quicksand, will be self-sustaining over a greater or less area and for a greater or less time after excavation is made, and the work consists in excavating some material and immediately propping up the exposed surface by timbering and poling-boards. The excavation of the crosssection begins with cutting out a "heading," which is a small horizontal drift whose breast is constantly kept 15 feet or more in advance of the full cross-sectional excavation. In solid self-sustaining rock, which will not decompose upon exposure to air, it becomes simply a matter of excavating the rock with the least possible expenditure of time and energy. In soft ground the heading must be heavily timbered, and as the heading is gradually enlarged the timbering must be gradually extended and perhaps replaced, according to some regular system, so that

when the full cross-section has been excavated it is supported by such timbering as is intended for it. The heading is sometimes made on the center line near the top; with other plans, on the center line near the bottom; and sometimes two simultaneous headings are run in the two lower corners. Headings near the bottom serve the purpose of draining the material above it and facilitating the excavation. The simplest case of heading timbering is that shown in Fig. 92, in which cross-timbers are placed at intervals just under the roof, set in notches

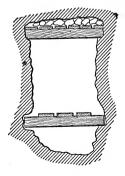
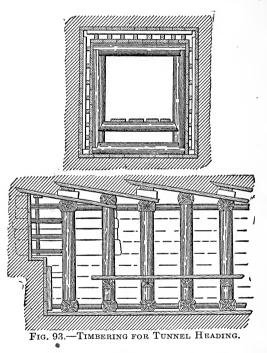


FIG. 92.

cut in the side walls and supporting poling-boards which sus-

tain whatever pressure may come on them. Cross-timbers near the bottom support a flooring on which vehicles for transporting material may be run and under which the drainage may freely escape. As the necessity for timbering becomes greater, side timbers and even bottom timbers must be added, these timbers supporting poling-boards, and even the breast of the heading must be protected by boards suitably braced.



as shown in Fig. 93. The supporting timbers are framed into collars in such a manner that added pressure only increases their rigidity.

170. Enlargement. Enlargement is accomplished by removing the poling-boards, one at a time, excavating a greater or less amount of material, and immediately supporting the exposed material with poling-boards suitably braced. (See Figs. 93 and 94.) This work being systematically done, space is thereby obtained in which the framing for the full cross-section may be gradually introduced. The framing is constructed with a crosssection so large that the masonry lining may be constructed within it.

171. Distinctive features of various methods of construction. There are six general systems, known as the English, German, Belgian, French, Austrian, and American. They are so named

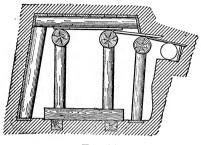
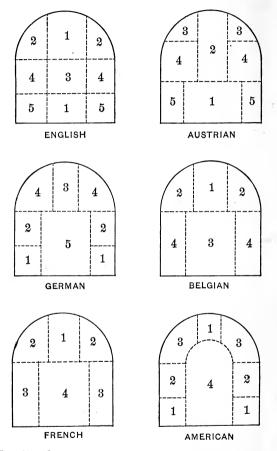


FIG. 94.

from the origin of the methods, although their use is not confined to the countries named. Fig. 95 shows by numbers (1 to 5) the order of the excavation within the cross-sections. The English, Austrian, and American systems are alike in excavating the entire cross-section before beginning the construction of the masonry lining. The German method leaves a solid core (5) until practically the whole of the lining is complete. This has the disadvantage of extremely cramped quarters for work, poor ventilation, etc. The Belgian and French methods agree in excavating the upper part of the section, building the arch at once, and supporting it temporarily until the side walls are built. The Belgian method then takes out the core (3), removes very short sections of the sides (4) immediately underpinning the arch with short sections of the side walls and thus gradually constructing the whole side wall. The French method digs out the sides (3), supporting the arch temporarily with timbers and then replacing the timbers with masonry; the core (4) is taken out last. The French method has the same disadvantage as the German-working in a cramped space. The Belgian and French systems have the disadvantage that the arch, supported temporarily on timber, is very apt to be strained and cracked by the slight settlement that so frequently occurs in soft material. The English, Austrian, and American methods differ mainly in the

design of the timbering. The English support the roof by lines of very heavy *longitudinal* timbers which are supported at comparatively wide intervals by a heavy framework occupying the





whole cross-section. The Austrian system uses such frequent cross-frames of timber-work that poling-boards will suffice to support the material between the frames. The American system agrees with the Austrian in using frequent cross-frames supporting poling-boards, but differs from it in that the "crossframes" consist simply of arches of 3 to 15 wooden voussoirs, the voussoirs being blocks of  $12'' \times 12''$  timber about 2 to 8 feet long and cut with joints normal to the arch. These arches are put together on a centering which is removed as soon as the arch is keyed up and thus immediately opens up the full cross-section, so that the center core (4) may be immediately dug out and the masonry constructed in a large open space. The American system has been used successfully in very soft ground, but its advantages are greater in loose rock, when it is much cheaper than the other methods which employ more timber. Fig. 90 and Plate III, illustrate the use of the American system. Fig. 90 shows the wooden arch in place. The masonry arch may be placed when convenient, since it is possible to lay the track and commence traffic as soon as the wooden arch is in place. The student is referred to Drinker's "Tunneling" and to Rziha's "Lehrbuch der Gesammten Tunnelbaukunst" for numerous illustrations of European methods of tunnel timbering.

172. Ventilation during construction. Tunnels of any great length must be artificially ventilated during construction. Tf the excavated material is rock so that blasting is necessary, the need for ventilation becomes still more imperative. The invention of compressed-air drills simultaneously solved two difficul-It introduced a motive power which is unobjectionable in ties. its application (as gas would be), and it also furnished at the same time a supply of just what is needed-pure air. If no blasting is done (and frequently even when there is blasting), air must be supplied by direct pumping. The cooling effect of the sudden expansion of compressed air only reduces the otherwise objectionably high temperature sometimes found in tunnels. Since pure air is being continually pumped in, the foul air is thereby forced out.

173. Excavation for the portals. Under normal conditions there is always a greater or less amount of open cut preceding and following a tunnel. Since all tunnel methods depend (to some slight degree at least) on the capacity of the exposed material to act as an arch, there is implied a considerable thickness of material above the tunnel. This thickness is reduced to nearly zero over the tunnel portals and therefore requires special treatment, particularly when the material is very soft. Fig. 96 \*

<sup>\*</sup> Rziha, "Lehrbuch der Gesammten Tunnelbaukunst."

illustrates one method of breaking into the ground at a portal. The loose stones are piled on the framing to give stability to the framing by their weight and also to retain the earth on the

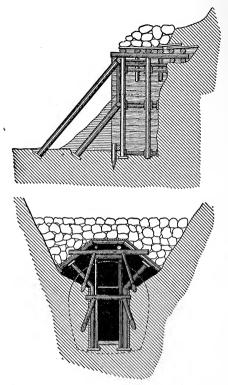
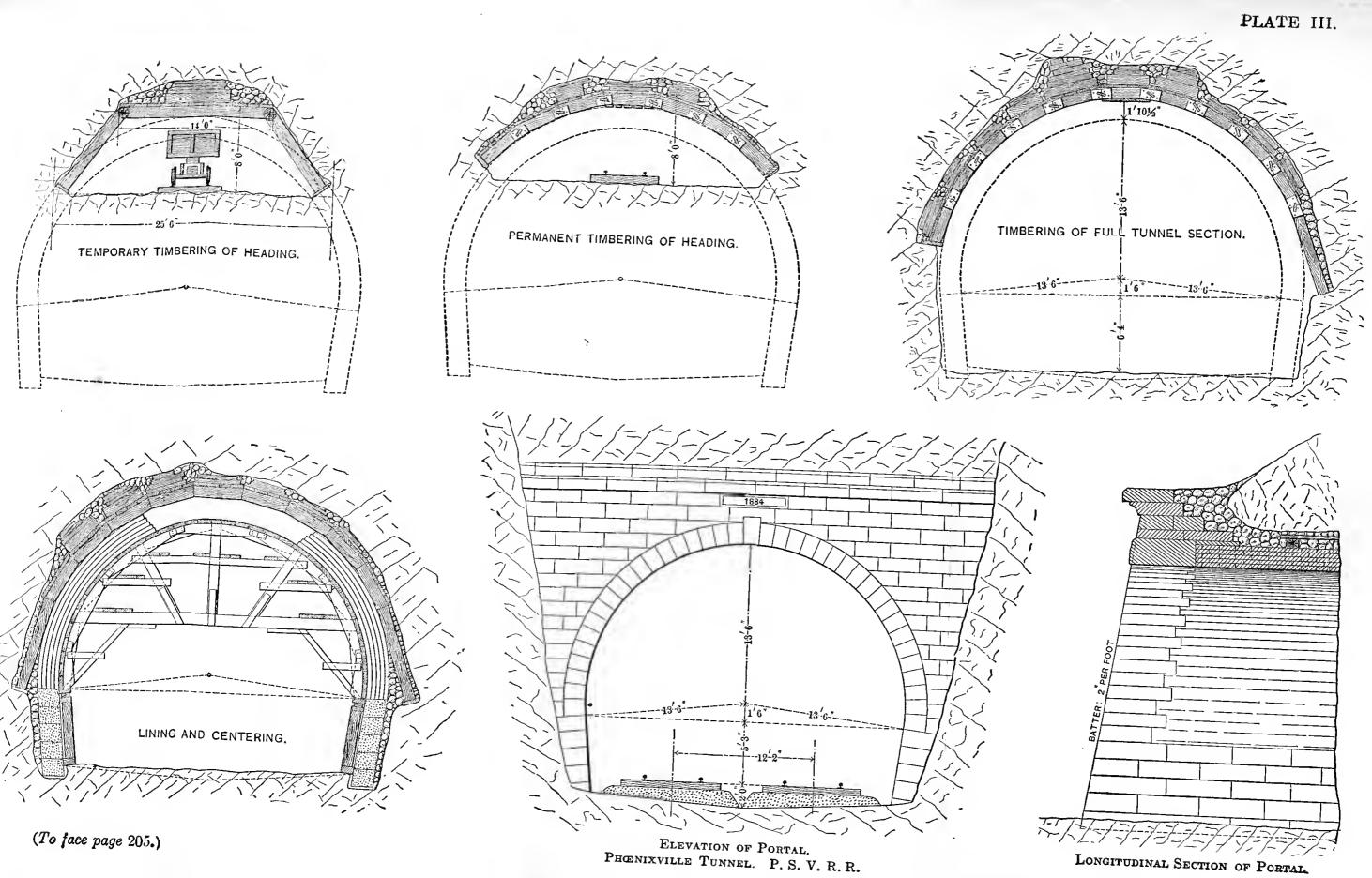
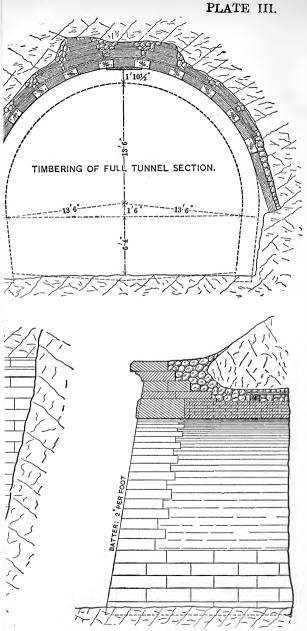


FIG. 96.-TIMBERING FOR TUNNEL PORTAL.

slope above. Another method is to sink a temporary shaft to the tunnel near the portal; immediately enlarge to the full size and build the masonry lining; then work back to the portal. This method is more costly, but is preferable in very treacherous ground, it being less liable to cause landslides of the surface material.

174. Tunnels vs. open cuts. In cases in which an open cut rather than a tunnel is a possibility the ultimate consideration is generally that of first cost combined with other financial con-





LONGITUDINAL SECTION OF PORTAL.

§ 175.

siderations and annual maintenance charges directly or indirectly connected with it. Even when an open cut may be constructed at the same cost as a tunnel (or perhaps a little cheaper) the tunnel may be preferable under the following conditions:

1. When the soil indicates that the open cut would be liable to landslides.

2. When the open cut would be subject to excessive snowdrifts or avalanches.

3. When land is especially costly or it is desired to run under existing costly or valuable buildings or monuments. When running through cities, tunnels are sometimes constructed as open cuts and then arched over.

These cases apply to tunnels vs. open cuts when the alignment is fixed by other considerations than the mere topography. The broader question of excavating tunnels to avoid excessive grades or to save distance or curvature, and similar problems, are hardly susceptible of general analysis except as questions of railway economics and must be treated individually.

175. Cost of tunneling. The cost of any construction which involves such uncertainties as tunneling is very variable. It depends on the material encountered, the amount and kind of timbering required, on the size of the cross-section, on the price of labor, and especially on the *reconstruction* that *may* be necessary on account of mishaps.

• Headings generally cost \$4 to \$5 per cubic yard for excavation, while the remainder of the cross-section in the same tunnel may cost about half as much. The average cost of a large number of tunnels in this country may be seen from the following table:\*

Materia.	Cost per cubic yard.				Cost p <b>er</b> lineal foot.	
	Excavation.		Masonry.			
	Single.	Double.	Single.	Double.	Single.	Double.
Hard rock Loose rock Soft ground	\$5.89 3.12 3.62		$\$12.00 \\ 9.07 \\ 15.00$			\$142.82 119.20 174.42

\* Figures derived from Drinker's "Tunneling."

A considerable variation from these figures may be found in individual cases, due sometimes to unusual skill (or the lack of it) in prosecuting the work, but the figures will generally be sufficiently accurate for preliminary estimates or for the comparison of two proposed routes.

## CHAPTER VI.

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## CULVERTS AND MINOR BRIDGES.

176. Definition and object. Although a variable percentage of the rain falling on any section of country soaks into the ground and does not immediately reappear, yet a very large percentage flows over the surface, always seeking and following the lowest channels. The roadbed of a railroad is constantly intersecting these channels, which frequently are normally dry. In order to prevent injury to railroad embankments by the impounding of such rainfall, it is necessary to construct waterways through the embankment through which such rainflow may freely pass. Such waterways, called culverts, are also applicable for the bridging of very small although perennial streams. and therefore in this work the term culvert will be applied to all water-channels passing through a railroad embankment which are not of sufficient magnitude to require a special structural design, such as is necessary for a large masonry arch or a truss bridge.

177. Elements of the design. A well-designed culvert must afford such free passage to the water that it will not "back up" over the adjoining land nor cause any injury to the embankment or culvert. The ability of the culvert to discharge freely all the water that comes to it evidently depends chiefly on the area of the waterway, but also on the form, length, slope, and materials of construction of the culvert and the nature of the approach When the embankment is very low and the amount and outfall. of water to be discharged very great, it sometimes becomes necessary to allow the water to discharge "under a head," i.e., with the surface of the water above the top of the culvert. Safety then requires a much stronger construction than would otherwise be necessary to avoid injury to the culvert or embankment by washing. The necessity for such construction should be avoided if possible.

#### AREA OF THE WATERWAY.

178. Elements involved. The determination of the required area of the waterway involves such a multiplicity of indeterminate elements that any close determination of its value from purely theoretical considerations is a practical impossibility. The principal elements involved are:

a. Rainfall. The real test of the culvert is its capacity to discharge without injury the flow resulting from the extraordinary rainfalls and "cloud bursts" that may occur once in many years. Therefore, while a knowledge of the average annual rainfall is of very little value, a record of the maximum rainfall during heavy storms for a long term of years may give a relative idea of the maximum demand on the culvert.

**b.** Area of watershed. This signifies the total area of country draining into the channel considered. When the drainage area is very small it is sometimes included within the area surveyed by the preliminary survey. When larger it is frequently possible to obtain its area from other maps with a percentage of accuracy sufficient for the purpose. Sometimes a special survey for the purpose is considered justifiable.

c. Character of soil and vegetation. This has a large influence on the rapidity with which the rainflow from a given area will reach the culvert. If the soil is hard and impermeable and the vegetation scant, a heavy rain will run off suddenly, taxing the capacity of the culvert for a short time, while a spongy soil and dense vegetation will retard the flow, making it more nearly uniform and the maximum flow at any one time much less.

d. Shape and slope of watershed. If the watershed is very long and narrow (other things being equal), the water from the remoter parts will require so much longer time to reach the culvert that the flow will be comparatively uniform, especially when the slope of the whole watershed is very low. When the slope of the remoter portions is quite steep it may result in the nearly simultaneous arrival of a storm-flow from all parts of the watershed, thus taxing the capacity of the culvert.

e. Effect of design of culvert. The principles of hydraulics show that the slope of the culvert, its length, the form of the cross-section, the nature of the surface, and the form of the approach and discharge all have a considerable influence on the area of cross-section required to discharge a given volume of water in a given time, but unfortunately the combined hydraulic effect of these various details is still a very uncertain quantity.

179. Methods of computation of area. There are three possible methods of computation.

(a) Theoretical. As shown above it is a practical impossibility to estimate correctly the combined effect of the great multiplicity of elements which influence the final result. The nearest approach to it is to estimate by the use of empirical formulæ the amount of water which will be presented at the upper end of the culvert in a given time and then to compute, from the principles of hydraulics, the rate of flow through a culvert of given construction, but (as shown in § 178, e) such methods are still very unreliable, owing to lack of experimental knowledge. This method has apparently greater scientific accuracy than other methods, but a little study will show that the elements of uncertainty are as great and the final result no more reliable. The method is most reliable for streams of uniform flow, but it is under these conditions that method (c) is most useful. The theoretical method will not therefore be considered further.

(b) Empirical. As illustrated in § 180, some formulæ make the area of waterway a function of the drainage area, the formula being affected by a coefficient the value of which is estimated between limits according to the judgment. Assuming that the formulæ are sound, their use only narrows the limits of error, the final determination depending on experience and judgment.

(c) From observation. This method, considered by far the best for permanent work, consists in observing the high-water marks on contracted channel-openings which are on the same stream and as near as possible to the proposed culvert. If the country is new and there are no such openings, the wisest plan is to bridge the opening by a temporary structure in wood which has an ample waterway (see § 126, b, 4) and carefully observe all high-water marks on that opening during the 6 to 10 years which is ordinarily the minimum life of such a structure. As shown later, such observations may be utilized for a close computation of the required waterway. Method (b) may be utilized for an approximate calculation for the required area for the tem-

porary structure, using a value which is intentionally excessive, so that a permanent structure of sufficient capacity may subsequently be constructed *within* the temporary structure.

180. Empirical formulæ. Two of the best known empirical formulæ for area of the waterway are the following:

# (a) Myer's formula:

Area of waterway in square feet  $=C \times \sqrt{\text{drainage area in acres}}$ , where C is a coefficient varying from 1 for flat country to 4 for mountainous country and rocky ground. As an illustration, if the drainage area is 100 acres, the waterway area should be from 10 to 40 square feet, according to the value of the coefficient chosen. It should be noted that this formula does not regard the great variations in rainfall in various parts of the world nor the design of the culvert, and also that the final result depends largely on the choice of the coefficient.

# (b) Talbot's formula:

Area of waterway in square feet =  $C \times \sqrt[4]{(\text{drainage area in acres})^3}$ . "For steep and rocky ground C varies from  $\frac{2}{3}$  to 1. For rolling agricultural country subject to floods at times of melting snow. and with the length of the valley three or four times its width, Cis about 1: and if the stream is longer in proportion to the area. decrease C. In districts not affected by accumulated snow, and where the length of the valley is several times the width,  $\frac{1}{5}$  or  $\frac{1}{5}$ . or even less, may be used. C should be increased for steep side slopes, especially if the upper part of the valley has a much greater fall than the channel at the culvert." \* As an illustration, if the drainage area is 100 acres the area of waterway should be  $C \times 31.6$ . The area should then vary from 5 to 31 square feet, according to the character of the country. Like the previous estimate, the result depends on the choice of a coefficient and disregards local variations in rainfall, except as they may be arbitrarily allowed for in choosing the coefficient.

181. Value of empirical formulæ. The fact that these formulæ, as well as many others of similar nature that have been suggested, depend so largely upon the choice of the coefficient shows that they are valuable "more as a guide to the judgment than as a working rule," as Prof. Talbot explicitly declares in

<sup>\*</sup> Prof. A. N. Talbot, "Selected Papers of the Civil Engineers' Club of the Univ. of Illinois,"

commenting on his own formula. In short, they are chiefly valuable in indicating a probable maximum and minimum between which the true result probably lies.

182. Results based on Observation. As already indicated in § 179, observation of the stream in question gives the most reliable results. If the country is new and no records of the flow of the stream during heavy storms has been taken, even the life of a temporary wooden structure may not be long enough to include one of the unusually severe storms which must be allowed for, but there will usually be some high-water mark which will indicate how much opening will be required. The following quotation illustrates this: "A tidal estuary may generally be safely narrowed considerably from the extreme water lines if stone revetments are used to protect the bank from Above the true estuary, where the stream cuts through wash. the marsh, we generally find nearly vertical banks, and we are safe if the faces of abutments are placed even with the banks. In level sections of the country, where the current is sluggish, it is usually safe to encroach somewhat on the general width of the stream, but in rapid streams among the hills the width that the stream has cut for itself through the soil should not be lessened, and in ravines carrying mountain torrents the openings must be left very much larger than the ordinary appearance of the banks of the stream would seem to make necessarv." \*

As an illustration of an observation of a storm-flow through a temporary trestle, the following is quoted: "Having the flood height and velocity, it is an easy matter to determine the volume of water to be taken care of. I have one ten-bent pile trestle 135 feet long and 24 feet high over a spring branch that ordinarily runs about six cubic inches per second. Last summer during one of our heavy rainstorms (four inches in less than three hours) I visited this place and found by float observations the surface velocity at the highest stage to be 1.9 feet per second. I made a high-water mark, and after the floodwater receded found the width of stream to be 12 feet and an average depth of  $2\frac{3}{4}$  feet. This, with a surface velocity of 1.9 feet per second, would give approximately a discharge of 50

<sup>\*</sup> J. P. Snow, Boston & Maine Railway. From Report to Association of Railway Superintendents of Bridges and Buildings. 1897.

cubic feet, or 375 gallons, per second. Having this information it is easy to determine size of opening required." \*

183. Degree of accuracy required. The advantages resulting from the use of standard designs for culverts (as well as other structures) have led to the adoption of a comparatively small number of designs. The practical use made of a computation of required waterway area is to determine which one of several standard designs will most nearly fulfill the requirements. For example, if a 24-inch iron pipe, having an area of 3.14 square feet, is considered to be a little small, the next size (30-inch) would be adopted; but a 30-inch pipe has an area of 4.92 square feet, which is 56% larger. A similar result, except that the percentage of difference might not be quite so marked, will be found by comparing the areas of consecutive standard designs for stone box culverts.

The advisability of designing a culvert to withstand any storm-flow that may *ever* occur is considered doubtful. Several years ago a record-breaking storm in New England carried away a very large number of bridges, etc., hitherto supposed to be safe. It was not afterward considered that the design of those bridges was faulty, because the extra cost of constructing bridges capable of withstanding such a flood, added to interest for a long period of years, would be enormously greater than the cost of repairing the damages of such a storm once or twice in a century. Of course the element of danger has some weight, but not enough to justify a great additional expenditure, for common prudence would prompt unusual precautions during or immediately after such an extraordinary storm.

#### PIPE CULVERTS.

184. Advantages. Pipe culverts, made of cast iron or earthenware, are very durable, readily constructed, moderately cheap, will pass a larger volume of water in proportion to the area than many other designs on account of the smoothness of the surface, and (when using iron pipe) may be used very close to the track when a low opening of large capacity is required. Another advantage lies in the ease with which they may be inserted through a somewhat larger opening that has been

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<sup>\*</sup> A. J. Kelley, Kansas City Belt Railway. From Report to Association of Railway Superintendents of Bridges and Buildings. 1897.

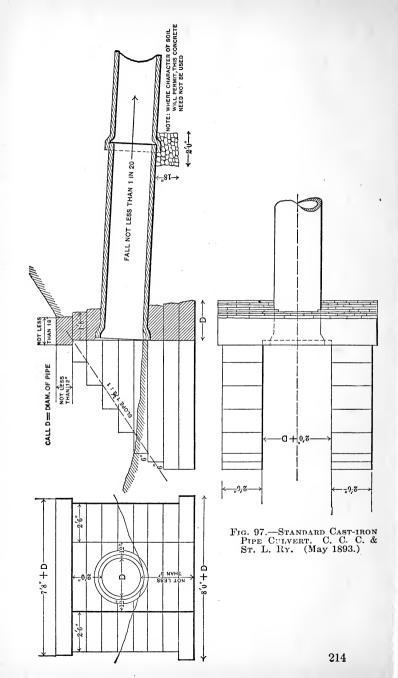
temporarily lined with wood, without disturbing the roadbed or track.

185. Construction. Permanency requires that the foundation shall be firm and secure against being washed out. To accomplish this, the soil of the trench should be hollowed out to fit the lower half of the pipe, making suitable recesses for the bells. In very soft treacherous soil a foundation-block of concrete is sometimes placed under each joint, or even throughout the whole length. When pipes are laid through a slightly larger timber culvert great care should be taken that the pipes are properly supported, so that there will be no settling nor development of unusual strains when the timber finally decays and gives way. To prevent the washing away of material around the pipe the ends should be protected by a bulkhead. This is best constructed of masonry (see Fig. 97), although wood is sometimes used for cheap and minor constructions. The joints should be calked, especially when the culvert is liable to run full or when the outflow is impeded and the culvert is liable to be partly or wholly filled during freezing weather. The cost of a calking of clay or even hydraulic cement is insignificant compared with the value of the additional safety afforded. When the grade of the pipe is perfectly uniform, a very low rate of grade will suffice to drain a pipe culvert, but since some unevenness of grade is inevitable through uneven settlement or imperfect construction, a grade of 1 in 20 should preferably be required, although much less is often used. The length of a pipe culvert is approximately determined as follows:

Length = 2s (depth of embankment) + (width of roadbed),

in which s is the slope ratio (horizontal to vertical) of the banks. In practice an even number of lengths should be used which will equal or exceed the length given by this formula.

186. Iron-pipe culverts. Simple cast-iron pipes are used in sizes from 12" to 48" diameter. These are usually made in lengths of 12 feet with a few lengths of 6 feet, so that any required length may be more nearly obtained. The lightest pipes made are sufficiently strong for the purpose, and even those which would be rejected because of incapacity to withstand considerable internal pressure may be utilized for this work. In Fig. 97 are shown the standard plans used on the C. C. C. & St. L. Ry., which may be considered as typical plans.



Pipes formed of cast-iron segments have been used up to 12 feet diameter. The shell is then made comparatively thin, but is stiffened by ribs and flanges on the outside. The segments break joints and are bolted together through the flanges. The joints are made tight by the use of a tarred rope, together with neat cement.

187. Tile-pipe culverts. The pipes used for this purpose vary from 12" to 24" in diameter. When a larger capacity is required two or more pipes may be laid side by side, but in such a case another design might be preferable. It is frequently specified that "double-strength" or "extra-heavy" pipe shall be used, evidently with the idea that the stresses on a culvertpipe are greater than on a sewer-pipe. But it has been conclusively demonstrated that, no matter how deep the embankment, the pressure cannot exceed a somewhat uncertain maximum, also that the greatest danger consists in placing the pipe so near the ties that shocks may be directly transferred to the pipe without the cushioning effect of the earth and ballast. When the pipes are well bedded in *clear* earth and there is a

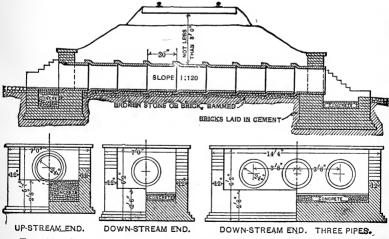


FIG. 98.—STANDARD VITRIFIED-PIPE CULVERT. PLANT SYSTEM. (1891.)

sufficient depth of earth over them to avoid direct impact (at least three feet) the ordinary sewer-pipe will be sufficiently strong. "Double-strength" pipe is frequently less perfectly burned, and the supposed extra strength is not therefore obtained. In Fig. 98 are shown the standard plans for vitrifiedpipe culverts as used on the "Plant system." Tile pipe is much cheaper than iron pipe, but is made in much shorter lengths and requires much more work in laying and especially to obtain a uniform grade.

### BOX CULVERTS.

**188.** Wooden box culverts. This form serves the purpose of a cheap temporary construction which allows the use of a ballasted roadbed. As in all temporary constructions, the area should be made considerably larger than the calculated area \$ (179-182), not only for safety but also in order that, if the smaller area is demonstrated to be sufficiently large, the permanent construction (probably pipe) may be placed inside without disturbing the embankment. All designs agree in using heavy timbers (12"×12", 10"×12", or 8"×12") for the side walls, cross-timbers for the roof, every fifth or sixth timber being notched down so as to take up the thrust of the side walls, and planks for the flooring. Fig. 99 shows some of the standard designs as used by the C., M & St. P. Ry.

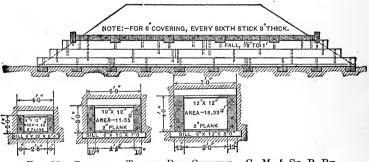


FIG. 99.—STANDARD TIMBER BOX CULVERT. C., M. & ST. P. Ry. (Feb. 1889.)

189. Stone box culverts. In localities where a good quality of stone is cheap, stone box culverts are the cheapest form of permanent construction for culverts of medium capacity, but their use is decreasing owing to the frequent difficulty in obtaining really suitable stone within a reasonable distance of the culvert. The clear span of the cover-stones varies from 2 to 4 feet. The required thickness of the cover-stones is sometimes calculated by the theory of transverse strains on the basis of certain assumptions of loading—as a function of the height of the embankment and the unit strength of the stone used. Such a method is simply another illustration of a class of calculations which look very precise and beautiful, but which are worse than useless (because misleading) on account of the hopeless uncer-

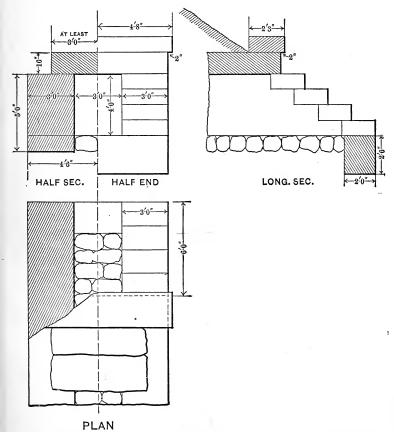


FIG. 100.—STANDARD SINGLE STONE CULVERT (3'×4'). N. & W. R.R. (1890.)

tainty as to the true value of certain quantities which must be used in the computations In the first place the true value of the unit tensile strength of stone is such an uncertain and variable quantity that calculations based on any assumed value for it are of small reliability. In the second place the weight of the prism of earth lying directly above the stone, plus an allowance for live load, is by no means a measure of the load on the stone nor of the forces that tend to fracture it. All earthwork will tend to

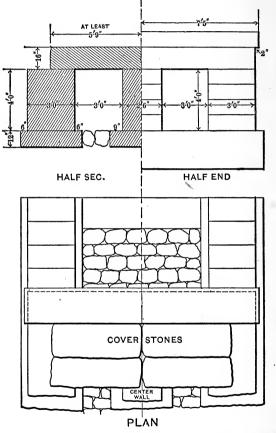


FIG. 100a.—Standard Double Stone Culvert  $(3' \times 4')$ . N. & W. R. R. (1890.)

form an arch above any cavity and thus relieve an uncertain and probably variable proportion of the pressure that might otherwise exist. The higher the embankment the *less* the *pro*- portionate loading, until at some uncertain height an increase in height will not increase the load on the cover-stones. The effect of frost is likewise large, but uncertain and not computable. The usual practice is therefore to make the thickness such as experience has shown to be safe with a good quality of stone, i.e., about 10 or 12 inches for 2 feet span and up to 16 or 18 inches for 4 feet span. The side walls should be carried down deep enough to prevent their being undermined by scour or heaved by frost. The use of cement mortar is also an important feature of first-class work, especially when there is a rapid scouring current or a liability that the culvert will run under a head. In Figs. 100 and 100a are shown standard plans for single and double stone box culverts as used on the Norfolk and Western R. R.

190. Old-rail culverts. It sometimes happens (although very rarely) that it is necessary to bring the grade line within 3 or 4 feet of the bottom of a stream and yet allow an area of 10 or 12 square feet. A single large pipe of sufficient area could not be used in this case. The use of several smaller pipes side by side would be both expensive and inefficient. For similar reasons neither wooden nor stone box culverts could be used. In such cases, as well as in many others where the head-room is not so limited, the plan illustrated in Fig. 101 is a very satisfactory

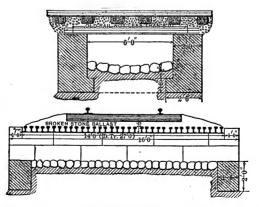


FIG. 101.-STANDARD OLD-RAIL CULVERT. N. & W. R.R. (1895.)

solution of the problem. The old rails, having a length of 8 or 9 feet, are laid close together across a 6-foot opening. Sometimes the rails are held together by long bolts passing through the webs of the rails. In the plan shown the rails are confined by low end walls on each abutment. This plan requires only 15 inches between the base of the rail and the top of the culvert channel. It also gives a continuous ballasted roadbed.

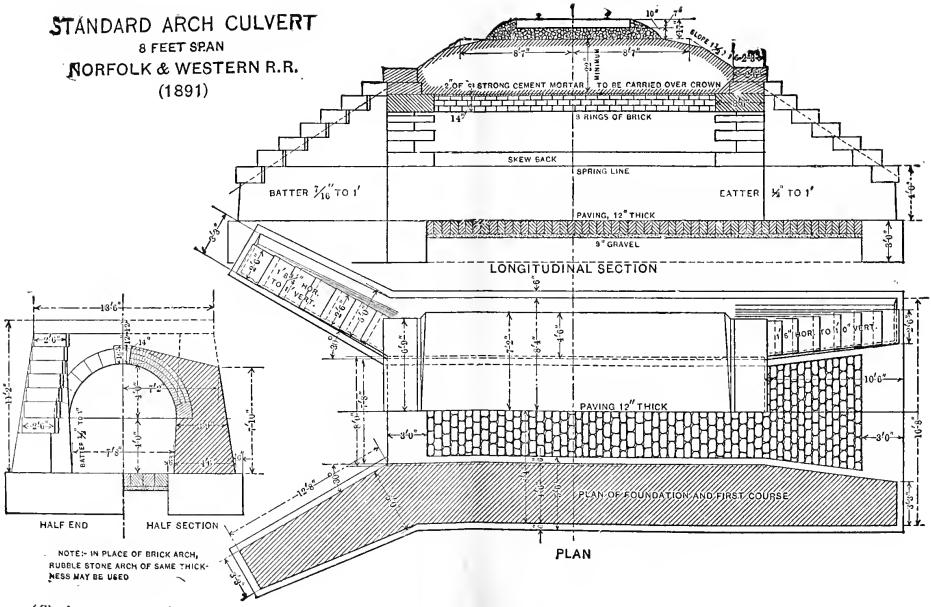
190a. Reinforced Concrete Culverts. The development of reinforced concrete as a structural material is illustrated in its extensive adoption for arches and also for culverts. One of the special types which has been adopted is that of a box culvert which has a concrete bottom. Since this bottom can be made so that it will withstand an upward transverse stress, it furnishes a broad foundation for the whole culvert, and thus entirely eliminates the necessity for extensive footing to the side walls of the culvert, such as are necessary in soft ground with an ordinary Another advantage is that the inside of the culstone culvert. vert may be made perfectly smooth and thus offer less resistance to the passage of water through it. As may be noticed from Fig. 101a, such a culvert is provided with flaring head walls, and sunken end walls, so that the water may not scour underneath the culvert, and other features common to other types. No attempt will here be made to discuss the design of reinforced concrete, except to say that all four sides of such a box culvert are designed to withstand a computed bursting pressure which tends to crush the flat sides inward. In Fig. 101a is shown one illustration of the many types of culverts which have been designed of reinforced concrete.

#### ARCH CULVERTS.

191. Influence of design on flow. The variations in the design of arch culverts have a very marked influence on the cost and efficiency. To combine the least cost with the greatest efficiency, due weight should be given to the following elements: (a) amount of masonry. (b) the simplicity of the constructive work, (c) the design of the wing walls, (d) the design of the junction of the wing walls with the barrel and faces of the arch, and (e) the safety and permanency of the construction. These elements are more or less antagonistic to each other, and the defects of most designs are due to a lack of proper proportion in the design of these opposing interests. The simplest construction (satisfying elements b and e) is the straight barrel arch

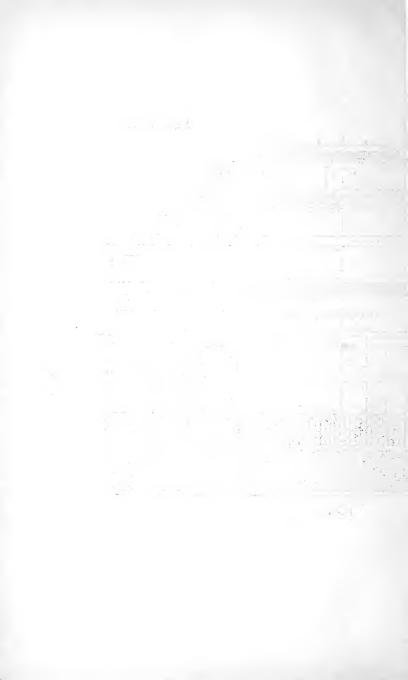


PLATE IV

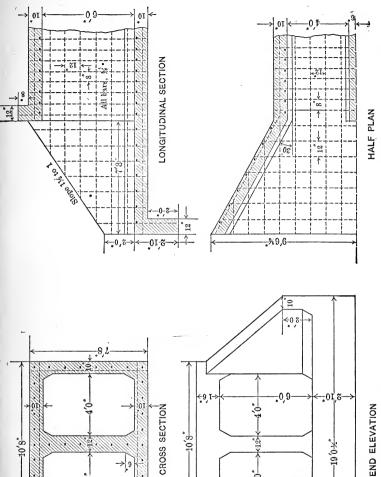


(To face page 221.)





<u>e</u> ↑



ELEVATION Fig. 101a.—Reinforced Concrete Box Culvert. between two parallel vertical head walls, as sketched in Fig. 102, a. From a hydraulic standpoint the design is poor, as the water eddies around the corners, causing a great resistance which decreases the flow. Fig. 102, b, shows a much better de-

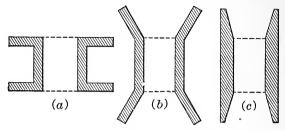


FIG. 102.—Types of Culverts.

sign in many respects, but much depends on the details of the design as indicated in elements (b) and (d). As a general thing a good hydraulic design requires complicated and expensive masonry construction, i.e., elements (b) and (d) are opposed. Design 102, c, is sometimes inapplicable because the water is liable to work in behind the masonry during floods and perhaps cause scour. This design uses less masonry than (a) or (b).

192. Example of arch culvert design. In Plate IV is shown the design for an 8-foot arch culvert according to the standard of the Norfolk and Western R. R. Note that the plan uses the flaring wing walls (Fig. 102, b) on the up-stream side (thus protecting the abutments from scour) and straight wing walls (similar to Fig. 102, c) on the down-stream end. This economizes masonry and also simplifies the constructive work. Note also the simplicity of the junction of the wing walls with the barrel of the arch, there being no re-entrant angles below the springing line of the arch. The design here shown is but one of a set of designs for arches varying in span from 6' to 30'.

### MINOR OPENINGS.

193. Cattle-guards. (a) Pit guards. Cattle-guards will be considered under the head of minor openings, since the oldfashioned plan of pit guards, which are even now defended and preferred by some railroad men, requires a break in the continuity of the roadbed. A pit about three feet deep, five feet

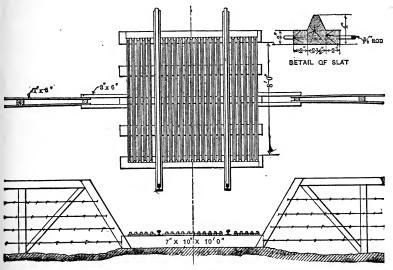


FIG. 103 .- CATTLE-GUARD WITH WOODEN SLATS.

long, and as wide as the width of the roadbed, is walled up with stone (sometimes with wood), and the rails are supported on heavy timbers laid longitudinally with the rails. The break in the continuity of the roadbed produces a disturbance in the elastic wave running through the rails, the effect of which is noticeable at high velocities. The greatest objection, however, lies in the dangerous consequences of a derailment or a failure of the timbers owing to unobserved decay or destruction by fire—caused perhaps by sparks and cinders from passing locomotives. The very insignificance of the structure often leads to careless inspection. But if a single pair of wheels gets off the rails and drops into the pit, a costly wreck is inevitable.

(b) Surface cattle-guards. These are fastened on top of the ties; the continuity of the roadbed is absolutely unbroken and thus is avoided much of the danger of a bad wreck owing to a possible derailment. The device consists essentially of overlaying the ties (both inside and outside the rails) with a surface on

which cattle will not walk. The multitudinous designs for such a surface are variously effective in this respect. An objection,

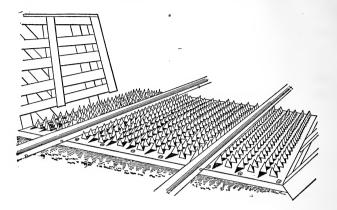


FIG. 104.-SHEFFIELD CATTLE-GUARD.

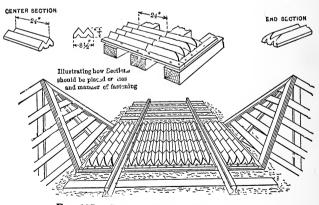


FIG. 105.-CLIMAX CATTLE-GUARD (TILE).

which is often urged indiscriminately against all such designs, is the liability that a brake-chain which may happen to be dragging *may* catch in the rough bars which are used. The bars are sometimes "home-made," of wood, as shown in Fig. 103. Steel guards may be made as shown in Fig. 104. The general construction is the same as for the wooden bars. The metal bars have far greater durability, and it is claimed that they are more effective in discouraging cattle from attempting to cross.

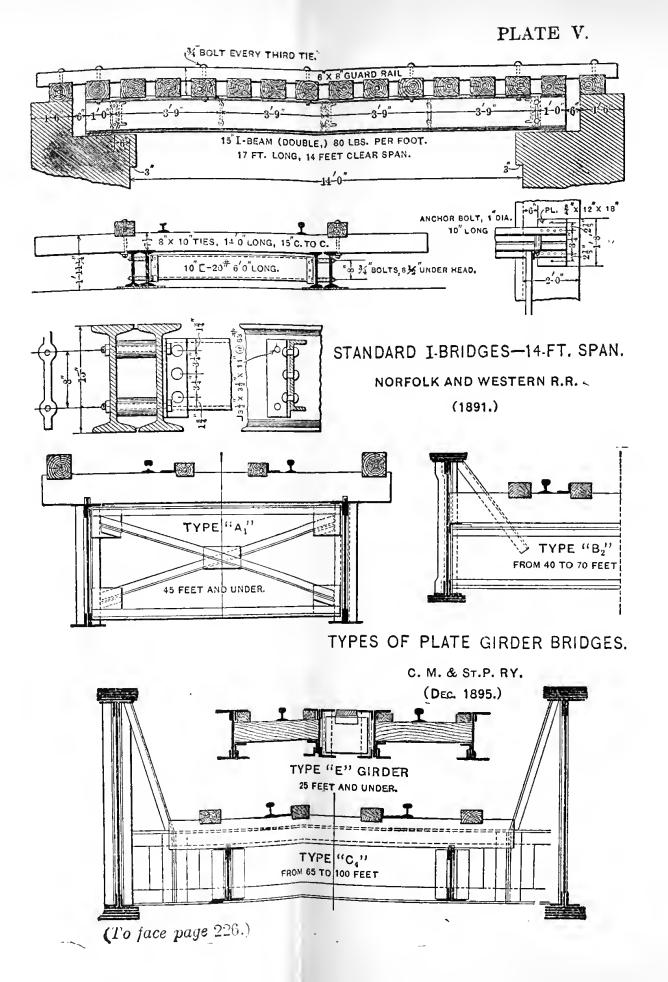
104. Cattle-passes. Frequently when a railroad crosses a farm on an embankment, cutting the farm into two parts, the railroad company is obliged to agree to make a passageway through the embankment sufficient for the passage of cattle and perhaps even farm-wagons. If the embankment is high enough so that a stone arch is practicable, the initial cost is the only great objection to such a construction; but if an open wooden structure is necessary, all the objections against the old-fashioned cattle-guards apply with equal force here. The avoidance of a grade crossing which would otherwise be necessary is one of the great compensations for the expense of the construction and maintenance of these structures. The construction is sometimes made by placing two pile trestle bents about 6 to 8 feet apart, supporting the rails by stringers in the usual way, the special feature of this construction being that the embankments are filled in behind the trestle bents, and the thrust of the embankments is mutually taken up through the stringers, which are notched at the ends or otherwise constructed so that they may take up such a thrust. The designs for old-rail culverts and arch culverts are also utilized for cattle-passes when suitable and convenient, as well as the designs illustrated in the following section, and the reinforced concrete design of § 190a.

195. Standard stringer and I-beam bridges. The advantages of standard designs apply even to the covering of short spans with wooden stringers or with I beams—especially since the methods do not require much vertical space between the rails and the upper side of the clear opening, a feature which is often of prime importance. These designs are chiefly used for culverts or cattle-passes and for crossing *over* highways—providing such a narrow opening would be tolerated. The plans all imply stone abutments, or at least abutments of sufficient stability to withstand all thrust of the embankments. Some of the designs are illustrated in Plate V. The preparation of these standard designs should be attacked by the same general methods as already illustrated in § 156. When computing the required

§ 195.

transverse strength, due allowance should be made for lateral bracing, which should be amply provided for. Note particularly the methods of bracing illustrated in Plate V. The designs calling for iron (or steel) stringers may be classed as permanent constructions, which are cheap, safe, easily inspected and maintained, and therefore a desirable method of construction.









## CHAPTER VIL

### BALLAST.

196. Purpose and requirements. "The object of the ballast is to transfer the applied load over a large surface; to hold the timber work in place horizontally; to carry off the rain-water from the superstructure and to prevent freezing up in winter; to afford means of keeping the ties truly up to the grade line; and to give elasticity to the roadbed." This extremely condensed statement is a description of an ideally perfect ballast. The value of any given kind of ballast is proportional to the extent to which it fulfills these requirements. The ideally perfect ballast is not necessarily the most economical ballast for all roads. Light traffic generally justifies something cheaper, but a very common error is to use a very cheap ballast when a small additional expenditure would procure a much better ballast, which would be much more economical in the long run.

197. Materials. The materials most commonly employed are gravel and broken stone. In many sections of the country other materials which more or less perfectly fulfill the requirements as given above, are used. The various materials including some of these special types have been defined by the American Railway Engineering and Maintenance of Way Association as follows:

## DEFINITIONS.

Ballast. Selected material placed on the roadbed for the purpose of holding the track in line and surface.

Broken or crushed stone. Stone broken by artificial means into small fragments of specified sizes.

Burnt clay. A clay or gumbo which has been burned into material for ballast.

Chats. Tailings from mills in which zinc and lead ores are separated from the rocks in which they occur.

Chert. An impure flint or hornstone occurring in beds.

Cinders. The residue from the fuel used in locomotives and other furnaces.

Gravel. Small worn fragments of rock, coarser than sand, occurring in natural deposits.

Gumbo. A term commonly used for a peculiarly tenacious clay, containing no sand.

Sand. Any hard, granular, comminuted rock material, finer than gravel and coarser than dust.

Slag. The waste product, in a more or less vitrified form, of furnaces for reduction of ore. Usually the product of a blastfurnace.

There is still another classification which may or may not be considered as ballast. It is perhaps hardly correct to speak of the natural soils as ballast, yet many miles of cheap railways are "ballasted" with the natural soil, which is then called Mud ballast.

Broken or crushed stone. Rock ballast is generally specified to be that which may all be passed through a  $1\frac{1}{2}$  inch (or 2 inch) ring, but which cannot pass through a  $\frac{3}{4}$ -inch mesh. It is most easily handled with forks. This method also has the advantage that when it is being rehandled the fine chips which would interefere with effectual drainage will be screened out. Rock ballast is more expensive in first cost and is also more troublesome to handle, but in heavy traffic especially, the track will be kept in better surface and will require less work for maintenance after the ties have become thoroughly bedded.

Burnt clay. This material has been used in many sections of the country where broken stone or gravel are unobtainable except at a prohibitive cost, and where a suitable quality of clay is readily obtained. This clay should be of "gumbo" variety and contain no gravel. It is sometimes burnt in a kiln, or it is sometimes burnt by piling the clay in long heaps over a mass of fuel, the pile being formed in such a way that a temporary but effectual kiln is made. It is necessary that a clear, clean fuel shall be used and that the firing shall be done by a man who is experienced in maintaining such a fire until the burning is completed. Such ballast may be burned very hard and it will last from four to six years. The cost of burning varies from 30 to 60 cents per cubic yard, according to the circumstances.

Chats. This is a form of ballast which is peculiar to Southwestern Missouri and Southeastern Kansas. When this material was first used it was obtained from the refuse piles of the mills which treated the zinc and lead ores mined in those regions. With the processes then employed the material was obtained in lumps as large as broken stone, and they were considered to be as valuable as broken stone for ballast. Improvements in the processes of treating the ores have resulted in making this by-product very much smaller grained and of less value as ballast, although it is still considered a desirable form of ballast where it may readily be obtained. It should be noted that it is classed with gravel and cinders in the forms of cross-section shown later.

Chert. This is a form of flint or hornstone which occurs in nodules of a size that is suitable for ballast, and is a very good type of ballast wherever it is found, but its occurrence is comparatively infrequent. It is classed with cemented gravel in the design of cross-sections of ballast.

Cinders. This is one of the most universal forms of ballast, since it is a by-product of every road which uses coal as fuel. The advantages consist in the fairly good drainage, the ease of handling and the cheapness—after the road is in operation. One of the greatest disadvantages is the fact that the cinders are readily reduced to dust, which in dry weather becomes very objectionable. Cinders are usually considered preferable to gravel in yards.

Gravel. This is one of the most common forms of good ballast. There are comparatively few railroads which cannot find, at some place along their line, a gravel pit which will afford a suitable supply of gravel for ballast. Sometimes it is unnecessary to screen it, but usually it is better to screen the gravel over a screen having a  $\frac{1}{2}$ -inch mesh so as to screen out all the dirt and the finer stones.

Sand. Railroads which run along the coast are frequently ballasted merely with the sand obtained in the immediate neighborhood. One great advantage lies in the almost perfect drainage which is obtained.

Slag. When slag is readily obtainable it furnishes an excellent ballast which is free from dust and perfect in drainage

qualities. Slag is classified with crushed rock in the crosssections shown below, but it should be noted that this only applies to the best qualities of slag, since its quality is quite variable.

Mud ballast. When the natural soil is gravelly so that rain will drain through it quickly, it will make a fair roadbed for light traffic, but for heavy traffic, and for the greater part of the length of most roads, the natural soil is a very poor material for ballast; for, no matter how suitable the soil might be along limited sections of the road, it would practically never happen that the soil would be uniformly good throughout the whole length of the road. Considering that a heavy rain will in one day spoil the results of weeks of patient "surfacing" with mud ballast, it is seldom economical to use "mud" if there is a gravel-bed or other source of ballast anywhere on the line of the road.

108. Cross-sections. The required depth of the cross-section to the sub-soil depends largely on the weight of the rolling stock which is to pass over the track. A careful examination of a roadbed to determine the changes which take place under the ties and also an examination of the track and ties during the passage of a heavy train shows that the heavy loads which are now common on railroad tracks force the tie into the ballast with the passage of every wheel load. The effect on the ballast is a greater or less amount of crushing of the ballast. Even the very hardest grades of broken stone are more or less crushed by grinding against each other during the passage of a train. The softer and weaker forms of ballast are ground up much more quickly. One result is the formation of a fine dust which interferes with the proper drainage of water through the ballast. A second result is the compression of the ballast immediately under the tie into the sub-soil. In a comparatively short time a hole is formed under the tie which acts virtually like a pump. With every rise and fall of the tie under each wheel load, the tie actually pumps the water from the surrounding ballast and sub-soil into these various holes. When the ballast is of such a character that the water does not drain through it easily, the water will settle in these holes long onough to seriously deteriorate the ties. When the track becomes so much out of line or level, or so loose that it needs to be tamped up, the process of tamping has practically the effect of deepen-

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ing the amount of ballast immediately under the tie, while the sub-soil is forced up between the ties. A longitudinal section of the sub-soil of a track which has been frequently tamped generally has a saw-tooth appearance, and the sub-soil, instead of being a uniform line, has a high spot between each tie, while the ballast is considerably below its normal level immediately under the tie.

The variation in the traffic on railroads has caused the American Railway Engineering and Maintenance of Way Association to divide railroads into three classes with respect to the standards of construction which should be adopted for ballasting, as well as other details of construction. The three classes are as follows (quoted from the Association Manual):

"Class 'A' shall include all districts of a railway having more than one main track, or those districts of a railway having a single main track with a traffic that equals or exceeds the following:

Freight-car mileage passing over districts per year per mile..... 150,000 or,

Passenger-car mileage per annum per mile of district... 10,000

with maximum speed of passenger-trains of 50 miles per hour. "Class 'B' shall include all districts of a railway having a single main track with a traffic that equals or exceeds the following:

Freight-car mileage passing over districts per year per

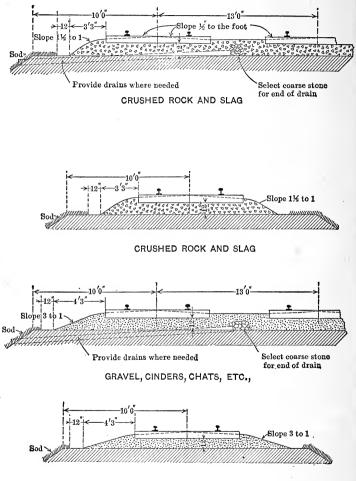
Passenger-car mileage per annum per mile of district ... 5,000

with maximum speed of passenger-trains of 40 miles per hour.

"Class 'C' shall include all districts of a railway not meeting the traffic requirements of Classes 'A' or 'B.""

The classification was adopted on the consideration that *quality* of traffic as well as mere tonnage should determine the classification of a railroad. For example, it is considered that a road which operates a train at a speed of 50 miles an hour should adopt the first class or Class "A" standards, even though there is but one train per day on that railroad. It

likewise means that any road whose traffic makes necessary the construction of a regular double track should adopt the firstclass specifications.



GRAVEL, CINDERS, CHATS, ETC.,

FIG. 106.-CROSS-SECTIONS OF BALLAST FOR CLASS "A ' ROADS.

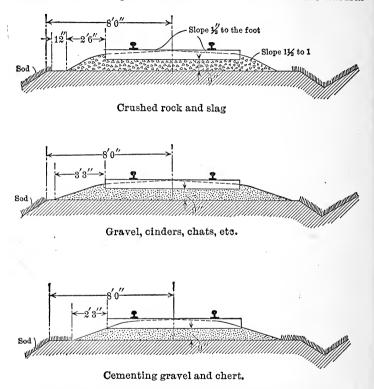
In Fig. 106 are shown a series of cross-sections which were recommended by that association for Class "A" traffic. It

should be noticed that in each case the cross-section of the roadbed from shoulder to shoulder of the roadbed is 20 feet plus the space between track centers for double track if any. The width of side ditches is merely added to that of the roadbed. The clear thickness of the ballast underneath the ties is made 12 inches, but even this should be considered as the minimum depth and is recommended for use only on the firmest, most substantial and well-drained subgrades. The slope of  $\frac{1}{2}$  inch to the foot from the center of the track to the end of the tie. which is common to all the cross-sections, is designed with the idea of allowing a clear space of 1 inch underneath the rail. The ballast is then rounded off on a curve of 4 feet radius and finally reaches the subsoil on a slope which is  $1\frac{1}{2}$ :1 for broken stone, and 3:1 for all other materials. The flat slope adopted for gravel, etc., which adds considerably to the required width of roadbed, has been so designed in order that the considerable mass of material at the ends of the ties shall be better able to hold the track in place laterally. The sod on the embankment over the shoulder of the roadbed up to within 12 inches of the edge of the ballast is strongly recommended on account of the protection it affords to the shoulder of the roadbed. It should be noticed that the latest decision of that association regarding the form of subgrade is that the subgrade should be made level and not crowned, as suggested and discussed in § 63.

In Fig. 107 are shown a series of cross-sections for various classes of ballast for railroads that belong to Class "B." It may be noted that the thickness of the ballast under the tie is 9 inches for this class. The width of roadbed between the shoulders, recommended for Class "B" is 16 feet. As before, the width of the ditches is supposed to be added to this width. It should be noted that when using cementing gravel and chert the slope of 3:1 is made to begin at the bottom of the tie instead of at a point about 2 inches below the top of the tie. This is done in order to prevent water from accumulating around the end of the tie in a material which is less permeable than the other forms of ballast.

In Fig. 108 are shown two cross-sections for ballast for roads belonging to Class "C." On roads of this class it is assumed that crushed rock will not be used for ballast. The width of roadbed between shoulders is 14 feet, while the depth of ballast underneath the tie is 6 inches.

It should be noticed that the above sections issued by the association do not include any cross-section which is recommended when no special ballast is used other than the natural





soil. In such a case a cross-section very similar to the sections shown for cementing gravel and chert should be used. The essential feature of such a section is that the soil, which is probably not readily permeable, should be kept away from the ends of the ties. Specifications for the placing of mud ballast, as well as other forms of ballast, have frequently specified that the ballast should be crowned about 1 inch above the level of the tops of the ties in the center of the track. This

### BALLAST.

## § 199.

feature of any cross-section, although proposed, was rejected by the association, in spite of the fact that when a tie is so imbedded it certainly will have a somewhat greater holding power in the ballast.

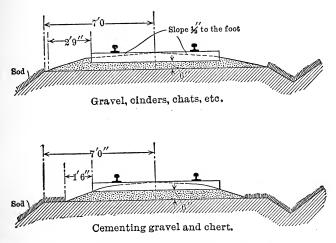


FIG. 108.—CROSS-SECTIONS OF BALLAST FOR CLASS "C" ROADS.

199. Methods of laying ballast. The cheapest method of laying ballast on new roads is to lay ties and rails directly on the prepared subgrade and run a construction train over the track to distribute the ballast. Then the track is lifted up until sufficient ballast is worked under the ties and the track is properly surfaced. This method, although cheap, is apt to injure the rails by causing bends and kinks, due to the passage of loaded construction trains when the ties are very unevenly and roughly supported, and the method is therefore condemned and prohibited in some specifications. The best method is to draw in carts (or on a contractor's temporary track) the ballast that is required under the level of the bottom of the ties. Spread this ballast carefully to the required surface. Then lay the ties and rails, which will then have a very fair surface and uniform support. A construction train can then be run on the rails and distribute sufficient additional ballast to pack around and between the ties and make the required cross-section.

The necessity for constructing some lines at an absolute

minimum of cost and of opening them for traffic as soon as possible has often led to the policy of starting traffic when there is little or no ballast—perhaps nothing more than a mere tamping of the natural soil under the ties. When this is done ballast may subsequently be drawn where required by the trainload on flat cars and unloaded at a minimum of cost by means of a "plough." The plough has the same width as the cars and is guided either by a ridge along the center of each car or by short posts set up at the sides of the cars. It is drawn from one end of the train to the other by means of a cable. The cable is sometimes operated by means of a small hoisting-engine carried on a car at one end of the train. Sometimes the locomotive is detached temporarily from the train and is run ahead with the cable attached to it.

200. Cost. The cost of ballast in the track is quite a variable item for different roads, since it depends (a) on the first cost of the material as it comes to the road, (b) on the distance from the source of supply to the place where it is used, and (c) on the method of handling. The first cost of cinder or slag is frequently insignificant. A gravel-pit may cost nothing except the price of a little additional land beyond the usual limits of the right of way. Broken stone will usually cost \$1 or more per cubic yard. If suitable stone is obtainable on the company's land, the cost of blasting and breaking should be somewhat less than this. The cost of hauling will depend on the distance hauled, and also, to a considerable extent, on the limitations on the operation of the train due to the necessity of keeping out of the way of regular trains. There is often a needless waste in this way. The "mud train" is considered a pariah and entitled to no rights whatever, regardless of the large daily cost of such a train and of the necessary gang of men. The cost of broken-stone ballast in the track is estimated at \$1.25 per cubic vard. The cost of gravel ballast is estimated at 60 c. per cubic yard in the track. The cost of placing and tamping gravel ballast is estimated at 20 c. to 24 c. per cubic yard, for cinders 12 c. to 15 c. per cubic yard. The cost of loading gravel on cars, using a steam-shovel, is estimated at 6 c. to 10 c. per cubic yard.\*

\* Report Roadmasters' Association, 1885.

## CHAPTER VIII.

#### TIES,

## AND OTHER FORMS OF RAIL SUPPORT.

201. Various methods of supporting rails. It is necessary that the rails shall be sufficiently supported and braced, so that the gauge shall be kept constant and that the rails shall not be subjected to excessive transverse stress. It is also preferable that the rail support shall be neither rigid (as if on solid rock) nor too yielding, but shall have a *uniform* elasticity throughout. These requirements are more or less fulfilled by the following methods.

(a) Longitudinals. Supporting the rails throughout their entire length. This method is very seldom used in this country except occasionally on bridges and in terminals when the longitudinals are supported on cross-ties. In § 224 will be described a system of rails, used to some extent in Europe, having such broad bases that they are self-supporting on the ballast and are only connected by tie-rods to maintain the gauge.
(b) Cast-iron "bowls" or "pots." These are castings resem-

(b) Cast-iron "bowls" or "pots." These are castings resembling large inverted bowls or pots, having suitable chairs on top for holding and supporting the rails, and tied together with tie-rods. They will be described more fully later (§ 223).

(c) Cross-ties of metal or wood. These will be discussed in the following sections.

202. Economics of ties. The true cost of ties depends on the relative total cost of maintenance for long periods of time. The first cost of the ties delivered to the road is but one item in the economics of the question. Cheap ties require frequent renewals, which cost for the labor of each renewal practically the same whether the tie is of oak or of hemlock. Cheap ties make a poor roadbed which will require more track labor to keep even in tolerable condition. The roadbed will require to be disturbed so frequently on account of renewals that the ties never get an opportunity to get settled and to form a smooth roadbed for any length of time. Irregularity in width, thickness, or length of ties is especially detrimental in causing the ballast to act and wear unevenly. The life of ties has thus a more or less direct influence on the life of the rails, on the wear of rolling stock, and on the speed of trains. These last items are not so readily reducible to dollars and cents, but when it can be shown that the total cost, for a long period of time, of several renewals of

cheap ties, with all the extra track labor involved, is as great as or greater than that of a few renewals of durable ties, then there is no question as to the real economy. In the following discussions of the merits of untreated ties (either cheap or costly), chemically treated ties, or metal ties, the true question is therefore of the ultimate cost of maintaining any particular kind of ties for an indefinite period, the cost including the first cost of the ties, the labor of placing them and maintaining them to surface, and the somewhat uncertain (but not therefore nonexistent) effect of frequent renewals on repairs of rolling stock, on possible speed, etc.

## WOODEN TIES.

203. Choice of wood. This naturally depends, for any particular section of country, on the supply of wood which is most readily available. The woods most commonly used, especially in this country, are oak and pine, oak being the most durable and generally the most expensive. Redwood is used very 'extensively in California and proves to be extremely durable, so far as decay is concerned, but it is very soft and is much injured by "rail-cutting." This defect is being partly remedied by the use of tie-plates, as will be explained later. Cedar, chestnut, hemlock, and tamarack are frequently used in this country. In tropical countries very durable ties are frequently obtained from the hard woods peculiar to those countries. According to a bulletin of the U.S. Department of Agriculture (Forestry service, No. 124) the number and value of the cross-ties used by the steam and street railroads of the United States during the year 1906, was as follows:

Kind of wood.	Number of ties.	Per cent.	Total value.	Aver. value
Oaks	18,841,210	$     \begin{array}{r}                                     $	\$23,278,052 9,567,745 3,010,392	\$0.51 .51 .42
Cedar Chestnut Cypress	7,083,442 6,588,975 5,104,496	$6.9 \\ 6.4 \\ 5.0$	3.310,116 2,995,942 1,862,135	.47 .49 .36
Western pine Tamarack Hemlock Redwood	2,576,859 2,058,198	$3.9 \\ 2.5 \\ 2.0 \\ 1.2$	$\begin{array}{r}1,698,027\\889,561\\582,968\\536,172\end{array}$	.43 .35 .28 .43
Lodgepole pine White pine	554,738	$     \begin{array}{c}       1.2 \\       0.5 \\       0.3 \\       1.8     \end{array} $	210,818 151,052 726,144	$     \begin{array}{r}             .38 \\             .40 \\             .40         \end{array}     $
Total	102,834,042	100.0	\$48,819,124	\$0.47

The limitations of timber supply have somewhat diminished the use of oak and increased the use of the softer woods in recent years.

204. Durability. The durability of ties depends on the climate; the drainage of the ballast; the volume, weight, and speed of the traffic; the curvature, if any; the use of tie-plates; the time of year of cutting the timber; the age of the timber and the degree of its seasoning before placing in the track; the nature of the soil in which the timber is grown; and, chiefly, on the species of wood employed. The variability in these items will account for the discrepancies in the reports on the life of various woods used for ties.

White oak is credited with a life of 5 to 12 years, depending principally on the traffic. It is both hard and durable, the hardness enabling it to withstand the cutting tendency of the rail-flanges, and the durability enabling it to resist decay. Pine and redwood resist decay very well, but are so soft that they are badly cut by the rail-flanges and do not hold the spikes very well, necessitating frequent respiking. Since the spikes must be driven within certain very limited areas on the face of each tie, it does not require many spike-holes to "spike-kill" the tie. On sharp curves, especially with heavy traffic, the wheelflange pressure produces a side pressure on the rail tending to overturn it, which tendency is resisted by the spike, aided sometimes by rail-braces. Whenever the pressure becomes too great the spike will yield somewhat and will be slightly withdrawn. The resistance is then somewhat less and the spike is soon so loose that it must be redriven in a new hole. If this occurs very often, the tie may need to be replaced long before any decay. has set in. When the traffic is very light, the wood very durable, and the climate favorable, ties have been known to last 25 years.

205. Dimensions. The usual dimensions for the best roads (standard gauge) are 8' to 9' long, 6" to 7" thick, and 8" to 10" wide on top and bottom (if they are hewed) or 8" to 9" wide if they are sawed. For cheap roads and light traffic the length is shortened sometimes to 7' and the cross-section also reduced. On the other hand a very few roads use ties 9'6" long.

Two objections are urged against sawed ties: first, that the grain is torn by the saw, leaving a woolly surface which induces decay; and secondly, that, since timber is not perfectly straightgrained, some of the fibers are cut obliquely, exposing their ends, which are thus liable to decay. The use of a "planer-saw" obviates the first difficulty. Chemical treatment of ties obviates both of these difficulties. Sawed ties are more convenient to handle, are a necessity on bridges and trestles, and it is even claimed, although against commonly received opinion, that actual trial has demonstrated that they are more durable than hewed ties.

206. Spacing. The spacing is usually 14 to 16 ties to a 30foot rail. This number is sometimes reduced to 12 and even 10, and on the other hand occasionally increased to 18 or 20 by employing narrower ties. There is no economy in reducing the number of ties very much, since for any required stiffness of track it is more economical to increase the number of supports than to increase the weight of the rail. The decreasing cost of rails and the increasing cost of ties have materially changed the relation between number of ties and weight of rail to produce a given stiffness at minimum cost, but many roads have found it economical to employ a large number of ties rather than increase the weight of the rail. On the other hand there is a practical limit to the number that may be employed, on account of the necessary space between the ties that is required for proper tamping. This width is ordinarily about twice the width of the tie. At this rate, with light ties 6" wide and with 12" clear space, there would be 20 ties per 30-foot rail, or 3520 per mile. The smaller ties can generally be bought much cheaper (proportionately) than the larger sizes, and hence the economy.

Track instructions to foremen generally require that the spacing of ties shall *not* be uniform along the length of any rail. Since the joint is generally the weakest part of the rail structure, the joint requires more support than the center of the rail. Therefore the ties are placed with but 8" or 10" clear space between them at the joints, this applying to 3 or 4 ties at each joint; the remaining ties, required for each rail length, are equally spaced along the remaining distance.

207. Specifications. The specifications for ties are apt to include the items of size, kind of wood, and method of construction, besides other minor directions about time of cutting, seasoning, delivery, quality of timber, etc.

(a) Size. The particular size or sizes required will be somewhat as indicated in § 205. (b) Kind of wood. When the kind or kinds of wood are specified, the most suitable kinds that are available in that section of country are usually required.

(c) Method of construction. It is generally specified that the ties shall be hewed on two sides; that the two faces thus made shall be parallel planes and that the bark shall be removed. It is sometimes required that the ends shall be sawed off square; that the timber shall be cut in the winter (when the sap is down); and that the ties shall be seasoned for six months These last specifications are not required or lived up to as much as their importance deserves. It is sometimes required that the ties shall be delivered on the right of way, neatly piled in rows, the alternate rows at right angles, piled if possible on ground not lower than the rails and at least seven feet away from them, the lower row of ties resting on two ties which are themselves supported so as to be clear of the ground.

(d) Quality of timber. The usual specifications for sound timber are required, except that they are not so rigid as for a better class of timber work The ties must be sound, reasonably straight-grained, and not very crooked—one test being that a line joining the center of one end with the center of the middle shall not pass outside of the other end. Splits or shakes, especially if severe, should cause rejection.

Specifications sometimes require that the ties shall be cut







from single trees, making what is known as "pole ties" and definitely condemning those which are cut or split from larger trunks, giving two "slab

FIG. 109.-METHODS OF CUTTING TIES.

ties" or four "quarter ties" for each cross-section, as is illustrated in Fig. 109. Even if pole ties are better, their exclusive use means the rapid destruction of forests of young trees.

208. Regulations for laying and renewing ties. The regulations issued by railroad companies to their track foremen will generally include the following, in addition to directions regarding dimensions, spacing, and specifications given in §§ 204-207. When hewn ties of somewhat variable size are used, as is frequently the case, the largest and best are to be selected for use as joint ties. If the upper surface of a tie is found to be warped (contrary to the usual specifications) so that one or both rails do

not get a full bearing across the whole width of the tie, it must be adzed to a true surface along its whole length and not merely notched for a rail-seat. When respiking is necessary and spikes have been pulled out, the holes should be immediately plugged with "wooden spikes," which are supplied to the foreman for that express purpose, so as to fill up the holes and prevent the decay which would otherwise take place when the hole becomes filled with rain-water. Ties should always be laid at right angles to the rails and never obliquely Minute regulations to prevent premature rejection and renewal of ties are frequently made. It is generally required that the requisitions for renewals shall be made by the actual count of the individual ties to be renewed instead of by any wholesale estimates. It is unwise to have ties of widely variable size, hardness, or durability adjacent to each other in the track, for the uniform elasticity, so necessary for smooth riding, will be unobtainable under those circumstances.

209. Cost of ties. When railroads can obtain ties cut by farmers from woodlands in the immediate neighborhood, the price will frequently be as low as 20 c for the smaller sizes, running up to 50 c for the larger sizes and better qualities, especially when the timber is not very plentiful. Sometimes if a railroad cannot procure suitable ties from its immediate neighborhood, it will find that adjacent railroads control all adjacent sources of supply for their own use and that ties can only be procured from a considerable distance, with a considerable added cost for transportation. First-class oak ties cost about 75 to 80 c. and frequently much more Hemlock ties can generally be obtained for 35 c. or less.

### PRESERVATIVE PROCESSES FOR WOODEN TIES.

**210.** General principle. Wood has a fibrous cellular structure, the cells being filled with sap or air. The woody fiber is but little subject to decay unless the sap undergoes fermentation. Preservative processes generally aim at removing as much of the water and sap as possible and filling up the pores of the wood with an antiseptic compound The most common methods (except one) all agree in this general process and only differ in the method employed to get rid of the sap and in the antiseptic chemical with which the fibers are filled One valuable feature of these processes lies in the fact that the softer cheaper woods

(such as hemlock and pine) are more readily treated than are the harder woods and yet will produce practically as good a tie as a treated hard-wood tie and a very much better tie than an untreated hard-wood tie. The various processes will be briefly described, taking up first the process which is fundamentally different from the others, viz., vulcanizing.

211. Vulcanizing. The process consists in heating the timber to a temperature of 300° to 500° F. in a cylinder, the air being under a pressure of 100 to 175 lbs. per square inch. By this process the albumen in the sap is coagulated, the water evaporated, and the pores are partially closed by the coagulation of the albumen. It is claimed that the heat sterilizes the wood and produces chemical changes in the wood which give it an antiseptic character. It was once very extensively used on the elevated lines of New York City, but the process has now been abandoned as unsatisfactory.

212. Creosoting.—This process consists in impregnating the wood with wood-creosote or with dead oil of coal-tar. Woodcreosote is one of the products of the destructive distillation of wood—usually long-leaf pine. Dead oil of coal-tar is a prod-uct of the distillation of coal-tar at a temperature between 480° and 760° F. It would require about 35 to 50 pounds of creo-sote to completely fill the pores of a cubic foot of wood. But But it would be impossible to force such an amount into the wood. nor is it necessary or desirable. About 10 pounds per cubic foot, or about 35 pounds per tie, is all that is necessary. For piling placed in salt water about 18 to 20 pounds per cubic foot is used, and the timber is then perfectly protected against the ravages of the teredo navalis. To do the work, long cylinders, which may be opened at the ends, are necessary. Usually the timbers are run in and out on iron carriages running on rails fastened to braces on the inside of the cylinder. When the load has been run in, the ends of the cylinder are fastened on. The water and air in the pores of the wood are first drawn out by subjecting the wood alternately to steam-pressure and to the action of a vacuum-pump. This is continued for several hours. Then, after one of the vacuum periods, the cylinder is filled with creosote oil at a temperature of about 170° F. The pumps are kept at work until the pressure is about 80 to 100 pounds per square inch, and is maintained at this pressure from one to two hours according to the size of the timber. The oil is then

§ 213.

withdrawn, the cylinders opened, the train pulled out and another load made up in 40 to 60 minutes. The average time required for treating a load is about 18 or 20 hours, the absorption about 10 or 11 pounds of oil per cubic foot, and the cost (1894) from \$12.50 to \$14.50 per thousand feet B. M.

213. Burnettizing (chloride-of-zinc process). This process is very similar to the creosoting process except that the chemical is chloride of zinc, and that the chemical is not heated before use. The preliminary treatment of the wood to alternate vacuum and pressure is not continued for quite so long a period as in the creosoting process. Care must be taken, in using this process. that the ties are of as uniform quality as possible, for seasoned ties will absorb much more zinc chloride than unseasoned (in the same time), and the product will lack uniformity unless the seasoning is uniform. The A., T. & S. Fé R. R. has works of its own at which ties are treated by this process at a cost of about 25 c. per tie. The Southern Pacific R. R. also has works for burnettizing ties at a cost of 9.5 to 12 c per tie The zing chloride solution used in these works contains only 1.7% of zinc chloride instead of over 3% as used in the Santa Fé works, which perhaps accounts partially for the great difference in cost per tie. One great objection to burnettized ties is the fact that the chemical is somewhat easily washed out, when the wood again becomes subject to decay Another objection, which is more forcible with respect to timber subject to great stresses, as in trestles, than to ties, is the fact that when the solution of zinc chloride is made strong (over 3%) the timber is made very brittle and its strength is reduced. The reduction in strength has been shown by tests to amount to  $\frac{1}{4}$  to  $\frac{1}{10}$  of the ultimate strength, and that the elastic limit has been reduced by about 1.

214. Kyanizing (bichloride-of-mercury or corrosive-sublimate process). This is a process of "steeping" It requires a much longer time than the previously described processes, but does not require such an expensive plant. Wooden tanks of sufficient size for the timber are all that is necessary. The corrosive sublimate is first made into a concentrated solution of one part of chemical to six parts of *hot* water. When used in the tanks this solution is weakened to 1 part in 100 or 150. The wood will absorb about 5 to 6.5 pounds of the bichloride per 100 cubic feet, or about one pound for each 4 to 6 ties. The timber is allowed to soak in the tanks for several days, the general rule being about one day for each inch of least thickness and one day over—which means seven days for six-inch ties, or thirteen (to fifteen) days for 12" timber (least dimension). The process is somewhat objectionable on account of the chemical being such a virulent poison, workmen sometimes being sickened by the fumes arising from the tanks. On the Baden railway (Germany) kyanized ties last 20 to 30 years. On this railway the wood is always air-dried for two weeks after impregnation and before being used, which is thought to have an important effect on its durability. The solubility of the chemical and the liability of the chemical washing out and leaving the wood unprotected is an element of weakness in the method.

215. Wellhouse (or zinc-tannin) process. The last two methods described (as well as some others employing similar chemicals) are open to the objection that since the wood is impregnated with an aqueous solution, it is liable to be washed out very rapidly if the wood is placed under water, and will even disappear, although more slowly, under the action of moisture and rain. Several processes have been proposed or patented to prevent this. Many of them belong to one class, of which the Wellhouse process is a sample. By these processes the timber is successively subjected to the action of two chemicals, each individually soluble in water, and hence readily impregnating the timber, but the chemicals when brought in contact form insoluble compounds which cannot be washed out of the woodcells. By the Wellhouse process, the wood is first impregnated with a solution of chloride of zinc and glue, and is then subjected to a bath of tannin under pressure. The glue and tannin combine to form an insoluble leathery compound in the cells, which will prevent the zinc chloride from being washed out. It is being used by the A., T. &. S. Fé R. R., their works being located at Las Vegas, New Mexico, and also by the Union Pacific R. R. at their works at Laramie, Wyo. In 1897 Mr. J. M. Meade, a resident engineer on the A., T. & S. Fé, exhibited to the Roadmasters Association of America a piece of a tie treated by this process which had been taken from the tracks after nearly 13 years' service. The tie was selected at random, was taken out for the sole purpose of having a specimen, and was still in sound condition and capable of serving many years longer. The cost of the treatment was then quoted as 13 c. per tie. It was claimed that the treatment trebled the life of the tie besides adding to its spike-holding power.

In spite of this apparently favorable showing, the process was abandoned on the A. T. & S. F. R. R. in 1898 on the ground that the results did not justify the added expense.

216. Cost of Treating. The cost of treating ties by the various methods has been estimated as follows \*-assuming that the plant was of sufficient capacity to do the work economically: creosoting, 25 c. per tie; vulcanizing, 25 c. per tie; burnettizing (chloride of zinc), 8.25 c. per tie; kyanizing (steeping in corrosive sublimate), 14.6 c. per tie; Wellhouse process (chloride of zinc and tannin), 11.25 c. per tie. These estimates are only for the net cost at the works and do not include the cost of hauling the ties to and from the works, which may mean 5 to 10 c. per tie. Some of these processes have been installed on cars which are transported over the road and operated where most convenient. An estimate made in 1907 by Prof. Gellert Alleman on the cost of treating ties, each assumed to have a volume of 3 cubic feet, the cost "not including royalty on patents, profit, interest, or depreciation, all of which vary widely at the various plants," is as follows:

Zinc chloride			16	cents
"	" "	and creosote	27	66
Creoso	te, 10	pounds to the cubic foot	55	**

The very great, increase in these prices, especially for creosoting, is due to the enormous increase in late years in the consumption and in the price of creosote.

217. Economics of treated ties. The fact that treated ties are not universally adopted is due to the argument that the added life of the tie is not worth the extra cost. If ties can be bought for 25 c., and cost 25 c. for treatment, and the treatment only doubles their life, there is apparently but little gained except the work of placing the extra tie in the track, which is more or less offset by the interest on 25 c. for the life of the untreated tie, and the larger initial outlay makes a stronger impression on the mind than the computed ultimate economy. But when (utilizing some statistics from the Pittsburg, Ft. Wayne &

<sup>\*</sup> Bull. No. 9, U. S. Dept. of Agric., Div. of Forestry. App. No. 1, by Henry Flad.

Chicago Railroad) it is found that white oak ties laid in rock ballast had a life of 10.17 years, and that hemlock ties treated with the zinc-tannin process and laid in the same kind of ballast lasted 10.71 years, then the economy is far more apparent. Unfortunately no figures were given for the cost of these ties nor for the cost of the treatment; but if we assume that the white oak ties cost 75 c. and the hemlock ties 35 c. plus 20 c. for treatment, there is not only a saving of 20 c. on each tie, but also the advantage of the slightly longer life of the treated In the above case the total life of the two kinds of ties tie. is so nearly the same that we may make an approximation of their relative worth by merely comparing the initial cost; but usually it is necessary to compare the value of two ties one of which may cost more than the other, but will last considerably The mathematical comparison of the real value of longer. two ties under such conditions may be developed as follows: The real cost of a tie, or any other similar item of constructive work. is measured by the cost of perpetually maintaining that item in proper condition in the structure. It will be here assumed that the annual cost of the trackwork, which is assignable to the tie, is the same for all kinds of ties, although the difference probably lies in favor of the more expensive and most durable ties. By assuming this expense as constant, the remaining expense may be considered as that due to the cost of the new ties whenever necessary, plus the cost of placing them in the track. We also may combine these two items in one, and consider that the cost of placing a tie in the track, which we will assume at the constant value of 20 c. per tie, regardless of the kind of tie, is merely an item of 20 c. in the total cost of the tie. We will assume that  $T_1$  is the present cost of a tie, the cost including the preservative treatment if any, and the cost of placing in the track. The tie is assumed to last n years. At the end of n years another tie is placed in the track, and, for lack of more precise knowledge, we will assume that this cost  $T_2$  equals  $T_1$ . The "present worth" of  $T_2$  is the sum which, placed at compound interest, would equal  $T_2$  at the end of *n* years, and is expressed by the quantity

 $\frac{T_2}{(1+r)^n}$ , in which r equals the rate of interest. Similarly at the end of 2n years we must expend a sum  $T_3$  to put in the third tie, and the present worth of the cost of that third tie is ex-

pressed by the fraction  $\frac{T_3}{(1+r)^{2n}}$ . We may similarly express the present worths of the cost of ties for that particular spot for an indefinite period. The sum of all these present worths is given by the sum of a converging series and equals (assuming that all the T's are equal)  $\frac{T \times (1+r)^n}{(1+r)^n - 1}$ . But instead of laying aside a sum of money which will maintain a tie in that particular place in perpetuity, we may compute the annual sum which must be paid at the end of each year, which would be the equivalent. We will call that annual payment A, and then the present worths of all these items are as follows:

For the first payment	$\frac{A}{(1+r)}$ ;
For the second payment	$\frac{A}{(1+r)^2};$
For the third payment	
For the <i>n</i> th payment	$\frac{A}{(1+r)n}$

After the next tie is put in place we have the present worths of the annual payments on the second tie, of which the first one would be

For the (n+1) payment  $\dots$   $\frac{A}{(1+r)^{(n+1)}}$ 

Similarly after x ties have been put in place the last payment for the x tie would have a present worth  $\frac{A}{(1+r)^{nx}}$ . The sum of all these present worths is represented by the sum of a converging series and equals the very simple expression  $\frac{A}{r}$ . But since the sum of the present worths of these annual payments must equal the sum of the present worths of the payments made at intervals of n years, we may place these two summations equal to each other, and say that

$$A = \frac{r \times T \times (1+r)^n}{(1+r)^n - 1}$$

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Values of A for various costs of a tie T on the basis that requals 5% have been computed and placed in Table XXXIV. To illustrate the use of this table, assume that we are comparing the relative values of two ties, both untreated, one of them a white oak tie which will cost, say 75 c., and will last twelve years, the other a yellow pine tie which will cost, say 35 c., and will last six years. Assuming a charge for each case of 20 c. for placing the tie in the track, we have as the annual charge against the white oak tie, which costs 95 c. in the track, 10.72 c. The pine tie, costing 55 c. in the track and lasting six years, will be charged with an annual cost of 10.48 c., which shows that the costs are practically equal. It is probably true that the track work for maintaining the white oak would be less than that for the pine tie, but since the initial cost of the pine tie is less than that of the oak tie, it would probably be preferred in this case, especially if money was difficult to obtain. It may be interesting to note that if a comparison is made from a similar table which is computed on the basis of compounding the money at 4% instead of 5%, the annual charges would be 10.13 and 10.49 c. for the oak and pine ties respectively, thus showing that when money is "easier" the higher priced tie has the greater advantage.

EXAMPLE 2. Considering again the comparison previously made of a white oak untreated tie which was assumed to cost 75 c., and a hemlock treated tie, which cost 35 c. for the tie and 20 c. for the treatment, the total costs of these ties laid in the track would therefore be 95 c. and 75 c. respectively. These ties had practically the same life (10.17 and 10.71 years), but in order to use the table, we will call it ten years for each tie. The annual charge against the oak tie would therefore be 12.30 c., while that against the hemlock tie would be 9.72 c. This gives an advantage in the use of the treated tie of 2.58 c. per year, which capitalized at 5% would have a capitalized value of 51.6 c.

The Atchison, Topeka and Santa Fé R. R. has compiled a record of treated pine ties removed in 1897, '98, '99, and 1900, showing that the *average* life of the ties removed had been about 11 years. On the Chicago, Rock Island and Pacific R. R., the average life of a very large number of treated hemlock and tamarack ties was found to be 10.57 years. Of one lot of 21,850 ties, 12% still remained in the track after 15 years' exposure.

It has been demonstrated that much depends on the minor

details of the process—whatever it may be. As an illustration, an examination of a batch of ties, treated by the zinccreosote process, showed 84% in service after 13 years' exposure; another batch, treated by another contractor by the same process (nominally), showed 50% worthless after a service of six years.

# METAL TIES.

218. Extent of use. In 1894 \* there were nearly 35000 miles of "metal track" in various parts of the world. Of this total, there were 3645 miles of "longitudinals" (see § 224), found exclusively in Europe, nearly all of it being in Germany. There were over 12000 miles of "bowls and plates" (see § 223), found almost entirely in British India and in the Argentine Republic. The remainder, over 18000 miles, was laid with metal cross-ties of various designs. There were over 8000 miles of metal crossties in Germany alone, about 1500 miles in the rest of Europe, over 6000 miles in British India, nearly 1000 miles in the rest of Asia, and about 1500 miles more in various other parts of the world. Several railroads in this country have tried various designs of these ties, but their use has never passed the experimental stage. These 35000 miles represent about 9% of the total railroad mileage of the world—nearly 400000 miles. They represent about 17.6% of the total railroad mileage, exclusive of the United States and Canada, where they are not used at all. except experimentally.<sup>†</sup> In the four years from 1890 to 1894 the use of metal track increased from less than 25000 miles to nearly 35000 miles. This increase was practically equal to the total increase in railroad mileage during that time, exclusive of the increase in the United States and Canada. This indicates a large growth in the percentage of metal track to total mileage, and therefore an increased appreciation of the advantages to be derived from their use.

219. Durability. The durability of metal ties is still far from being a settled question, due largely to the fact that the best form for such ties is not yet determined, and that a large part of the apparent failures in metal ties have been evidently due to defective design. Those in favor of them estimate the life as from 30 to 50 years. The opponents place it at not more

<sup>\*</sup> Bulletin No. 9, U. S. Dept. of Agriculture, Div. of Forestry.

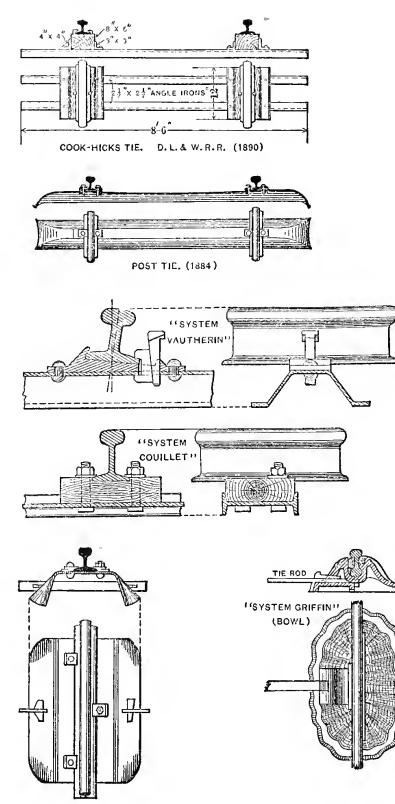
<sup>†</sup> See § 220 for a later development.

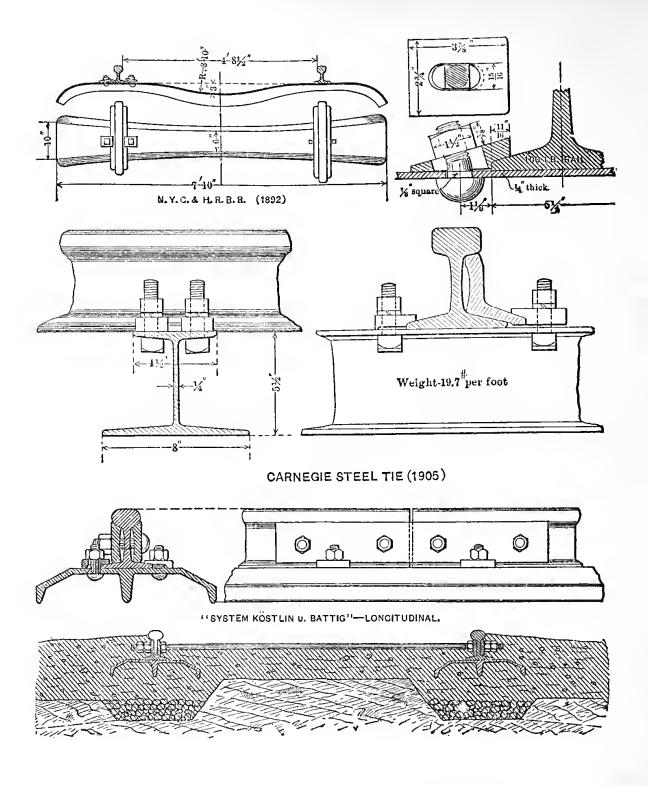
than 20 years, or perhaps as long as the best of wooden ties. Unlike the wooden tie, however, which deteriorates as much with time as with usage, the life of a metal tie is more largely a function of the traffic. The life of a well-designed metal tie has been estimated at 150000 to 200000 trains; for 20 trains per day, or say 6000 per year, this would mean from 25 to 33 years. 20 trains per day on a single track is a much larger number than will be found on the majority of railroads. Metal ties are found to be subject to rust, especially when in damp localities, such as tunnels; but on the other hand it is in such confined localities. where renewals are troublesome, that it is especially desirable to employ the best and longest-lived ties. Paint, tar, etc., have been tried as a protection against rust, but the efficacy of such protection is as yet uncertain, the conditions preventing any renewal of the protection—such as may be done by repainting a bridge, for example. Failures in metal cross-ties have been largely due to cracks which begin at a corner of one of the square holes which are generally punched through the tie, the holes being made for the bolts by which the rails are fastened to the The holes are generally *punched* because it is cheaper. tie. Reaming the holes after punching is thought to be a safeguard against this frequent cause of failure. Another method is to round the corners of the square punch with a radius of about  $\frac{1}{2}$ ". If a crack has already started, the spread of the crack may be prevented by drilling a small hole at the end of it.

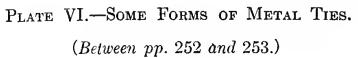
220. Form and dimensions of metal cross-ties. Since stability in the ballast is an essential quality for a tie, this must be accomplished either by turning down the end of the tie or by having some form of lug extending downward from one or more points of the tie. The ties are sometimes depressed in the center (see Plate VI, N. Y. C. & H. R. R. R. tie) to allow for a thick covering of ballast on top in order to increase its stability in the This form requires that the ties should be sufficiently ballast. well tamped to prevent a tendency to bend out straight, thus widening the gauge. Many designs of ties are objectionable because they cannot be placed in the track without disturbing adjacent ties. The failure of many metal cross-ties, otherwise of good design, may be ascribed to too light weight. Those weighing much less than 100 pounds have proved too light. From 100 to 130 pounds weight is being used satisfactorily on German railroads. The general outside dimensions are about

the same as for wooden ties, except as to thickness. The metal is generally from  $\frac{1}{4}$ " to  $\frac{2}{3}$ " thick. They are, of course, only made of wrought iron or steel, cast iron being used only for "bowls" or "plates" (see § 223). The details of construction for some of the most commonly used ties may be seen by a study of Plate VI.

The Carnegie tie is perhaps the only tie whose use on steam railroads in this country has passed the experimental stage. The Bessemer and Lake Erie R. R. in 1910 had 188 miles of track laid with these ties, and other roads are making extensive experiments. One practical difficulty, which is not of course insuperable, arises from the common practice of using the rails as parts of an electrical circuit for a block-signal system, which requires that the rails shall be insulated from each other. This requires that these metal ties shall be insulated from the rails. A method of insulation which is altogether satisfactory and inexpensive is yet to be determined. It is claimed that, on account of the better connection between the rail and the tie. there is less wear and more uniform wear to the rail. It is also claimed that there is greater lateral rigidity in the rails and ties (considered as a structure) and that this decreases the trackwork necessary to maintain alinement. These ties weigh 19.7 pounds per linear foot, or about 167 pounds for an 8 foot 6 inch tie. Even at the lowest possible price per pound the cost of the tie and its fastenings must be two or three times that of the best oak tie with spikes and even tie plates. It has been impossible to estimate the probable life of these ties. Until a reasonably close estimate of the life of steel ties can be determined, no proper comparison can be made of their economy relative to that of wooden ties. A study of Table XXXIV will show that a tie which costs, say three times as much as a cheap tie, must last more than three times as long in order that the annual charge against the tie shall be as low as that of the cheaper tie. For example, let us assume that the cost of a metal tie, laid in the track, is \$2.55 and that it will last 20 years. From Table XXXIV we may find that the annual charge against \$2.55 at 5% for 20 years =  $(2 \times 8.02)$  + 4.41 = 20.45 c. Compared with a tie costing 65 c., plus 20 c. for track laving, we find that the cheaper tie will only cost 19.63 c. per year even if it only lasts 5 years. Of course the claimed advantage of better track and less cost for track maintenance, using steel ties, will tend to offset, so far as it is true,







LIVESEY BOWL. (1864)



the disadvantage of the extra cost of the metal tie. Even if the extra work per tie amounts to only one-half hour for one man in a year, the cost of it, say 6 c., will utterly change the relative economics of the two ties.

221. Fastenings. The devices for fastening the rails to the ties should be such that the gauge may be widened if desired on curves, also that the gauge can be made true regardless of slight inaccuracies in the manufacture of the ties, and also that shims may be placed under the rail if necessary during cold weather when the tie is frozen into the ballast and cannot be easily disturbed. Some methods of fastening require that the base of the rail be placed against a lug which is riveted to the tie or which forms a part of it. This has the advantage of reducing the number of pieces, but is apt to have one or more of the disadvantages named above. Metal keys or wooden wedges are sometimes used, but the majority of designs employ some form of bolted clamp. The form adopted for the experimental ties used by the N.Y.C. & H. R. R. R. (see Plate VI) is especially ingenious in the method used to vary the gauge or allow for inaccuracies of manufacture. Plate VI shows some of the methods of fastening adopted on the principal types of ties.

222. Cost. The cost of metal cross-ties in Germany averages about 1.6 c. per pound or about \$1.60 for a 100-lb. tie. The ties manufactured for the N. Y. C. & H. R. R. R. in 1892 weighed about 100 lbs. and cost \$2.50 per tie, but if they had been made in larger quantities and with the present price of steel the cost would possibly have been much lower. The item of freight from the place of manufacture to the place where used is no inconsiderable item of cost with some roads. Metal cross-ties have been used by some street railroads in this country. Those used on the Terre Haute Street Railway weigh 60 pounds and cost about 66 c. for the tie, or 74 c. per tie with the fastenings.

223. Bowls or plates. As mentioned before, over 12000 miles of railway, chiefly in British India and in the Argentine Republic, are laid with this form of track. It consists essentially of large cast-iron inverted "bowls" laid at intervals under each rail and opposite each other, the opposite bowls being tied together with tie-rods. A suitable chair is riveted or bolted on to the top of each bowl so as to properly hold the rail. Being

\$ 224.

made of cast iron, they are not so subject to corrosion as steel or wrought iron. They have the advantage that when old and worn out their scrap value is from 60% to 80% of their initial cost, while the scrap value of a steel or wrought-iron tie is practically nothing. Failure generally occurs from breakage, the failures from this cause in India being about 0.4% per annum. They weigh about 250 lbs. apiece and are therefore quite expensive in first cost and transportation charges. There are miles of them in India which have already lasted 25 years and are still in a serviceable condition. Some illustrations of this form of tie are shown in Plate VI.

224. Longitudinals.\* This form, the use of which is confined almost exclusively to Germany, is being gradually replaced on many lines by metal cross-ties. The system generally consists of a compound rail of several parts, the upper bearing rail being very light and supported throughout its length by other rails, which are suitably tied together with tie-rods so as to maintain the proper gauge, and which have a sufficiently broad base to be properly supported in the ballast. One great objec-

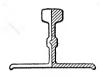


Fig. 110.

tion to this method of construction is the difficulty of obtaining proper drainage especially on grades, the drainage having a tendency to follow along the lines of the rails. The construction is much more complicated on sharp curves and at frogs and switches. Another fundamentally different form of

longitudinal is the Haarman compound "self-bearing" rail, having a base 12" wide and a height of 8", the alternate sections breaking joints so as to form a practically continuous rail.

Some of the other forms of longitudinals are illustrated in Plate VI.

For a very complete discussion of the subject of metal ties, see the "Report on the Substitution of Metal for Wood in Railroad Ties" by E. E. Russell Tratman, it being Bulletin No. 4, Forestry Division of the U. S. Dept. of Agriculture.

<sup>\*</sup> Although the discussion of longitudinals might be considered to be long more properly to the subject of RAILS, yet the essential idea of all designs must necessarily be the *support* of a rail-head on which the rolling stock may run, and therefore this form, unused in this country, will be briefly described here.

224a. Reinforced Concrete Ties.—The wide application of reinforced concrete to various structural purposes, combined with its freedom from decay, has led to its attempted adoption for ties. At present (1908) their use is wholly in the experimental stage. In the annual Proceedings of the American Railway Engineering and Maintenance of Way Association for 1907 is a report on over a dozen different designs, the most of which were shown to be incapable of enduring traffic except on sidings. The ties are particularly subject to fracture if struck by a derailed car. A similar progress report, made in 1911, again indicated that a practicable concrete tie for general use has not yet been invented.

One of the most successful of these ties is the "Buhrer," which consists of one-fourth part of a thirty-foot scrap rail, which is inverted so that the base forms the seat of the running rails. This rail is imbedded in a mass of concrete whose form is somewhat like that of a huge "pole" tie. Several thousands of these are in use on various roads, but many of them have already required renewal and none of them have yet had time to show a service which would make them more economical than wooden ties.

# CHAPTER IX.

# RAILS.

225. Early forms. The first rails ever laid were wooden stringers which were used on very short tram-roads around coalmines. As the necessity for a more durable rail increased. owing chiefly to the invention of the locomotive as a motive power, there were invented successively the cast-iron "fishbelly" rail and various forms of wrought-iron strap rails which finally developed into the T rail used in this country and the double-headed rail, supported by chairs, used so extensively in The cast-iron rails were cast in lengths of about 3 England. feet and were supported in iron chairs which were sometimes set upon stone piers. A great deal of the first railroad track of this country was laid with longitudinal stringers of wood placed upon cross-ties, the inner edge of the stringers being protected by wrought iron straps. The "bridge" rails were first rolled in this country in 1844. The "pear" section was an approach to the present form, but was very defective on account of the difficulty of designing a good form of joint. The "Stevens" section was designed in 1830 by Col. Robert L. Stevens, Chief Engineer of the Camden and Amboy Railroad; although quite defective in its proportions, according to the present knowledge of the requirements, it is essentially the present form. In 1836, Charles Vignoles invented essentially the same form in England; this form is therefore known throughout England and Europe as the Vignoles rail.

226. Present standard forms. The larger part of modern railroad track is laid with rails which are either "T" rails or the double-headed or "bull-headed" rails which are carried in chairs. The double-headed rail was designed with  $\circ$  symmetrical form with the idea that after one head had been worn out by traffic the rail could be reversed, and that its life would be practically doubled. Experience has shown that the wear of the

256

rail in the chairs is very great; so much so that when one head has been worn out by traffic the whole rail is generally useless.

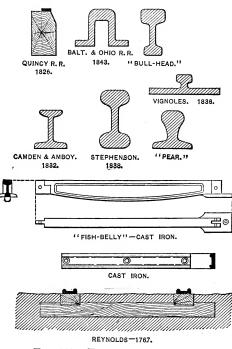


FIG. 111.-EARLY FORMS OF RAILS.

If the rail is turned over, the worn places, caused by the chairs, make a rough track and the rail appears to be more brittle and subject to fracture, possibly due to the crystallization that may have occurred during the previous usage and to the reversal of stresses in the fibers. Whatever the explanation, experience has



FIG. 112. — BULL-HEADED RAIL AND CHAIR. demonstrated the *fact*. The "bull-headed" rail has the lower head only large enough to properly hold the wooden keys with which the rail is secured to the chairs (see Fig. 112) and furnish the necessary strength. The use of these rails requires the use of two cast-iron chairs for each tie. It is claimed that

such track is better for heavy and fast traffic, but it is more

expensive to build and maintain. It is the standard form of track in England and some parts of Europe.

Until a few years ago there was a very great multiplicity in the designs of "T" rails as used in this country, nearly every prominent railroad having its own special design, which perhaps differed from that of some other road by only a very minute and insignificant detail, but which nevertheless would require a complete new set of rolls for rolling. This certainly must have had a very appreciable effect on the cost of rails. In 1893, the American Society of Civil Engineers, after a very exhaustive investigation of the subject, extending over several years. having obtained the opinions of the best experts of the country. adopted a series of sections which have been very extensively adopted by the railroads of this country. Instead of having the rail sections for various weights to be geometrically similar figures, certain dimensions are made constant, regardless of the It was decided that the metal should be distributed weight. through the section in the proportions of-head 42%, web 21%, and flange 37%. The top of the head should have a radius of

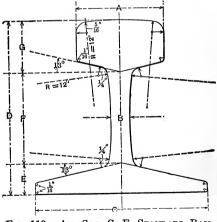


FIG. 113.-AM. Soc. C. E. STANDARD RAIL SECTION.

12"; the top corner radius of head should be  $\frac{5}{16}$ "; the lower corner radius of head should be  $\frac{1}{16}$ "; the corners of the flanges,  $\frac{1}{16}$ " radius; side radius of web, 12"; top and bottom radii of web corners,  $\frac{1}{4}$ "; and angles with the horizontal of the under side

#### RAILS.

# § 227.

of the head and the top of the flange, 13°. The sides of the head are vertical.

The height of the rail (D) and the width of the base (C) are always made equal to each other.

		Weight per Yard.											
	40	45	50∙	55	60	65	70	75	80	85	90	95	10 <b>0</b>
A	17"	2″	$2\frac{1}{8}''$	21″	23"	$2\frac{13''}{32}$	277"	$2\frac{15''}{32}$	$2\frac{1}{2}''$	2 9″	2§″	$2\frac{11''}{16''}$	23*
В	25 64	27 64	7 16	$\frac{15}{32}$	31 64	1/2	33 64	$\frac{17}{32}$	35 64	រទ	18 18	9 16	9 18
C & D	3 <del>1</del>	$3\frac{11}{16}$	3 <del>7</del>	41 <sup>1</sup> 6	41	$4\frac{7}{16}$	4§	$4\frac{13}{16}$	<b>5</b>	$5^{3}_{16}$	5흫	$5_{16}^{9}$	$5\frac{2}{4}$
E	뤃	$\frac{21}{32}$	11	23 32	<u>49</u> 64	$\frac{25}{32}$	18	$\frac{27}{32}$	풓	57 64	<u>59</u> 64	$\frac{15}{16}$	$\frac{31}{32}$
F	185	$1\frac{31}{32}$	$2_{16}^{1}$	$2\frac{11}{64}$	$2\frac{17}{64}$	$2\frac{3}{8}$	$2\frac{15}{32}$	$2\frac{35}{64}$	2 <del>§</del>	$2\frac{3}{4}$	$2\frac{55}{64}$	$2\frac{63}{64}$	355
G	1 54	$1\frac{1}{16}$	1 <del>1</del>	162	$1\frac{7}{32}$	$1\frac{9}{32}$	$1\frac{11}{32}$	127	$1\frac{1}{2}$	135	$1\frac{19}{32}$	$1\frac{41}{64}$	125
		1											

The chief features of disagreement among railroad men relate to the radius of the upper corner of the head and the slope of the side of the head. The radius  $(\frac{5}{16}'')$  adopted for the upper corner (constant for all weights) is a little more than is advocated by those in favor of "sharp corners" who often use a radius of  $\frac{1}{4}''$ . On the other hand it is much less than is advocated by those

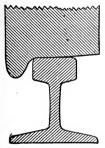


FIG. 114.—RELATION OF RAIL TO WHEEL-TREAD. who consider that it should be nearly equal to (or even greater than) the larger radius universally adopted for the corner of the wheel-flange. The discussion turns on the relative rapidity of rail wear and the wear of the wheel-flanges as affected by the relation of the form of the wheel-tread to that of the rail. It is argued that sharp rail corners wear the wheel-flanges so as to produce sharp flanges, which are liable to cause derailment at switches and also to require that the tires of engine-drivers

must be more frequently turned down to their true form. On the other hand it is generally believed that rail wear is much less rapid while the area of contact between the rail and wheel-flange is small, and that when the rail has worn down, as it invariably does, to nearly the same form as the wheel-flange, the rail wears away very quickly.

227. Weight for various kinds of traffic. The heaviest rails in regular use weigh 100 lbs. per yard, and even these are only used on some of the heaviest traffic sections of such roads as the

N. Y. Central, the Pennsylvania, the N. Y., N. H. & H., and a few others. Probably the larger part of the mileage of the country is laid with 60- to 75-lb. rails-considering the fact that "the larger part of the mileage" consists of comparatively lighttraffic roads and may exclude all the heavy trunk lines. Very light-traffic roads are sometimes laid with 56-lb. rails. Roads with fairly heavy traffic generally use 75- to 85-lb. rails, especially when grades are heavy and there is much and sharp curvature. The tendency on all roads is toward an increase in the weight, rendered necessary on account of the increase in the weight and capacity of rolling stock, and due also to the fact that the price of rails has been so reduced that it is both better and cheaper to obtain a more solid and durable track by increasing the weight of the rail rather than by attempting to support a weak rail by an excessive number of ties or by excessive track labor in tamping. It should be remembered that in buying rails the mere weight is, in one sense, of no importance. The important thing to consider is the STRENGTH and the STIFFNESS. Tf we assume that all weights of rails have similar cross-sections (which is nearly although not exactly true), then, since for beams of similar cross-sections the strength varies as the cube of the homologous dimensions and the stiffness as the fourth power, while the area (and therefore the weight per unit of length) only varies as the square, it follows that the stiffness varies as the square of the weight, and the strength as the 3 power of the Since for ordinary variations of weight the price per weight. ton is the same, adding (say) 10% to the weight (and cost) adds 21% to the stiffness and over 15% to the strength. As another illustration, using an 80-lb. rail instead of a 75-lb. rail adds only  $6\frac{2}{5}\%$  to the cost, but adds about 14% to the stiffness and nearly 11% to the strength. This shows why heavier rails are more economical and are being adopted even when they are not absolutely needed on account of heavier rolling stock. The stiffness. strength, and consequent durability are increased in a much greater ratio than the cost.

228. Effect of stiffness on traction. A very important but generally unconsidered feature of a stiff rail is its effect on tractive force. An extreme illustration of this principle is seen when a vehicle is drawn over a soft sandy road. The constant compression of the sand in front of the wheel has virtually the same effect on traction as drawing the wheel up a grade whose

steepness depends on the radius of the wheel and the depth of the rut. On the other hand, if a wheel, made of perfectly elastic material, is rolled over a surface which, while supported with absolute rigidity, is also perfectly elastic, there would be a forward component, caused by the expanding of the compressed metal just behind the center of contact, which would just balance the backward component. If the rail was supported throughout its length by an absolutely rigid support, the high elasticity of the wheel-tires and rails would reduce this form of resistance to an insignificant quantity, but the ballast and even the ties are comparatively inelastic. When a weak rail yields, the ballast is more or less compressed or displaced, and even though the elasticity of the rail brings it back to nearly its former place, the work done in compressing an inelastic material is wholly lost. The effect of this on the fuel account is certainly very considerable and yet is frequently entirely overlooked. Tt is practically impossible to compute the saving in tractive power, and therefore in cost of fuel, resulting from a given increase in the weight and stiffness of the rail, since the yielding of the rail is so dependent on the spacing of the ties, the tamping, etc. But it is not difficult to perceive in a general way that such an economy is possible and that it should not be neglected in considering the value of stiffness in rails.

229. Length of rails. The recommended standard minimum length of rails is 33 feet. In recent years many roads have been trying 45-foot and even 60-foot rails. The argument in favor of longer rails is chiefly that of the reduction in track-joints, which are costly to construct and to maintain and are a fruitful source of accidents. Mr. Morrison of the Lehigh Valley R. R.\* declares that, as a result of extensive experience with 45-foot rails on that road, he finds that they are much less expensive to handle, and that, being so long, they can be laid around sharp curves without being curved in a machine, as is necessary with the shorter rails. The great objection to longer rails lies in the difficulty in allowing for the expansion, which will require, in the coldest weather, an opening at the joint of nearly  $\frac{3}{4}$ " for a 60-foot rail. The Pennsylvania R. R. and the Norfolk and Western R. R. each have a considerable mileage laid with 60-foot rails.

<sup>\*</sup> Report, Roadmasters Association, 1895.

230. Expansion of rails. Steel expands at the rate of .0000065 of its length per degree Fahrenheit. The extreme range of temperature to which any rail will be subjected will be about 160°, or say from  $-20^{\circ}$  F. to  $+140^{\circ}$  F. With the above coefficient and a rail length of 60 feet the expansion would be 0.0624 foot, or about  $\frac{3}{4}$  inch. But it is doubtful whether there would ever be such a range of motion even if there were such a range of temperature. Mr. A. Torrey, chief engineer of the Mich. Cent. R. R., experimented with a section over 500 feet long, which, although not a single rail, was made "continuous" by rigid splicing, and he found that there was no appreciable additional contraction of the rail at any temperature below  $+20^{\circ}$  F. The reason is not clear, but the *fact* is undeniable.

The heavy girder rails, used by the street railroads of the country, are bonded together with perfectly tight rigid joints which do not permit expansion. If the rails are laid at a temperature of 60° F. and the temperature sinks to 0°, the rails have a tendency to contract .00039 of their length. If this tendency is resisted by the friction of the pavement in which the rails are buried, it only results in a tension amounting to .00039 of the modulus of elasticity, or say 10920 pounds per square inch. assuming 28 000 000 as the modulus of elasticity. This stress is not dangerous and may be permitted. If the temperature rises to 120° F., a tendency to expansion and buckling will take place, which will be resisted as before by the pavement, and a compression of 10920 pounds per square inch will be induced, which will likewise be harmless. The range of temperature of rails which are buried in pavement is much less than when they are entirely above the ground and will probably never reach the above extremes. Rails supported on ties which are only held in place by ballast must be allowed to expand and contract almost freely, as the ballast cannot be depended on to resist the distortion induced by any considerable range of temperature, especially on curves.

231. Rules for allowing for temperature. Track regulations generally require that the track foremen shall use iron (not wooden) shims for placing between the ends of the rails while splicing them. The thickness of these shims should vary with the temperature. Some roads use such approximate rules as the following: "The proper thickness for coldest weather is  $\frac{5}{16}$  of an inch; during spring and fall use  $\frac{1}{8}$  of an inch, and in the very

hottest weather  $\frac{1}{16}$  of an inch should be allowed." This is on the basis of a 30-foot rail. When a more accurate adjustment than this is desired, it may be done by assuming some very high temperature (100° to 125° F.) as a maximum, when the joints should be *tight*; then compute in tabular form the spacing for each temperature, varying by 25°, allowing 0".0643 (very nearly  $\frac{1}{16}$ ") for each 25° change. Such a tabular form would be about as follows (rail length 33 feet):

Temperature	Over 100°	100°–75°	75°–50°	50°–25°	25°-0°	Below 0°
Rail opening	Close	16″	18''	$\frac{3}{16}''$	14″	<u>5</u> ////

One practical difficulty in the way of great refinement in this work is the determination of the real temperature of the rail when it is laid. A rail lying in the hot sun has a very much higher temperature than the air. The temperature of the rail cannot be obtained even by exposing a thermometer directly to the sun, although such a result might be the best that is easily obtainable. On a cloudy or rainy day the rail has practically the same temperature as the air; therefore on such days there need be no such trouble.

232. Chemical composition.— About 98 to 99.5% of the composition of steel rails is iron, but the value of the rail, as a rail, is almost wholly dependent upon the large number of other chemical elements which are, or may be, present in very small amounts. The manager of a steel-rail mill once declared that their aim was to produce rails having in them—

Carbon	0.32 to $0.40%$
Silicon	0.04 to 0.06%
Phosphorus.	0.09 to 0.105%
Manganese	1.00 to 1.50%

The analysis of 32 specimens of rails on the Chic., Mil. & St. Paul R. R. showed variations as follows:

Carbon	0.211	to $0.52\%$
Silicon	0.013	to 0.256%
Phosphorus	0.055	to 0.181%
Manganese	0.35	to 1.63%

These quantities have the same general relative proportions as the rail-mill standard given above, the differences lying mainly in the broadening of the limits. Increasing the percentage of carbon by even a few hundredths of one per cent makes the rail harder, but likewise more brittle. If a track is well ballasted and not subject to heaving by frost, a harder and more brittle rail may be used without excessive danger of breakage, and such a rail will wear much longer than a softer tougher rail, although the softer tougher rail may be the better rail for a road having a less perfect roadbed.

A small but objectionable percentage of sulphur is sometimes found in rails, and very delicate analysis will often show the presence, in very minute quantities, of several other chemical elements. The use of a very small quantity of nickel or aluminum has often been suggested as a means of producing a more durable rail. The added cost and the uncertainty of the amount of advantage to be gained has hitherto prevented the practical use or manufacture of such rails.

233. Proposed standard specifications for steel rails. The following specifications for steel rails are those proposed by a committee of the American Railway Engineering Association in March, 1910:

## PROCESS OF MANUFACTURE.

1. The entire process of manufacture shall be in accordance with the best current state of the art.

(a) Ingots shall be kept in a vertical position until ready to be rolled, or until the metal in the interior has had time to solidify.

(b) Bled ingots shall not be used.

# CHEMICAL COMPOSITION.

2. The chemical composition of the steel from which the rails are rolled shall be within the following limits:

	Bess	emer.	Open-hearth.			
	80 lbs. and under.	85 to 100 lbs. inclusive.	80 lbs. and under.	85 to 100 lbs. inclusive.		
Carbon Manganese Silicon Bhearbarus pot to or	0.80 to 1.10 0.10 to 0.20	0.45 to 0.55 0.85 to 1.15 0.10 to 0.20	0.75 to 1.00	0.63 to 0.76 0.75 to 1.00 0.10 to 0.20		
Phosphorus not to ex- ceed Sulphur not to exceed .	0.10	0.10 0:075	0.04 0.06	0.04 0.06		

RAILS.

3. When lower phosphorus can be secured in Bessemer or open-hearth steel, the carbon shall be increased at the rate of 0.035 for each 0.01 reduction in phosphorus.

The percentages of carbon, manganese, and silicon in an entire order of rails shall average as high as the mean percentages between the upper and lower limits.

### SHEARING.

4. There shall be sheared from the end of the bloom formed from the top of the ingot, sufficient discard to insure sound rails. All metal from the top of the ingot, whether cut from the bloom or the rail, is the top discard.

#### SHRINKAGE.

5. The number and passes and speed of train shall be so regulated that, on leaving the rolls at the final pass, the temperature of the rails will not exceed that which requires a shrinkage allowance at the hot saws, for a 33-ft. rail of 100 lbs. section of  $6\frac{1}{2}$  ins., and  $\frac{1}{8}$  in. less for each 10 lbs. decrease of section, these allowances to be decreased at the rate of  $\frac{1}{100}$  in. for each second. of time elapsed between the rail leaving the finishing rolls and being sawed. The bars shall not be held for the purpose of reducing their temperature, nor shall any artificial means of cooling them be used between the leading and finishing passes, nor after they leave the finishing pass.

#### SECTION.

6. The section of rail shall conform as accurately as possible to the templet furnished by the railroad company. A variation in height of  $\frac{1}{64}$  in. less or  $\frac{1}{32}$  in. greater than the specified height, and  $\frac{1}{16}$  in. in width of flange, will be permitted; but no variations shall be allowed in the dimensions affecting the fit of splice bars.

#### WEIGHT.

7. The weight of the rail shall be maintained as nearly as possible, after complying with the preceding paragraph, to that specified in the contract.

A variation of one-half of one per cent from the calculated

weight of section, as applied to an entire order, will be allowed.

Rails will be accepted and paid for according to actual weight.

#### LENGTH.

8. The standard length of rail shall be 33 ft. Ten per cent of the entire order will be accepted in shorter lengths varying as follows: 30 ft., 28 ft., and 26 ft. A variation of  $\frac{1}{4}$  in. from the specified length will be allowed.

All No. 1 rails less than 33 ft. shall be painted green on both ends.

#### STRAIGHTENING.

9. Care shall be taken in hot-straightening rails, and it shall result in their being left in such condition that they will not vary throughout their entire length more than four (4) ins. from a straight line in any direction when delivered to the cold-straightening presses. Those which vary beyond that amount, or have short kinks, shall be classed as second quality rails and be so marked. The distance between supports of rails in the straightening press shall not be less than forty-two (42) ins.; supports to have flat surfaces and out of wind. Rails shall be straight in line and surface and smooth on head when finished, final straightening being done while cold. They shall be sawed square at ends, variations to be not more than  $\frac{1}{32}$  in., and prior to shipment shall have the burr caused by the saw cutting removed and the ends made clean.

#### DRILLING.

10. Circular holes for joint bolts shall be drilled in accordance with specifications of the purchaser. They shall in every respect conform accurately to drawing and dimensions furnished and shall be free from burrs.

#### BRANDING.

11. The name of the maker, the weight of the rail, and the month and year of manufacture shall be rolled in raised letters and figures on the side of the web. The number of the heat and a letter indicating the portion of the ingot from which the rail was made shall be plainly stamped on the web of each rail, where it will not be covered by the splice bars. Rails to be lettered

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#### RAILS.

consecutively A, B, C, etc., the rail from the top of the ingot being A. In case of a top discard of twenty or more per cent the letter A will be omitted. Open-hearth rails to be branded "O. H."

## DROP TESTS.

12. Drop tests shall be made on pieces of rail rolled from the top of the ingot, not less than four (4) ft. and not more than six (6) ft. long, from each heat of steel. These test pieces shall be cut from the rail bar next to either end of the top rail, as selected by the inspector.

The temperature of the test piece shall be between forty (40) and one hundred (100) degrees Fahrenheit.

The test pieces shall be placed head upward on solid supports, five (5) ins. top radius, three (3) ft. between centers, and subjected to impact tests, the tup falling free from the following heights:

60- and 70-lb. rail	16 ft.
80-, 85-, and 90-lb. rail	18 ft.
100-lb. rail	20 ft.

The test pieces which do not break under the first drop shall be nicked and tested to destruction.

## DEFLECTION.

13. It is proposed to prescribe, under this head, the requirements in regard to deflection, fixing maximum and minimum limits, as soon as proper deflection limits have been decided on.

(a) Two pieces shall be tested from each heat of steel. If either of these test pieces breaks, a third piece shall be tested. If two of the test pieces break without showing physical defect, all rails of the heat will be rejected absolutely. If two of the test pieces do not break, all rails of the heat will be accepted as No. 1 or No. 2 classification, according as the deflection is less or more, respectively, than the prescribed limit.\*

(b) If, however, any test piece broken under test "A" shows physical defect, the top rail from each ingot of that heat shall be rejected.

(c) Additional tests shall then be made of test pieces selected by the inspector from the top end of any second rails of the same

<sup>\*</sup> This clause to be added when the deflection limits are specified.

heat. If two of out three of these second test pieces break, the remainder of the rails of the heat will also be rejected. If two out of three of these second test pieces do not break, the remainder of the rails of the heat will be accepted, provided they conform to the other requirements of these specifications, as No. 1 or No. 2 classification, according as the deflection is less or more, respectively, than the prescribed limit.\*

(d) If any test piece, test "A," does not break, but when nicked and tested to destruction shows interior defect, the top rails from each ingot of that heat shall be rejected.

#### DROP-TESTING MACHINE.

14. The drop-testing machine shall be the standard of the American Railway Engineering and Maintenance of Way Association, and have a tup of 2000 lbs. weight, the striking face of which shall have a radius of five (5) ins.

The anvil block shall be adequately supported and shall weigh 20 000 lbs.

The supports shall be a part of or firmly secured to the anvil.

# NO. 1 RAILS.

15. No. 1 rails shall be free from injurious defects and flaws of all kinds.

# NO. 2 RAILS.

16. Rails which, by reason of surface imperfections, are not accepted as No. 1 rails, will be classed as No. 2 rails, but rails which in the judgment of the inspector contain physical defects which impair their strength, shall be rejected.

No. 2 rails to the extent of five (5) per cent of the whole order will be received. All rails accepted as No. 2 rails must have the ends painted white, and shall have two prick punch marks on the side of the web near the heat number near the end of the rail, so placed as not to be covered by the splice bars.

Rails improperly drilled or straightened, or from which the burrs have not been properly removed, shall be rejected, but may be accepted after being properly finished.

All classes of rails must be kept separate from each other and shipped in separate cars.

All rails must be loaded in the presence of the inspector.

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<sup>\*</sup> This clause to be added when the deflection limits are specified.

#### INSPECTION.

17. (a) Inspectors representing the purchaser shall have free entry to the works of the manufacturer at all times while the contract is being executed, and shall have all reasonable facilities afforded them by the manufacturer to satisfy them that the rails have been made in accordance with the terms of the specifications.

(b) For Bessemer steel the manufacturer shall, before the rails are shipped, furnish the inspector daily with carbon determinations for each heat, and two complete chemical analyses every twenty-four hours representing the average of the other elements contained in the steel, for each day and night turn. These analyses shall be made on drillings taken from small test ingots. The drillings for analyses shall be taken from the ladle test ingot at a distance of  $\frac{1}{4}$  in. beneath the surface.

For open-hearth steel, the makers shall furnish the inspectors with the complete chemical analysis for each melt.

(c) On request of the inspector, the manufacturer shall furnish a portion of the test ingot for check analysis.

(d) All tests and inspections shall be made at the place of manufacture, prior to shipment, and shall be so conducted as not to unnecessarily interfere with the operation of the mill.

(e) Rails to be accepted must meet all of the requirements of the specifications.

234. Rail wear on tangents. When the wheel loads on a rail are abnormally heavy, and particularly when the rail has but little carbon and is unusually soft, the concentrated pressure

on the rail is frequently greater than the elastic limit, and the metal "flows" so that the head, although greatly abraded, will spread somewhat outside of its original lines, as shown in Fig. 115. The rail wear that occurs on tangents is almost exclusively on top. Statistics show that the rate of rail wear on tangents decreases as the rails are more worn. Tests of a large number of

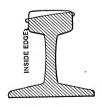


FIG. 115.

rails on tangents have shown a rail wear averaging nearly one pound per yard per 10 000 000 tons of traffic. There is about 33 pounds of metal in one yard of the head of an 80-lb. rail. As an extreme value this may be worn down one-half, thus giving a tonnage of 165 000 000 tons for the life of the rail. Other estimates bring the tonnage down to 125 000 000 tons. Since the locomotive is considered to be responsible for one-half (and possibly more) of the damage done to the rail, it is found that the rate of wear on roads with shorter trains is more rapid in proportion to the tonnage, and it is therefore thought that the life of a rail should be expressed in terms of the number of trains. This has been estimated at 300 000 to 500 000 trains.

235. Rail wear on curves. On curves the maximum rail wear occurs on the inner side of the head of the outer rail, giving a worn form somewhat as shown in Fig. 116. The dotted line

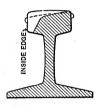


FIG. 116.

shows the nature and progress of the rail wear on the inner rail of a curve. Since the pressure on the outer rail is somewhat lateral rather than vertical, the "flow" does not take place to the same extent, if at all, on the outside, and whatever flow would take place on the inside is immediately worn off by the wheel-flange. Unlike the wear on tangents, the wear on curves is at a greater rate as the rail becomes more worn.

The inside rail on curves wears chiefly on top, the same as on a tangent, except that the wear is much greater owing to the longitudinal slipping of the wheels on the rail, and the lateral slipping that must occur when a rigid four-wheeled truck is guided around a curve. The outside rail is subjected to a greater or less proportion of the longitudinal slipping, likewise to the lateral slipping, and, worst of all, to the grinding action of the flange of the wheel, which grinds off the side of the head.

The results of some very elaborate tests, made by Mr. A M. Wellington, on the Atlantic and Great Western R. R., on the wear of rails, seem to show that the rail wear on curves may be expressed by the formula: "Total wear of rails on a d degree curve in pounds per yard per 10 000 000 tons  $duty = 1 + 0.03d^2$ ." "It is not pretended that this formula is strictly correct even in theory, but several theoretical considerations indicate that it may be nearly so." According to this formula the average rail wear on a 6° curve will be about twice the rail wear on a tan-While this is approximately true, the various causes gent. modifying the rate of rail wear (length of trains, age and quality of rails, etc.) will result in numerous and large variations from the above formula, which should only be taken as indicating an approximate law.

236. Cost of rails. In 1873 the cost of steel rails was about \$120 per ton, and the cost of iron rails about \$70 per ton Although the steel rails were at once recognized as superior to iron rails on account of more uniform wear, they were an expensive luxury. The manufacture of steel rails by the Bessemer process created a revolution in prices, and they steadily dropped in price until, several years ago, steel rails were manufactured and sold for \$22 per ton. For several years past the price has been very uniform at \$28 per ton at the mill. At such prices there is no longer any demand for iron rails, since the cost of manufacturing them is substantially the same as that of steel rails, while their durability is unquestionably inferior to that of steel rails. Rail quotations are generally on the basis of "long tons" of 2240 pounds.

The freight charge for transporting rails from the mill to the place where used is usually so large that it adds a very appreciable amount to the cost per ton. As an approximation, the freight may be estimated as 0.6 c. per ton-mile, or \$3.00 per ton for haul of 500 miles.

# CHAPTER X.

### RAIL-FASTENINGS.

#### RAIL-JOINTS

237. Theoretical requirements for a perfect joint. A perfect rail-joint is one that has the same strength and stiffness-no more and no less-as the rails which it joins, and which will not interfere with the regular and uniform spacing of ties. Tt should also be reasonably cheap both in first cost and in cost of Since the action of heavy loads on an elastic rail maintenance. is to cause a wave of translation in front of each wheel, any change in the stiffness or elasticity of the rail structure will cause more or less of a shock, which must be taken up and resisted by the joint. The greater the change in stiffness the greater the shock, and the greater the destructive action of the shock. The perfect rail-joint must keep both rail-ends truly in line both laterally and vertically, so that the flange or tread of the wheel need not jump or change its direction of motion suddenly in passing from one rail to the other. A consideration of all the above requirements will show that only a perfect welding of rail-ends would produce a joint of uniform strength and stiffness which would give a uniform elastic wave ahead of each wheel. As welding is impracticable for ordinary railroad work (see § 230), some other contrivance is necessary which will approach this ideal as closely as may be.

238. Efficiency of the ordinary angle-bar. Throughout the middle portion of a rail the rail acts as a continuous girder. If we consider for simplicity that the ties are unyielding, the deflection of such a continuous girder between the ties will be but one-fourth of the deflection that would be found if the rail were cut half-way between the ties and an equal concentrated load were divided equally between the two unconnected ends. The maximum stress for the continuous girder would be but one-half of that in the cantilevers. Joining these ends with rail-joints will give the ordinary "suspended" joint. In order to main-

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tain uniform strength and stiffness the angle-bars must supply the deficiency. These theoretical relations are modified to an unknown extent by the unknown and variable yielding of the ties From some experiments made by the Association of Engineers of Maintenance of Way of the P. R. R.\* the following deductions were made:

1. The capacity of a "suspended" joint is greater than that of a "supported" joint—whether supported on one or three ties. (See § 240)

2. That (with the particular patterns tested) the angle-bars alone can carry only 53 to 56% of a concentrated load placed on a joint.

3. That the capacity of the whole joint (angle-bars and rail) is only 524% of the strength of the unbroken rail.

4. That the ineffectiveness of the angle-bar is due chiefly to a deficiency in compressive resistance.

Although it has been universally recognized that the anglebar is not a perfect form of joint, its simplicity, cheapness, and reliability have caused its almost universal adoption. Within a very few years other forms (to be described later) have been adopted on trial sections and have been more and more extended, until their present use is very large. These designs all agree in using metal below the base of the rail, as is shown in the several designs on Plate VII, but the general type shown in Fig. 119 is still (1912) in most common use.

239. Effect of rail gap at joints. It has been found that the jar at a joint is due almost entirely to the *deflection* of the joint and scarcely at all to the small gap required for expansion. This gap causes a drop equal to the versed sine of the arc having a chord equal to the gap and a radius equal to the radius of the wheel. Taking the extreme case (for a 30-foot rail) of a  $\frac{3}{3}$ " gap and a 33" freight-car wheel, the drop is about  $\frac{1}{1000}$ ". In order to test how much the jarring at a joint is due to a gap between the rails, the experiment was tried of cutting shallow notches in the top of an otherwise solid rail and running a locomotive and an inspection car over them. The resulting jarring was practically imperceptible and not comparable to the jar produced at joints. Notwithstanding this fact, many plans have

<sup>\*</sup> Roadmasters Association of America-Reports for 1897.

been tried for avoiding this gap. The most of these plans consist essentially of some form of compound rail, the sections breaking joints. (Of course the design of the compound rail has also several other objects in view.) In Fig. 117 are shown a



FIG. 117.—COMPOUND RAIL SECTIONS.

few of the very many designs which have been proposed. These designs have invariably been abandoned after trial. Another plan, which has been extensively tried on the Lehigh Valley R. R., is the use of mitered joints. The advantages gained by their use are as yet doubtful, while the added expense is unquestionable. The "Roadmasters Association of America" in 1895 adopted a resolution recommending mitered joints for double track, but their use has been abandoned.

240. "Supported," "suspended," and "bridge" joints. In a supported joint the ends of the rails are on a tie. If the angleplates are short, the joint is entirely supported on one tie; if very long, it may be possible to place three ties under one anglebar and thus the joint is virtually supported on three ties rather than one. In a suspended joint the ends of the rails are midway between two ties and the joint is supported by the two. There have always been advocates of both methods, but suspended joints are more generally used than supported joints. The opponents of three-tie joints claim that either the middle tie will be too strongly tamped, thus making it a supported joint, or that, if the middle tie is weakest, the joint becomes a very long (and therefore weak) suspended joint between the outer jointties. or that possibly one of the outer joint-ties gives way, thus breaking the angle-plate at the joint. Another objection which is urged is that unless the bars are very long (say 44 inches, as used on the Mich. Cent. R. R.) the ties are too close for proper tamping. The best answer to these objections is the successful use of these joints on several heavy-traffic roads

"Bridge"-joints are similar to suspended joints in that the joint is supported on two ties, but there is the important difference that the bridge joint supports the rail from *underneath* and there is no transverse stress in the rail, whereas the suspended joint requires the combined transverse strength of both anglebars and rail. A serious objection to bridge-joints lies in the fact of their considerable thickness between the rail base and the tie. When joints are placed "staggered" (as is now the invariable standard practice), rather than "opposite," the ties supporting a bridge-joint must either be notched down, thus weakening the tie and promoting decay at the cut, or else the tie must be laid on a slope and the joint and the opposite rail do not get a fair bearing.

241. Failures of rail-joints. It has been observed on doubletrack roads that the maximum rail wear occurs a few inches beyond the rail gap at the joint in the direction of the traffic. On single-track roads the maximum rail wear is found a few inches each side of the joint rather than at the extreme ends of the rail, thus showing that the rail end deflects down under the wheel until (with fast trains especially) the wheel actually jumps the space and strikes the rail a few inches beyond the joint, the impact producing excessive wear. This action, which is called the "drop," is apt to cause the first tie beyond the joint to become depressed, and unless this tie is carefully watched and maintained at its proper level, the stresses in the angle-bar may actually become reversed and the bar may break at the top. The angle-bars of a suspended joint are normally in compression at the top. The mere reversal of the stresses would cause the bars

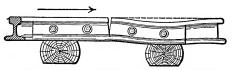
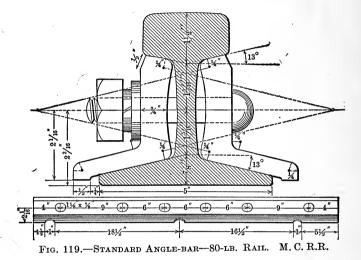


FIG. 118.--EFFECT OF "WHEEL DROP" (EXAGGERATED).

to give way with a less stress than if the stress were always the same in kind. A supported joint, and especially a three-tie joint (see § 240), is apt to be broken in the same manner.

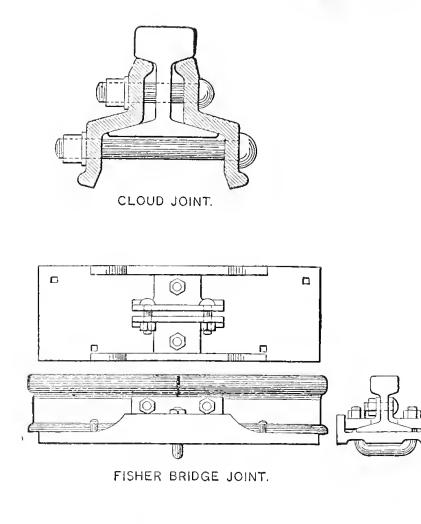
242. Standard angle-bars. An angle-bar must be so made as to closely fit the rails. The great multiplicity in the designs of rails (referred to in Chapter IX) results in nearly as great variety in the detailed dimensions of the angle-bars. The sections here illustrated must be considered only as types of the variable forms necessary for each different shape of rail. The absolutely essential features required for a fit are (1) the angles of the upper and lower surfaces of the bar where they fit against the rail, and (2) the height of the bar. The bolt-holes in the bar and rail must also correspond. The holes in the angle-plates are elongated or made oval, so that the track-bolts, which are

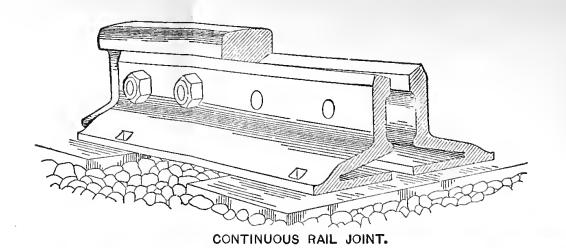


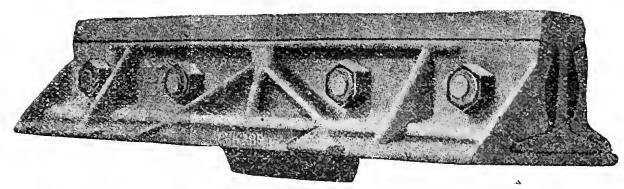
made of corresponding shape immediately under the head, will not be turned by jarring or vibration. The holes in the rails are made of larger diameter (by about  $\frac{3}{16}$ ") than the bolts, so as to allow the rail to expand with temperature.

The proper length of angle-bars has not yet been standardized, but the above dimensions point very closely to the proper length. If the centers of the middle pair of holes in the angleplate are made  $4\frac{7}{8}$  inches apart, and the holes in the rails are  $\frac{3}{16}$  inch larger in diameter than the bolts, it will allow for an extreme variation in the length of the rails of  $\frac{3}{8}$  inch—due to expansion. Adding 4 inches at each end of the joint, from

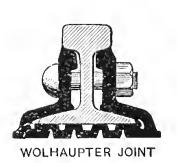
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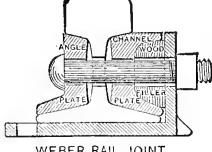






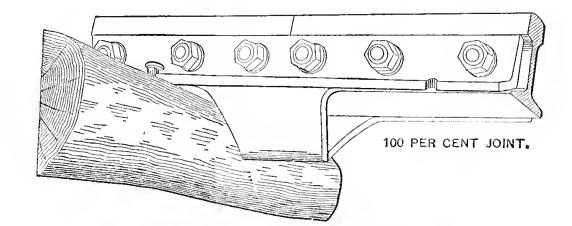
ATLAS SUSPENDED RAIL JOINT.

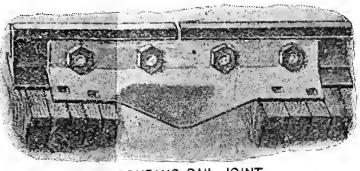




WEBER RAIL JOINT.

PLATE VII.—Some forms of RAIL JOINTS. (Between pp. 274 and 275.)





BONZANO RAIL JOINT.



the center of the last hole to the end of the angle-plate, will make a length of  $22\frac{7}{8}$  inches for a four-hole and  $32\frac{7}{8}$  inches for a six-hole joint. This is considerably less than the M. C. R. R. joint shown above, but this joint was purposely lengthened so that it could be used for a three-tie joint.

243. Later designs of rail-joints. In Plate VII are shown various designs which are competing for adoption. The most prominent of these (judging from the discussion in the convention of the Roadmasters Association of America in 1897) are the "Continuous" and the "Weber." Each of them has been very extensively adopted, and where used are universally preferred to angle-plates. Nearly all the later designs embody more or less directly the principle of the bridge-joint, i.e., support the rail from underneath. An experience of several years will be required to demonstrate which form of joint best satisfies the somewhat opposed requirements of minimum cost (both initial and for maintenance) and minimum wear of rails and rolling stock.

243a. Proposed specifications for steel splice-bars. The following specifications for steel splice-bars were proposed in 1900 by Committee No. 1, American Section, International Association for Testing Materials.

1. Steel for splice-bars may be made by the Bessemer or openhearth process.

2. Steel for splice-bars shall conform to the following limits in chemical composition:

	Per cent.
Carbon shall not exceed	0.15
Phosphorus shall not exceed	0.10
Manganese.	0.30 to $0.60$

3. Splice-bar steel shall conform to the following physical qualities:

Tensile strength, pounds per square inch	54000 to 64000
Yield point, pounds per square inch	32000
Elongation, per cent in eight inches shall not	
be less than	25

4. (a) A test specimen cut from the head of the splice-bar shall bend  $180^{\circ}$  flat on itself without fracture on the outside of the bent portion.

(b) If preferred the bending test may be made on an unpunched splice-bar, which, if necessary, shall be first flattened and shall then be bent  $180^{\circ}$  flat on itself without fracture on the outside of the bent portion.

5. A test specimen of 8-inch gauged length, cut from the head of the splice-bar, shall be used to determine the physical properties specified in paragraph No. 3.

6. One tensile specimen shall be taken from the rolled splicebars of each blow or melt, but in case this develops flaws, or breaks outside of the middle third of its gauged length, it may be discarded and another test specimen submitted therefor.

7. One test specimen cut from the head of the splice-bar shall be taken from a rolled bar of each blow or melt, or if preferred the bending test may be made on an unpunched splice-bar, which, if necessary, shall be flattened before testing. The bending test may be made by pressure or by blows.

8. For the purposes of this specification, the yield point shall be determined by the careful observation of the drop of the beam or halt in the gauge of the testing machine.

9. In order to determine if the material conforms to the chemical limitations prescribed in paragraph No. 2 herein, analysis shall be made of drillings taken from a small test ingot.

10. All splice-bars shall be smoothly rolled and true to templet. The bars shall be sheared accurately to length and free from fins or cracks, and shall perfectly fit the rails for which they are intended. The punching and notching shall accurately conform in every respect to the drawing and dimensions furnished.

11. The name of the maker and the year of manufacture shall be rolled in raised letters on the side of the splice-bar.

12. The inspector representing the purchaser shall have all reasonable facilities afforded to him by the manufacturer, to satisfy him that the finished material is furnished in accordance with these specifications. All tests and inspections shall be made at the place of manufacture, prior to shipment.

#### TIE-PLATES.

244. Advantages. (a) As already indicated in § 204, the life of a soft-wood tie is very much reduced by "rail-cutting" and "spike-killing," such tics frequently requiring renewal long

before any serious decay has set in. It has been practically demonstrated that the "rail-cutting" is not due to the mere pressure of the rail on the tie, even with a maximum load on the rail, but is due to the impact resulting from vibration and to the longitudinal working of the rail. It has been proved that this rail-cutting is practically prevented by the use of tieplates. (b) On curves there is a tendency to overturn the outer rail due to the lateral pressure on the side of the head. This produces a concentrated pressure of the outer edge of the base on the tie which produces rail-cutting and also draws the inner spikes. Formerly the only method of guarding against this was by the use of "rail-braces," one pattern of which is shown in Fig. 120. But it has been found that tie-plates serve the purpose even better, and rail-braces have been abandoned where tie-plates are used. (c) Driving spikes through holes in the plate enables the spikes on each side of the rail to mutually support each other, no matter in which (lateral) direction the rail may tend to move, and this probably accounts in large

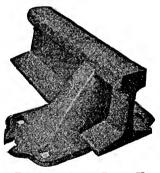
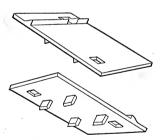


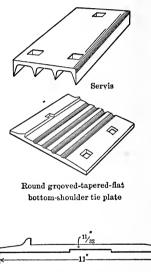
FIG. 120.-ATLAS BRACE K.

measure for the added stability obtained by the use of tie-plates. (d) The wear in spikes, called "necking," caused by the vertical vibration of the rail against them, is very greatly reduced. (e) The cost is very small compared with the value of the added life of the tie, the large reduction in the work of track maintenance, and the smoother running on the better track which is obtained. It has been estimated that by the use of tie-plates the life of hard-wood ties is increased from one to three years, and the life of soft-wood ties is increased from three to six years. From the very nature of the case, the value of tie-plates is greater when they are used to protect soft ties. 245. Elements of the design. There is still a great diversity of opinion regarding the relative advantages of tie-plates which are flat on the bottom and those which are corrugated or provided with teeth or claws which are imbedded in the tie. Those used in Europe are without exception flat on the bottom. The Pennsylvania Railroad and the Southern Pacific have also been using flat tie-plates. On the other hand, it is claimed that the pressure required to force a corrugated plate into a tie is about 20% greater than that required to imbed a flat



Wolhaupter







Claw and shoulder tie plate

FIG. 121.-VARIOUS FORMS OF TIE-PLATES.

plate of equal thickness in the tie. It is also claimed that tests have shown that the force required to spread the rails when they are fastened with corrugated plates under the rails is from 36% to 100% greater than that required when a flat tie-plate is used. It is especially important that the plate shall be so firmly imbedded in the tie that it cannot move or "rock" with each motion of the rail over it. Instances are known where a treated tie has become unfit for service because § 245.

the tie-plate has rocked back and forth until it has worn a hole in the tie. Rain-water filling this hole has leached out the zinc chloride, and the tie has decayed at this point and become unserviceable, when the remainder of the tie showed no decay. The creeping of the rails over the ties is sometimes the cause of failure of ties which have been effectually secured against decay by the use of preservatives. This particular form of tie deterioration has been guarded against on a French railroad by using a tie-plate made of *creosoted* wood, which is 8 inches long, the same width as the width of the base of the rail. and 1 inch thick. Such wooden plates, which will last a year and a half to two years, are made of poplar, or any other hard wood, and cost about \$2.00 per thousand. It should be observed that they are used in connection with wooden screws instead of the ordinary track spikes. When they are worn out, it is only necessary to turn the screw one or two upward turns; the new plate may then be put in endwise and the screwspikes again fastened down.

A fault of the earlier designs of metal tie-plates was that they were made of plates which were so thin that they would buckle under the pressure of the rail. The claim made for the corrugated plates is that their transverse stress is far greater than that of a flat plate for the same amount of material; but this is not vital provided the flat plates are made sufficiently thick so that they will not buckle. The tie-plate used on the Southern Pacific Railroad has a slightly beveled surface, the plate being  $\frac{3}{8}$  inch thick under the outer edge of the rail and  $\frac{19}{4}$  inch thick at the inner edge of the rail.

The holes in a tie-plate should be about  $\frac{1}{16}$  inch larger than the size of the intended spike. For example, the holes are generally punched with  $\frac{5}{8}'' \times \frac{3}{4}''$  holes for a  $\frac{9}{16}$  inch spike, or with holes  $\frac{3}{4}$  inch square for a  $\frac{5}{3}$  inch spike. The length of the plate (perpendicular to the rail) should be about 3 inches more than the base of the rail; this usually means about 8 inches. For very heavy traffic, the thickness should be  $\frac{5}{16}$  inch to  $\frac{3}{8}$  inch; for average traffic it may be as thin as  $\frac{1}{4}$  inch; some plates are made only  $\frac{3}{16}$  inch thick. For flat-bottom plates the thickness may be as great as half an inch. The tie-plates under the joint ties must be somewhat longer than the intermediates, in order to allow for the extra length from out to out of the angleplates.

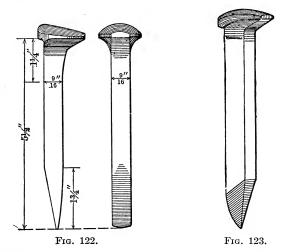
246. Method of setting. A very important detail in the process of setting the tie-plates on the ties is that the plates should be rigidly attached to the ties in their intended position during the process of setting. If tie-plates with flat bottoms are used, the surface of the tie must be adzed, so that it is not only plane but level, so that there will be no danger that the plate will rock on the tie. When using tie-plates which are corrugated on the under surface, it is necessary to force them into the tie until the under side of the plate is flush with the surface of the tie. This requires a pressure of several thousand pounds. Sometimes trackmen have depended on the easy process of waiting for passing trains to force the corrugations into the tie until the plate is in its intended position. Until the plates are finally set the spikes cannot be driven home. and this apparently cheap and easy process generally results in loose spikes and rails. The best method for new work is to drive the plates into the tie before setting the tie in position. A tie-plate gauge holds both tie-plates in their proper relative position, and both plates may be driven by the use of heavy beetles. When it is necessary to place the plate under the rail and drive it in, it is somewhat difficult to drive it by striking the plate with a swage on each side of the rail alternately. When it is struck on one side, the other side flies up unless held down by a wedge driven between the plate and the rail on the other side of the rail. A straddler, which straddles the rail somewhat like an inverted U, is very useful for this purpose. since it makes it possible to strike the head of the straddler and force down both sides of the plate at once. The Southern Pacific Railroad Company has rigged up a small pile-driver on a hand-car, which is used in connection with a straddler to drive the tie-plates into position. Some western railroads have even adopted the process of rigging up a flat car with a machine which will press the tie-plates into place in the ties before the ties are placed in the track.

#### SPIKES.

247. Requirements. The rails must be held to the ties by a fastening which will not only give sufficient resistance, but which will retain its capacity for resistance. It must also be cheap and easily applied. The ordinary track-spike fulfills the last

§ 246.

requirements, but has comparatively small resisting power, compared with screws or bolts. Worse than all, the tendency to



vertical vibration in the rail produces a series of upward pulls on the spike that soon loosens it. When motion has once begun the capacity for resistance is greatly reduced, and but little more vibration is required to pull the spike out so much that redriving is necessary. Driving the spike to place again in the same hole is of small value except as a very temporary expedient, as its holding power is then very small. Redriving the spikes in new holes very soon "spike-kills" the tie. Many plans have been devised to increase the holding power of spikes, such as making them jagged, twisting the spike, swelling the spike at about the center of its length, etc. But it has been easily demonstrated that the fibers of the wood are generally so crushed and torn by driving such spikes that their holding power is less than that of the plain spike.

The ordinary spike (see Fig. 122) is made with a square crosssection which is uniform through the middle of its length, the lower  $1\frac{3}{4}$ " tapering down to a chisel edge, the upper part swelling out to the head. The Goldie spike (see Fig. 123) aims to improve this form by reducing to a minimum the destruction of the fibers. To this end, the sides are made smooth, the edges are clean-cut, and the point, instead of being chisel-shaped, is ground down to a pyramidal form. Such fiber-cutting as occurs is thus accomplished without much crushing, and the fibers are thus pressed away from the spike and slightly downward. Anv tendency to draw the spike will therefore cause the fibers to press still harder on the spike and thus increase the resistance.

248. Driving. The holding power of a spike depends largely If the blows on how it is driven. are eccentric and irregular in direction, the hole will be somewhat enlarged and the holding power largely decreased. The spikes on each side of the rail in any one tie should not be directly opposite, but should Placing them directbe staggered ly opposite will tend to split the tie, or at least decrease the holding power of the spikes. The direction of staggering should be reversed in the two pairs of spikes in any one

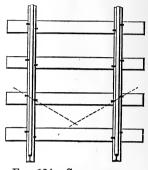
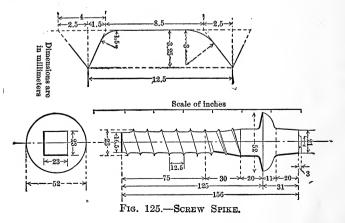


FIG. 124.—SPIKE-DRIVING.

tie (see Fig. 124). This will tend to prevent any twisting of the tie in the ballast, which would otherwise loosen the rail from the tie.

240. Screws and bolts. The use of these abroad is very extensive, but their use in this country has not passed the experimental stage. The screws are "wood"-screws (see Fig. 125).



# § 250.

having large square heads, which are screwed down with a trackwrench. Holes, having the same diameter as the base of the screw-heads, should be first bored into the tie, at exactly the right position and at the proper angle with the vertical. A light wooden frame is sometimes used to guide the auger at the proper angle. Sometimes the large head of the screw bears directly against the base of the rail, as with the ordinary spike. Other designs employ a plate, made to fit the rail on one side, bearing on the tie on the other side, and through which the screw passes. These screws cost much more than the spikes and require more work to put in place, but their holding power is much greater and the work of track maintenance is very much less. Screw-bolts, passing entirely through the tie, having the head at the bottom of the tie and the nut on the upper side, are also used abroad. These are quite difficult to replace, requiring that the ballast be dug out beneath the tie, but on the other hand the

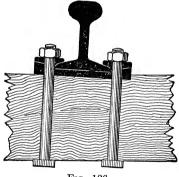


Fig. 126.

occasions for replacing such a bolt are comparatively rare, as their durability is very great. The use of screws or bolts increases the life of the tie by the avoidance of "spike-killing." It is capable of demonstration that the reduced cost of maintenance and the resulting improvement in track would much more than repay the added cost of screws and bolts, but it seems impossible to induce railroad directors to authorize a large and immediate additional expenditure to make an annual saving whose value, although unquestionably considerable, cannot be exactly computed.

250. "Wooden spikes." Among the regulations for tracklaying given in § 208, mention was made of wooden "spikes," or plugs, which are used to fill up the holes when spikes are withdrawn. The value of the policy of filling up these holes is unquestionable, since the expense is insignificant compared with the loss due to the quick and certain decay of the tie if these holes are allowed to fill with water and remain so. But the method of making these plugs is variable. On some roads they are "hand-made" by the trackmen out of otherwise use-

less scraps of lumber, the work being done at odd moments. This policy, while apparently cheap, is not necessarily so, for the hand-made plugs are irregular in size and therefore more or less inefficient. It is also quite probable that if the trackmen are required to make their own plugs, they would spend time on these very cheap articles which could be more profitably employed otherwise. Since the holes made by the spikes are larger at the top than they are near the bottom, the plugs should not be of uniform cross-section but should be slightly wedge-shaped. The "Goldie tie-plug" (see Fig. 127) has been designed to fill these requirements. Being machine-made, they are uniform in size; they are of a shape which will best fit the hole: they can be furnished of any desired wood, and at a cost which makes it a wasteful economy to attempt  $F_{IG}$ . 127.



to cut them by hand.

### TRACK-BOLTS AND NUT-LOCKS.

251. Essential requirements. The track-bolts must have sufficient strength and must be screwed up tight enough to hold the angle-plates against the rail with sufficient force to develop the full transverse strength of the angle-bars. On the other hand the bolts should not be screwed so tight that slipping may not take place when the rail expands or contracts with temperature. It would be impossible to screw the bolts tight enough to prevent slipping during the contraction due to a considerable fall of temperature on a straight track, but when the track is curved, or when expansion takes place, it is conceivable that the resistance of the ties in the ballast to lateral motion may be less than the resistance at the joint. A test to determine this resistance was made by Mr. A. Torrey, chief engineer of the Mich. Cent. R. R., using 80-lb. rails and ordinary angle-bars, the bolts being screwed up as usual. If required a force of about 31000 to

35000 lbs. to start the joint, which would be equivalent to the stress induced by a change of temperature of about 22°. But if the central angle of any given curve is small, a comparatively small lateral component will be sufficient to resist a compression of even 35000 lbs. in the rails. Therefore there will ordinarily be no trouble about having the joints screwed too tight. The vibration caused by the passage of a train reduces the resistance to slipping. This vibration also facilitates an objectionable feature, viz., loosening of the nuts of the track-bolts. The bolt is readily prevented from turning by giving it a form which is not circular immediately under the head and making corresponding holes in the angle-plate. Square holes would answer the purpose, except that the square corners in the holes in the angle-plates would increase the danger of fracture of the plates. Therefore the holes (and also the bolts, under the head) are made of an oval form, or perhaps a square form with rounded corners, avoiding angles in the outline.

The nut-locks should be simple and cheap, should have a life at least as long as the bolt, should be effective, and should not lose their effectiveness with age. Many of the designs that have been tried have been failures in one or more of these particulars as will be described in detail below.

252. Design of track-bolts.—In Fig. 128 is shown a common design of track-bolt. In its general form this represents the

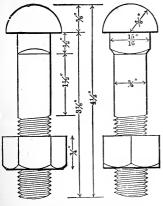


FIG. 128.-TRACK-BOLT.

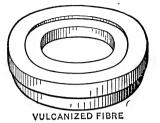
bolt used on nearly all roads, being used not only with the common angle-plates, but also with many of the improved designs of rail-joints. The variations are chiefly a general increase in size to correspond with the increased weight of rails, besides variations in detail dimensions which are frequently unimportant. The diameter is usually  $\frac{3}{4}''$  to  $\frac{7}{4}''$ ; 1" bolts are sometimes used for the heaviest sections of rails. As to length. the bolt should not extend more than  $\frac{1}{2}$  outside of the nut when

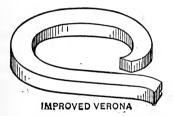
it is screwed up. If it extends farther than this it is liable to be

broken off by a possible derailment at that point. The lengths used vary from  $3\frac{1}{4}''$ , which may be used with 60-lb. rails, to 5'', which is required with 100-lb. rails. The length required depends somewhat on the type of nut-lock used.

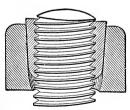
253. Design of nut-locks. The designs for nut-locks may be divided into three classes: (a) those depending entirely on an elastic washer which absorbs the vibration which might otherwise induce turning; (b) those which jam the threads of the bolt and nut so that, when screwed up, the frictional resistance is too great to be overcome by vibration; (c) the "positive" nut-locks-those which mechanically hold the nut from turning. Some of the designs combine these principles to some extent. The "vulcanized fiber" nut-lock is an example of the first class. It consists essentially of a rubber washer which is protected by an iron ring. When first placed this lock is effective, but the rubber soon hardens and loses its elasticity and it is then ineffective and worthless. Another illustration of class (a) is the use of wooden blocks, generally 1" to 2" oak, which extend the entire length of the angle-bar, a single piece forming the washer for the four or six bolts of a joint. This form is cheap, but the wood soon shrinks, loses its elasticity, or decays so that it soon becomes worthless, and it requires constant adjustment to keep it in even tolerable condition. The "Verona" nut-lock is another illustration of class (a) which also combines some of the positive elements of class (c). It is made of tempered steel and, as shown in Fig. 129, is warped and has sharp edges or points. The warped form furnishes the element of elastic pressure when the nut is screwed up. The steel being harder than the iron of the angle-bar or of the nut, it bites into them, owing to the great pressure that must exist when the washer is squeezed nearly flat, and thus prevents any backward movement, although forward movement (or tightening the bolt) is not interfered The "National" nut-lock is a type of the second class (b), with. in which, like the "Harvey" nut-lock, the nut and lock are combined in one piece. With six-bolt angle-bars and 30-foot rails, this means a saving of 2112 pieces on each mile of single track. The "National" nuts are open on one side. The hole is drilled and the thread is cut slightly smaller than the bolt, so that when the nut is screwed up it is forced slightly open and therefore presses on the threads of the bolt with such force that vibration cannot jar it loose. Unlike the "National" nut, the "Harvey"











Columbia Nut Lock

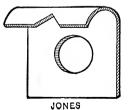


FIG. 123.-TYPES OF NUT-LOCKS.

nut is solid, but the form of the thread is progressively varied so that the thread pinches the thread of the bolt and the frictional resistance to turning is too great to be affected by vibration.

The "Columbia" nut-lock is a two-piece nut, both parts of which must turn simultaneously. As shown in the figure, one section wedges into the other. The greater the tension in the bolt, the greater the wedging action and the greater the friction to prevent turning.

The "Jones" nut-lock, belonging to class (c), is a type of a nut-lock that does not depend on elasticity or jamming of screwthreads. It is made of a thin flexible plate, the square part of which is so large that it will not turn after being placed on the bolt. After the nut is screwed up, the thin plate is bent over so that the re-entrant angle of the plate engages the corner of the nut and thus mechanically prevents any turning. The metal is supposed to be sufficiently tough to endure without fracture as many bendings of the plate as will ever be desired. Nutlocks of class (c) are not in common use.

## CHAPTER XI.

## SWITCHES AND CROSSINGS.

#### SWITCH CONSTRUCTION.

254. Essential elements of a switch. Flanges of some sort are a necessity to prevent car-wheels from running off from the rails on which they may be moving. But the flanges, although a neccssity, are also a source of complication in that they require some special mechanism which will, when desired, guide the wheels out from the controlling influence of the main-line rails. This must either be done by raising the wheels high enough so that the flanges may pass over the rails, or by breaking the continuity of the rails in such a way that channels or "flange spaces" are formed through the rails. An ordinary stub-switch breaks the continuity of the main-line rails in three places, two of them at the switch-block and one at the frog. The Wharton switch avoids two of these breaks by so placing inclined planes that the wheels, rolling on their flanges, will surmount these inclines until they are a little higher than the rails. Then the wheels on the side toward which the switch runs are guided over and across the main rail on that side This rise being accomplished in a short distance, it becomes impracticable to operate these switches except at slow speeds, as any sudden change in the path of the center of gravity of a car causes very destructive jars both to the switch and to the rolling stock. The other general method makes a break in one main rail (or both) at the switch-block. In both methods the wheels are led to one side by means of the "lead rails," and finally one line of wheels passes through the main rail on that side by means of a "frog." There are some designs by which even this break in the main rail is avoided, the wheels being led over the main rail by means of a short movable rail which is on occasion placed across the main rail, but such designs have not come into general use.

255. Frogs. Frogs are provided with two channel-ways or "flange spaces" through which the flanges of the wheels move.

Each channel cuts out a parallelogram from the tread area. Since the wheel-tread is always wider than the rail, the wing rails will support the wheel not only across the space cut out by the channel, but also until the tread has passed the point of the frog and can obtain a broad area of contact on the tongue of the frog. This is the theoretical idea, but it is very imperfectly

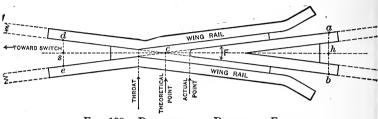


FIG. 130.-DIAGRAMMATIC DESIGN OF FROG.

realized. The wing rails are sometimes subjected to excessive wear owing to "hollow treads" on the wheels-owing also to the frog being so flexible that the point "ducks" when the wheel approaches it. On the other hand the sharp point of the frog will sometimes cause destructive wear on the tread of the wheel. Therefore the tongue of the frog is not carried out to the sharp theoretical point, but is purposely somewhat blunted. But the break which these channels make in the continuity of the tread area becomes extremely objectionable at high speeds, being mutually destructive to the rolling stock and to the frog. The jarring has been materially reduced by the device of "spring frogs"-to be described later. Frogs were originally made of cast iron-then of cast iron with wearing parts of cast steel. which were fitted into suitable notches in the cast iron. This form proved extremely heavy and devoid of that elasticity of track which is necessary for the safety of rolling stock and track at high speeds. The present universal practice is to build the frog up of pieces of rails which are cut or bent as required. These pieces of rails (at least four) are sometimes assembled by riveting them to a flat plate, but this method is now but little used, except for very light work. The usual practice is now chiefly divided between "bolted" and "keyed" frogs. In each case the space between the rails, except a sufficient flange-way, is filled with a cast-iron filler and the whole assemblage of parts



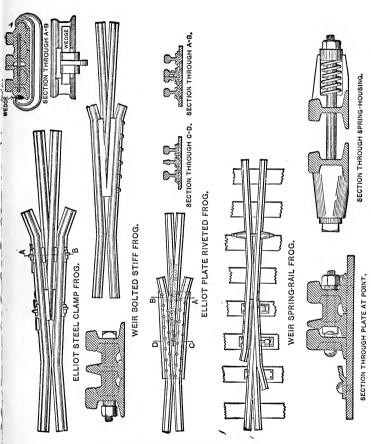


PLATE VIII.-Some Types of Frogs.

is suitably bolted or clamped together, as is illustrated in Plate VIII. The operation of a spring-rail frog is evident from the figure. Since a siding is usually operated at slow speed, while the main track may be operated at fast speed, a spring-rail frog will be so set that the tread is continuous for the main track and broken for the siding. This also means that the spring-rail will only be moved by trains moving at a (presumably) slow speed on to the siding. For the fast trains on the main line such a frog is substantially a "fixed" frog and has a tread which is practically continuous.

256. To find the frog number. The frog number (n) equals the ratio of the distance of any point on the tongue of the frog from the theoretical point of the frog divided by the width of the tongue at that point, i.e.  $=hc \div ab$  (Fig. 130). This value may be directly measured by applying any convenient unit of measure (even a knife, a short pencil, etc.) to some point of the tongue where the width just equals the unit of measure, and then noting how many times the unit of measure is contained in the distance from that place to the theoretical point. But since c, the theoretical point, is not so readily determinable with exactitude, it being the imaginary intersection of the gauge lines, it may be more accurate to measure de, ab, and hs; then n, the frog number,  $=hs \div (ab+de)$ . If the frog angle be called F, then

i.e.,

$$n = hc \div ab = hs \div (ab + de) = \frac{1}{2} \operatorname{cot} \frac{1}{2}F;$$
  

$$\operatorname{cot} \frac{1}{2}F = 2n.$$

257. Stub switches. The use of these, although once nearly universal, has been practically abandoned as turnouts from main track except for the poorest and cheapest roads. In some States their use on main track is prohibited by law. They have the sole merit of cheapness with adaptability to the circumstances of very light traffic operated at slow speed when a considerable element of danger may be tolerated for the sake of economy. The rails from A to B (see Fig. 131\*) are not fastened

<sup>\*</sup> The student should at once appreciate that in Fig. 131, as well as in nearly all the remaining figures in this chapter, it becomes necessary to use excessively large frog angles, short radii, and a very wide gauge in order to illustrate the desired principles with figures which are sufficiently small for the page. In fact, the proportions used in the figures are such that serious mechanical difficulties would be encountered if they were used. These difficulties are here ignored because they can be neglected in the proportions used in practice.

to the ties; they are fastened to each other by tie-rods which keep them at the proper gauge; at and back of B they are

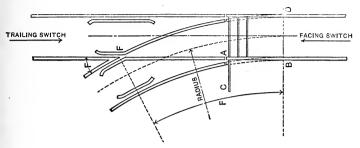


FIG. 131.-STUB SWITCH.

securely spiked to the ties, and at A they are kept in place by the connecting bar (C) fastened to the switch-stand. One great objection to the switch is that, in its usual form, when operated as a trailing switch, a derailment is inevitable if the switch is misplaced. The very least damage resulting from such a derailment must include the bending or breaking of the tie-rods of the switch-rail. Several devices have been invented to obviate this objection, some of which succeed very well mechanically, although their added cost precludes any economy in the total cost of the switch. Another objection to the switch is the looseness of construction which makes the switches objectionable at high speeds. The gap of the rails at the head-block is always considerable, and is sometimes as much as two inches. A driving-

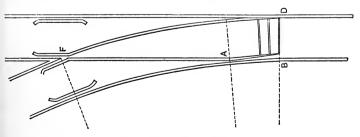


FIG. 132.—POINT SWITCH.

wheel with a load of 12000 to 20000 pounds, jumping this gap with any considerable velocity, will do immense damage to the

§ 258.

farther rail end, besides producing such a stress in the construction that a breakage is rendered quite likely, and such a breakage might have very serious consequences.

**258.** Point switches. The essential principle of a point switch is illustrated in Fig. 132. As is shown, one main rail and also one of the switch-rails is unbroken and immovable. The other main rail (from A to F) and the corresponding portion of the other lead rail are substantially the same as in a stub switch. A portion of the main rail (AB) and an equal length of the opposite lead rail (usually 15 to 24 feet long) are fastened together by tie-rods. The end at A is jointed as usual and the other end is pointed, both sides being trimmed down so that the feather edge at B includes the web of the rail. In order to retain in it as much strength as possible, the point-rail  $\frac{1}{2}$ 

is raised so that it rests on the base of the stock-rail, one side of the base of the point-rail being entirely cut away. As may be seen in Fig. 133, although the influence of the point of the rail in moving the wheel-flange away from the stock-rail is really zero at that point, yet the rail has all the strength of the web and about onehalf that of the base—a very fair angleiron. The planing runs back in *straight* lines, until at about six or seven feet back from the point the full width of the head is

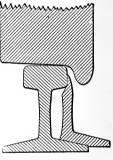


FIG. 133.

obtained. The full width of the base will only be obtained at about 13 feet from the point. The A. R. E. A. standard switch rail is always cut on the basis that the distance between gauge lines at the heel of the switch (the distance MN in Fig. 140) is  $6\frac{1}{4}$  inches and that the "point" is  $\frac{1}{4}$  inch wide. Then, using four standard lengths, 11,  $16\frac{1}{2}$ , 22, and 33 feet, the angles vary from 2° 36′ 19″ to 0° 52′ 05″, as shown in Table III.

259. Switch-stands. The simplest and cheapest form is the "ground lever," which has no target. The radius of the circle described by the connecting-rod pin is precisely one-half the throw. From the nature of the motion the device is practically

self-locking in either position, padlocks being only used to prevent malicious tampering. The numerous designs of upright stands are always combined with targets, one design of which is

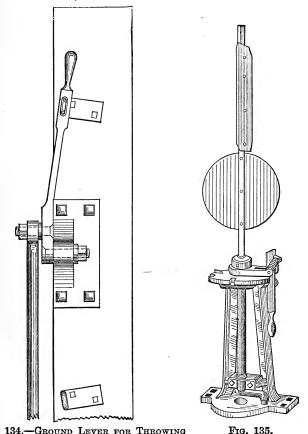
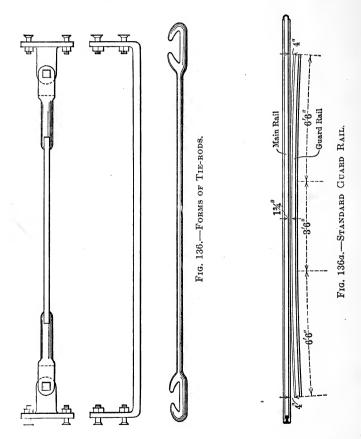


FIG. 134.—GROUND LEVER FOR THROWING A SWITCH.

illustrated in Fig. 135. When the road is equipped with interlocking signals, the switch-throw mechanism forms a part of the design

260. Tie-rods. These are fastened to the webs of the rails by means of lugs which are bolted on, there being usually a hingejoint between the rod and the lug. Four such tie-rods are generally necessary. The first rod is sometimes made without hinges, which gives additional stiffness to the comparatively weak rail-points. The old-fashioned tie-rod, having jaws fitting the base of the rail, was almost universally used in the days of stub switches. One great inconvenience in their use lies in the fact that they must be slipped on, one by one, over the *free* ends of the switch-rails.



261. Guard-rails. As shown in Figs. 131 and 132, guard-rails are used on both the main and switch tracks opposite the frogpoint. Their function is not only to prevent the possibility of

the wheel-flanges passing on the wrong side of the frog-point, but also to save the side of the frog-tongue from excessive wear. The flange-way space between the heads of the guard-rail and wheel-rail should equal  $1\frac{3}{4}$  inches. Since this is less than the space between the heads of ordinary (say 80-pound) rails when placed base to base, to say nothing of the  $\frac{3}{4}$ " required for spikes, it becomes necessary to cut the flange of the guard-rail. The length of the rail should be 16 feet 6 inches, the middle portion being straight for a length of 3 feet 6 inches, and the ends, each being 6 feet 6 inches long, curved out so that the side of the rail head at each end is 4 inches from the main rail head, when the flange-way at the center is  $1\frac{3}{4}$  inches. See Fig. 136a

## MATHEMATICAL DESIGN OF SWITCHES.

In all of the following demonstrations regarding switches, turnouts, and crossovers, the lines are assumed to represent the gauge-lines—i.e., the lines of the *inside* of the head of the rails.

262. Design with circular lead-rails. The simplest method

is to consider that the lead-rails curve out from the main trackrails by arcs of circles which are tangent to the main rails and which extend to the frog-point F. The simple curve from D to F is of such radius that  $(r+\frac{1}{2}g)$  vers F=g, in which F=the frog angle, g=gauge, L=the "lead" (BF), and r=the radius of the center of the switch-rails.

$$\therefore r + \frac{1}{2}g = \frac{g}{\operatorname{vers} F}.$$
 (74)

Also,	$BF \div BD = \cot \frac{1}{2}F;  BD = g;  BF = L.$
	$\therefore  L = g \cot \frac{1}{2}F.  .  .  .  .  .  .  .  .  . $
Also,	$L = (r + \frac{1}{2}g) \sin F;$ (76)
	$QT = 2r \sin \frac{1}{2}F.  .  .  .  .  .  .  .  .  . $

These formulæ involve the angle F. As shown in Table III, the angles (F) are always odd quantities, and their trigonometric functions are somewhat troublesome to obtain closely with

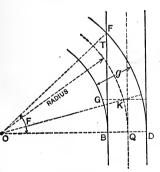


FIG. 137.

ordinary tables. The formulæ may be simplified by substituting the frog-number n, from the relation that  $n = \frac{1}{2} \cot \frac{1}{2}F$ . Since

 $r - \frac{1}{2}g = L \cot F$  and  $r + \frac{1}{2}g = L \operatorname{cosec} F$ ,

then	$r = \frac{1}{2}L$ (cot	F -	+ co	osed	e F	)								
	$=\frac{1}{2}g \cot$	$\frac{1}{2}F($	$\cot$	F -	-cc	sec	$F_{j}$	)						
	$=\frac{1}{2}g \cot^2$	$\frac{1}{2}F$ ,	s	inc	e (d	$\operatorname{ot}$	a +	- co	sec	a)	=c	$\mathbf{ot}$	$\frac{1}{2}a$	
	$=2gn^2$ .		•						•			•		(78)
Also,	L = 2gn, .	•	•	•	•	•	•	•	•	•	•	•		(79)
from which	$r=n \times L$ .	•	•	٠	•	•	•	•	•	•	•	•	•	(80)

These extremely simple relations may obviate altogether the necessity for tables, since they involve only the frog-number and the gauge. On account of the great simplicity of these rules, they are frequently used as they are, regardless of the fact that the curve is never a uniform simple curve from switch-block to frog. In the first place there is a considerable length of the gauge-line within the frog, which is straight unless it is purposely curved to the proper curve while being manufactured, which is seldom if ever done-except for the very large-angled frogs used for street-railway work, etc. It is also doubtful whether the switch-rails (BA, Fig. 131) are bent to the computed curve when the rails are set for the switch. The switch-rails of point switches are straight, thus introducing a stretch of straight track which is about one-fifth of the total length of the lead-rails. The effect of these modifications on the length and radius of the leadrails will be developed and discussed in the next four sections.

The throw (t) of a stub switch depends on the weight of the rail, or rather on the width of its base. The throw must be at least  $\frac{3}{4}''$  more than that width. The head-block should therefore be placed at such a distance from the heel of the switch (B) that the versed sine of the arc equals the throw. These points *must* be opposite on the two rails, but the points on the two rails where these relations are exactly true will not be opposite. Therefore, instead of considering either of the two radii  $(r+\frac{1}{2}g)$  and  $(r-\frac{1}{2}g)$ , the mean radius r is used. Then (see Fig. 137)

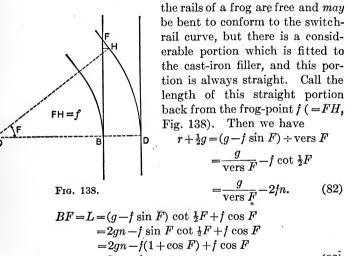
vers  $KOQ = t \div r$ ,

and the length of the switch-rails is

 $QK = r \sin KOQ. \qquad (81)$ 

Stub-switches are generally used with large frog angles. For small frog angles (large frog-numbers) the values of QK are so great that the length of rail left unspiked is too great for a safe track. If this were obviated by spiking down a portion of the lead the theoretical accuracy of the switch would be lost. The values of QK for various frog-numbers is given in Table III. These are based on a uniform throw (t) of  $5\frac{1}{2}$  inches.

263. Effect of straight frog-rails. A portion of the ends of



$$=2gn-f.$$
 (83)

Since  $r - \frac{1}{2}g = (L - f \sec F) \cot F$ , and

 $r+\frac{1}{2}g=(L-f\cos F)\operatorname{cosec} F,$ 

 $r = \frac{1}{2}L(\cot F + \csc F) - \frac{1}{2}j \sec F \cot F - \frac{1}{2}j \cos F \csc F$ 

$$=Ln - \frac{1}{2}f\left(\frac{1+\cos f}{\sin f}\right).$$

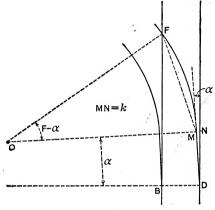
$$r = Ln - \frac{1}{2}f\cot \frac{1}{2}F$$

$$= Ln - fn. \text{ Then from (83)}$$

$$r = 2gn^2 - 2fn. \qquad (84)$$

264. Effect of straight point-rails. The "point switches," now so generally used, have straight switch-rails. This requires

an *angle* in the alignment rather than turning off by a tangential curve. The angle is, however, very small (between  $1^{\circ}$  and  $3^{\circ}$ ), and the disadvantages of this angle are small compared with the very great advantages of the device.





$$FM = \frac{g-k}{\sin \frac{1}{2}(F+a)};$$

$$r + \frac{1}{2}g = \frac{FM}{2\sin\frac{1}{2}(F-a)}$$

$$= \frac{g - k}{2 \sin \frac{1}{2}(F + a) \sin \frac{1}{2}(F - a)}$$

$$=\frac{g-k}{\cos a-\cos F}.$$
 (85)

$$BF = L = FM \cos \frac{1}{2}(F+a) + DN = (g-k) \cot \frac{1}{2}(F+a) + DN. \quad . \quad . \quad . \quad (86)$$

265. Combined effect of straight frog-rails and straight pointrails. It becomes necessary in this case to find a curve which shall be tangent to both the point-rail and the frog-rail. The curve therefore begins at M, its tangent making an angle of a(varying from 0° 52' to 2° 36') with the main rail, and runs to H. j

The central angle of the curve is therefore (F-a). The angle of the chord HM with the main rails is therefore

$$\frac{1}{2}(F-a) + a = \frac{1}{2}(F+a);$$

$$HM = \frac{g-f \sin F - k}{\sin \frac{1}{2}(F+a)};$$

$$r + \frac{1}{2}g = \frac{HM}{2 \sin \frac{1}{2}(F-a)}$$

$$= \frac{g-f \sin F - k}{2 \sin \frac{1}{2}(F+a) \sin \frac{1}{2}(F-a)}$$

$$= \frac{g-f \sin F - k}{\cos a - \cos F}; \quad \dots \quad \dots \quad (87)$$

$$ST = 2r \sin \frac{1}{2}(F-a)...$$
 (88)

$$BF = L = HM \cos \frac{1}{2}(F+a) + f \cos F + DN = (g - f \sin F - k) \cot \frac{1}{2}(F+a) + f \cos F + DN. \quad . \quad . \quad (89)$$

It may be more simple, if  $(r+\frac{1}{2}g)$  has already been computed, to write

$$L = 2(r + \frac{1}{2}g) \sin \frac{1}{2}(F - a) \cos \frac{1}{2}(F + a) + f \cos F + DN$$
  
=  $(r + \frac{1}{2}g)(\sin F - \sin a) + f \cos F + DN$ . . . . . (90)

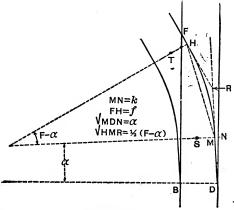


FIG. 140.

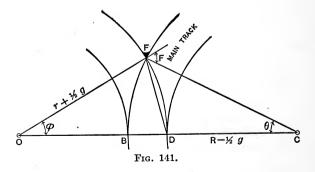
266. Comparison of the above methods. Computing values for r and L by the various methods, on the uniform basis of a

No. 9 frog, standard gauge 4'  $8\frac{1}{2}$ ", f=6'.00,  $k=6\frac{1}{4}$ "=0'.521, DN=16'6'', and  $a=1^{\circ}44'11''$ , we may tabulate the comparative results:

	§ 262. Simple circle. Curved frog- rail. Curved switch-rail.	§ 263. Straight frog-rail. Curved switch-rail.	§ 264. Curved frog- rail. Straight switch-rail.	§ 265. Straight frog-rail. Straight switch-rail,
Deg. of curve $L$	$762.757^{\circ} 31'84.75$	$654.74 \\ 8^{\circ} 46' \\ 78.75$	733.68 7° 49' 75.68	616.63 9° 18' 72.27

This shows that the effect of using straight frog-rails and straight switch-rails is to sharpen the curve and shorten the lead in each case separately, and that the combined effect is still greater. The effect of the straight switch-rails is especially marked in reducing the length of lead, and therefore Eq. 78 to 80, although having the advantage of extreme simplicity, cannot be used for point-switches without material error. The effect of the straight frog-rail is less, and since it can be materially reduced by bending the free end of the frog-rails, the influence of this feature is frequently ignored, the frog-rails are assumed to be curved, and Eq. 85 and 86 are used. (See § 276 for a further discussion of this point.)

267. Dimensions for a turnout from the OUTER side of a curved



track. In this demonstration the switch-rails will be considered as uniformly circular from the switch-points to the frog-point.

In the triangle FCD (Fig. 141) we have  $(FC+CD):(FC-CD)::\tan \frac{1}{2}(FDC+DFC):\tan \frac{1}{2}(FDC-DFC);$ but  $\frac{1}{2}(FDC+DFC) = 90^{\circ} - \frac{1}{2}\theta$ and  $\frac{1}{2}(FDC-DFC) = \frac{1}{2}F.$ Also, FC+CD=2R and FC-CD=g;  $\therefore 2R:g::\cot \frac{1}{2}\theta:\tan \frac{1}{2}F$  $::\cot \frac{1}{2}F:\tan \frac{1}{2}\theta;$ 

Also, 
$$OF: FC:: \sin \theta : \sin \phi;$$
 but  $\phi = (F-\theta);$ 

then

$$r + \frac{1}{2}g = (R + \frac{1}{2}g)\frac{\sin\theta}{\sin(F-\theta)}$$
. (92)

$$BF = L = 2(R + \frac{1}{2}g) \sin \frac{1}{2}\theta.$$
 (93)

If the curvature of the main track is very sharp or the frog angle unusually small, F may be less than  $\theta$ ; in which case the center O will be on the same side of the main track as C. Eq. 92 will become (by calling r = -r and changing the signs)

$$(r-\frac{1}{2}g) = (R+\frac{1}{2}g)\frac{\sin\theta}{\sin(\theta-F)} \cdot \cdot \cdot \cdot \cdot \cdot (94)$$

If we call d the degree of curve corresponding to the radius r, and D the degree of curve corresponding to the radius R, also d' the degree of curve of a turnout from a straight track (the frog angle F being the same), it may be shown that d=d'-D (very nearly). To illustrate we will take three cases, a number 6 frog (very blunt), a number 9 frog (very commonly used), and a number 12 frog (unusually sharp). Suppose  $D=4^{\circ}$  0'; also  $D=10^{\circ}$  0'; g=4'  $8\frac{1}{2}''=4'.708$ .

A brief study of the tabular form on p. 304 will show that the error involved in the use of the approximate rule for ordinary curves (4° or less) and for the usual frogs (about No. 9) is really insignificant, and that, even for sharper curves (10° or more), or for very blunt frogs, the error would never cause damage, considering the lower probable speed. In the most unfavorable case noted above the change in radius is about 1%. On account of the closeness of the approximation the method is frequently used. The remarkable agreement of the computed values of L

Frog	D=4°.										"L" for	
num- ber.		d			d'-D			Erroi		L	straight track.	
6 9 12	12° 3 0	54' 30 13	20'' 27 33	12° 3 0	57' 31 13	$52'' \\ 04 \\ 36$	0° 0 0	03' 0 0	32'' 37 03	$56.57 \\ 84.85 \\ 112.72$	$56.50 \\ 84.75 \\ 113.00$	
Frog						D=10	)°.				"L" for	
Frog num- ber.		d			l' — I			Error	.	L,	"L" for straight track.	

with the corresponding values for a straight main track (the lead rails circular throughout) shows that the error is insignificant in using the more easily computed values.

268. Dimensions for a turnout from the INNER side of a curved track. (Lead rails circular throughout.) From Fig. 142 we have, from the triangle DFC,

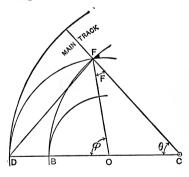


FIG. 142.

 $DC+FC: DC-FC :: \tan \frac{1}{2}(DFC+FDC): \tan \frac{1}{2}(DFC-FDC);$ but and  $\frac{1}{2}(DFC+FDC) = 90^{\circ} - \frac{1}{2}\theta$  $\therefore 2R: g: \cot \frac{1}{2}\theta: \tan \frac{1}{2}F;$  $\therefore \tan \frac{1}{2}\theta = \frac{gn}{R}.$  (95) SWITCHES AND CROSSINGS.

§ 269.

From OFC,

$$OF': FC::\sin\theta:\sin(F'+\theta).$$

$$(r+\frac{1}{2}g) = (R-\frac{1}{2}g)\frac{\sin\theta}{\sin(F+\theta)}.$$

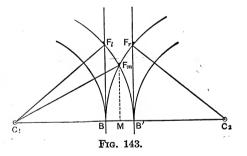
$$(96)$$

$$L = BF = 2(R-\frac{1}{2}g)\sin\frac{1}{2}\theta$$

$$(97)$$

As in § 267, it may be readily shown that the degree of the turnout (d) is *nearly* the *sum* of the degree of the main track (D) and the degree (d') of a turnout from a straight track when the frog angle is the same. The discrepancy in this case is somewhat greater than in the other, especially when the curvature of the main track is sharp. If the frog angle is also large, the curvature of the turnout is excessively sharp. If the frog angle is very small, the liability to derailment is great. Turnouts to the inside of a curved track should therefore be avoided, unless the curvature of the main track is small.

269. Double turnout from a straight track. In Fig. 143 the frogs  $F_l$  and  $F_r$  are generally made equal. Then, if there are



uniform curves from B' to  $F_l$  and from B to  $F_r$ , the required value of  $F_m$  is obtained from

vers 
$$\frac{1}{2}F_m = \frac{g}{2(r+\frac{1}{2}g)}, \ldots \ldots$$
 (98)

r being found from Eq. 78, in which n is the frog number of  $F_i$  or  $F_r$ .

$$MF_m = r \tan \frac{1}{2}F_m;$$

but since  $n_m = \frac{1}{2} \cot \frac{1}{2} F_m$ ,

Since vers  $F_l = \frac{g}{(r+\frac{1}{2}g)}$ ,

vers  $\frac{1}{2}F_m = \frac{1}{2}$  vers  $F_l$ . . . . (100) Also, since  $(C_1F_m)^2 = (MF_m)^2 + (C_1M)^2$ , we have

• 
$$(r + \frac{1}{2}g)^2 = \left(\frac{r}{2n_m}\right)^2 + r^2;$$
  
 $r^2 + rg + \frac{1}{4}g^2 = \frac{r^2}{4n_m^2} + r^2.$ 

Simplifying and substituting,  $r=2gn^2$ , we have

$$2g^{2}n^{2} + \frac{1}{4}g^{2} = \frac{4g^{2}n^{4}}{4nm^{2}};$$
$$nm^{2} = \frac{n^{4}}{2n^{2} + \frac{1}{4}}.$$

Dropping the  $\frac{1}{4}$ , which is always insignificant in comparison with  $2n^2$ , we have

$$n_m = \frac{n}{\sqrt{2}} = n \times .707$$
(approx.). . . . (101)

Frogs are usually made with angles corresponding to integral values of n, or sometimes in "half" sizes, e.g. 6,  $6\frac{1}{2}$ , 7,  $7\frac{1}{2}$ , etc. If No.  $8\frac{1}{2}$  frogs are used for  $F_l$  and  $F_r$ , the exact frog number for  $F_m$  is 6.01. This is so nearly 6 that a No. 6 frog may be used without sensible inaccuracy. Numbers 7 and 10 are a less perfect combination. If sharp frogs must be used,  $8\frac{1}{2}$  and 12 form a very good combination

If it becomes necessary to use other frogs because the right combination is unobtainable, it may be done by compounding the curve at the middle frog.  $F_l$  and  $F_r$  should be greater than  $\frac{1}{2}F_m$ . If equal to  $\frac{1}{2}F_m$ , the rails would be straight from the middle frog to the outer frogs. In Fig. 144,  $\theta_1 = F_l - \frac{1}{2}F_m$ . Drawing the chord  $\overline{F_lF_m}$ ,

$$\overline{KF_{l}F_{m}} = F_{l} - \frac{1}{2}\theta_{1} = F_{l} - \frac{1}{2}F_{l} + \frac{1}{4}F_{m} = \frac{1}{2}(F_{l} + \frac{1}{2}F_{m});$$

$$\overline{F_{l}F_{m}} = \frac{\overline{KF_{m}}}{\sin \overline{KF_{l}F_{m}}} = \frac{g}{2\sin \frac{1}{2}(F_{l} + \frac{1}{2}F_{m})}; \quad . \quad (102)$$

$$\overline{KF_{l}} = \overline{KF_{m}} \cot \overline{KF_{l}F_{m}} = \frac{1}{2}g \cot \frac{1}{2}(F_{l} + \frac{1}{2}F_{m}); \quad (103)$$

$$(r_{1} + \frac{1}{2}g) = \frac{F_{l}F_{m}}{2\sin\frac{1}{2}\theta} = \frac{g}{4\sin\frac{1}{2}(F_{l} + \frac{1}{2}F_{m})\sin\frac{1}{2}(F_{l} - \frac{1}{2}F_{m})} = \frac{\frac{1}{2}g}{\cos\frac{1}{2}F_{m} - \cos\frac{F_{l}}{2}} \cdot \cdot \cdot \cdot \cdot \cdot (104)$$

If three frogs, all different, must be used, the largest may be selected as  $F_m$ ; the radius of the lead rails may be found by an inversion of Eq. 98;  $F_m$  may be located in the center of the tracks by Eq. 99; then each of the smaller frogs may be located

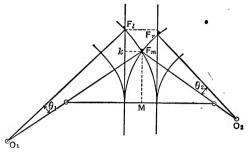


FIG. 144.

by separate applications of Eq. 102 or 103, the radius being determined by Eq. 104.

270. Two turnouts on the same side. In Fig. 145, let  $O_1$  bisect  $O_2D$ . Then  $(r_1+\frac{1}{2}g)=\frac{1}{2}(r_2+\frac{1}{2}g)$ ; also,  $O_1O_2=O_1F_l$  and  $F_r=F_l$ .

vers 
$$F_m = \frac{g}{r' + \frac{1}{2}g} = \frac{2g}{r + \frac{1}{2}g};$$
 . . . (105)

$$BF_m = (r' + \frac{1}{2}g) \sin F_m$$
. . . . (106)

It may readily be shown that the relative values of  $F_r$ ,  $F_l$ , and  $F_m$  are almost identical with those given in § 269; as may be

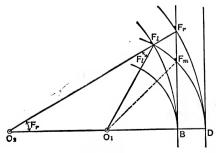
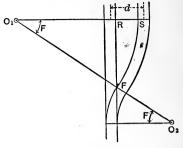


Fig. 145.

apparent when it is considered that the middle switch may be regarded simply as a curved main track, and that, as developed

in § 267, the dimensions of turnouts are nearly the same whether the main track is straight or slightly curved.

271. Connecting curve from a straight track. The "connecting curve'' is the track lying between the frog and the side track where it becomes parallel to the main track (FS in Fig. 146 or 147). Call d the distance between track centers. The angle  $FO_1R = F$  (see Fig. 146). Call r' the radius of the connecting curve. Then



$$(r' - \frac{1}{2}g) = \frac{a-g}{\operatorname{vers} F};$$
 (107) Fig. 146.  
 $FR = (r' - \frac{1}{2}g) \sin F.$  . . . . (108)

If it is considered that the distance FR consumes too much track room it may be shortened by the method indicated in Fig. 151.

272. Connecting curve from a curved track to the OUTSIDE. When the main track is curved, the required quantities are the

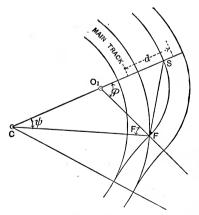


FIG. 147.

radius r of the connecting curve from F to S, Fig. 147, and its In the triangle CSFlength or central angle.

 $CS+CF:CS-CF::\tan \frac{1}{2}(CFS+CSF):\tan \frac{1}{2}(CFS-CSF);$ 

but  $\frac{1}{2}(CFS+CSF) = 90 - \frac{1}{2}\psi$ ; and, since the triangle  $O_1SF$  is isosceles,  $\frac{1}{2}(CFS-CSF) = \frac{1}{2}F$ ;

$$\therefore 2R+d:d-g::\cot \frac{1}{2}\psi:\tan \frac{1}{2}F$$
$$::\cot \frac{1}{2}F:\tan \frac{1}{2}\psi;$$

$$t. \quad \tan \frac{1}{2} \psi = \frac{2n(d-g)}{2R+d}. \quad . \quad . \quad . \quad . \quad (109)$$

From the triangle  $CO_1F$  we may derive

1

$$r-\frac{1}{2}g:R+\frac{1}{2}g::\sin \psi:\sin (F+\psi);$$

$$r - \frac{1}{2}g = (R + \frac{1}{2}g)\frac{\sin \psi}{\sin (F + \psi)}$$
. . . . . (110)

$$FS = 2(r - \frac{1}{2}g) \sin \frac{1}{2}(F + \psi).$$
 (111)

273. Connecting curve from a curved track to the INSIDE.

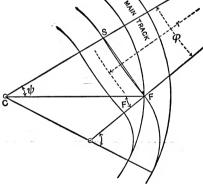


FIG. 148.

As above, it may readily be deduced from the triangle CFS (see Fig. 148) that

$$(2R-d): (d-g):: \cot \frac{1}{2}\psi: \tan \frac{1}{2}F,$$

and finally that

$$\tan \frac{1}{2}\psi = \frac{2n(d-g)}{2R-d}.$$
(112)

Similarly we may derive (as in Eq. 110)

$$(r-\frac{1}{2}g) = (R-\frac{1}{2}g)\frac{\sin \phi}{\sin (F-\phi)}$$
. (113)

Also

$$FS = 2(r - \frac{1}{2}g) \sin \frac{1}{2}(F - \psi)$$
.... (114)

Two other cases are possible. becomes infinite (see Fig. 149), then  $F = \psi$ . In such a case we may write, by substituting in Eq. 112,

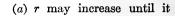
$$2R - d = 4n^2(d - g)$$
. (115)

This equation shows the value of R, which renders this case possible with the given values of n, d, and g. (b)  $\phi$  may be greater than F. As before (see Fig. 150)

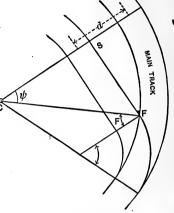
 $2R - d: d - g:: \cot \frac{1}{2}\psi: \tan \frac{1}{2}F;$ 

$$\tan \frac{1}{2}\psi = \frac{2n(d-g)}{2R-d},$$

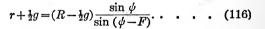
the same as Eq. 112, but



§ 273.







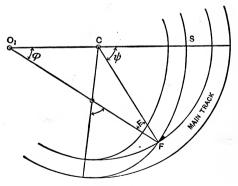


FIG. 150.

**Problem.** To find the dimensions of a connecting curve running to the INSIDE of a curved main track; number 9 frog, 4° 30' curve, d=13', g=4' 82''.

## § 274.

### SWITCHES AND CROSSINGS.

Solution.

Eq. 112.	d = 13.000
	g = 4.708
	(d-g) = 8.292
R = 1273	.6
2R = 2547	.2
2R - d = 2534	.2
$\log\left(2R-d\right)=3.40$	384

Eq. 116. R = 1273.6  $\frac{1}{2}g = \frac{2.35}{1271.25}$   $(\Psi - F) = 1373'', \log = 3.13767$   $\frac{4.68557}{10g \sin (\Psi - F)} = 7.82324$ 

Eq. 114.  

$$\frac{1}{2}(\Psi - F) = 686.^{\prime\prime}5 \dots 2.83664$$
  
 $\frac{4.68557}{7.52221}$ 

$$274$$
. Clossover between two p

Fig. 151.

40

 $\begin{array}{c} \log 2n = 1.25527\\ \log (d-g) = .91866\\ \mathrm{co-log}\;(2R-d) = 6.59616\\ \log \tan \frac{1}{2}\Psi = 8.77009\\ \frac{1}{2}\Psi = 3^{\circ}\,22'\,14''\\ \Psi = 6^{\circ}\,44'\,28''\\ F = 6^{\circ}\,21'\,35''\\ (\Psi - F) = 0^{\circ}\,22'\,53'\\ \log (R - \frac{1}{2}g) = 3.10423\\ \log \sin \Psi = 9.06960\\ \mathrm{co-log}\;\sin(\Psi - F) = 2.17676\\ (r + \frac{1}{2}g) = 22418.0..4.35059\\ r = 22415.6\\ \underline{d = 0^{\circ}}\,15'\\ \end{array}$ 

2	.0.30103
$(r + \frac{1}{2}g) = 22418.0.$	.4.35059
$\sin \frac{1}{2}(\Psi - F)$ .	$.7.5222\overline{1}$
FS = 149.22	.2.17384

parallel straight tracks. (See Fig. 151.) The turnouts are as usual. The crossover track may be straight. as shown by the full lines, or it may be a reversed curve, as shown by the dotted lines. The reversed curve shortens the total length of track required, but is somewhat objectionable. The first method requires that both frogs must be equal. The second method permits unequal frogs, although equal frogs

are preferable. The length of straight crossover track is  $F_1T$ .

 $F_1T \sin F_1 + g \cos F_1 = d - g;$ 

$$F_1T = \frac{d-g}{\sin F_1} - g \cot F_1.$$
 . . . . (117)

The total distance along the track may be derived as follows:

If a reversed curve with equal frogs is used, we have

vers 
$$\theta = \frac{d}{2r};$$
 . . . . . . . (119)

$$DQ = 2r\sin\theta \qquad (120)$$

If the frogs are unequal, we will have (see Fig. 152)

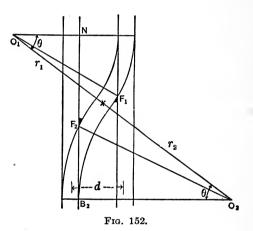
 $r_2$  vers  $\theta + r_1$  vers  $\theta = d$ ;

 $\therefore \quad \text{vers } \theta = \frac{d}{r_1 + r_2}; \quad \dots \quad \dots \quad (121)$ 

also the distance along the track

$$B_2N = (r_1 + r_2) \sin \theta$$
. . . . . (122)

Problem. A crossover is to be placed between two parallel straight tracks, 12' 2" between centers, using a No. 8 and a No. 9



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also

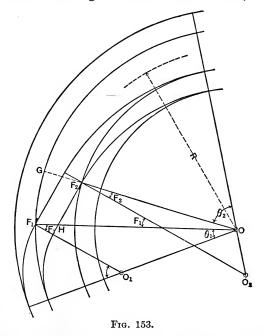
## § 274. SWITCHES AND CROSSINGS.

frog, and with a reversed curve between the frogs. Required the total distance between switch-points (the distance  $B_2N$  in Fig. 152).

Solution. If straight point rails and straight frog rails are used, the radii,  $r_1$  and  $r_2$ , taken from the middle section of Table III, are 527.91 and 681.16.

vers  $\theta = \frac{d}{r_1 + r_2}$ Eq. 122. d = 12' 2'' = 12.16, = 527.91 $\log = 1.08517$  $\tau_1$ = 681.16  $\log(r_1 + r_2) = 3.08245$ 79  $r_1 + r_2 = 1209.07$ log vers  $\theta = 8.00272$  $\theta = 8^{\circ} \ 08' \ 06''$ Eq. 122.  $\log(r_1+r_2) = 3.08245$  $\log \sin \theta = 9.15077$  $B_2N = 171.09$  $\log 171.09 = 2.2332\overline{2}$ 

The length of the curve from  $B_2 = 100(\theta \div d) = 100(8^\circ 08' 06'' \div 8^\circ 25') = 96.65$ . The length of the other curve is  $100(8^\circ 08' 06' \div 100) = 100(8^\circ 08' 06' \div 100)$ 



 $10^{\circ} 52'$  = 74.86. As a check, 96.65 + 74.86 = 171.51, which is slightly in excess of 171.09, as it should be.

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275. Crossover between two parallel curved tracks. (a) Using a straight connecting curve. This solution has limitations. If one frog  $(F_1)$  is chosen,  $F_2$  becomes determined, being a function of  $F_1$ . If  $F_1$  is less than some limit, depending on the width (d) between the parallel tracks, this solution becomes impossible. In Fig. 153 assume  $F_1$  as known. Then  $F_1H = g \sec F_1$ . In the triangle  $HOF_2$  we have

$$\sin HF_2O: \sin F_2HO:: HO: F_2O;$$
  

$$\sin F_2HO = \cos F_1; \quad HF_2O = 90^\circ + F_2;$$
  

$$\therefore \quad \sin HF_2O = \cos F_2.$$
  

$$HO = R + \frac{1}{2}d - \frac{1}{2}g - g \sec F_1; \quad F_2O = R - \frac{1}{2}d + \frac{1}{2}g;$$
  

$$\therefore \quad \cos F_2 = \cos F_1 \frac{R + \frac{1}{2}d - \frac{1}{2}g - g \sec F_1}{R - \frac{1}{2}d + \frac{1}{2}g}. \quad . \quad . \quad . \quad . \quad (123)$$

Knowing  $F_2$ ,  $\theta_2$  is determinable from Eq. 91. Fig. 153 shows the case where  $\theta_2$  is greater than  $F_2$ . Fig. 154 shows the case where it is less. The demonstration of Eq. 123 is applicable to

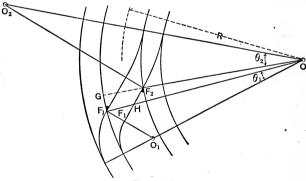


FIG. 154.

both figures. The relative position of the frogs  $F_1$  and  $F_2$  may be determined as follows, the solution being applicable to both Figs. 153 and 154:

$$HOF_2 = 180^{\circ} - (90^{\circ} - F_1) - (90^{\circ} + F_2) = F_1 - F_2.$$

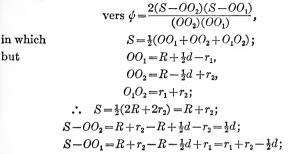
 $GF_1 = 2(R + \frac{1}{2}d - \frac{1}{2}g) \sin \frac{1}{2}(F_1 - F_2)$ . . . . (124)

Since  $F_2$  comes out *any* angle, its value will not be in general that of an even frog number, and it will therefore need to be made to order.

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Then

(b) Continuing the switch-rail curves until they meet as a reversed curve. In this case  $F_1$  and  $F_2$  may be chosen at pleasure (within limitations), and they will of course be of regular sizes and equal or unequal as desired.  $F_1$  and  $F_2$  being known,  $\theta_1$ and  $\theta_2$  are computed by Eq. 95 and 91. In the triangle  $OO_1O_2$ (see Fig. 155)



but

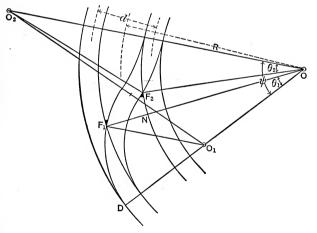


FIG. 155.

vers 
$$\psi = \frac{d(r_1 + r_2 - \frac{1}{2}d)}{(R - \frac{1}{2}d + r_2)(R + \frac{1}{2}d - r_1)};$$
 (125)

$$\sin OO_2O_i = \sin \psi \frac{OO_1}{O_1O_2} = \sin \psi \frac{R + \frac{1}{2}d - r_1}{r_1 + r_2}; \quad . \quad . \quad (126)$$

$$O_2 O_1 D = \dot{\psi} + O_1 O_2 O; \qquad (127)$$

$$NF_2 = 2(R - \frac{1}{2}d + \frac{1}{2}d) \sin \frac{1}{2}(\psi - \theta_1 - \theta_2) \qquad (128)$$

Although the above method introduces a reversed curve, yet it uses up less track than the first method and permits the use of ordinary frogs rather than those having some special angle which must be made to order. But the above solution implies the use of circular lead rails. We may compute dimensions and lay track between  $F_1$  and  $F_2$  on this basis and then change the switch rails as desired. Strictly,  $r_1$  and  $r_2$  should be computed by Eq. 92 and 96, but for an easy main-line curve the approximate rule is sufficiently accurate.

Problem.—Required the dimensions of a crossover on a 4° 30′ curve when the distance between track centers is 13 feet. The frog for the outer main track ( $F_1$  in Fig. 155) is No. 9;  $F_2$  is No. 7. Then R=1273.6;  $R_1$ , for the outer main track, =1280.1;  $D_1=4^{\circ}29'$ ;  $R_2=1267.1$ ;  $D_2=4^{\circ}31'$ ;  $r_1=$  radius for  $(d_1+D_1)^{\circ}$  curve=radius for  $(7^{\circ}31'+4^{\circ}29')$  curve=478.34;  $r_2=$  radius for  $(d_2-D_2)^{\circ}$  curve=radius for  $(12^{\circ}26'-4^{\circ}31')$  curve=724.31. (See §§ 267-268.)

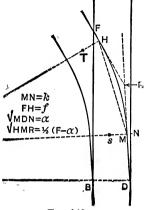
Eq. 125	d = 13	$\log = 1.11394$
$r_1 + r_2 - \frac{1}{2}d = 1196.15$		$\log = 3.0777\overline{8}$
	1	colog = 6.69086
$R - \frac{1}{2}d + r_2 = 1991.31$	$\log = 3.30914$	
$R + \frac{1}{2}d - r_1 = 801.76$	$\log = 2.9040\overline{4}$	$colog = 7.0959\overline{5}$
$\psi = 7^{\circ} 52' 26''$		$\log \operatorname{vers} \psi = 7.97854$
Eq. 126		$\log \sin \psi = 9.13670$
	log	$q(R+\frac{1}{2}d-r_1)=2.9040\overline{4}$
$r_1 + r_2 = 1202.65$	$\log = 3.0801\overline{3}$	$colog = 6.9198\overline{6}$
1112 200100	$OO_2O_1 = 5^\circ \ 14' \ 24''$	$\sin OO_2O_1 = 8.96061$
Eq. 127 $O_2O_1D = 7^{\circ}$	$52' 26'' + 5^{\circ} 14' 24'' = 13^{\circ} 0$	6' 50''
TE 01	$\frac{1}{2}\theta_1 = \frac{gn}{R} = \frac{4.708 \times 9}{1280.1} = \frac{42.37}{1280.1}$	$\log = 1.62708$
Eq. 91 tan	$\frac{1}{2} v_1 = \frac{1}{R} = \frac{1}{1280.1} = \frac{1}{1280.1}$	$log = 3.1072\bar{4}$
		$\log \tan \frac{1}{2}\theta_1 = 8.5198\overline{3}$
	(Using Table VI)	5.31426
$A_{1} = 3^{\circ} 47' 30''$	$\frac{1}{2}\theta_1 = 1^\circ 53' 45''$	$\log 6825 = 3.83410$
$\theta_1 = 3^{\circ} 47' 30''$	201 1 00 10	
T 05	$gn_4.708 \times 7_32.956$	$\log = 1.5179\overline{3}$
Eq. 95	$\frac{gn}{R} = \frac{4.708 \times 7}{1267.1} = \frac{32.956}{1267.1}$	$\log = 3.10281$
		$\tan \frac{1}{2}\theta_2 = 8.4151\overline{2}$
		5.31433
A	$\frac{1}{2}\theta_2 = 1^\circ 29' 24''$	$\log 5364 = 3.72945$
$\theta_2 = 2^\circ 58' 48''$	202-1 23 24	100 0001 0.72040
Eq. 128		$2 \log = 0.30103$
-	$R - \frac{1}{2}d + \frac{1}{2}g = 1269.45$	$\log = 3.1036\overline{1}$
1// 0 0	10.000.000	log ain _4.68555
$\frac{1}{2}(\psi-\theta_1-\theta_2)$	$=1^{\circ}00^{\circ}08^{\circ}$	$\log \sin = \frac{4.68555}{3.59857}$
$NF_2 = 48.84$		$\log 48.84 = 1.6887\overline{6}$
2112-10.01		1.00010

Length of curve with radius  $r_1 = 100 \frac{13^\circ 06' 50''}{12^\circ 0'} = 109.18$ " " " " "  $r_2 = 100 \frac{5^\circ 14' 24''}{7^\circ 55'} = 66.16$ Total length of curve between switch points = 175.34

As an approximate check, the mean length subtending the angle  $\psi$  with radius R is similarly computed as 174.98. Note that the length of the curve with the radius  $r_2$  is 66.16, which is but little more than the length of lead rails (65.92) for a No. 7 frog using circular lead rails, which means that the point of reversed curve is but little beyond the frog point. If the computations had apparently indicated the point of reversed curve coming between the frog point and the switch point, it would have shown the impracticability of the combination of No. 7 and No. 9 frogs with this particular degree of curve. gauge of track, and distance between track centers. If both frogs were made No. 9, the total length of track between switch points would be increased to over 198 feet and the point of reversed curve would be nearly at the middle point. This shows that the frog numbers should be nearly equal, but also shows that there is some choice "within limitations."

276. Practical rules for switch-laying. A consideration of the previous sections will show that the formulæ are comparatively simple when the lead rails are assumed as circular; that they become complicated, even for turnouts from a straight main track, when the effect of straight frog and point rails is allowed for, and that they become hopelessly complicated when allowing for this effect on turnouts from a curved main track. It is also shown (§ 267) that the length of the lead is practically the same whether the main track is straight or is curved with such curves as are commonly used, and that the degree of curve of the lead rails from a curved main track may be found with close approximation by mere addition or subtraction. From this it may be assumed that if the length of lead (L) and the radius of the lead rails (r) are computed from Eq. 87 and 90 for various frog angles, the same leads may be used for curved main track; also, that the degree of curve of the lead rails may be found by addition or subtraction, as indicated in § 267, and that the approximations involved will not be of practical detriment. In accordance with this plan Table III has been computed from

Eq. 87, 88, and 90. The *leads* there given may be used for all main tracks, straight or curved. The table gives the degree of





curve of the lead rails for *straight* main track; for a turnout to the *inside*, *add* the degree of curve of the main track; for a turnout to the *outside*, *subtract* it.

But there are complications resulting from practical and economical switch construction. A committee of of the A. R. E. A. in 1910 adopted certain standards in details, which when applied to Eqs. 87 to 90 give the values for switch dimensions as quoted in the second section of Table III. They adopted four lengths of switch rails. In each case the "point" is always  $\frac{1}{4}$ " thick. The gauge line

at the other end is always to be placed  $6\frac{1}{4}''$  from the gauge line of the main rail, and the planing is so done that when in this position the switch rail lies against the main rail. Therefore the angle  $\alpha$  is always an angle whose sine equals 6 inches (or 0.5 foot) divided by the length of the switch rail in feet. In Fig. 140, the point *D* is not on the gauge line of the main rail but at a point  $\frac{1}{4}''$  away from it, and the point M  $6\frac{1}{4}''$  away from

it. The straight rail BF consists of a point rail at one end, the "closure rails," and one of the wing rails of the frog at the other end. The closure rails will in general consist of one rail cut to a computed length and one or more rails from 24 to 33 feet long, the lengths being in even feet. The curved rail DFwill also consist of a point rail, a frog wing-rail, and one or more lengths of closure rail, but the closure rails in this case are slightly longer than those for the straight rail. Since it is always practically easier to measure to the "actual point" of a frog (see Fig. 130) rather than to the theoretical point, Table III gives the distance L', which is the distance L, =BF, plus the "frog bluntness," which

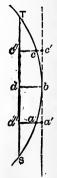


FIG. 156.

is found by multiplying  $\frac{1}{2}$ " (=0.0417 foot) by the frog number. The curvature for a curved switch rail (for a straight track)

ORDINATES	$\mathbf{OF}$	CURVEI	D
SWITCH	I RA	IL.	

Frog No.	Center.		Quarter points.		
10.	Ft.	Ft. Ins.		Ins.	
$ \begin{array}{r}     4 \\     5 \\     6 \\     7 \\     8 \\     9 \\     9 \\     10 \\     11 \\     12 \\     15 \\     18 \\     20 \\     24 \\ \end{array} $	$     \begin{array}{r}       .59\\       .550\\       .58\\       .550\\       .49\\       .552\\       .61\\       .53\\       .50\\       .44     \end{array} $	7667557455514355143555 35 66766555667665	$\begin{array}{r}.44\\.41\\.38\\.43\\.41\\.38\\.37\\.36\\.41\\.39\\.46\\.40\\.37\\.33\end{array}$	55455544544445444	

may be determined by measuring offsets at the quarter points from a string stretched between the points H and M. These offsets are as given in the tabular form. The distance HM may be computed from the equation in § 265.

If the position of the switch-block is definitely determined, then the rails must be cut accordingly; but when some freedom is allowable (which never need exceed 16.5 feet and may require but a few inches), one rail-cutting may be avoided. Mark on the rails at B, F, and D; measure off the length of the switch-rails DN and locate the point

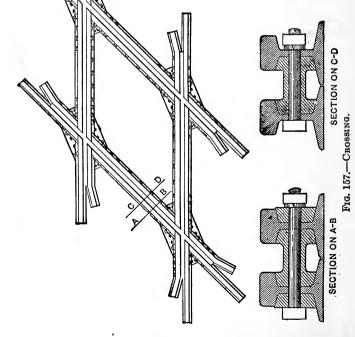
M at the distance k from N. If the frog must be placed during the brief period between the running times of trains, it will be easier to joint up to the frog a piece of rail at one or both ends of just such a length that they may be quickly substituted for an equal length of rail taken out of the track. When the frog is thus in place the point H becomes located. The chord MH may be measured on the ground as a check. The curve between M and H is of known radius. Substituting in Eq. 31 the value of chord and R, we may compute x(=db). Locate the middle point d and the quarter points a'' and c''. Then a''a and c''c each equal three-fourths of db. Theoretically this gives a parabola rather than a circle, but the difference for all practical cases is too small for measurement. See Fig. 156.

*Example.*—Given a main track on a 4° curve—a turnout to the outside, using a No. 9 frog; gauge 4'  $8\frac{1}{2}''$ ; f=6'.00;  $k=6\frac{1}{4}''$ ; DN=16' 6'' and  $a=1^{\circ}$  44' 11''. Then for a straight track r would equal 616.27 [ $d=9^{\circ}$  18' 27'']. For this curved track d will be nearly 9° 18'  $-4^{\circ}=5^{\circ}$  18', or r will be 1081.4. L for the straight track would be 72.61; but since the lead is slightly increased (see §267) when the turnout is on the outside of a curve, L may here be called 72.9. H and M may be located as described above. HM may be measured on the ground as a check on the value (in this case 49.90) computed as in § 265. Since it is slightly more for a turnout to the outside of a curve, it may be called 50.00. Then, for the outer rail,  $x=db=\frac{(50.0)^2}{8\times1083.75}=$  0.288 feet, and aa'' and cc''=0.216 foot.

**276a.** Slips. Track movements in crowded yards are facilitated by using "slips" (see Fig. 156*a*), which may be "single" or "double." The crossing of two rails is done either by operating two movable rails or by using fixed "frogs," but a comparison of the continuity of the running rails, using ordinary frogs (see Fig. 130) and these frogs, will show their radical difference. These slips can be used for frog angles from No. 6 to No. 15. The levers are so connected that the several operations necessary to set the rails for any desired train movement are accomplished by one motion.

#### CROSSINGS.

277. Two straight tracks. When two straight tracks cross each other, four frogs are necessary, the angles of two of them being supplementary to the angles of the other. Since such crossings are sometimes operated at high speeds, they should be



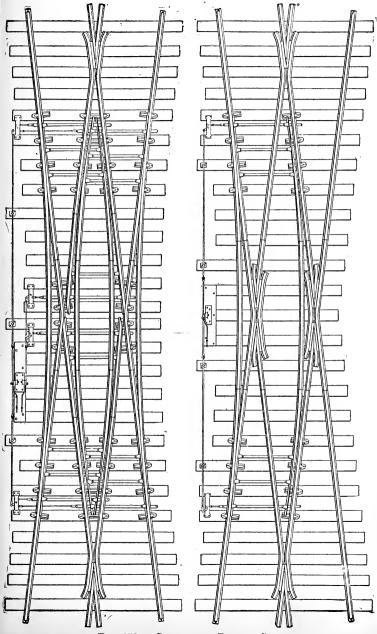


FIG. 156a .- SINGLE AND DOUBLE SLIPS.

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very strongly constructed, and the angles should preferably be 90° or as near that as possible. The frogs will not in general be "stock" frogs of an even number, especially if the angles are large, but must be made to order with the required angles as measured. In Fig. 157 are shown the details of such a crossing. Note the fillers, bolts, and guard-rails.

278. One straight and one curved track. Structurally the crossing is about the same as above, but the frog angles are all unequal. In Fig. 158, R is known, and the angle M, made by the center lines of the tracks at their point of intersection, is also known. M = NCM.  $NC = R \cos M$ .  $(R - \frac{1}{2}g) \cos F_1 = NC + \frac{1}{2}g;$  $\therefore \cos F_1 = \frac{R \cos M + \frac{1}{2}g}{R - \frac{1}{2}g}$ .

Similarly

$$\begin{array}{l} y \\ \cos F_{2} = \frac{R \cos M + \frac{1}{2}g}{R + \frac{1}{2}g}, \\ \cos F_{3} = \frac{R \cos M - \frac{1}{2}g}{R + \frac{1}{2}g}, \\ \cos F_{4} = \frac{R \cos M - \frac{1}{2}g}{R - \frac{1}{2}g}. \end{array}$$
(129)  
$$\begin{array}{l} F_{1}(129) \\ F_{2}(129) \\ F_{2}(129) \\ F_{3}(129) \\ F_{4}(129) \\ F_{5}(129) \\ F_{5}(1$$

**279.** Two curved tracks. The four frogs are unequal, and the angle of each must be computed. The radii  $R_1$  and  $R_2$  are known; also the angle M.  $r_1, r_2, r_3$ , and  $r_4$  are therefore known by adding or subtracting  $\frac{1}{2}g$ , but the lines are so indicated for brevity. Call the angle  $MC_1C_2=C_1$ , the angle  $MC_2C_1=C_2$ , and the line  $C_1C_2=c$ . Then

$$\frac{1}{2}(C_1+C_2) = 90^\circ - \frac{1}{2}M$$

and

$$\tan \frac{1}{2}(C_1 - C_2) = \cot \frac{1}{2}M \frac{R_2 - R_1}{R_2 + R_1}$$
. (131)

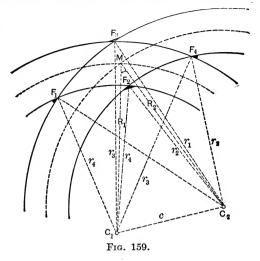


$$c = C_1 C_2 = R_2 \frac{\sin M}{\sin C_1}$$
. (132)

§ 279.

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In the triangle  $F_1C_1C_2$ , call  $\frac{1}{2}(c+r_1+r_4) = s_1$ ;  $s_2 = \frac{1}{2}(c+r_2+r_4)$ ;



 $s_3 = \frac{1}{2}(c+r_1+r_3)$ ; and  $s_4 = \frac{1}{2}(c+r_2+r_3)$ . Then, by formula 29, Table XXX,

from which the chords  $F_1F_2$  and  $F_2F_4$  are readily computed.

$$\operatorname{vers} F_{1} = \frac{2(s_{1} - r_{1})(s_{1} - r_{4})}{r_{1}r_{4}},$$

$$\operatorname{vers} F_{2} = \frac{2(s_{2} - r_{2})(s_{2} - r_{4})}{r_{2}r_{4}},$$

$$\operatorname{vers} F_{3} = \frac{2(s_{3} - r_{1})(s_{3} - r_{3})}{r_{1}r_{3}},$$

$$\operatorname{vers} F_{4} = \frac{2(s_{4} - r_{2})(s_{4} - r_{3})}{r_{2}r_{2}},$$

$$\operatorname{sin} C_{1}C_{2}F_{4} = \operatorname{sin} F_{4}\frac{r_{5}}{c};$$

$$\operatorname{sin} C_{1}C_{2}F_{2} = \operatorname{sin} F_{2}\frac{r_{4}}{c};$$

$$\therefore F_{2}C_{2}F_{4} = C_{1}C_{2}F_{4} - C_{1}C_{2}F_{2}, \dots \dots (134)$$

$$\operatorname{sin} F_{1}C_{1}C_{2} = \operatorname{sin} F_{2}\frac{r_{2}}{c},$$

$$\therefore F_{1}C_{1}F_{2} = F_{1}C_{1}C_{2} - F_{2}C_{1}C_{2}; \dots \dots (135)$$

Similarly

 $F_1F_2$  and  $F_2F_4$  are nearly equal. When the tracks are straight and the gauges equal, the quadrilateral is equilateral.

Problem. Required the frog angles and dimensions for a crossing of two curves  $(D_1=4^\circ; D_2=3^\circ)$  when the angle of their tangents at the point of intersection  $=62^\circ 28'$  (the angle M in Fig. 159).

Solution

 $R_1 = 1432.7; R_2 = 1910.1;$  $r_1 = R_2 + \frac{1}{2}g = 1910.1 + 2.35 = 1912.45;$  $r_2 = R_2 - \frac{1}{2}g = 1910.1 - 2.35 = 1907.75;$  $r_3 = R_1 + \frac{1}{2}g = 1432.7 + 2.35 = 1435.05;$  $r_4 = R_1 - \frac{1}{2}g = 1432.7 - 2.35 = 1430.35.$  $\log \cot \frac{1}{2}M = 0.21723$ Eq. 131.  $R_2 - R_1 = 477.4$ ;  $\log = 2.67888$  $R_2 + R_1 = 3342.8$ ; log = 3.52411; co-log = 6.47589  $\frac{1}{2}(C_1 - C_2) = 13^\circ 15' 07''; \tan 13^\circ 15' 07'' = 9.37200$  $[\frac{1}{2}(C_1+C_2)=90^\circ-\frac{1}{2}M]$  $\frac{1}{2}(C_1+C_2)=58^{\circ}46'$  $C_1 = 72^\circ 01' 07''$  $C_{2} = 45^{\circ} 30' 53''$  $\log R_2 = 3.28105$ Eq. 132.  $\log \sin M = 9.94779$  $\log \sin C_1 = 9.97825$ ; co-log = 0.02175  $c = C_1 C_2 = 1780.7;$  $\log C_1 C_2 = 3.2505\bar{9}$ Eq. 133. c = 1780.7c = 1780.7c = 1780.7c = 1780.7 $r_2 = 1907.75$  $r_2 = 1907.75$  $r_1 = 1912.45$  $r_1 = 1912.45$  $r_4 = 1430.35$  $r_3 = 1435.05$  $r_4 = 1430.35$  $r_3 = 1435.05$ 2 5123.50 2 5118.80 2 5128.20 2 5123.50  $s_2 = 2559.40$  $s_3 = 2564.10$  $s_4 = 2561.75$  $s_1 = 2561.75$  $s_1 - r_1 = 649.30$  $s_2 - r_2 = 651.65$  $s_3 - r_1 = 651.65$  $s_4 - r_2 = 654.00$  $s_1 - r_4 = 1131.40$  $-r_4 = 1129.05$  $s_3 - r_3 = 1129.05$  $s_4 - r_3 = 1126.70$  $\log 2 = 0.30103$  $(s_1 - r_1); \log 649.30 = 2.81244$  $(s_1 - r_4); \log 1131.40 = 3.05361$ co-log = 6.71841 $\log = 3.28159;$  $r_1 = 1912.45;$ co-log = 6.84456 $\log = 2.15544$ ;  $r_4 = 1430.35;$ log vers  $62^{\circ} 25' 31'' = 9.73006$  $F_1 = 62^\circ \ 25' \ 31'';$  $\log 2 = 0.30103$  $(s_2 - r_2); \log 651.65 = 2.81401$  $(s_2 - r_4); \log 1129.05 = 3.0527\overline{1}$ co-log = 6.71948 $r_2 = 1907.75;$  $\log = 3.28052;$ co-log = 6.84456 $r_4 = 1430.35;$  $\log = 3.15544$ ; log vers 62° 33' 55" = 9.73180  $F_2 = 62^\circ \ 33' \ 55'';$ 

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#### RAILROAD CONSTRUCTION

 $(s_3 - r_1); \log 651.65 = 2.81401$  $(s_3 - r_3); \log 1129.05 = 3.05271$  $\tau_1 = 1912.45$ ;  $\log = 3.28159$ ; co-log = 6.71841co-log = 6.84313 $r_3 = 1435.05;$  $\log = 3.15686$ ; F3=62° 21' 57";  $\cdot \log \text{ vers } 62^{\circ} 21' 57'' = 9.72930$  $\log 2 = 0.30103$  $(s_4 - r_2); \log 654.00 = 2.81558$  $(s_4 - r_3); \log 1126.70 = 3.05181$  $r_2 = 1907.75; \log = 3.28052;$ co-log = 6.71948 $r_3 = 1435.05; \log = 3.1568\overline{6};$ co-log = 6.84313 $\log \text{ vers } 62^{\circ} 30' 14'' = 9.73103$  $F_4 = 62^\circ 30' 14'';$ 

As a check, the mean of the frog angles =  $62^{\circ} 27' 54'$ , which is within 6" of the value of M.

 $\log \sin F_4 = 9.9479\overline{4}$ Eq. 134.  $\log r_3 = 3.15686$  $\log c = 3.2505\overline{9};$ co-log c = 6.74940 $C_1C_2F_4 = 45^\circ 37' 51''$ :  $\sin C_1 C_2 F_4 = 9.8542\overline{1}$  $\log \sin F_2 = 9.9481\bar{8}$  $\log r_4 = 3.15544$  $co-log c = 6.7494\bar{0}$  $C_1C_2F_2 = 45^\circ 28' 17'';$  $\sin C_1 C_2 F_2 = \overline{9.85303}$  $F_2C_2F_4 = 45^\circ 37' 51'' - 45^* 28' 17'' = 0^\circ 09' 34''.$  $\log 2 = 0.30103$  $\log r_2 = 3.28052$  $\log \sin = \begin{pmatrix} 4.68557 \\ 2.45788 \end{pmatrix}$  $\frac{1}{2}(0^{\circ} \ 09' \ 34'') = 0^{\circ} \ 04' \ 47'';$  $F_2F_4 = 5.309;$  $\log F_2 F_4 = 0.72500$ Eq. 135.  $\sin F_1 = 9.9476\bar{3}$  $\log r_1 = 3.28159$ co-log c = 6.74940 $F_1C_1C_2 = 72^\circ 10' 22''$  $\sin F_1 C_1 C_2 = 9.97863$  $\sin F_2 = 9.9481\bar{8}$  $\log r_2 = 3.28052$  $co-log c = 6.7494\bar{0}$  $F_2C_1C_2 = 71^\circ 57' 38'';$  $\sin F_2 C_1 C_2 = 9.97811$  $F_1C_1F_2 = 72^\circ 10' 22'' - 71^\circ 57' 38'' = 0^\circ 12' 44''.$  $\log 2 = 0.30103$  $\log r_4 = 3.15544$  $\log \sin = \binom{4.68557}{2.58206}$  $\frac{1}{2}(0^{\circ} 12' 44'') = 0^{\circ} 06' 22''$  $F_1F_2 = 5.298;$  $\log F_1 F_2 = 0.72411$ 

As a check,  $F_2F_4$  and  $F_1F_2$  are very nearly equal, as they should be.

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 $\log 2 = 0.30103$ 

### CHAPTER XII.

### MISCELLANEOUS STRUCTURES AND BUILDINGS.

#### WATER-STATIONS AND WATER-SUPPLY.

The water-tank on the tender of a locomo-280. Location. tive has a capacity of from 3000 to 7000 gallons-sometimes less. rarely very much more. The consumption of water is very variable, and will correspond very closely with the work done by the engine. On a long down grade it is very small; on a ruling grade going up it may amount to 150 gallons per mile in exceptional cases, although 60 to 100 gallons would be a more usual figure. A passenger locomotive can run 60 miles or more on one tankful, but freight work requires a shorter interval between water-stations. On roads of the smallest traffic, 15 to 20 miles should be the maximum interval between stations: 10 miles is a more common interval on heavy traffic-roads. But these intervals are varied according to circumstances. In the early history of some of the Pacific railroads it was necessary to attach one or more tank-cars to each train in order to maintain the supply for the engine over stretches of 100 miles and over where there was no water. Since then water-stations have been obtained at great expense by boring artesian wells. The individual locations depend largely on the facility with which a sufficient supply of suitable water may be obtained. Streams intersecting the railroad are sometimes utilized, but if such a stream passes through a limestone region the water is apt to be too hard for use in the boilers. More frequently wells are dug or bored. When the local supply at some determined point is unsuitable. and yet it is necessary to locate a water-station there, it may be found justifiable to pipe the water several miles. The construction of municipal water-works at suitable places along the line has led to the frequent utilization of such supplies. In such cases the railroad is generally the largest single consumer and obtains the most favorable rates. When possible, water-stations are located at regular stopping points and at division termini.

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281. Required qualities of water. Chemically pure water is unknown except as a laboratory product. The water supplied by wells, springs, etc., is always more or less charged with calcium and magnesium carbonates and sulphates, as well as other impurities. The evaporation of water in a boiler precipitates these impurities to the lower surfaces of the boiler, where they sometimes become incrusted and are difficult to remove. The protection of the iron or steel of a boiler from the fierce heat of the fire depends on the presence of water on the other side of the surface, which will absorb the heat and prevent the metal from assuming an excessively high temperature. If the water side of the metal becomes covered or incrusted with a deposit of chemicals, the conduction of heat to the water is much less free, the metal will become more heated and its deterioration or destruction will be much more rapid. An especially common effect is the production of leaks around the joints between tubes and tube-sheets and the joints in the boiler-plates. Such injury can only be prevented by the application of one (or both) of two general methods—(a) the frequent cleaning of the boilers and (b) the chemical purification of the water before its introduction into the boiler. Although "manholes" and "handholes" are made in boilers, it is physically impossible to clean out every corner of the inside of a boiler where deposits will form and where they are especially objectionable-on the tube-sheets. Such a cleaning is troublesome and expensive.

Chemical purification is generally accomplished by treating the water before it enters the boiler. The reagents chiefly employed are quicklime and sodium carbonate. Lime precipitates the bicarbonate of lime and magnesia. Sodium carbonate gives, by double decomposition in the presence of sulphate of lime, carbonate of lime, which precipitates, and soluble sulphate of soda, which is non-incrustant. When this is done in a purifying tank, the purified water is drawn off from the top of the tank and supplied pure to the engines. The precipitants are drawn off from the settling-basin at the bottom of the tank. This purification, which makes no pretense of being chemically perfect, may be accomplished for a few cents per 1000 gallons. It is used much more extensively in Europe than in this country, the Southern Pacific being the only railroad which has employed such methods on a large scale. Reliance is frequently placed on the employment of a "non-incrustant" which is introduced

directly into the boiler. When no incrustation takes place the accumulation of precipitant and mud in the bottom of the boiler may be largely removed by mere "blowing off" or by washing out with a hose.

On the other hand, there is the exceptional case that the water may be too pure. It is well known that distilled water has a very strong corrosive action on iron and that it is possible for the water to be so pure that corrosion of the boiler tubes will be accelerated and that the boilers will rapidly deteriorate in this way. It is therefore occasionally necessary to add a small portion of lime to a very son water, so that a very thin scale will form over the surface of the iron, which will protect the iron from corrosion.

American practice may therefore be summarized as follows: (a) Employing as pure water as possible; (b) cleaning out boilers by "blowing off" or by washing out with a hose or by physical scraping at more or less frequent intervals or when other repairs are being made; (c) the occasional employment of nonincrustants; (d) the occasional chemical treatment of water before it enters the tender-tank.

282. Tanks. Whatever the source, the water must be led or pumped into tanks which are supported on frames so that the

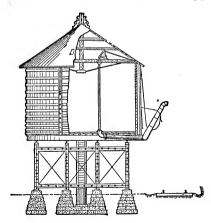


FIG. 160.-WATER-TANK.

bottoms of the tanks are about 12 feet above the rails. Wooden tanks having a diameter of 24 feet, 16 feet high, and with a capacity of over 50,000 gallons, are frequently employed. Iron or steel tanks are also used.

In Table XIV is shown the capacity of cylindrical water-tanks in United States standard gallons of 231 cubic inches. From this table the dimensions of a tank of any desired capacity may

readily be found. Two or more tanks are sometimes used rather than construct one of excessive size. The smaller sizes

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TABLE XIV. — CAPACITY OF CYLINDRICAL WATER-TANKS IN UNITED STATES STANDARD GALLONS OF 231 CUBIC INCHES.

Height		Diameter of tank in feet.						
feet.	10	12	14	16	18	20	22	24
6 7 8 9 10	$3525 \\ 4113 \\ 4700 \\ 5288 \\ 5875$	$5076 \\ 5922 \\ 6768 \\ 7614 \\ 8460$	$\begin{array}{r} 6909 \\ 8061 \\ 9212 \\ 10364 \\ 11515 \end{array}$	$\begin{array}{r} 9024 \\ 10528 \\ 12032 \\ 13536 \\ 15041 \end{array}$	$11421 \\13325 \\15229 \\17132 \\19036$	$14101 \\ 16451 \\ 18801 \\ 21151 \\ 23501$	$17062 \\ 19905 \\ 22749 \\ 25592 \\ 28436$	$\begin{array}{r} 20305\\ 23689\\ 27073\\ 30457\\ 33841 \end{array}$
$     \begin{array}{r}       11 \\       12 \\       13 \\       14 \\       15     \end{array} $	$\begin{array}{r} 6463 \\ 7050 \\ 7638 \\ 8225 \\ 8813 \end{array}$	$\begin{array}{r} 9306 \\ 10152 \\ 10998 \\ 11844 \\ 12690 \end{array}$	$\begin{array}{r} 12667 \\ 13819 \\ 14970 \\ 16122 \\ 17273 \end{array}$	$16545 \\18049 \\19553 \\21057 \\22561$	$\begin{array}{r} 20939\\ 22843\\ 24746\\ 26650\\ 28554\end{array}$	$\begin{array}{c} 25851 \\ 28201 \\ 30551 \\ 32901 \\ 35251 \end{array}$	$\begin{array}{c c} 31280 \\ 34123 \\ 36967 \\ 39810 \\ 42654 \end{array}$	$\begin{array}{r} 37225\\ 40609\\ 43994\\ 47378\\ 50762 \end{array}$
16 17 18 19 20	$\begin{array}{r} 9400\\9988\\10575\\11163\\11750\end{array}$	$\begin{array}{r} 13536 \\ 14383 \\ 15229 \\ 16075 \\ 16921 \end{array}$	$\begin{array}{r} 18425 \\ 19576 \\ 20728 \\ 21879 \\ 23031 \end{array}$	$\begin{array}{r} 24065\\ 25569\\ 27073\\ 28577\\ 30081 \end{array}$	$\begin{array}{r} 30457\\ 32361\\ 34264\\ 36168\\ 38071 \end{array}$	$\begin{array}{r} 37601 \\ 39951 \\ 42301 \\ 44652 \\ 47002 \end{array}$	$\begin{array}{r} 45498 \\ 48341 \\ 51185 \\ 54028 \\ 56872 \end{array}$	$\begin{array}{r} 54146 \\ 57530 \\ 60914 \\ 64298 \\ 67682 \end{array}$
$21 \\ 22 \\ 23 \\ 24 \\ 25$	$\begin{array}{c} 12338\\ 12925\\ 13513\\ 14101\\ 14688 \end{array}$	$17767 \\18613 \\19459 \\20305 \\21151$	$\begin{array}{r} 24182 \\ 25334 \\ 26485 \\ 27637 \\ 28789 \end{array}$	$\begin{array}{r} 31585\\ 33089\\ 34593\\ 36097\\ 37601 \end{array}$	$\begin{array}{r} 39975\\ 41879\\ 43782\\ 45686\\ 47589 \end{array}$	$\begin{array}{r} 49352\\51702\\54052\\56402\\58752\end{array}$	$\begin{array}{c} 59716\\ 62559\\ 65403\\ 68246\\ 71090 \end{array}$	7106774451778358121984603

shown in the table are of course too small for ordinary use, but that part of the table was filled out for its possible convenience otherwise. On single-track roads where all engines use one track the tank may be placed 8' 5" from the track center; this gives sufficient clearance and yet permits the use of a single swinging pipe which will reach from the bottom of the tank to the tender manhole. In Fig, 160 is illustrated one form of wooden tank. They are preferably manufactured by those who make a special business of it and who by the use of special machinery can insure tight joints. When it is inconvenient to place the tank near the track, or when there is a double track, a "stand-pipe" becomes necessary. See § 285. One of the most difficult and troublesome problems is to prevent freezing, particularly in the valves and pipes. Not only are the pipes carefully covered but fires must be maintained during cold When the pumping is accomplished by means of a weather. steam-pump, supplied from a steam-boiler in the pump-house under the tank, coils of steam-pipe may be employed to heat the water or to heat the pipes Partial protection may be obtained by means of a double roof and double bottom, the spaces being filled with sawdust or some other non-conductor of heat.

283. Pumping. The pumping is done most reliably with steam-pumps or gas-engines, although hot-air engines, windmills, and even man-power are occasionally employed. Economy of operation requires that the water-stations shall be so located that each tank shall be used regularly and that each pump shall be regularly operated for maintaining the water-supply. On the other hand, the pump should not be required to regularly work at night to maintain the supply and should have an excess capacity of say 25%. When a tank is but little used, it will still require the labor of an attendant, and his time will be largely wasted unless he can be utilized for other labor about the station. In recent years gasoline has been extensively employed as a fuel for the pumping-engines. The chief advantages of its use lies in the extreme simplicity of the mechanism and the very slight attention it requires, which permits their being operated by station-agents and others, who are paid \$10 per month extra, instead of paving a regular pumper \$35 per month. "Screenings," "slack coal," etc., are used as fuel for steam-pumps and may frequently be delivered at the pump-house at a cost not exceeding 30 cents per ton, but even at that price the cost of pumping per thousand gallons, although dependent on the horizontal and vertical distances to the source of supply and to the tank, will generally run at 2 cents to 6 cents per 1000 gallons. In many cases where steam plants have been replaced by gasoline plants, the cost of pumping per 1000 gallons has been reduced to one third or even one fourth of the cost of steam pumping. Of course the cost, using windmills, is reduced to the mere maintenance of the machinery, but the unreliability of wind as a motive power and the possibility of its failure to supply water when it is imperatively needed has made this form of motive . power unpopular. (See report to Ninth Annual Convention of the Association of Railway Superintendents of Bridges and Buildings, Oct. 1899.)

284. Track tanks. These are chiefly required as one of the means of avoiding delays during fast-train service. A trough, made of steel plate, is placed between the rails on a stretch of *perjectly level* track. A scoop on the end of a pipe is lowered from under the tender into the tank while the train is in motion. The rapid motion scoops up the water, which then flows into the tender tank. The following brief description of an installation on the Baltimore & Ohio Railroad between Baltimore and

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Philadelphia will answer as a general description of the method. The trough is made of  $\frac{3}{16}''$  steel plate, 19" wide, 6" deep, and has a length of 1200 feet. There is riveted on each side a line of  $1\frac{1}{5}'' \times 2'' \times \frac{1}{4}''$  angle bars. These angle bars rest on the ties. Ordinary track spikes hold these angle bars to the ties, but permit expansion as with rails. The tanks are firmly anchored at the center, the ends being free to expand or contract. The plates are 15 feet long and are riveted with  $\frac{7}{15}$ rivets, 20 rivets per joint. At each end is an inclined plane 13' S'' long. If the fireman should neglect to raise the scoop before the end of the tank is reached, the inclined plane will raise it automatically and a catch will hold it raised. Water is supplied to the tanks by a No. 9 Blake pump having a capacity of 260 gallons per minute. During cold weather, freezing is prevented by injecting into the side of the tanks, at intervals of 45 feet, jets of steam, which come through 1" holes. Two boilers of 80 and 95 H.P. are required for pumping and to keep the water from freezing. During warm weather an upright 25 H.P. boiler suffices for the pumping. The cost of installation was about \$10,000 to \$11,000, the cost of maintenance being about \$132.50 per month.

**285.** Stand-pipes. These are usually manufactured by those who make a specialty of such track accessories, and who can ordinarily be trusted to furnish a correctly designed article. In Fig. 161 is shown a form manufactured by the Sheffield Car Co. Attention is called to the position of the valve and to the device for holding the arm parallel to the track when not in use so that it will not be struck by a passing train. When a stand pipe is located between parallel tracks, the strict requirements of clearance demand that the tracks shall be bowed outward slightly. If the tracks were originally straight, they may be shoved over by the trackmen, the shifting gradually running out at about 100 feet each side of the stand-pipe. If the tracks were originally curved, a slight change in radius will suffice to give the necessary extra distance between the tracks.

### BUILDINGS.

286. Station platforms. These are most commonly made of planks at minor stations. Concrete is used in better-class work, also paving brick. An estimate of the cost of a platform of paving brick laid at Topeka, Kan., was \$4.89 per 100 square feet when laid flat and \$7.24 per 100 square feet when laid on edge. The curbing cost 36 cents per linear foot. Cinders, curbed by timbers

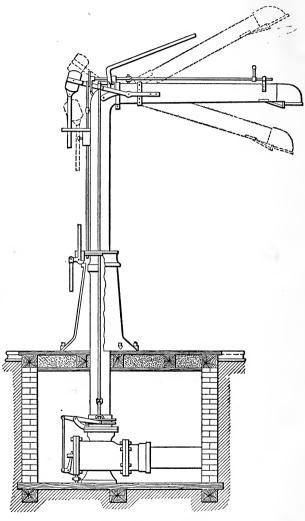


FIG. 161.-STAND-PIPE.

or stone, bound by iron rods, make a cheap and fairly durable platform, but in wet weather the cinders will be tracked into

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the stations and cars. Three inches of crushed stone on a cinder foundation is considered to be still better, after it is once thoroughly packed, than a cinder surface.

**Elevation.**—The elevation of the platform with respect to the rail has long been a fruitful source of discussion. Some roads make the platforms on a level with the top of the rail, others 3" above, others still higher. As a matter of convenience to the passengers, the majority find it easier to enter the car from a high platform, but experience proves that accidents are more numerous with the higher platforms, unless steps are discarded altogether and the cars are entered from level platforms, as is done on elevated roads. As a railroad must generally pay damages to the stumbling passenger, they prefer to build the lower platform. Convenience requires that the rise from the platform to the lowest step should not be greater than the rise of the car steps. This rise is variable, but with the figures usually employed the application of the rule will make the platform 5" to 15" above the rail.

Position with respect to tracks.—Low platforms are generally built to the ends of the ties, or, if at the level of the top of the rail, are built to the rail head. Car steps usually extend 4' 6" from the track center and are 14" to 24" above the rail. The platform must have plenty of clearance, and when the platform is high its edge is generally required to be 5' 6" from the track center.

287. Minor stations. For a complete discussion of the design of stations of all kinds, including the details, the student is referred to "Buildings and Structures of American Railroads," by Walter G. Berg, once Chief Engineer of the Lehigh Valley Railroad. The subject is too large for adequate discussion here, but a few fundamental principles will be referred to.

**Rooms required.** An office and waiting-room is the minimum. A baggage-room, toilet-rooms, and express office are successively added as the business increases. In the Southern States a separate waiting-room for colored people is generally provided. It used to be common to have separate waiting-rooms for men and women. Experience proved that the men's waiting-room became a lounging place and smoking-room for loafers, and now large single waiting-rooms are more common even in the more pretentious designs, smoking being excluded. The office usually has a bay window, so that a more extended view of the track is obtainable. The women's toilet-room is entered from the waiting-room. The men's toilet-room, although built immediately adjoining the other in order to simplify the plumbing, is entered from outdoors. Old-fashioned designs built the station as a residence for the station-agent; later designs have very generally abandoned this idea. "Combination" stations (passenger and freight) are frequently built for small local stations, but their use seems to be decreasing and there is now a tendency to handle the freight business in a separate building.

288. Section-houses. These are houses built along the rightof-way by the railroad company as residences for the trackmen. The liability of a wreck or washout at any time and at any part of the road, as well as the convenience of these houses for ordinary track labor, makes it all but essential that the trackmen should live on the right-of-way of the road, so that they may be easily called on for emergency service at any time of day or night. This is especially true when the road passes through a thinly settled section, where it would be difficult if not impossible to obtain suitable boarding-places. It is in no sense an extravagance for a railroad to build such houses. Even from the direct financial standpoint the expense is compensated by the corresponding reduction in wages, which are thus paid partly in free house rent. And the value of having men on hand for emergencies will often repay the cost in a single night. Where the country is thickly settled the need for such houses is not so great, and railroads will utilize or perhaps build any sort of suitable house. but on Southern or Western roads, where the need for such houses is greater, standard plans have been studied with great care, so as to obtain a maximum of durability, usefulness, comfort, and economy of construction. (See Berg's Buildings, etc., noted above.) On Northwestern roads, protection against cold and rain or snow is the chief characteristic; on Southern roads good ventilation and durability must be chiefly considered. Such houses may be divided into two general classes—(a) those which are intended for trackmen only and which may be built with great simplicity, the only essential requirements being a living-room and a dormitory, and (b) those which are intended for families, the houses being then distinguished as "dwellinghouses for employees.

289. Engine-houses. Small engine-houses are usually built rectangular in plan. Their minimum length should be some-

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what greater than that of the longest engine on the road. They may be built to accommodate two engines on one track, but then they should be arranged to be entered at either end, so that neither engine must wait for the other. In width there may be as many tracks as desired, but if the demand for stalls is large, it will probably be preferable to build a "roundhouse." Rectangular engine-houses are usually entered by a series of parallel tracks switching off from one or more main tracks, no turn-table being necessary. If a turn-table is placed outside (because one

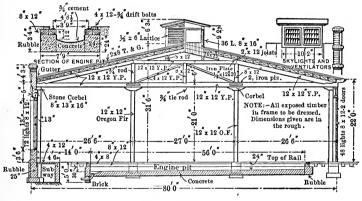


FIG. 162.—ENGINE-HOUSE.

is needed at that part of the road) enough track should be allowed between the house and the turn-table so that engines may be quickly removed from the engine-house in case of fire without depending on the turn-table to get them out of danger.

Roundhouses. The plan of these is generally polygonal rather than circular. The straight walls are easier to build; the construction is more simple, and the general purpose is equally well served. They may be built as a part of a circle or a complete circle, a passageway being allowed, so that there are two entrances instead of one. When space is very limited a roundhouse with turn-table will accommodate more engines in proportion to the space required (including the approaches) than a rectangular house. The enlarged space on the outer side of each segment of a roundhouse furnishes the extra space which is needed for the minor repairs which are usually made in a roundhouse. One disadvantage is that supervision is not quite so easy or effective as in rectangular houses. Of course such houses are used not only for storing and cleaning engines, but also for minor repairs which do not require the engine to be sent to the shops for a general overhauling.

**Construction.** The outer walls are usually of brick. The inner walls consist almost entirely of doors and the piers between them, although there is usually a low wall from the top of the door frames to the roof line, which usually slopes outward so as to turn rain-water away from the central space.

**Roofs.** Many roofs have been built of slate with iron truss framing, with the idea of maximum durability. The slate is good, but experience shows that the iron framing deteriorates very rapidly from the action of the gases of combustion of the engines which must be "fired" in the houses before starting. Roof frames are therefore preferably made of wood.

Floors. These are variously constructed of cinders, wood, brick, and concrete. Brick has been found to be the best material. Anything short of brick is a poor economy; concrete is very good if properly done but is somewhat needlessly expensive.

Ventilation. This is a troublesome more expensive. The general plan is to have "smoke-jacks" which drop down over the stack of each engine as it reaches its precise place in its stall and which will carry away all smoke and gas. Such a movable stack is most easily constructed of thin metal—say galvanized iron—but these will be corroded by the gases of combustion in two or three years. Vitrified pipe, cast iron, expanded metal and cement, and even plain wood painted with "fireproof" paint, have been variously tried, but all methods have their unsatisfactory features. (For an extended discussion of roundhouse floors and ventilation see the Proc. Assoc. of Railway Supts. of Bridges and Buildings for 1898, pp. 112–135.)

### SNOW STRUCTURES.

• 290. Snow-fences. Snow structures are of two distinct kinds—fences and sheds. A snow-fence implies drifting snow snow carried by wind—and aims to cause all drifting snow to be deposited away from the track. Some designs actually succeed in making the wind an agent for clearing snow from the track where it has naturally fallen. A snow-fence is placed at right angles to the prevailing direction of the wind and 50 to 100 feet away from the tracks. When the road line is at right angles to

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the prevailing wind, the right-of-way fence may be built as a snow-fence-high and with tight boarding. Hedges have sometimes been planted to serve this purpose. When the prevailing wind is oblique, the snow fences must be built in sections where they will serve the best purpose. The fences act as wind breakers, suddenly lowering the velocity of the wind and causing the snow carried by the wind to be deposited along the fence. Portable fences are frequently used, which are placed (by permission of the adjoining property owners) outside of the rightof-way. If a drift forms to the height of the portable fence the fence may be replaced on the top of the drift, where it may act as before, forming a still higher drift. When the prevailing wind runs along the track line, snow-fences built in short sections on the sides will cause snow to deposit around them while it scours its way along the track line, actually clearing it. Such a method is in successful operation at some places on the White Mountain and Concord divisions of the Boston & Maine Railroad. Snow-fences, in connection with a moderate amount of shoveling and plowing, suffice to keep the tracks clear on railroads not troubled with avalanches. In such cases snow-sheds are the only alternative.

201. Snow-sheds. These are structures which will actually keep the tracks clear from snow regardless of its depth outside. Fortunately they are only necessary in the comparatively rare situations where the snowfall is excessive and where the snow is liable to slide down steep mountain slopes in avalanches. These avalanches frequently bring down with them rocks, trees, and earth, which would otherwise choke up the road-bed and render it in a moment utterly impassable for weeks to come. The sheds are usually built of  $12'' \times 12''$  timber framed in about the same manner as trestle timbering; the "bents" are sometimes placed as close as 5 feet, and even this has proved insufficient to withstand the force of avalanches. The sheds are therefore so designed that the avalanche will be *deflected* over them instead of spending its force against them. Although these sheds are only used in especially exposed places, yet their length is frequently very great and they are liable to destruction by fire. To confine such a fire to a limited section, "fire-breaks" are made-i.e., the shed is discontinued for a length of perhaps 100 feet. Then, to protect that section of track, a V-shaped deflector will be placed on the uphill side which will deflect all

descending material so that it passes over the sheds. Solid crib work is largely used for these structures. Fortunately suitable timber for such construction is usually plentiful and cheap where these structures are necessary. Sufficient ventilation is obtained by longitudinal openings along one side immediately under the roof. "Summer" tracks are usually built outside the sheds to avoid the discomfort of passing through these semitunnels in pleasant weather. The fundamental elements in the design of such structures is shown in Fig. 163, which illustrates some of the sheds used on the Canadian Pacific Railroad.

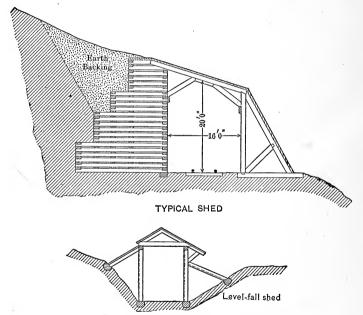


FIG. 163.—SNOW-SHEDS—CANADIAN PACIFIC RAILROAD.

292. Turn-tables. The essential feature of a turn-table is a carriage of sufficient size and strength to carry a locomotive, the carriage turning on a pivot of sufficient size to carry such a load. The carriage revolves in a circular pit whose top has the same general level as the surrounding tracks. The carriages were formerly made largely of wood; very many of those still in use are of cast iron. Structural steel is now uni-

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versally employed for all modern work and since the construction of the carriage and the pivot is a special problem in structures, no further attention will here be paid to the subject. except to that part which the railroad engineer must work out -laying out the site and preparing the foundation. The minimum length of such a carriage (and therefore the diameter of the pit) is evidently the length over all of the longest engine and tender in use on the road. Usually 60-foot turn-tables will suffice for an ordinary road, and for light-traffic roads employing small engines, 50 feet or even less may be sufficient. Many of the heavier freight engines of recent make have a total length of 65 to 70 feet; therefore 75-foot turn-tables are a better standard for heavy-traffic roads. A retaining-wall should be built around the pit. The stability of this wall immediately under the tracks should be especially considered. The most important feature is the stability of the foundation of the pivot. which must sustain a concentrated pressure, more or less eccentric, of perhaps 300 tons. When firm soil or rock may be easily reached, this need give no trouble, but in a soft, treacherous soil a foundation of concrete or piling may be necessary. If the soil is very porous, it may be depended on to carry away all rain-water which may fall into the pit before the foundations are affected, but when the soil is tenacious it may be necessary to drain the subsoil thoroughly and carry off immediately all surface drainage by means of subsoil pipes which have a suitable outfall.

The location of the turn-table in the yard is a part of the general subject of "Yards," and will be considered in the next chapter.

# CHAPTER XIII.

### YARDS AND TERMINALS.

203. Value of proper design. A large part of the total cost of handling traffic, particularly freight, is that incurred at terminals In illustration of this, consider the relative total and stations. cost of handling a car-load of coal and a car-load (of equal weight) of mixed merchandise. The coal will be loaded in bulk on the cars at the mines, where land is comparatively cheap, and the cars grouped into a train without regard to order, since they are (usually) uniform in structure, loading, and con-When the terminal or local station is reached they are tents. run on tracks occupying property which is usually much cheaper than the site of the terminal tracks and freight-houses: they are unloaded by gravity into pockets or machine conveyors and the empty cars are rapidly hauled by the train-load out of the way. On the other hand, the merchandise is loaded by hand on the car from a freight-house occupying a central and valuable location. the car is hauled out into a yard occupying valuable ground, is drilled over the yard tracks for a considerable aggregate mileage before starting for its destination, where the same process is repeated in inverse order. In either case the terminal expenses are evidently a large percentage of the total cost and, once loaded, it makes but little difference just how far the car is hauled to the other terminal. But the very evident increase in terminal charges for general merchandise over those for coal (large as they are) gives a better idea of the magnitude of terminal charges.

Many yards are the result of growth, adding a few tracks at a time, without much evidence of any original plan. In such cases the yard is apt to be very inefficient, requiring a much larger aggregate of drilling to accomplish desired results, requiring much more *time* and hence blocking traffic and finally adding greatly to the cost of terminal service, although the fact of its being a needless addition to cost may be unsuspected or not fully appreciated. An unwillingness or inability to spend money for the necessary changes, and the difficulty of making the changes while the yard is being used, only prolong the bad state of affairs and an inefficient makeshift is frequently adopted. Assume that an improvement in the design of the yard will permit a saving of the use of one switching engine, or for example, that the work may be accomplished with three switching engines instead of four. Assuming a daily cost of \$25, we have in 313 working days an annual saving of \$7825, which, capitalized at 5%, gives \$156,500, enough to reconstruct any ordinary yard.\*

294. Divisions of the subject. The subject naturally divides itself into three heads—(a) Yards for receiving, classifying, and distributing freight cars, called more briefly freight yards; (b)yards and conveniences for the care of engines, such as ash tracks, turn-tables, coal-chutes, sand-houses, water-tanks, or water stand-pipes, etc., and (c) passenger terminals.

### FREIGHT YARDS.

295. General principles. It should be recognized at the start that at many places an ideally perfect yard is impossible, or at least impracticable, generally because ground of the required shape or area is practically unobtainable. But there are some general principles which may and should be followed in every yard and other ideals which should be approached as nearly as possible. Nevertheless every yard is an independent problem. Before taking up the design of freight yards, it is first necessary to consider the general object of such yards and the general principles by which the object is accomplished. These may be briefly stated as follows:

1. A yard is a device, a machine, by which incoming cars are sorted and classified—some sent to warehouses for unloading, some sent to connecting railroads, some made up for local distribution along the road, some sent for repairs, and, in short a device by which all cars are sent *through* and *out* of the yard as quickly as possible.

2. Except when a road's business is decreasing, or when its equipment is greater than its needs and its cars must be stored, efficiency of management is indicated by the rapidity with which the passage of cars *through* the yard is accomplished.

3. When a yard is the terminal of a "division," the freight

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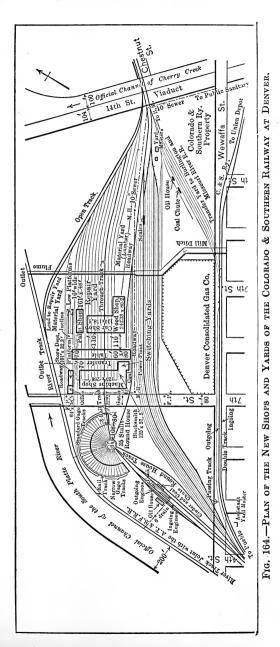
<sup>\*</sup> Estimate of Mr. H. G. Hetzler, C., B. & Q. Ry.

trains will be pulled into a "receiving track" and the engine and caboose detached. The caboose will be run on to a "caboose track," which should be conveniently near, and the engine is run off to the engine yard. If the train is a "through" train and no change is to be made in its make-up, it will only need to wait for another engine and perhaps another caboose. If the cars are to be distributed, they will be drawn off by a switching engine to the "classification yard."

4. The design of a yard is best studied by first picking out the ladder tracks and the through tracks which lead from one division of the yard to another. These are tracks which must always be kept open for the passage of trains, in contradistinction to the tracks on which cars may be left standing, even though it is only for a few moments, while drilling is being done. Such a set of tracks, which may be called the skeleton of the yard, is shown by heavy lines in Fig. 164. Each line indicates a pair of rails. The tracks of the storage yards are shown by the lighter lines.

5. There is a distinct advantage in having all storage tracks double-ended—except "team tracks." Team tracks are those which have spaces for the accommodation of teams, so that loading or unloading may be done directly between the cars and teams. To avoid the necessity of teams passing over the tracks, these are best placed on the outskirts of the yard and consist of short stubsidings arranged in pairs. But storage tracks should have an outlet at each end so as to reduce the amount of drilling neces sary to reach a car which may be at the extreme end of a long string of cars. This is done usually by means of two "ladder" tracks, parallel to each other, which thus make the storage tracks between them of equal length.

6. The equality of length of these storage tracks is a point insisted on by many, but on the other hand, trains are not always of uniform length even on any one division. Loaded trains and trains of empties will vary greatly in length, and the various styles and weights of freight engines employed necessitate other variations in the weights and lengths of trains hauled. With storage tracks of somewhat variable length a larger percentage of track length may be utilized, there will be less hauling over a useless length of track, and (assuming that the plot of ground available for yard purposes has equally favorable conditions for yard design) more business may be handled in a yard of given area. § 295.



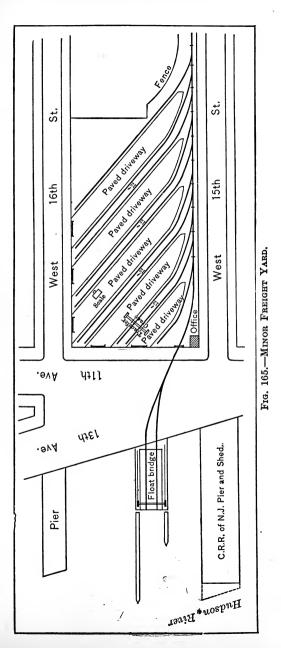
7 Yards are preferably built so that the tracks have a grade of 0.5%—sometimes a little more than this—in the direction of the traffic through the yard. This grade, which will overcome a tractive resistance of 10 pounds per ton, will permit cars to be started down the ladder tracks by a mere push from the switching engine. They are then switched on to the desired storage track\_and run down that track by gravity until stopped at the desired place by a brakeman riding on the cars

8. Although not absolutely necessary, there is an advantage in having all frog numbers and switch dimensions uniform. No. 7 frogs are most commonly used. Sharper-angled frogs make easier riding, less resistance and less chance of derailment, but on the other hand require longer leads and more space. No. 6 and even No. 5 frogs are sometimes used on account of economy of space, but they have the disadvantages of greater tractive resistance, greater wear and tear on track and rolling stock, and greater danger of derailment.

206. Relation of yard to main tracks. Safety requires that there should be no connection between the yard tracks and the main tracks except at each end of the vard, where the switches should be amply protected by signals. Sometimes the main tracks run through the yard, making practically two yards-one for the traffic in either direction-but this either requires a double layout of tracks and houses (such as ash tracks, coal-chutes, sandhouses, etc.), or a very objectionable amount of crossing of the main-line tracks. The preferable method is to have the main line tracks entirely on the outside of the vard. A method which is in one respect still better is to spread the main tracks so that they run on each side of the yard. In this case there is never any necessity to cross one main track to pass from the yard to the other main track; a train may pass from the yard to either main track and still leave the other main track free and open. The ideal arrangement is that by which some of the tracks cross over or under all opposing tracks. By this means all connections between the yard and the main tracks may be by "trailing" switches; that is, trains will run on to the main track in the direction of motion on that main track. Of course all this applies only to *double* main track.

An important element of yard design is to have a few tracks immediately adjoining the main tracks and separate from the yard proper on which outgoing trains may await their orders to take § 296.





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the main track. When the orders come, they may start at once without any delay, without interfering with any yard operations, and they are not occupying tracks which may form part of the system needed for switching.

207. Minor freight yards. The term here refers to the substations, only found in the largest cities, to which cars will be sent to save in the amount of necessary team hauling and also to relieve a congestion of such loading and unloading at the main freight terminal. The cars are brought to these yards sometimes on floats (as is done so extensively at various points around New York Harbor), or they are run down on a long siding running perhaps through the city streets. But the essential feature of these vards is the maximum utilization of every square foot of yard space, which is always very valuable and which is frequently of such an inconvenient shape that a great ingenuity is required to obtain good results. There is generally a temptation to use excessively sharp curves. When the radii are greater than 175 feet no especial trouble is encountered. Curves with radius as short as 50 feet have been used in some vards. On such curves the long cars now generally used make a sharper angle with each other than that for which the couplers were designed and special coupler-bars become necessary. The two general methods of construction are (a) a series of parallel team tracks (as previously described and as illustrated further in Fig. 165), and (b) the "loop system," as is illustrated in Fig. 166.

208. Transfer cranes. These are almost an essential feature for vards doing a large business. The transportation of builtup girders, castings for excessively heavy machinery, etc., which weigh five to thirty tons and even more, creates a necessity for machinery which will easily transfer the loads from the car to the truck and vice versa. An ordinary "gin-pole" will serve the purpose for loads which do not much exceed five tons. A fixed framework, covering a span long enough for a car track and a team space, with a trolley traveling along the upper chord, is the next design in the order of cost and convenience. Increasing the span so that it covers two car tracks and two team spaces will very materially increase the capacity. Making the frame movable so that it travels on tracks which are parallel to the car tracks, giving the frame a longitudinal motion equal to two or three car lengths, and finally operating the raising and traveling mechanism by power, the facility for rapidly disposing of

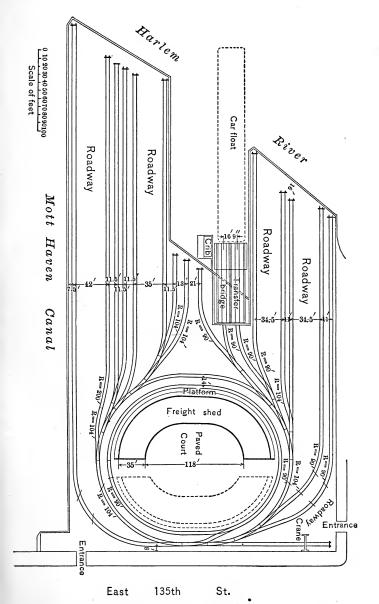


FIG. 166.-MINOR FREIGHT YARD ON A HARBOR FRONT.

heavy articles of freight is greatly increased. Of course only a very small proportion of freight requires such handling, and the business of a yard must be large or perhaps of a special character to justify and pay for the installation of such a mechanism. Figs. 165 and 166 each indicate a transfer crane, evidently of the fixed type.

299. Track scales. The location of these should be on one of the receiving tracks near the entrance to the yard, but not on the main track. It is always best to have a "dead track" over the scales—i.e., a track which has one rail on the solid side wall of the scale pit and the other supported at short intervals by posts which come up through the scale platform and yet do not touch it. These rails and the regular scale rails switch into one track by means of point rails a few feet beyond each end of the scales. The switches should be normally set so that all trains will use the dead track, unless the scales are to be operated. It has been found possible in a gravity yard to weigh a train with very little loss of time by running each car slowly by gravity over the scales and weighing them as they pass over.

### ENGINE YARDS.

300. General principles. Engine yards must contain all the tracks, buildings, structures, and facilities which are necessary for the maintenance, care, and storage of locomotives and for providing them with all needed supplies. The supplies are fuel, water. sand. oil. waste, tallow, etc. Ash-pits are generally necessary for the prompt and economical disposition of ashes; enginehouses are necessary for the storage of engines and as a place where minor repairs can be quickly made. A turn-table is another all but essential requirement. The arrangement of all these facilities in an engine yard should properly depend on the form of the yard. In general they should be grouped together and should be as near as possible to the place where through engines drop the trains just brought in and where they couple on to assembled outgoing trains, so that all unnecessary running light may be avoided. In Figs. 164 and 167 are shown two designs which should be studied with reference to the relative arrangement of the yard facilities.

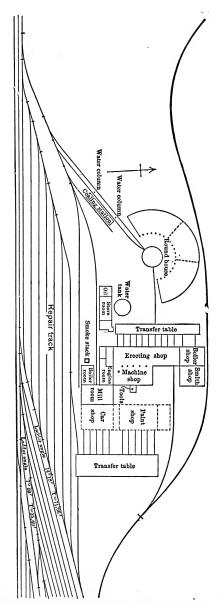


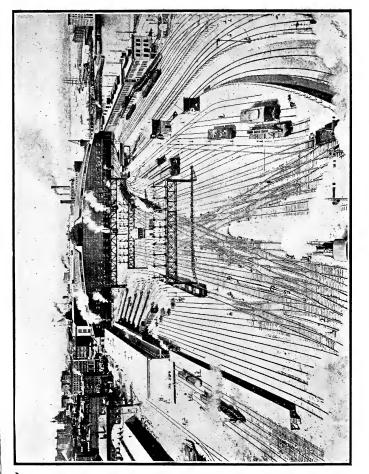
FIG. 167.-ENGINE YARD AND SHOPS, URBANA, ILL.

#### RAILROAD CONSTRUCTION.

## PASSENGER TERMINALS.

(Passenger terminals are one of the logical subdivisions of this chapter, but their construction does not concern one engineer in a thousand. The local conditions attending their construction are so varied that each case is a special problem in itself—a problem which demands in many respects the services of the architect rather than the engineer. The student who wishes to pursue this subject is referred to an admirable chapter ir "Buildings and Structures of American Railroads," by Walter G. Berg, Chief Engineer of the Lehigh Valley Railroad.)

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To face p. 350.) (Published through courtesy of Union Switch and Signal Co.)



## CHAPTER XIV.

## BLOCK SIGNALING.

#### GENERAL PRINCIPLES.

**301.** Two fundamental systems. The growth of systems of block signaling has been enormous within the last few years—both in the amount of it and in the development of greater perfection of detail. The development has been along two general lines: (a) the manual, in which every change of signal is the result of some definite action on the part of some signalman, but in which every action is so controlled or limited or subject to the inspection of others that a mistake is nearly, if not quite, impossible; (b) the *automatic*, in which the signals are operated by mechanism, which cannot set a wrong signal as long as the mechanism is maintained in proper order. The fundamental principles of the two systems will be briefly outlined, after which the chief details of the most common systems will be pointed out.

**302.** Manual systems. Any railroad which has a telegraph line and an operator at all regular stations may (and frequently does) operate its trains according to the fundamental principles of the manual block system even though it makes no claim to a block-signal system. The basic idea of such a system is that after a train has passed a given telegraph- or signal-station, no other train will be permitted to follow it into that "block" until word is telegraphed from the next station ahead that the first train has passed out of that block. With a double-track road the operation is very simple; trains may be run at short intervals with long blocks; with an average speed of 30 miles per hour and blocks 5 miles long, trains *could* be run on a ten minute interval (nearly). A road with any such traffic would, of course, have much shorter blocks, and, practically, they would need to be considerably shorter.

With a single-track road the operation is much more complex, since the operator must keep himself informed of the movements of the trains in both directions. The ratio of length of block to train interval would be only one half (and practically much less than half) what it could be with a double-track road. When such a system is adhered to rigidly, it is called an absolute block system. But when operating on this system, a delay of one train will necessarily delay every other train that follows closely after. A portion, if not all, of the delay to subsequent trains may be avoided, although at some loss of safety, by a system of permissive blocking. By this system an operator may give to a succeeding train a "clearance card" which permits it to pass into the next block, but at a reduced speed and with the train under such control that it may be stopped on very short notice, especially near curves. One element of the danger of this system is the *discretionary* power with which it invests the signalmen, a discretion which may be wrongfully exercised. A modification (which is a fruitful source of collisions on single-track roads) is to order two trains to enter a block approaching each other, and with instructions to pass each other at a passing siding at which there is no telegraphstation. When the instructions are properly made out and literally obeyed, there is no trouble, but every thousandth or ten thousandth time there is a mistake in the orders, or a misunderstanding or disobedience, and a collision is the result. The telegraph line, a code of rules, a corps of operators, and signals under the immediate control of the operators, are all that is absolutely needed for the simple manual system.

303. Development of the manual system. One great difficulty with the simple system just described is that each operator is practically independent of others except as he may receive general or specific orders from a train-dispatcher at the division headquarters. Such difficulties are somewhat overcome by a very rigid system of rules requiring the signalmen at each station to keep the adjacent signalmen or the train-dispatcher informed of the movements of all trains past their own stations. When these rules (which are too extensive for quotation here) are strictly observed, there is but little danger of accident, and a neglect by any one to observe any rule will generally be apparent to at least one other man. Nevertheless the safety of trains depends on *each* signalman doing his duty, and a little carelessness or forgetfulness on the part of any one man may cause an accident. The signaling between stations *may* be done by ordinary telegraphic messages or by telephone, but is frequently done by electric bells, according to a code of signals, since these may be readily learned by men who would have more difficulty in learning the Morse code.

In order to have the signalmen mutually control each other, the "controlled manual" system has been devised. The first successful system of this kind which was brought into extensive use is the "Sykes" system, of which a brief description is as follows: Each signal is worked by a lever; the lever is locked by a latch, operated by an electro-magnet, which, with other necessary apparatus, is inclosed in a box. When a signal is set at danger, the latch falls and locks the lever, which cannot be again set free until the electro-magnet raises the latch. The magnet is energized only by a current, the circuit of which is closed by a "plunger" at the next station ahead; just above the plunger is an "indicator," also operated by the current, which displays the words *clear* or *blocked*. (There are variations on this detail.) When a train arrives at a block station (A), the signalman should have previously signaled to the station ahead (B) for permission to free the signal. The man ahead (B)pushes in the "plunger" on his instrument (assuming that the previous train has already passed him), which electrically opens the lock on the lever at the previous station (A). The signal at A can then be set at "safety." As soon as the train has passed A the signal at A must be set at "danger." A further development is a device by which the mere passage of the train over the track for a few feet beyond the signal will automatically throw the signal to "danger." After the signal once goes to danger, it is automatically locked and cannot be released except by the man in advance (B), who will not do so until the train has passed him. The "indicator" on B's instrument shows "blocked" when A's signal goes to danger after the train has passed A, and B's plunger is then locked, so that he cannot release A's signal while a train is in the block. As soon as the train has passed A, B should prepare to get his signals ready by signaling ahead to C, so that if the block between B and Cis not obstructed, B may have his signals at "safety" so that the train may pass B without pausing. The student should note the great advance in safety made by the Sykes system; a signal cannot be set free except by the combined action of two men, one the man who actually operates the signal and

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the other the man at the station ahead, who frees the signal electrically and who by his action certifies that the block immediately ahead of the train is clear.

A still further development makes the system still more "automatic" (as described later), and causes the signal to fall to danger or to be kept locked at danger, if even a single pair of wheels comes on the rails of a block, or if a switch leading from a main track is opened.

304. Permissive blocking. "Absolute" blocking renders accidents due to collisions almost impossible unless an engineer runs by an adverse signal. The signal mechanism is usually so designed that, if it gets out of order, it will inevitably fall to "danger," i.e., as described later, the signal-board is counterbalanced by a weight which is much heavier. If the wire breaks, the counterweight will fall and the board will assume the horizontal position, which always indicates "danger." But it sometimes happens that when a train arrives at a signal-station, the signalman is unable to set the signal at safety. This may be because the previous train has broken down somewhere in the next block, or because a switch has been left open, or a rail has become broken, or there is a defect of some kind in the electrical connections. In such cases, in order to avoid an indefinite blocking of the whole traffic of the road, the signalman may give the engineer a "caution-card" or a "clearance card," which authorizes him to proceed slowly and with his train under complete control into the block and through it if possible. If he arrives at the next station without meeting any obstruction it merely indicates a defective condition of the mechanism, which will, of course, be promptly remedied. Usually the next section will be found clear, and the train may proceed as usual. On roads where the "controlled manual" system has received its highest development, the rules for permissive blocking are so rigid that there is but little danger in the practice. unless there is an absolute disobedience of orders.

305. Automatic systems. By the very nature of the case, such systems can only be used to indicate to the engineers of trains something with reference to the passage of previous trains. The complicated shifting of switches and signals which is required in the operation of yards and terminals can only be accomplished by "manual" methods, and the only automatic features of these methods consist in the mechanical checks (electric and otherwise), which will prevent wrong combinations of signals. But for long stretches of the road, where it is only required to separate trains by at least one block length, an automatic system is generally considered to be more reliable. As expressed forcibly by a railroad manager, "an automatic system does not go to sleep, get drunk, become insane, or tell lies when there is any trouble." The same cannot always be said of the employés of the manual system.

The basic idea of all such systems is that when a train passes a signal-station (A), the signal automatically assumes the "danger" position. This may be accomplished electrically, pneumatically, or even by a direct mechanism. When the train reaches the end of the block at B and passes into the next one, the signal at B will be set at danger and the signal at A will be set at safety. The lengths of the blocks are usually so great that the only practicable method of controlling from B a mechanism at A is by electricity, although the actual motive power at A may be pneumatic or mechanical. At one time the current from A to B was carried on ordinary wires. This method has the very positive advantage of reliability, definite resistance to the current, and small probability of short-circuiting or other derangement. But now all such systems use the rails for a track circuit and this makes it possible to detect the presence of a single pair of wheels on the track anywhere in the block, or an open switch, or a broken rail. Any such circumstances, as well as a defect in the mechanism, will break or short-circuit the current and will cause the signal to be set at danger. To prevent an indefinite blocking of traffic owing to a signal persistently indicating danger, most roads employing such a system have a rule substantially as follows: When a train finds a signal at danger, after waiting one minute (or more, depending on the rules), it may proceed slowly, expecting to find an obstruction of some sort: if it reaches the next block without finding any obstruction and finds the next signal clear. it may proceed as usual, but must promptly report the case to the superintendent. Further details regarding these methods will be given later. See § 310.

306. "Distant" signals. The close running of trains that is required on heavy-traffic roads, especially where several branches combine to enter a common terminal, necessitates the use of very short blocks. A heavy train running at high speed can hardly make a "service" stop in less than 2000 feet, while the curves of a road (or other obstructions) frequently make it difficult to locate a signal so that it can be seen more than a few hundred feet away. It would therefore be impracticable to maintain the speed now used with heavy trains if the engineer had no foreknowledge of the condition in which he will find a signal until he arrives within a short distance of it. To overcome this difficulty the "distant" signal was devised. This is placed about 1800 or 2000 feet from the "home" signal, and is interlocked with it so that it gives the same signal. The distant signal is frequently placed on the same pole as the home signal of the previous block. When the engineer finds the distant signal "clear," it indicates that the succeeding home signal is also clear, and that he may proceed at full speed and not expect to be stopped at the next signal; for the distant signal cannot be cleared until the succeeding home signal is cleared, which cannot be done until the block succeeding that is clear. A clear distant signal therefore indicates a clear track for two succeeding blocks. When the engineer finds the distant signal blocked, he need not stop (providing the home signal is clear). It simply indicates that he must be prepared to stop at the next home signal and must reduce speed if necessary. It may happen that by the time he reaches the succeeding home signal it has already been cleared, and he may proceed without stopping. This device facilitates the rapid running of trains, with no loss of safety, and vet with but a moderate addition to the signaling plant.

307. "Advance" signals. It sometimes becomes necessary to locate a signal a few hundred feet short of a regular passenger-station. A train might be halted at such a signal because it was not cleared from the signal-station ahead—perhaps a mile or two ahead. For convenience, an "advance" signal may be erected immediately beyond the passenger-station. The train will then be permitted to enter the block as far as the advance signal and may deliver its passengers at the station. The advance signal is interlocked with the home signal back of it, and cannot be cleared until the home signal is cleared and the entire block ahead is clear. In one sense it adds another block, but the signal is entirely controlled from the signal station back of it.

### MECHANICAL DETAILS.

**308.** Signals. The primitive signal is a mere cloth flag. A better signal is obtained when the flag is suspended in a suitable place from a fixed horizontal support, the flag weighted at the bottom, and so arranged that it may be drawn up and out of sight by a cord which is run back to the operator's office. The next step is the substitution of painted wood or sheet metal for the cloth flag, and from this it is but a step to the standard semaphore on a pole, as is illustrated in Fig. 168. The simple flag, operated for convenience with a cord, is the signal employed on thousands of miles of road, where they perhaps make no claim to a block-signal system, and yet where the trains are run according to the fundamental rules of the simple manual block method.

Semaphore boards. These are about 5 feet long, 8 inches wide at one end, and tapered to about 6 inches wide at the hinge end. The boards are fastened to a casting which has a ring to hold a red glass which may be swung over the face of a lantern, so as to indicate a red signal. "Distant" signal-boards usually have their ends notched or pointed; the "home" signal-boards are square ended. The boards\_are always to the *right* of the hinge when a train is approaching them. The "home" signals are generally painted red and the "distant" signals green, although these colors are not invariable. The backs of the boards are painted white. Therefore any signal-board which appears on the *left* side of its hinge will also appear *white*, and is a signal for traffic in the opposite direction, and is therefore of no concern to an engineman.

Poles and bridges. When the signals are set on poles, they are generally placed on the right-hand side of the track. When there are several tracks, four or more, a bridge is frequently built and then each signal is over its own track. When switches run off from a main track, there may be several signal-boards over one track. The upper one is the signal for the main track and the lower ones for the several switches. In Fig. 169 is shown a "bridge" with its various signal-boards controlling the several tracks and the switches running off from them.

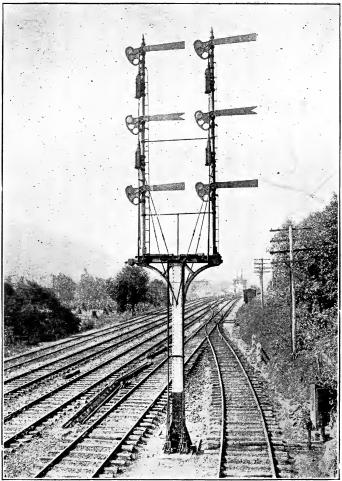
"Banjo" signals. This name is given to a form of signal, illustrated in Fig. 170, in which the indication is taken from the color of a round disk inclosed with glass. This is the distinctive signal of the Hall Signal Company, and is also used by the Union Switch and Signal Company. The great argument in their favor is that they may be worked by an electric current of low voltage, which is therefore easily controlled; that the mechanism is entirely inside of a case, is therefore very light, and is not exposed to the weather. The argument urged against them is that it is a signal of *color* rather than *form* or *position*, and that in foggy weather the signal cannot be seen so easily; also that unsuspected color-blindness on the part of the engineman may lead to an accident. Notwithstanding these objections, this form of signal is used on thousands of miles of line in this country.

309. Wires and pipes. Signals are usually operated by levers in a signal-cabin, the levers being very similar to the reversinglever of a locomotive. The distance from the levers to the signals is, of course, very variable, but it is sometimes 2000 feet. The connecting-link for the most distant signals is usually No. 9 wire; for nearer signals and for all switches operated from the cabin it may be 1-inch pipe. When not too long, one pipe will serve for both motions, forward and back. When wires are used, it is sometimes so designed (in the cheaper systems) that one wire serves for one motion, gravity being depended on for the other, but now all good systems require two wires for each signal.

**Compensators.** Variations of temperature of a material with as high a coefficient as iron will cause very appreciable difference of length in a distance of several hundred feet, and a dangerous lack of adjustment is the result. To illustrate: A fall of  $60^{\circ}$  F. will change the length of 1000 feet of wire by

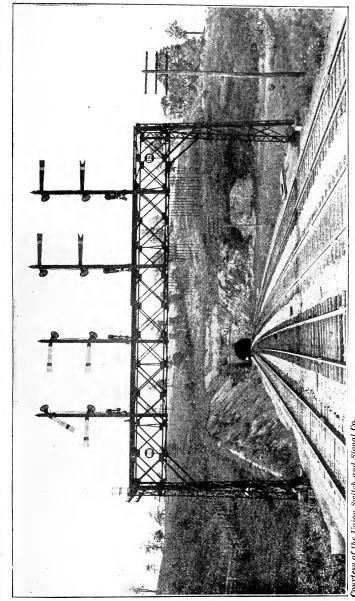
## $1000 \times 60 \times .0000065 = 0.39$ foot = 4.68 inches.

A much less change than this will necessitate a readjustment of length, unless automatic compensators are used. A compensator for pipes is very readily made on the principle illustrated in Fig. 171. The problem is to preserve the distance between a and d constant regardless of the temperature. Place the compensator half-way between a and d, or so that ab = cd. A fall of temperature contracts ab to ab'. Moving b to b' will cause c to move to c', in which bb' = cc'. But cd has also shortened to c'd; therefore d remains fixed in position. (To face page 358.)



Courtesy of the Union Switch and Signal Co. Fig. 168.—SEMAPHOREA.





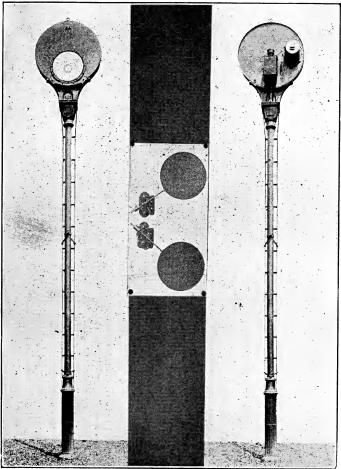
(To face page 358.)

Fig. 169.—Signal Bridge.

Courtesy of the Union Switch and Signal Co.



# (To face page 358.)



Courtesy of the Union Switch and Signal Co. Fig. 170.—" BANJO" SIGNALS.



The regulations of the A. R. E. & M. W. Assoc. require that "A compensator shall be provided for each pipe line over fifty (50) feet in length and under eight hundred (800) feet, with crank-arms eleven by thirteen  $(11 \times 13)$  inch centers. From eight hundred (800) to twelve hundred (1200) feet in length, crank-arms shall be eleven by sixteen  $(11 \times 16)$  inch centers. Pipe lines over twelve hundred (1200) feet in length shall be provided with an additional compensator.

"Compensators shall have one sixty (60) degree and one one hundred and twenty (120) degree angle-cranks and connecting

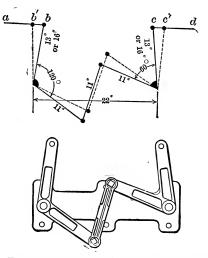


FIG. 171.-STANDARD PIPE COMPENSATOR.

link, mounted in cast iron base, having top of center pins supported. The distance between center of pin-holes shall be twenty-two (22) inches."

The compensator should be placed in the middle of the length when only one is used. When two are used they should be placed at the quarter points. Note that in operating through a compensator the *direction* of motion changes; i.e., if a moves to the right, d moves to the left, or if there is compression in abthere is tension in cd, and vice versa. Therefore this form of compensator can only be used with pipes which will withstand compression. It has seemed impracticable to design an equally

§ 309.

satisfactory compensator for wires, although there are several designs on the market.

The change of length of these bars is so great that allowance must be made for the temperature at the time of installation. On the basis of 50° as the mean temperature, the pipes are so adjusted that the distance between the points b and c of Fig. 171 is made greater or less than 22 inches, according to the temperature of installation. For example, if the temperature were  $80^{\circ}$  and the length of the piping were 900 feet, the length of the pipes should be adjusted so that bc is less than 22 inches by an amount equal to  $900 \times (80^{\circ} - 50^{\circ}) \times .0000065 = 0.1755$  feet= 2.106 inches. The length should therefore be 19.9 inches instead of 22 inches. If the mean temperature was very different (say in Florida) some higher temperature should be taken as normal, so that the extreme range above and below the normal shall be approximately the same.

Guides around curves and angles. When wires are required to pass around curves of large angle, pulleys are used, and a length of chain is substituted for the wire. For pipes, when the curve is easy the pipes are slightly bent and are guided through pulleys. When the angle is sharper, "angles" are used. The operation of these details is self-evident from an inspection of Fig. 172.

310. Track circuit for automatic signaling. The several systems of automatic signaling differ in the minor details, but nearly all of them agree in the following particulars. A current of low potential is run from a battery at one end of a section through one line of rails to the other end of the section, then through a relay, and then back to the battery through the other

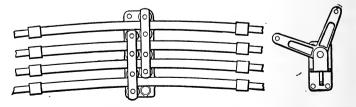
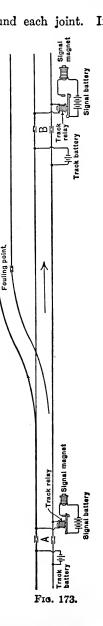


FIG. 172.—DEFLECTING-RODS.

line of rails. To avoid the excessive resistance which would occur at rail joints which may become badly rusted, a wire

suitably attached to the rails is run around each joint. In order to insulate the rails of one section from the rails at either end and yet maintain the rails structurally continuous, the ends of the rails at these dividing points are separated by an insulator and the joint pieces are either made of wood or have some insulating material placed between the rails and the ordinary metal joint. The bolts must also be insulated. When the relay is energized by a current, it closes a local circuit at the signalstation, which will set the signal there at "safety." The resistance of the relay is such that it requires nearly the whole current to work it and to keep the local circuit closed. Therefore. when there is any considerable loss of current from one rail to the other, the relay will not be sufficiently energized, the local circuit will be broken, and the signal will automatically fall to danger. This diversion of current from one rail to the other before the current reaches the relay may be caused in several ways: the presence of a pair of wheels on the rails anywhere in the section will do it; also the breakage of a rail; also the opening of a switch anywhere in the section; also the presence of a pair of wheels on a siding between the "fouling point" and the switch. (The "fouling point" of a siding is that point where the rails first commence to approach the main track.) In Fig. 173 is shown all of the above details as well as some others. At A, B, and the "fouling point" are shown the insulated joints. The batteries and signals are arranged for train motion



to the right. When a train has passed the points near A, where the wires leave the rails for the relay, the current from the "track battery" at B will pass through the wheels and axles, and although no electrical connection is broken, so much current will be shunted through the wheels and axles that the weak current still passing through the relay is not strong enough to energize it against its spring and the "signal-magnet" circuit is broken, and the signal A goes to "danger." At the turnout the rails between the fouling point and the switch are so connected (and insulated) that a pair of wheels on these rails will produce the same effect as a pair on the main track. This is to guard against the effect of a car standing too near the switch, even though it is not on the main track. When the train passes B, if there is no other interruption of the current, the track battery at B again energizes the relay at A, the signal-magnet circuit at A is closed, and the signal is drawn to "safety."

(The present edition has omitted several subdivisions of this general subject, notably the "staff system," used chiefly in England, and all discussions of "interlocking" which is an essential feature of the operation of large terminal yards. A future edition may supply these deficiencies, although an exhaustive treatment of the subject of Signaling would require **a** separate volume.)

## CHAPTER XV.

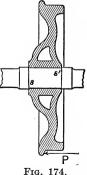
#### ROLLING-STOCK.

(It is perhaps needless to say that the following chapter is in no sense a course in the design of locomotives and cars. Its chief idea is to give the student the elements of the construction of those vehicles which are to use the track which he may design—to point out the mutual actions and reactions of vehicle against track and to show the effect on track wear of variations in the design of rolling-stock. The most of the matter given has a direct practical bearing on track-work, and it is considered that all of it is so closely related to his work that the civil engineer may study it with profit.)

#### WHEELS AND RAILS.

**311.** Effect of rigidly attaching wheels to their axles. The wheels of railroad rolling-stock are invariably secured rigidly to the axles, which therefore revolve with the wheels. The chief reason for this is to avoid excessive wear between the axles and the wheels.

Any axle must always be somewhat loose in its journals. A sidewise force P (see Fig. 174) acting against the circumference of the wheel will produce a much greater pressure on the axle at S and S', and if the wheel moves on the axle, the wear at S and S' will be excessive. But when the axle is fitted to the wheel with a "forced fit" and does not revolve, the mere *pressure* produced at S is harmless. When two wheels are fitted tight to an axle, as in Fig. 175, and the axle revolves in the journals aa, a sidewise pressure of the rail against



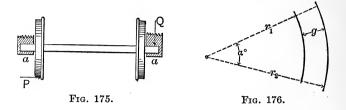
nals aa, a sidewise pressure of the rail against the wheel flange will only produce a slight and harmless increase of the journal pressure Q, although at Q there is sliding contact. Twist-363

## RAILROAD CONSTRUCTION.

in these superiorally and it is

§ 312.

ing action in the journals is thus practically avoided, since a small pressure at the journal-boxes at each end of the axle suffices to keep the axle truly in line.



On the other hand, when the wheels are rigidly attached to their axles, both wheels must turn together, and when rounding curves, the inner rail being shorter than the outer rail, one wheel must slip by an amount equal to that difference of length. The amount of this slip is readily computable:

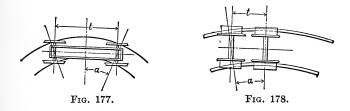
Longitudinal 
$$slip = \frac{2\pi a^{\circ}}{360^{\circ}}(r_2 - r_1) = \frac{2\pi g}{360^{\circ}}a^{\circ} = Ca^{\circ}$$
, (136)

in which C is a constant for any one gauge, and g = the track gauge =  $(r_2 - r_1)$ . For standard gauge (4.708) the slip is .08218 foot per degree of *central angle*. This shows that the longitudinal slipping around any curve of any given central angle will be independent of the degree of the curve. The constant (.08218) here given is really somewhat too small, since the true gauge that should be considered is the distance between the lines of tread on the rails. This distance is a somewhat indeterminate and variable quantity, and probably averages 4.90 feet, which would increase the constant to .086. The slipping may occur by the inner wheel slipping ahead or the outer wheel slipping back, or by both wheels slipping. The total slipping will be constant in any case. The slipping not only consumes power, but wears both the wheels and the rail. But even these disadvantages are not sufficient to offset the advantages resulting from rigid wheels and axles.

312. Effect of parallel axles. Trucks are made with two or three parallel axles (except as noted later), in order that the axles shall mutually guide each other and be kept approximately

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perpendicular to the rails. If the curvature is very sharp and the wheel-base comparatively long (as is notably the case on street railways at street corners), the front and rear wheels



will stand at the same angle (a) with the track, as shown in Fig. 177. But it has been noticed that for ordinary degrees of curvature, the rear wheels stand radial to the curve (see Fig. 178), and for steam railroad work this is the normal case. When the two parallel axles are on a curve (as shown), the wheels tend to run in a straight line. In order that they shall run on a curve they must slip laterally. The principle

is illustrated in an exaggerated form in Fig. 179. The wheel *tends* to roll from atoward b. Therefore in passing along the track from a to c it must actually slip laterally an amount bc which equals  $ac \sin a$ .

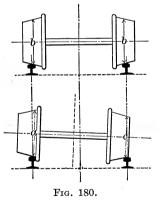
Fig. 179.

Let t = length of the wheel-base (Figs. 177 and 178); r = radius of curve; then for the first case (Fig. 177),  $\sin a = t \div 2r$ ; for the second and usual case (Fig. 178),  $\sin a = t \div r$ ; for t=5 feet and r = radius of a 1° curve,  $a = 0^{\circ} 03'$  for the second case. a varies (practically) as the degree of curve. The lateral slipping per unit of distance traveled therefore equals  $\sin a$ . As an illustration, given a 5-foot wheel-base on a 5° curve,  $a = 0^{\circ} 15'$ ,  $\sin a = .00436$ , and for each 100 feet traveled along the curve the lateral slipping of the front wheels would be 0.436 foot. There would be no lateral slipping of the rear wheels, assuming that the rear axle maintained itself radial.

From the above it might be inferred that the flanges of the forward wheels will have much greater wear than those of the rear wheels. Since cars are drawn in both directions about equally, no difference in flange wear due to this cause will occur, but locomotives (except switching-engines) run forward almost exclusively, and the excess wear of the front wheels of the pilotand tender-trucks is plainly observable.

For a given curve the angle  $\alpha$  (and the accompanying resistance) is evidently greater the greater the distance between the axles. On the other hand, if the two axles are very close together, there will be a tendency for the truck to twist and the wheels to become jammed, especially if there is considerable play in the gauge. The flange friction would be greater and would perhaps exceed the saving in lateral slipping. A general rule is that the axles should never be closer together than the gauge.

Although the slipping per unit of length along the curve varies directly as the degree of curvature, the length of curve necessary to pass between two tangents is inversely as the degree of curve, and the total slipping between the two tangents is independent of the degree of curve. Therefore when a train passes between



two tangents, the total slipping of the wheels on the rails, longitudinal and lateral, is a quantity which depends only on the central angle and is independent of the radius or degree of curve.

313. Effect of coning wheels. The wheels are always set on the axle so that there is some "play" or chance for lateral motion between the wheel-flanges and the rail. The treads of the wheel are also "coned." This coning and play of gauge are shown in an exaggerated form in Fig. 180. When the

wheels are on a tangent, although there will be occasional oscillations from side to side, the normal position will be the symmetrical position in which the circles of tread bb are equal. When centrifugal force throws the wheel-flange against the rail, the circle of tread a is larger than b, and much larger than c; therefore the wheels will tend to roll in a circle whose radius equals the slant height of a cone whose elements would pass through the unequal circles a and c. If this radius equaled the radius of the track, and if the axle were free to assume a radial position, the wheels would roll freely on the rails without any slipping or flange pressure. Under such ideal conditions, coning would be a valuable device, but it is impracticable to have all axles radial, and the radius of curvature of the track is an extremely variable quantity. It has been demonstrated that with parallel axles the influence of coning diminishes as the distance between the axle increases, and that the effect is practically inappreciable when the axles are spaced as they are on locomotives and car-trucks. The coning actually used is very slight (see Chapter XV, § 332) and has a different object. It is so slight that even if the axles were radial it would only prevent the slipping on a very light curve—say a 1° curve.

314. Effect of flanging locomotive driving-wheels. If all the wheels of all locomotives were flanged it would be practically impossible to run some of the longer types around sharp curves. The track-gauge is always widened on curves, and especially on sharp curves, but the widening would need to be excessive to permit a consolidation locomotive to pass around an 8° or 10° curve if all the drivers were flanged. The action of the wheels on a curve is illustrated in Figs. 181, 182, and 184. All small truck-wheels are flanged. The rear drivers are always flanged and four-driver engines usually have all the drivers flanged. Consolidation engines have only the front and rear drivers flanged. Mogul and ten-wheel engines have one pair of drivers blank. On Mogul engines it is always the middle pair. On ten-wheel engines, when used on a road having sharp curves, it is preferable to flange the front and rear drivingwheels and use a "swing bolster" (see § 315); when the curvature is easy, the middle and rear drivers may be flanged and the truck made with a rigid center. The blank drivers have the same total width as the other drivers and of course a much " wider tread, which enables these drivers to remain on the rail. even though the curvature is so sharp that the tread overhangs the rail considerably.

**315.** Action of a locomotive pilot-truck. The purpose of the pilot-truck is to guide the front end of a locomotive around a curve and to relieve the otherwise excessive flange pressure that would be exerted against the driver-flanges. There are two classes of pilot-trucks—(a) those having fixed centers and (b) those having shifting centers. This second class is again subdivided into two classes, which are radically different in their action— $(b_1)$  four-wheeled trucks having two parallel axles

and  $(b_2)$  two-wheeled trucks which are guided by a "radiusbar." The action of the four-wheeled fixed-centered truck (a)is shown in Fig. 181. Since the center of the truck is forced

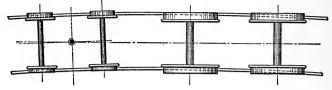


FIG. 181.-FIXED CENTER PILOT-TRUCK.

to be in the center of the track, the front drivers are drawn away from the outer rail. The rear outer driver tends to roll away from the outer rail rather than toward it, and so the effect

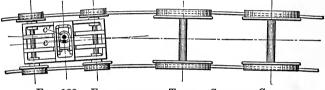


FIG. 182.—FOUR-WHEELED TRUCK—SHIFTING CENTER.

of the truck is to relieve the driver-flanges of any excessive pressure due to curvature. The only exception to this is the case where the curvature is sharp. Then the front inner driver may be pressed against the *inner* rail, as indicated in Fig. 181.

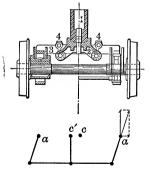


FIG. 183.—Action of Shifting Center.

This limits the use of this type of wheel-base on the sharper curves.

The next type— $(b_1)$  four-wheeled trucks with shifting centers—is much more flexible on sharp curvature; it likewise draws the front drivers away from the outer rail. The relative position of the wheels is shown in Fig. 182, in which c' represents the position of center-pin and c the displaced truck center. The structure and action of the truck is shown in Fig. 183. The "center-pin" (1) is

supported on the "truck-bolster" (2), which is hung by the "links" (4) from the "cross-ties" (3). The links are therefore in tension and when the wheels are forced to one side by the rails the *links* are inclined and the front of the engine is drawn inward by a force equal to the weight on the bolster times the tangent of the angle of inclination of the links. This assumes that all links are vertical when the truck is in the center. Frequently the opposite links are normally inclined to each other, which somewhat complicates the above simple relation of the forces, although the general principle remains identical.

The two-wheeled pilot-truck with shifting center is illustrated in Fig. 184. The figure shows the facility with which

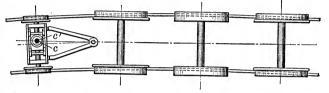
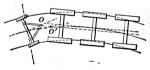


FIG. 184.-Two-wheeled Truck-Shifting Center.

an engine with long wheel-base may be made to pass around a comparatively sharp curve by omitting the flanges from the middle drivers and using this form of pilot-truck. As in the

previous case, the eccentricity of the center of the truck relative to the center-pin induces a centripetal force which draws the front of the engine inward. But the swing-truck is not the only source of such a force. If the





"radius-bar pin" were placed at O' (see Fig. 185), the truckaxle would be radial. But the radius-bar is always made somewhat shorter than this, and the pin is placed at O, a considerable distance ahead of O', thus creating a tendency for the truck to run toward the inner rail and draw the front of the locomotive in that direction. This tendency will be objectionably great if the radius-bar is made too short, as has been practically demonstrated in cases when the radius-bar has been subsequently lengthened with a resulting improvement in the running of the engine. This type of pilot truck is used on both Mogul and Consolidation locomotives and explains why these long engines can so easily operate on sharp curves.

## LOCOMOTIVES.

## GENERAL STRUCTURE.

316. Frame. The frame or skeleton of a locomotive consists chiefly of a collection of forged wrought-iron bars, as shown in Figs. 186 and 187. These bars are connected at the



FIG. 186.—ENGINE-FRAME.

front end by the "bumper" (c), which is usually made of wood. A little further back they are rigidly connected at bb by the cylinders and boiler-saddle. The boilers rest on the frames at *aaaa* by means of "pads," which are bolted to the fire-box, but which permit a free expansion of the boiler along the frame. This expansion is sometimes as much as  $\frac{5}{16}$ ". On a "consolidation" engine (frame shown in Fig. 187) it is frequently

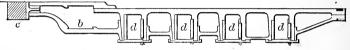


FIG. 187.-ENGINE-FRAME-CONSOLIDATION TYPE.

necessary to use vertical swing-levers about 12'' long instead of "pads." The swinging of the levers permit all necessary expansion. At the back the frames are rigidly connected by the iron "foot-plate." The driving-axles pass through the "jaws" *dddd*, which hold the axle-boxes. The frame-bars have a width (in plan) of 3" to 4". The depth (at *a*) is about the same. Fig. 186 shows a frame for an "American" type of locomotive; Fig. 187 shows a frame for a "Consolidation" type (see § 323).

317. Boiler. A boiler is a mechanism for transferring the latent heat of fuel to water, so that the water is transformed from cold water into high-pressure steam, which by its expansion will perform work. The efficiency of the boiler depends largely on its ability to do its work rapidly and to reduce to a minimum the waste of heat through radiation. The boiler contains a fire-box (see Fig. 188), in which the fuel is burned. The gases of consumption pass from the fire-box through the numerous boiler-tubes into the "smoke-box" S and out through the smoke-stack. The fire-box consists of an inner and outer

#### ROLLING-STOCK.

shell separated by a layer of water about 3'' thick. The exposure of water-surface to the influence of the fire is thus very complete. The efficiency of this transferal of heat is somewhat indicated by the fact that, although the temperature of the gases in the fire-box is probably from 3000° to 4000° F., the temperature in the smoke-box is generally reduced to 500° to

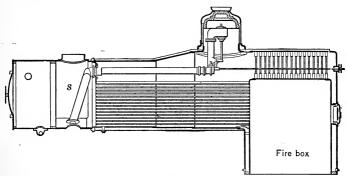


FIG. 188.-LOCOMOTIVE-BOILER.

 $600^{\circ}$  F. If the steam pressure is 180 lbs., the temperature of the water is about 380° F., and, considering that heat will not pass from the gas to the water unless the gas is hotter than the water, the water evidently absorbs a large part of the theoretical maximum. Nevertheless gases at a temperature of  $600^{\circ}$  F. pass out of the smoke-stack and such heat is utterly wasted.

The tubes vary from  $1\frac{4}{4}$ " to 2", inside diameter, with a thickness of about 0".10 to 0".12. The aggregate cross-sectional area of the tubes should be about one eighth of the grate area. The number will vary from 140 to 250. They are made as long as possible, but the length is virtually determined by the type and length of engine.

318. Fire-box. The fire-box is surrounded by water on the four sides and the top, but since the water is subjected to the boiler pressure, the plates, which are about  $\frac{5}{16}''$  thick, must be stayed to prevent the fire-box from collapsing. This is easily accomplished over the larger part of the fire-box surface by having the outside boiler-plates parallel to the fire-box plates and separated from them by a space of about 3". The plates are then mutually held by "stay-bolts." See Fig. 189. These are about  $\frac{7}{8}''$  in diameter and spaced 4" to  $4\frac{1}{2}''$ . The  $\frac{1}{16}''$  hole,

## § 317.

drilled 14" deep, indicated in the figure, will allow the escape of steam if the bolt breaks just behind the plate, and thus calls attention to the break. The stay-bolts are turned down to a diameter equal to that at the root of the screw-threads. This method of supporting the fire-box sheets is used for the two sides, the entire rear, and for the front of the fire-box up to the boiler-barrel. The "furnace tube-sheet"—the upper part of the front of the fire-box—is stayed by the tubes. But the top of the fire-box is troublesome. It must always be covered with water so that it will not be "burned" by the intense heat. It must therefore be nearly, if not quite, flat. There are three general methods of accomplishing this.

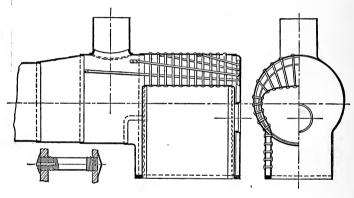


FIG. 189.

(a) Radial stays. This construction is indicated in Fig. 190. Incidentally there is also shown the diagonal braces for resisting the pressure on the back end of the boiler above the firebox. It may be seen that the stays are not perpendicular to either the crown-sheet or the boiler-plate. This is objectionable and is obviated by the other methods.

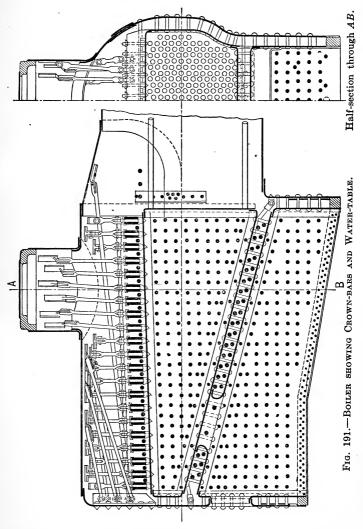
(b) Crown-bars. These bars are in pairs, rest on the side furnace-plates, and are further supported by stays. See Fig. 191.

(c) Belpaire fire-box. The boiler above the fire-box is rectangular, with rounded corners. The stays therefore are perpendicular to the plates. See Fig. 192.

Fire-brick arches. These are used, as shown in Fig. 193, to force all the gases to circulate through the upper part of the fire-

FIG. 190.

box. Perfect combustion requires that all the carbon shall be turned into carbon dioxide, and this is facilitated by the forced circulation.



Water-tables. The same object is attained by using a watertable instead of a brick arch—as shown in Fig. 191. But it has the further advantages of giving additional heating-surface and avoiding the continual expense of maintaining the bricks. One

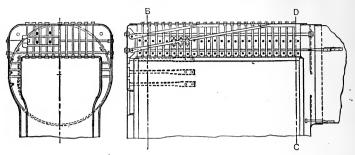


FIG. 192.—"BELPAIRE" FIRE-BOX. Half-section through *AB*. Half-section through *CD*.

feature of the design is the use of a number of steam-jets which force air into the fire-box and assist the combustion.

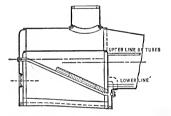
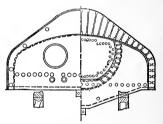
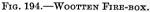


FIG. 193.-FIRE-BRICK ARCH.





Area. Fire-boxes are usually limited in width to the practicable width between the wheels—thus giving a net inside width of about 3 feet and a maximum length of 10 to 11 feet this being about the maximum distance over which the firemen can properly control the fire. About 37 square feet is the maximum area obtainable except when the "Wootten" firebox is used—illustrated in Fig. 194. Here the grate is raised above the driving-wheels and has (in the case shown) a width of 8'  $0\frac{1}{3}$ ". The fire-box area is over 76 square feet. Note that two furnace-doors are used.

319. Coal consumption. No form of steam-boiler (except a boiler for a steam fire-engine) requires as rapid production of steam, considering the size of the boiler and fire-box, as a locomotive. The combustion of coal per square foot of grate per hour for stationary boilers averages about 15 to 25 lbs. and seldom exceeds that amount. An ordinary maximum for a locomotive is 125 lbs. of coal per square foot of grate-area per hour, and in some recent practice 220 lbs. have been used. Of course such excessive amounts are wasteful of coal, because a considerable percentage of the coal will be blown out of the smoke-stack unconsumed, the draft necessary for such rapid consumption being very great. The only justification of such rapid and wasteful coal consumption is the necessity for rapid production of steam. The best quality of coal is capable of evaporating about 14 lbs. of water per pound of coal, i.e., change it from water at 212° to steam at 212°; the heat required to change water at ordinary temperatures to steam at ordinary working pressure is (roughly) about 20% more. From 6 to 9 lbs. of water per pound of coal is the average performance of ordinary locomotives, the efficiency being less with the higher rates of combustion. Some careful tests of locomotive coal consumption gave the following figures: when the consumption of coal was 50 lbs. per square foot of grate-area per hour, the rate of evaporation was 8 lbs. of water per pound of coal. When the rate of coal consumption was raised to 180, the evaporation dropped to 5 lbs. of water per pound of coal. It has been demonstrated that the efficiency of the boiler is largely increased by an increased length of boiler-tubes. The actual consumption of coal per mile is of course an exceedingly variable quantity, depending on the size and type of the engine and also on the work it is doing-whether climbing a heavy grade with its maximum train-load or running easily over a level or down grade. A test of a 50-ton engine, running without any train at about 20 to 25 miles per hour, showed an average consumption of 21 lbs. of coal per mile. Statistics of the Pennsylvania Rail road show a large increase (as might be expected, considering the growth in size of engines and weight of trains) in the average number of pounds of coal burned per train-mile-some of the figures being 55 lbs. in 1863, 72 lbs. in 1872, and nearly 84 lbs. in 1883. Figures are published showing an average consumption of about 10 lbs. of coal per passenger-car mile, and 4 to 5 lbs. per freight-car mile. But these figures are always obtained by dividing the total consumption per train-mile by the number of cars, the coal due to the weight of the engine

being thrown in Wellington developed a rule, based on the actual performance of a very large number of passenger-trains, that the number of pounds of coal per mile =21.1+6.74 times the number of passenger-cars. The amount of coal assigned to the engine agrees remarkably with the test noted above For freight-trains the amount assigned to the engine should be much greater (since the engine is much heavier), and that assigned to the individual cars much less, although the great increase in freight-car weights in recent years has caused an increase in the coal required per car.

320. Heating-surface. The rapid production of steam requires that the hot gases shall have a large heating-surface to which they can impart their heat. From 50 to 75 square feet of heating-surface is usually designed for each square foot of grate-area. A more recently used rule is that there should be from 60 to 70 square feet of tube heating-surface per square foot of grate-area for bituminous coal. 40 or 50 to 1 is more desirable for anthracite coal Almost the whole surface of the fire-box has water behind it, and hence constitutes heatingsurface. Although this surface forms but a small part of the total (nominally), it is really the most effective portion, since the difference of temperature of the gases of combustion and the water is here a maximum, and the flow of heat is therefore the most rapid. The heating-surface of the tubes varies from 85 to 93% of the total, or about 7 to 15 times the heating-surface in the fire-box. Sometimes the heating-surface is as much as 2300 square feet, but usually it is less than 2000, even for engines which must produce steam rapidly.

A "Mikado" type locomotive, wheel plan, 2-8-2 (see § 323), constructed in 1912, has cylinders 28" diameter, 32" stroke; drivers, 64" diameter; steam pressure, 180 lbs.; grate area, 78 sq.ft.; heating surface, 4627 sq.ft.; besides a superheating surface of 961 sq. ft.; total weight of engine and tender, 480,000 lbs.; weight of engine alone, 303,400 lbs.; weight on drivers, 231,000 lbs.; tractive power 60,000. There is about 71 sq.ft. of heating surface per square foot of grate area. The adhesion ratio is 1: 3.85 or about 26%.

Another rule used by designers is that the engine should have 1 sq. ft. of heating-surface for each 50 or 60 lbs. of weight, efficiency being indicated by a low weight. For the above engine the ratio is 54. 321. Loss of efficiency in steam pressure. The effective work done by the piston is never equal to the theoretical energy contained in the steam withdrawn from the boiler. This is due chiefly to the following causes:

(a) The steam is "wire-drawn," i.e., the pressure in the cylinder is seldom more than 85 to 90% of the boiler pressure. This is due largely to the fact that the steam-ports are so small that the steam cannot get into the cylinder fast enough to exert its full pressure. It is often purposely wire-drawn by partially closing the throttle, so that the steam may be used less rapidly.

(b) Entrained water. Steam is always drawn from a dome placed over the boiler so that the steam shall be as far above the water-surface as possible, and shall be as dry as possible. In spite of this the steam is not perfectly dry and carries with it water at a temperature of, say, 361°, and pressure of 140 lbs. per square inch. When the pressure falls during the expansion and exhaust, this hot water turns into steam and absorbs the necessary heat from the hot cylinder-walls. This heat is then carried out by the exhaust and wasted.

(c) The back pressure of the exhaust-steam, which depends on the form of the exhaust-passages, etc. This amounts to from 2 to 20% of the power developed.

(d) Clearance-spaces. When cutting off at full stroke this waste is considerable (7 to 9%), but when the steam is used expansively the steam in these clearance-spaces expands and so its power is not wholly lost.

(e) Radiation. In spite of all possible care in jacketing the cylinders, some heat is lost by radiation.

(f) Radiation into the exhaust-steam. This is somewhat analogous to (b). Steam enters the cylinder at a temperature of, say,  $361^\circ$ ; the walls of the cylinder are much cooler, say  $250^\circ$ ; some heat is used in raising the temperature of the cylinderwalls; some steam is vaporized in so doing; when the exhaust is opened the temperature and pressure fall; the heat temporarily absorbed by the cylinder-walls is reabsorbed by the exhaust-steam, re-evaporating the vapor previously formed, and thus a certain portion of heat-energy goes through the cylinder without doing any useful work. With an early cut-off the loss due to this cause is very great.

The sum of all these losses is exceedingly variable. They are usually less at lower speeds. The loss in *initial pressure*  (the difference between boiler pressure and the cylinder pressure at the beginning of the stroke) is frequently over 20%, but this is not all a net loss With an early cut-off the average cylinder pressure for the whole stroke is but a small part of the boiler pressure, yet the horse-power developed may be as great as, or greater than, that developed at a lower speed, later cut-off, and higher average pressure.

322. Tractive power The work done by the two cylinders during a complete revolution of the drivers evidently = area of pistons×average steam pressure×stroke×2×2. The resistance overcome evidently=tractive force at circumference of drivers times distance traveled by drivers (which is the circumference of the drivers) Therefore

$$\text{Tractive force} = \begin{cases} \text{area pistons} \times \text{average steam pressure} \\ \times \text{stroke} \times 2 \times 2. \\ \hline \text{circumference of drivers} \end{cases}.$$

Dividing numerator and denominator by  $\pi$  (3.1415), we have

$$Tractive force = \begin{cases} (diam piston)^2 \times average steam \\ pressure \times stroke \\ diameter of driver \end{cases}, \quad (137)$$

which is the usual rule Although the rule is generally stated in this form, there are several deductions In the first place the net effective area of the piston is less than the nominal on account of the area of the piston-rod. The ratio of the areas of the piston rod and piston varies, but the effect of this reduction is usually from 1.3 to 1.7%. No allowance has been made for friction—of the piston, piston-rod, cross-head, and the various bearings. This would make a still further reduction of several per cent. Nevertheless the above simple rule is used, because, as will be shown, no great accuracy can be utilized.

The tractive force is limited by the adhesion between the drivers and the rails, and this is a function of the weight on the drivers. Under the most favorable conditions this has been tested to amount to one-third the weight on the drivers, but such a ratio cannot be depended on. Wellington used the ratio one-fourth The Baldwin Locomotive Works in their "Locomotive Data" give tables and diagrams based on  $\frac{1}{4}$ ,  $\frac{3}{40}$ .

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and  $\frac{1}{5}$  adhesion. As low a value as  $\frac{1}{6}$  or even  $\frac{1}{7}$  is occasionally used, but such a low rate of adhesion would only be found when the rails were abnormally slippery. In a well-designed locomotive the tractive force, as computed above, and the tractive adhesion should be made about equal. The uncertainty in the coefficient of adhesion shows the futility of any refinement in the computation of the tractive force.

It is only at very slow speeds that an engine can utilize all of its tractive force. When running at a high speed, the utmost horse-power that the engine can develop will only produce a draw-bar pull, which is but a small part of the possible tractive force. Power is the product of force times velocity. If the power is constant and the velocity increases, the force must decrease. This fact is well shown in the figures of some tests of a locomotive. The dimensions were as follows: cylinders,  $18'' \times 24''$ ; drivers, 68''; weight on drivers, 60000 lbs.; heatingsurface, 1458 sq. ft.; grate-area, 17 sq. ft. During one test the average cylinder pressure was 83.3 lbs. (boiler pressure, 145; 14-inch. cut-off and throttle  $\frac{3}{4}$  open). By the above formula (137),

Tractive force = 
$$\frac{18^2 \times 83.3 \times 24}{-68} = 9525 \text{ lbs.}$$

At  $\frac{1}{4}$  adhesion the tractive force was 15000 lbs; even at  $\frac{1}{5}$  adhesion, it would be 12000 lbs. This shows that at the speed of this test (26.3 in. per hour) scarcely more than  $\frac{2}{3}$  of the tractive power was utilized. A still more marked case, shown by another test with the same engine, taken when the speed was 53.4 miles per hour, indicated an average cylinder pressure of 37.2 lbs., the throttle being  $\frac{1}{5}$  open and the valves cutting off at 8". In this case the tractive power, computed as before, equals 4254 lbs., about  $\frac{1}{14}$  of the weight on the drivers and about  $\frac{1}{2}$  of the tractive force which is possible at slow speeds. In the first case, the tractive power (9525) times the speed in feet per second (38.57) divided by 550 gives the indicated horse-power, 668. In the second case, although the tractive force developed was so much less, the speed was much greater and the horse-power was about the same, 606.

The above figures illustrate some of the foregoing statements regarding loss of efficiency. In both cases the steam was wiredrawn. The boiler pressure was 145 lbs., but when the throttle

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was only  $\frac{3}{4}$  open and the steam was cut-off at 14" (24" stroke) the average steam pressure in the cylinder was reduced to 83.3 lbs. With the throttle but  $\frac{1}{5}$  open and the valves cutting off at 8" ( $\frac{1}{5}$  of the stroke), the average pressure was cut down to 37.2 lbs.—about  $\frac{1}{4}$  of the boiler pressure. Note that the heating-surface per square foot of grate-area (1458÷17=86) is very large (see § 320). Note also that the horse-power developed divided by the grate-area (17) gives 39 and 36 H.P. per square foot of grate-area. This is exceptionally large—25 or 30 being a more common figure.

The maximum tractive power is required when a train is starting, and fortunately it is at low velocities that the maximum tractive force can be developed. The motion of the piston is so slow that there is but little reduction of steam pressure, and the valves are generally placed to cut off at full stroke. For the above engine, with 145 lbs. boiler pressure, the absolute maximum of tractive force is  $\frac{18^2 \times 145 \times 24}{145 \times 24}$ 16581 lbs. Of course, this maximum would never be reached unless the boiler pressure were increased. A common rule is to consider that the average effective cylinder pressure for slow speed and full stroke will be 80% of the boiler pressure. This would reduce the tractive force to the (nominal) value of 13265 lbs., and the corresponding cylinder pressure would be 116 lbs. per square inch. With an effective cylinder pressure of about 131 lbs. the tractive power is 15000 lbs., which is  $\frac{1}{4}$  of the total weight on the drivers. This illustrates the general rule, stated above, that the cylinders, drivers, and boiler pressure should be so proportioned that the maximum tractive force should

about equal the maximum adhesion which could be obtained. As another numerical example, the dimensions of a recently constructed heavy consolidation engine are quoted. The cylinders are  $24'' \times 32''$ ; diameter of drivers, 54''; total weight of engine and tender, 391400 lbs.; weight of engine, 250300 lbs.; weight on drivers, 225200 lbs.; capacity of tender, 7500 gallons; the boiler has 406 tubes,  $2_4''$  in diameter and 15' long; firebox,  $132'' \times 40_4''$ ; heating-surface of tubes, 3564 sq. ft.; of fire-box, 241 sq. ft.—total, 3805 sq. ft.; boiler pressure, 220 lbs. per square inch. Applying Eq. 132, we may compute 75093 lbs. as the absolute maximum of tractive power. In fact this is an unattainable limit, for reasons before stated. The trac-

## ROLLING-STOCK.

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tive force is given as 63000, which corresponds to an effective cylinder pressure of about 185 lbs., about 84% of the boiler pressure. This tractive force is 28% of the weight on the drivers, a tractive ratio of 1:3.6.

## RUNNING GEAR.

323. Types of running gear. (a) "American." This was once the almost universal type for both passenger and freight service. It is still very commonly used for passenger service, but it is not the best form for heavy freight work.

(b) "Columbia." Four drivers, one pair of pilot-truck wheels and one pair of trailing wheels behind the drivers. The low trailing  $\bigcirc \bigcirc \bigcirc \bigcirc \bigcirc$ wheels permit a desirable enlargement of the fire-box. This is a recent type, used exclusively for passenger service.

 $\underbrace{\bigcirc}_{\text{has four wheels instead of two.}}^{\text{(c) "Atlantic." Similar to}} \underbrace{\bigcirc}_{b \text{ except that the pilot-truck}}^{\text{(c) "Atlantic." Similar to}}$ 

(d) "Mogul." These are used for both passenger and freight service, but are not well  $\bigcirc$   $\bigcirc$   $\bigcirc$   $\bigcirc$   $\bigtriangleup$   $\bigtriangleup$  or great tractive power.

(e) "Ten-wheel." Similar to d except that the pilot-truck has four wheels instead of that of d.

(g) Switching-engines. These have four or six (and exceptionally even eight or ten) drivers and no truck-wheels. They are only adapted for slow speed when a maximum of tractive power is needed. Sometimes the water-tank and even a small fuel-box is loaded on. Since fuel is always near at hand for a yard-engine, the fuel-box need not be large.

(h) "Double-enders." As explained in § 315, truck-wheels are needed in front of the drivers to guide them around curves. If an ordinary engine is run backward, the flanges of the rear drivers will become badly worn, and if the speed is high, the danger of derailment is considerable. In suburban service,  $\angle O O O \Box O \Rightarrow$  when the runs are short, it is preferable to run the engines forward and backward, rather than turn them at each end of the route. Therefore a pilot-truck is placed at each end.

(i) "Miscellaneous types." Almost every conceivable combination of drivers and truck-wheels has been used. The "Mastodon" is similar to the "Consolidation" except that the pilot-truck has four wheels instead of two. The "Decapod" has ten driving-wheels. The "Forney" (named after the inventor) has been very extensively used on elevated roads. The weight of the boiler and machinery is carried on four drivingwheels; the engine-frame is extended so as to include a small tank and fuel-box, the weight of which is chiefly supported by a truck of two or four wheels. They run best when running "backward," i.e., tender first.

The great variation in types of running gear which has been developed in recent years, has started a convenient and unmistakable method of indicating the running gear. Commencing with the front of the engine (or pilot) always at the LEFT (instead of at the right, as in the illustrations above) the number of wheels of the pilot truck on *both* rails is indicated by 0, 2 or 4, according as there is *no* pilot truck, a two-wheeled or a fourwheeled pilot truck. Then the number of drivers on both rails is indicated by the next number and the number of trailing wheels by the third number. The running gear of the tender is not indicated. This method may be illustrated by applying it to the types indicated above:

American	440
Columbia	2-4-2
Atlantic	4-4-2
Mogul	260
Ten-wheel	4-6-0
Consolidation	2-8-0
Six-wheel switcher	0-6-0
Mastodon	4-8-0

The running gear of any new type may thus be unmistakably indicated by three figures.

324. Equalizing-levers. The ideal condition of track, from the standpoint of smooth running of the rolling stock, is that the rails should always lie in a plane surface. While this condition is theoretically possible on tangents, it is unobtainable on curves, and especially on the approaches to curves when the outer rail is being raised. Even on tangents it is impossible to maintain a perfect surface, no matter how perfectly the track may have been laid. In consequence of this, the points of contact of the wheels of a locomotive, or even of a fourwheeled truck, will not ordinarily lie in one plane. The rougher and more defective the track, the worse the condition in this respect. Since the frame of a locomotive is practically rigio. if the frame rests on the driver-axles through the medium of springs at each axle-bearing, the compression of the springs (and hence the pressure of the drivers on the rail) will be variable if the bearing-points of the drivers are not in one plane This variable pressure affects the tractive power and severely strains the frame. Applying the principle that a tripod will stand on an uneven surface, a mechanism is employed which virtually supports the locomotive on three points, of which one is usually the center-bearing of the forward truck. On each side the pressure is so distributed among the drivers that even if a driver rises or falls with reference to the others, the load carried by each driver is unaltered, and that side of the engine rises or falls by one nth of the rise or fall of the single driver. where n represents the number of wheels. The principle involved is shown in an exaggerated form in Fig. 195. In the diagram, MN represents the normal position of the frame when the wheels are on line. The frame is supported by the hangers at a, c, f, and h. ab, de, and gh are horizontal levers vibrating about the points H, K, and L, which are supported by the axles. While it is *possible* with such a system of levers to make MN assume a position not parallel with its natural position. yet, by an extension of the principle that a beam balance loaded with equal weights will always be horizontal, the effect of raising or lowering a wheel will be to move MN parallel to itself. It only remains to determine how much is the motion of MNrelative to the rise or drop of the wheel.

The dotted lines represent the positions of the wheels and levers when one wheel drops into a depression. The wheel center drops from p to q, a distance m. L drops to L', a distance m (see Fig. 195, b); M drops to M', an unknown distance x; therefore aa'=x; bb'=x; cc'=x; dd'=3x=ee'; ff'=x;  $\therefore gg'=5x$ ; hh'=x;  $LL'=\frac{1}{2}(gg'+hh')=\frac{1}{2}(6x)=m$ ;  $\therefore x=\frac{1}{3}m$ ; i.e., MN drops, parallel to itself, 1/n as much as the wheel drops, where n is the number of wheels. The resultant effect caused by the simultaneous motion of two wheels with refer-

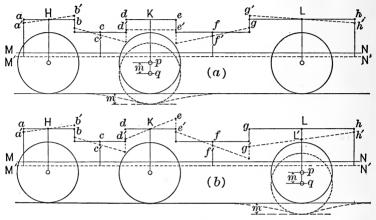


FIG. 195.—ACTION OF EQUALIZING-LEVERS.

ence to the third is evidently the algebraic sum of the effects of each wheel taken separately.

The practical benefits of this device are therefore as follows:

(a) When any driver reaches a rough place in the track, a high place or a low place, the stress in all the various hangers and levers is unchanged.

(b) The motion of the frame (represented by the bar MN in Fig. 195) is but 1/n of the motion of the wheel, and the jar and vibration caused by a roughness in the track is correspondingly reduced.

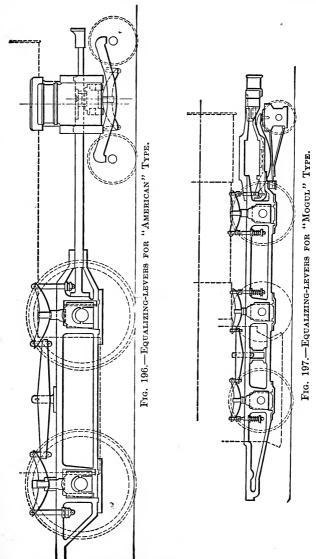
The details of applying these principles are varied, but in general it is done as follows;

(a) American and ten-wheeled types. Drivers on each side form a system. The center-bearing pilot-truck is the third point of support. The method is illustrated in Fig. 196.

(b) Mogul and consolidation types. The front pair of drivers is connected with the two-wheeled pilot-truck (as illustrated in Fig. 197) to form one system. The remaining drivers on each side are each formed into a system

The device of equalizers is an American invention. Until recently it has not been used on foreign locomotives. The necessity for its use becomes less as the track is maintained § 324.

with greater perfection and is more free from sharp curves. A locomotive not equipped with this device would deteriorate



very rapidly on the comparatively rough tracks which are usually found on light-traffic roads. It is still an open ques-

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tion to what extent the neglect of this device is responsible for the statistical fact that average freight-train loads on foreign trains are less in proportion to the weight on the drivers than is the case with American practice. The recent increasing use of this device on foreign heavy freight locomotives is perhaps an acknowledgment of this principle.

325. Counterbalancing. At very high velocities the centrifugal force developed by the weight of the rotating parts becomes a quantity which cannot be safely neglected. These rotating parts include the crank-pin, the crank-pin boss, the side rod, and that part of the weight of the connecting-rod which may be considered as rotating about the center of the crank-driver. As a numerical illustration, a driving-wheel 62" in diameter, running 60 miles per hour, will revolve 325 times per minute. The weights are:

Crank-pin	110 lbs.
" boss	150 ''
One-half side rod	240 ''
Back end of connecting-rod	190''
$\operatorname{Total}$	$\overline{690}$ lbs.

If the stroke is 24", the radius of rotation is 12", or 1 foot. Then  $\frac{Gv^2}{gr} = \frac{690 \times 4\pi^2 1^2 \times 325^2}{32.2 \times 1 \times 60^2} = 24821 \text{ lbs.},$ 

which is half as much again as the weight on a driver, 16000 lbs. Therefore if no counterbalancing were used, the pressure between the drivers and the rail would always be less (at any velocity) when the crank-pin was at its highest point. At a velocity of about 48 miles per hour the pressure would become zero, and at higher velocities the wheel would actually be thrown from the rail. As an additional objection, when the crank-pin was at the lowest point, the rail pressure would be increased (velocity 60 miles per hour) from 16000 lbs. to nearly 41000 lbs., an objectionably high pressure. These injurious effects are neutralized by "counterbalancing." Since all of the above-mentioned weights can be considered as concentrated at the center of the crank-pin, if a sufficient weight is so placed in the drivers that the center of gravity of the eccentric weight is diametrically opposite to the crank-pin, this centrifugal force can be wholly balanced. This is done by filling up a portion of the space between the spokes. If the center of gravity of the counterbalancing weight is 20" from the center,

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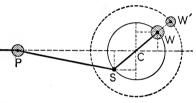
then, since the crank-pin radius 's 12", the required weight would be  $690 \times \frac{12}{20} = 414$  lbs.

In addition to the effect of these revolving parts there is the effect of the sudden acceleration and retardation of the reciprocating parts. In the engine above considered the weights of these reciprocating parts will be:

Front end of connecting-rod	150 lbs.
Cross-head	174''
Piston and piston-rod	300''
Total	

sidered as concentrated at one point, the point P of the diagram in Fig. 198. Since the

motion of P is horizontal only, the force required to overcome its inertia at any point will exactly equal the horizontal component of the force required to overcome the inertia of an equal



weight at S revolving in Fig. 198.—Action of CounterBalance. a circular path. Then evidently the horizontal component of the force required to keep W in the circular path will exactly balance the force required to overcome the inertia of P. Of course W=P. But a smaller weight W', whose weight is inversely proportional to its radius of rotation, will evidently accomplish the same result. In the above numerical case, if the center of gravity of the counterweights is 20" from the center, the required weight to completely counterbalance the reciprocating parts would be  $624 \times \frac{12}{20} = 374.4$  lbs. This counterweight need not be all placed on the driver carrying the main crank-pin, but can be (and is) distributed among all the drivers. Suppose it were divided between the two drivers in the above case. At 60 miles per hour such a counterweight would produce an additional pressure of 11211 lbs. when the counterweight was down, or a lifting force of the same amount when the counterweight was up. Although this is not sufficient to lift the driver from the rail, it would produce an objectionably high pressure on the rail (over 27000 lbs.), thus inducing just what it was desired to avoid on account of the eccentric rotating parts. Therefore a compromise must be made. Only a portion (one half to three fourths) of the weight of the reciprocating parts is balanced. Since the effect of the rotating weights is to cause variable pressure on the rail, while the effect of the reciprocating parts is to cause a horizontal wobbling or "nosing" of the locomotive, it is impossible to balance both. Enough counterweight is introduced to partially neutralize the effect of the reciprocating parts, still leaving some tendency to horizontal wobbling, while the counterweights which were introduced to reduce the wobbling cause some variation of pressure. By using hollow piston-rods of steel, ribbed crossheads, and connecting- and side-rods with an I section, the weight of the reciprocating parts may be greatly lessened without reducing their strength, and with a decrease in weight the effect of the unbalanced reciprocating parts and of the "excess balance" (that used to balance the reciprocating parts) is largely reduced.

Current practice is somewhat variable on three features:

(a) The proportion of the weight of the connecting-rod which should be considered as revolving weight.

(b) The proportion of the total reciprocating weight that should be balanced.

(c) The distribution among the drivers of the counterweight to balance the reciprocating parts.

An exact theoretical analysis of (a) shows that it is a function of the weights and dimensions of the reciprocating parts. The weight which may be considered as revolving equals \*

$$W_1\left(rac{r^2+k^2-rd\left(1+rac{r}{l}
ight)}{l^2-r^2}
ight)+W_2rac{r^2}{l^2-r^2},$$

in which r=radius of the crank, l=length of connecting-rod, k=distance of center of gyration from wrist-pin, d=distance of center of gravity from wrist-pin,  $W_1$ =weight of connectingrod in pounds, and  $W_2$ =weight of piston, piston-rod, and crosshead in pounds; all dimensions in feet. An application of this formula will show that for the dimensions of usual practice, from 51 to 57% of the weight of the connecting-rod should be considered as revolving weight.

The principal rules which have been formulated for counterbalancing may be stated as follows:

1. Each wheel should be balanced correctly for the revolving parts connected with it.

2. In addition, introduce counterbalance sufficient for 50% of the weight of the reciprocating parts for ordinary engines,

<sup>\*</sup> R. A. Parke, in R. R. Gazette, Feb. 23, 1894.

increasing this to 75% when the reciprocating parts are excessively heavy (as in compound locomotives) or when the engine is light and unable to withstand much lateral strain or when the wheel-base is short.

3. Consider the weight of the connecting-rod as  $\frac{1}{2}$  revolving and  $\frac{1}{2}$  reciprocating when it is over 8 feet long; when shorter than 8 feet, consider  $\frac{6}{10}$  of the weight as revolving and  $\frac{4}{10}$  as reciprocating.

4. The part of the weight of the connecting-rod considered as revolving should be entirely balanced in the crank-driver wheel

5. The "excess balance" should be divided equally among the drivers.

6. Place the counterbalance as near the rim of the wheel

as possible and also as near the outside of the wheel as possible in order that the center of gravity shall be as near as possible opposite the center of gravity of the rods, etc., which are all outside of even the plane of the face of the wheel.

In Fig. 199 is shown a section of a locomotive driver with the cavities in the casting for the accommodation of the lead which is used for the counterbalance weight. Incidentally several other features and dimensions are shown in the illustration. FIG. 199.—SECTION OF LOCOMOTIVE-DRIVER.

326. Mutual relations of the boiler power, tractive power, and cylinder power for various types. The design of a locomotive includes three *distinct* features which are varied in their mutual relations according to the work which the engine is expected to do.

(a) The boiler power. This is limited by the rate at which steam may be generated in a boiler of admissible size and weight. Engines which are designed to haul very fast trains which are comparatively light must be equipped with very large grates and heating surfaces so that steam may be developed with great rapidity in order to keep up with the very rapid consumption. Engines for very heavy freight work are run at very much lower velocity and at a lower piston speed in spite of the fact that more strokes are required to cover a given distance and the demand on the boiler for *rapid* steam production is not as great as with high-speed passenger-engines. The capacity of a boiler to produce steam is therefore limited by the limiting weight of the general type of engine required. Although improvements may be and have been made in the design of fireboxes so as to increase the steam-producing capacity without adding proportionately to the weight, yet there is a more or less definite limit to the boiler power of an engine of given weight.

(b) The tractive power. This is a function of the weight on the drivers. The absolute limit of tractive adhesion between a steel-tired wheel and a steel rail is about one third of the pressure, but not more than one fourth of the weight on the drivers can be depended on for adhesion and wet rails will often reduce this to one fifth and even less. The tractive power is therefore absolutely limited by the practicable weight of the engine. In some designs, when the maximum tractive power is desired, not only is the entire weight of the boiler and running gear thrown on the drivers, but even the tank and fuel-box are loaded on. Such designs are generally employed in switching-engines (or on engines designed for use on abnormally heavy mountain grades) in which the maximum tractive power is required, but in which there is no great tax on the boiler for rapid steam production (the speed being always very low), and the boiler and fire-box, which furnish the great bulk of the weight of an engine. are therefore comparatively light, and the requisite weight for traction must, therefore, be obtained by loading the drivers as much as possible. On the other hand, engines of the highest speed cannot possibly produce steam fast enough to maintain the required speed unless the load be cut down to a comparatively small amount. The tractive power required for this comparatively small load will be but a small part of the weight of the engine, and therefore engines of this class have but a small proportion of their weight on the drivers; generally have but two driving-axles and sometimes but one.

(c) Cylinder power. The running gear forms a mechanism which is simply a means of transforming the energy of the boiler into tractive force and its power is unlimited, within the practical conditions of the problem. The power of the running gear depends on the steam pressure, on the area of the piston, on the diameter of the drivers, and on the ratio of crank-pin radius to wheel radius, or of stroke to driver diameter. It

is always possible to increase one or more of these elements by a relatively small increase of expenditure until the cylinders are able to make the drivers slip, assuming a sufficiently great resistance. Since the power of the engine is limited by the power of its weakest feature, and since the running gear is the most easily controlled feature, the power of the running gear (or the "cylinder power") is always made somewhat excessive on all well-designed engines. It indicates a badly designed engine if it is stalled and unable to move its drivers, the steam pressure being normal. If it is attempted to use a freight-engine on *fast* passenger service, it will probably fail to attain the desired speed on account of the steam pressure falling. The tractive power and cylinder power are superabundant, but the boiler cannot make steam as fast as it is needed for high speed, especially when the drivers are small. The practical result would be a comparatively low speed kept up with a forced fire. If it is attempted to use a high-speed passenger-engine on heavy freight service, the logical result is a slipping of the drivers until the load is reduced. The boiler power and cylinder power are ample, but the weight on the drivers is so small that the tractive power is only sufficient to draw a comparatively small load.

These relations between boiler, cylinder, and tractive power are illustrated in the following comparative figures referring to a fast passenger-engine, a heavy freight-engine, and a switching-engine. The weights of the passenger- and freight-engines are about the same, but the passenger-engine has only 72% of

Kind.	Cylinders.	Total W ght.	Wt. on Driv'rs	Heat- ing Sur- face, sq. ft.	Grate area sq. ft.	Steam Pres- sure in Boiler.	Diam
Fast passenger.	19''  imes 24''	126700	81500	1831.8	26.2	180	$\frac{24}{78} = .31$
Heavy freight.	$20^{\prime\prime}\! imes\!24^{\prime\prime}$	128700	112600	1498.3	31.5	140	$\frac{24}{50} = .48$
Switcher	19″×24″	109000	109000	1498.0	22.8	160	$\frac{24}{50} = .48$

the tractive power of the freight. But the passenger-engine has 22% more heating-surface and can generate steam much faster; it makes less than two thirds as many strokes in covering a given distance, but it runs at perhaps twice the speed and probably consumes steam much faster. The switchengine is lighter in total weight, but the tractive power is nearly as great as the freight and much greater than the passengerengine. While the heating-surfaces of the freight- and switching-engines are practically identical, the grate area of the switcher is much less; its speed is always low and there is but little necessity for rapid steam development.

While these figures show the general tendency for the relative proportions, and in this respect may be considered as typical. there are large variations. The recent enormous increase in the dead weight of passenger-trains has necessitated greater tractive power. This has been provided sometimes by using "Mogul" and "ten-wheel" engines, which were originally designed for freight work. On the other hand, the demand for fast freight service, and the possibility of safely operating such trains by the use of air-brakes, has required that heavy freight-engines shall be run at comparatively high speeds, and that requires the rapid production of steam, large grate areas, and heating surfaces. But in spite of these variations, the normal standard for passenger service is a four-driver engine carrying about two thirds of the weight of the engine on the drivers, which are very large; the normal standard for freight work is the "consolidation," with perhaps 90% of the weight on the drivers, which are small, but which must have the pony truck for such speed as it uses; and finally the normal standard for switching service has all the weight on the drivers and has comparatively low steam-producing capacity.

327. Life of locomotives. The life of locomotives (as a whole) may be taken as about 800000 miles or about 22 to 24 years. While its life should be and is considered as the period between its construction and its final consignment to the scrap pile, parts of the locomotive may have been renewed more than once. The boiler and fire-box are especially subject to renewal. The mileage life is much longer than formerly. This is due partly to better design and partly to the custom of drawing the fires less frequently and thereby avoiding some of the destructive strains caused by extreme alternations of heat and cold. Recent statistics give the average annual mileage on twenty-three leading roads to be 41000 miles.

#### CARS.

328. Capacity and size of cars. The capacity of freight-cars has been enormously increased of late years. About thirty years ago the usual live-load capacity for a box-car was about 20000 lbs. In 1893 the standard box-car, gondola-cars, etc., of the Pennsylvania Railroad on exhibition at the Chicago Exposition, had a live-load capacity of 60000 lbs. and a dead weight of 30000 to 33000 lbs. With a full load, the weight on each wheel is nearly 12000 lbs, which equals or exceeds the load usually placed on the drivers of ordinary locomotives. But now cars with a live-load capacity of 100,000 lbs. are standard on many roads, and even larger cars are made for special service. (See Fig. 200.)

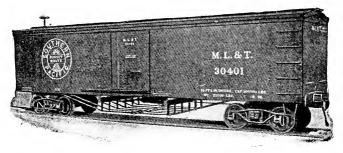
The limitation of the carrying capacity for some kinds of freight depends somewhat on the amount of live load that can be carried within given dimensions; for the cross-section of a car is limited to the extreme dimensions which may be safely run through the tunnels and through bridges as at present constructed, and the length is somewhat limited by the difficulty of properly supporting an excessively heavy load, distributed over an unusually long span, by a structure which is subjected to excessive jar, concussion, compression, and tension. The cross-sectional limit seems to have been scarcely reached yet, except, perhaps, in the case of furniture and carriagecars, whose load per cubic foot is not great. The usual width of freight-cars is about 8 to 9 feet, while parlor-cars and sleepers are generally 10 feet wide and sometimes 11 feet. The highest point of a train is usually the smoke-stack of the locomotive which is generally 14 feet above the rails and occasionally over 15 feet. A sleeping-car usually has the highest point of the car about 14 feet above the rails. Box-cars are usually about 8 feet high (above the sills), with a total height of about 11' 3". Refrigerator-cars are usually about 9' high and furniture-cars about 10' above the sills, the truck adding about 3' 3". The usual length is 34 feet, but 35 to 40 feet is not uncommon. Passenger-cars (day coaches) are usually 50 feet long, exclusive of the end platforms and weigh 45000 to 50000 lbs. Sixty passengers at 150 pounds apiece (a high average) will only add 9000 lbs. to the weight. A parlor-car or sleeper is generally about 65 feet long exclusive of the platforms, which add about 6' 6". The weight is anywhere from 60000 to 80000 lbs.

The weight of the 25 or 30 passengers it may carry is hardly worth considering in comparison.

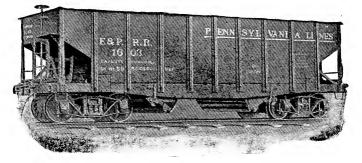
320. Stresses to which car-frames are subjected. A car is structurally a truss, supported at points at some distance from the ends and subjected to transverse stress. There is, therefore, a change of flexure at two points between the trucks. Besides this stress the floor is subjected to compression when the cars are suddenly stopped and to tension when in ordinary motion, the tension being greater as the train resistance is geater and as the car is nearer the engine. The shocks, jars, and sudden strains to which the car-frames are subjected are very much harder on them than the mere static strains due to their maximum loads if the loads were quiescent. Consequently any calculations based on the static loads are practically valueless, except as a very rough guide, and previous experience must be relied on in designing car bodies. As evidence of the increasing demand for strength in car-frames, it has been recently observed that freight-cars, built some years ago and built almost entirely of wood, are requiring repairs of wooden parts which have been *crushed* in service, the wood being perfectly sound as regards decay.

330. The use of metal. The use of metal in car construction is very rapidly increasing.. The demand for greater strength in car-frames has grown until the wooden framing has become so heavy that it is found possible to make steel frames and trucks at a small additional cost, the steel frames being twice as strong and yet reducing the dead weight of the car about 5000 lbs., a consideration of no small value, especially on roads having heavy grades. Another reason for the increasing use of metal is the great reduction in the price of rolled or pressed steel, while the cost of wood is possibly higher than before. The advocates of the use of steel advise steel floors, sides, etc. For box-cars a wooden floor has advantages. For ore and coal-cars an all-metal construction has advantages. (Fig. 200.) In Germany, where steel frames have been almost exclusively in use for many years, they have not yet been able to determine the normal age limit of such frames; none have yet worn out. The life is estimated at 50 to 80 years

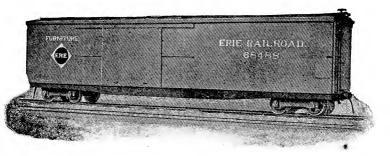
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:100,000-LB. BOX CAR.



STEEL COAL CAR.



WOODEN BOX CAR; STEEL FRAME.

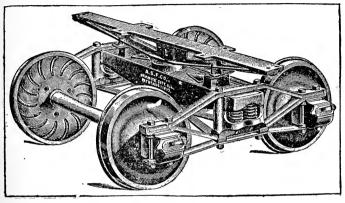
FIG. 200.—Some Heavy Freight Cars.

(To face page 394.)



Brake-beams are also best made of metal rather than wood, as was formerly done. Metal brake-beams are generally used on cars having air-brakes, as a wooden beam must be excessively large and heavy in order to have sufficient rigidity.

Truck-frames (see Fig. 201), which were formerly made principally of wood, are now largely made of pressed steel. It makes



F1G 201.

a reduction in weight of about 3000 lbs. per car. The increased durability is still an uncertain quantity.

331. Draft gear. The enormous increase in the weight and live load capacities of rolling stock have necessitated a corresponding development in draft gear. Even within recent years, "coal-jimmies," carrying a few tons have been made up into trains by dropping a chain of three big links over hooks on the ends of the cars. But the great stresses due to present loadings would tear such hooks from the cars or tear the cars apart if such cars were used in the make-up of long heavy trains as now operated. The next stage in the development of draft gear was the invention of the "spring coupler," by which the energy due to a sudden tensile jerk or the impact of compression may be absorbed by heavy springs and gradually imparted to the car body. Such devices, for which there are many designs, seemed to answer the purpose for cars of 25 to 40 tons capacity. The use of 100,000-pound steel cars soon proved the inadequacy of even spring couplers. The friction-draft gear was then invented. The general principle of such a gear is that, when

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C l Į. 1 N FIG. 202. ш Σ 2 <

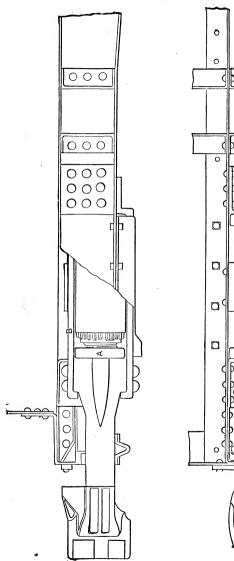
acting at or near its maximum capacity, it harmlessly transforms into heat the excessive energy developed by jerks or compression. There are several different designs of such gear, but the general principle underlying all of them may be illustrated by a description of the Westinghouse draft gear. The gear employs springs which have sufficient stiffness to act as ordinary spring-couplers for the ordinary pushing and pulling of train operations. Sections of the gear are shown in Fig. 202, while the method of its application to the framing of a car of the pressed steel type is shown in Fig. 203, a and b. When the draft gear is in tension the coupler, which is rigidly attached to B, is drawn to the left, drawing the follower Z with it. Compression is then exerted through the gear mechanism to the follower A which, being restrained by the shoulders RR, against which it presses, causes the gear to absorb the compression. The coil-spring C forces the eight wedges n against the eight corresponding segments E. The great compression of these surfaces against the outer shell produces a friction which retards the compression of the gear. The total possible movement of the gear, as determined by an official test, was 2.42 inches, when the maximum stress was 180,000 pounds. The work done in producing this stress amounted to 18,399 foot-pounds. Of this total energy 16,666 foot-pounds, or over 90%, represents the amount of energy absorbed and dissipated as heat by the frictional gear. The remaining 10% is given back by the recoil. The main release spring K is used for returning the segments and friction strips to their normal position after the force to close them has been removed. It also gives additional capacity to the entire mechanism. The auxiliary spring L releases the wedge D, while the release pin M releases the pressure of the auxiliary spring L against the wedge during frictional operation. If we omit from the above design the frictional features and consider only the two followers A and Z, separated by the springs C and K, acting as one spring, we have the essential elements of a spring-draft gear. In fact, this gear acts exactly like a spring-draft gear for all ordinary service, the frictional device only acting during severe tension and compression.

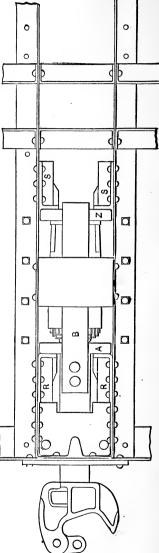
332. Gauge of wheels and form of wheel-tread.—In Fig. 204 is shown the standard adopted by the Master Car Builders' Association at their twentieth annual convention. Note the

# RAILROAD CONSTRUCTION.

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FIG. 203.





normal position of the gauge-line on the wheel-tread. In Fig. 114, p. 259, the relation of rail to wheel-tread is shown on a smaller scale. It should be noted that there is no definite position where the wheel-flange is absolutely "chock-a-block" against the rail. As the pressure increases the wheel mounts a little higher on the rail until a point is soon reached when the resistance is too great for it to mount still higher. By this means is avoided the shock of unvielding impact when the car sways from side to side. When the gauge between the inner faces of the wheels is greater or less than the limits given in the figure, the interchange rules of the Master Car Builders' Association authorize a road to refuse to accept a car from another road for transportation. At junction points of railroads inspectors are detailed to see that this rule (as well as many others) is complied with in respect to all cars offered for transfer.

#### TRAIN-BRAKES.

**333.** Introduction. Owing to the very general misapprehension that exists regarding the nature and intensity of the action of brakes, a complete analysis of the problem is considered justifiable. This misapprehension is illustrated by the common notion (and even practice) that the effectiveness of braking a car is proportional to the brake pressure, and therefore a brakeman is frequently seen using a bar to obtain a greater leverage on the brake-wheel and using his utmost strength to obtain the maximum pull on the brake-chain while the car is skidding along with locked wheels.

When a vehicle is moving on a track with a considerable velocity, the mass of the vehicle possesses kinetic energy of translation and the wheels possess kinetic energy of rotation. To stop the vehicle, this energy must be destroyed. The rotary kinetic energy will vary from about 4 to 8% of the kinetic energy of translation, according to the car loading (see § 347). On steam railroads brake action is obtained by pressing brake-shoes against car-wheel treads. As the brake-shoe pressure increases, the brake-shoes retard with increasing force the rotary action of the wheels. As long as the wheels do not slip or "skid." on the rails, the adhesion of the rails forces them to rotate with a circumferential velocity equal to the train velocity. The retarding action of the brake-shoe

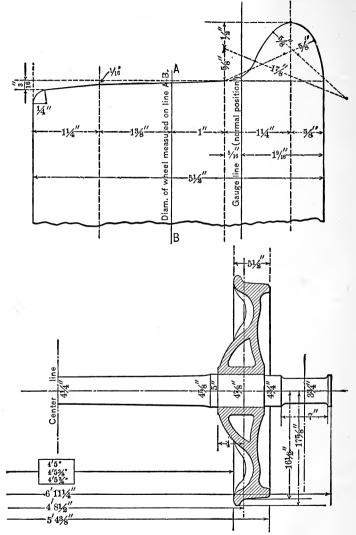


FIG. 204.-M. C. B. STANDARD WHEEL-TREAD AND AXLE.

checks first the rotative kinetic energy (which is small), and the remainder develops a *tendency* for the wheel to slip on the rail. Since the rotative kinetic energy is such a small per-centage of the total, it will hereafter be ignored, except as specifically stated, and it will be assumed for simplicity that the only work of the brakes is to overcome the kinetic energy of translation. The possible effect of grade in assisting or preventing retardation, and the effect of all other track resistances. is also ignored. The amount of the developed force which retards the train movement is limited to the possible adhesion or static friction between the wheel and the rail. When the friction between the brake-shoe and the wheel exceeds the adhesion between the wheel and the rail, the wheel skids, and then the friction between the wheel and the rail at once drops to a much less quantity. It must therefore be remembered at the outset that the retarding action of brakeshoes on wheels as a means of stopping a train is absolutely limited by the possible static friction between the braked wheels and the rails.

334. Laws of friction as applied to this problem. Much of the misapprehension regarding this problem arises from a very common and widespread misstatement of the general laws of friction. It is frequently stated that friction is independent of the velocity and of the unit of pressure. The first of these so-called laws is not even approximately true. A very exhaustive series of tests were made by Capt. Douglas Galton on the Brighton Railway in England in 1878 and 1879, and by M. George Marié on the Paris and Lyons Railway in 1879, with trains which were specially fitted with train-brakes and with dynagraphs of various kinds to measure the action of the brakes. Experience proved that variations in the condition of the rails (wet or dry), and numerous irregularities incident to measuring the forces acting on a heavy body moving with a high velocity, were such as to give somewhat discordant results, even when the conditions were made as nearly identical as possible. But the tests were carried so far and so persist-ently that the general laws stated below were demonstrated beyond question, and even the numerical constants were determined as closely as they may be practically utilized. These laws may be briefly stated as follows:

(a) The coefficient of friction between cast-iron brake-blocks

and steel tires is about .3 when the wheels are "just moving"; it drops to about .16 when the velocity is about 30 miles per hour, and is less than .10 when the velocity is 60 miles per hour. These figures fluctuate considerably with the condition of the rails, wet or dry.

(b) The coefficient of friction is greatest when the brakes are first applied; it then reduces very rapidly, decreasing nearly one third after the brakes have been applied 10 seconds, and dropping to nearly one half in the course of 20 seconds. Although the general truth of this law was established beyond question, the tests to demonstrate the law of the variation of friction with time of application were too few to determine accurately the numerical constants.

(c) The friction of skidded wheels on rails is always very much less than the adhesion when the wheel is rolling on the rail—sometimes less than one third as much.

(d) An analysis of the tests all pointed to a law that the friction developed does *not* increase as rapidly as the *intensity* of pressure increases, but this may hardly be considered as an established law.

(e) The adhesion between the wheel and the rail appears to be independent of velocity. The adhesion here means the force that must be developed before the wheel will slip on the rail.

The practical effect of these laws is shown by the following observed phenomena:

(a) When the brakes are first applied (the velocity being very high), a brake pressure far in excess of the weight on the wheel (even three or four times as much) may be applied without skidding the wheel. This is partly due to the fact that the wheel has a very high rotative kinetic energy (which varies as the square of the velocity, and which must be overcome first), but it is chiefly due to the fact that the coefficient of friction at the higher velocity is very small (at 60 miles per hour it is about .07), while the adhesion between the wheel and the rail is independent of the velocity.

(b) As the velocity decreases the brake pressure must be decreased or the wheels will skid. Although the friction decreases with the time required to stop and increases with the reduction of speed, and these two effects tend to neutralize each other, yet unless the stop is very slow, the increase in friction due to reduction of speed is much greater than the decrease due to time, and therefore the brake pressure must not be greater than the weight on the wheel, unless momentarily while the speed is still very high.

(c) The adhesion between wheels and rails varies from .20 to .25 and over when the rail is dry. When wet and slippery it may fall to .18 or even .15. The use of sand will always raise it above .20, and on a dry rail, when the sand is not blown away by wind, it may raise it to .35 or even .40.

(d) Experiments were made with an automatic valve by which the brake-shoe pressure against the wheel should be reduced as the friction increased, but since (1) the essential requirement is that the friction produced by the brake-shoes shall not exceed the adhesion between rail and wheel, and since (2) the rail-wheel adhesion is a very variable quantity, depending on whether the rail is wet or dry, it has been found impracticable to use such a valve, and that the best plan is to leave it to the engineer to vary the pressure, if necessary, by the use of the brake-valve.

# MECHANISM OF BRAKES.

335. Hand-brakes. The old style of brakes consists of brakeshoes of some type which are pressed against the wheel-treads by means of a brake-beam, which is operated by means of a hand-windlass and chain operating a set of levers. It is desirable that brakes shall not be set so tightly that the wheels shall be locked, and then slide over the track, producing flat places on them, which are very destructive to the rolling-stock and track afterward, on account of the impact occasioned at each revolution. With air-brakes the maximum pressure of the brake-shoes can be quite carefully regulated, and they are so designed that the maximum pressure exerted by any pair of brake-shoes on the wheels of any axle shall not exceed a certain per cent. of the weight carried by that axle when the car is *empty*, 90% being the figure usually adopted for passenger-cars and 70% for freight-cars. Consider the case of a freight-car of 100000 lbs. capacity, weighing 33100 lbs., or 8275 lbs. on an axle, and equipped with a hand-brake which operates the levers and brake-beams, which are sketched in Fig. 205. The dead weight on an axle is 8275 lbs.; 70% of

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this is 5792 lbs., which is the maximum allowable pressure per brake-beam, or 2896 lbs. per brake-shoe. With the dimensions shown, such a pressure will be produced by a pull of about 1158 lbs. on the brake-chain. The power gained by the brakewheel is not equal to the ratio of the brake-wheel diameter to the diameter of the shaft, about which the brake-chain winds, which is about 16 to  $1\frac{1}{2}$ . The ratio of the circumference of the brake-wheel to the length of chain wound up by one complete turn would be a closer figure. The loss of effi-

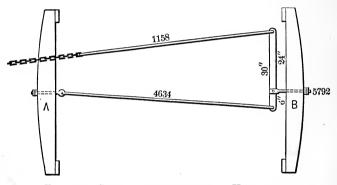


FIG. 205.—SKETCH OF MECHANISM OF HAND-BRAKE.

ciency in such a clumsy mechanism also reduces the effective ratio. Assuming the effective ratio as 6:1 it would require a pull of 193 lbs. at the circumference of the brake-wheel to exert 1158 lbs. pull on the brake-chain, or 5792 lbs. pressure on the wheels at B, and even this will not lock the wheels when the car is empty, much less when it is loaded. Note that the pressures at  $\hat{A}$  and B are unequal. This is somewhat objectionable, but it is unavoidable with this simple form of brakebeam. More complicated forms to avoid this are sometimes Hand-brakes are, of course, cheapest in first cost, and used. even with the best of automatic brakes, additional mechanism to operate the brakes by hand in an emergency is always provided, but their slow operation when a quick stop is desired makes it exceedingly dangerous to attempt to run a train at high speed unless some automatic brake directly under the control of the engineer is at hand. The great increase in the

average velocity of trains during recent years has only been rendered possible by the invention of automatic brakes.

336. "Straight" air-brakes. The essential constructive fea-330. "Straight" alf-brakes. The essential constructive fea-tures of this form of brake are (1) an air-pump on the engine, operated by steam, which compresses air into a reservoir on the engine; (2) a "brake-pipe" running from the reservoir to the rear of the engine and pipes running under each car, the pipes having flexible connections at the ends of the cars and engine: (3) a cylinder and piston under each car which operates the brakes by a system of levers, the cylinder being connected to the brake-pipe. The reservoir on the engine holds compressed air at about 45 lbs. pressure. To operate the brakes, a valve on the engine is opened which allows the com-pressed air to flow from the reservoir through the brake-pipe to each cylinder, moving the piston, which thereby moves the levers and applies the brakes. The *dejects* of this system are many: (1) With a long train, considerable time is required for the air to flow from the reservoir on the engine to the rear cars, and for an emergency-stop even this delay would often be fatal; (2) if the train breaks in two, the rear portion is not provided with power for operating the brakes, and a dangerous collision would often be the result; (3) if an air-pipe coupling bursts under any car, the whole system becomes absolutely helpless, and as such a thing might happen during some emer-gency, the accident would then be especially fatal.

This form of brake has almost, if not entirely, passed out of use. It is here briefly described in order to show the logical development of the form which is now in almost universal use, the automatic.

337. Automatic air-brakes. The above defects have been overcome by a method which may be briefly stated as follows: A reservoir for compressed air is placed under each car and the tender; whenever the pressure in these reservoirs is reduced for any reason, it is automatically replenished from the main reservoir on the engine; whenever the pressure in the brakepipe is reduced for any cause (opening a valve at any point of its length, parting of the train, or bursting of a pipe or coupler), valves are automatically moved under each car to operate the piston and put on the brakes. *All* the brakes on the train are thus applied almost simultaneously. If the train breaks in two, *both* sections will at once have *all* the brakes applied automati-

cally; if a coupling or pipe bursts, the brakes are at once int and attention is thereby attracted to the defect; if all by gency should arise, such that the conductor desires the train instantly without even taking time to signal engineer, he can do so by opening a valve placed on ea which admits air to the train-pipe, which will set the the tr on the whole train, and the engineer, being able to chuthe instantly what had occurred, would shut off steam : whatever else was necessary to stop the train as quickly sible. The most important and essential detail of this is the "automatic triple valve" placed under each car. Her to ing from the Westinghouse Air-brake Company's Insti Book, "A moderate reduction of air pressure in the traily, and causes the greater pressure remaining stored in the authis reservoir to force the piston of the triple valve and its tob valve to a position which will allow the air in the auxiet reservoir to pass directly into the brake-cylinder and appling brake. A sudden or violent reduction of the air in the tit. pipe produces the same effect, and in addition causes su tr mental valves in the triple valve to be opened, permitting pressure from the train-pipe to also enter the brake-cylinh augmenting the pressure derived from the auxiliary reserve about 20%, producing practically instantaneous action of brakes to their highest efficiency throughout the entire tra When the pressure in the brake-pipe is again restored to amount in excess of that remaining in the auxiliary reserve the piston- and slide-valves are forced in the opposite direct to their normal position, opening communication from the tra pipe to the auxiliary reservoir, and permitting the air in t brake-cylinder to escape to the atmosphere, thus releasing t If the engineer wishes to apply the brake, he move brakes. the handle of the engineer's brake-valve to the right, whi first closes a port, retaining the pressure in the main reservo and then permits a portion of the air in the train-pipe to escap To release the brakes, he moves the handle to the extrem left. which allows the air in the main reservoir to flow free into the brake-pipe, restoring the pressure therein."

338. Tests to measure the efficiency of brakes. Let v represent the velocity of a train in feet per second; W, its weight F, the retarding force due to the brakes; d, the distance in feer required to make a stop; and g, the acceleration of gravit

. . . . .

<sup>e</sup>); feet per square second); then the kinetic energy posby the train (disregarding for the present the rotative c energy of the wheels)  $=\frac{Wv^2}{2g}$ . The work done in stopthe train = Fd.  $\therefore Fd = \frac{Wv^2}{2g}$ . The ratio of the retarding to the weight,

$$\frac{F}{W} = \frac{v^2}{2gd} = .0155 \frac{v^2}{d}.$$

der to compare tests made under varying conditions, the  $f^{tr}F \div W$  should be corrected for the effect of grade (+ or -), in, and also for the proportion of the weight of the train is on braked wheels. For example, a train weighed 6 lbs., the proportion on braked wheels was 67%, speed Xet per second, length of stop 450 feet, track level. Sublying these values in the above formula, we find  $(F \div W)$ 4. This value is really unduly favorable, since the orditrack resistance helps to stop the train. This has a value m 6 to 20 lbs. per ton, averaging say 10 lbs. per ton durhe stop, or .005 of the weight. Since the effect of this is and is nearly constant for all trains, it may be ignored mparative tests. The grade in this case was level, and fore grade had no effect. But since only 67% of the at was on braked wheels, the ratio, on the basis of all the Is braked, or of the weight reduced to that actually on the d wheels, is  $0.124 \div .67 = 0.185$ . This was called a "good" although as high a ratio as 0.200 has been obtained.

**b.** Brake-shoes. Brake-shoes were formerly made of ght iron, but when it was discovered that cast-iron shoes 1 answer the purpose, the use of wrought-iron shoes was doned, since the cast-iron shoes are so much cheaper. A **b** practice is to form the brake-shoe and its head in one **c**, which is cheaper in first cost, but when the wearing-suris too far gone for further use, the whole casting must be ved. The "Christie" shoe, adopted by the Master Car lers' Association as standard, has a separate shoe which stened to the head by means of a wrought-iron key. The is beveled  $\frac{1}{4}$ " in a width of  $3\frac{2}{3}$ " to fit the coned wheel. is a greater bevel than the standard coning of a car-wheel. perhaps done to allow for some bending of the brake-

SR

beam and also so that the maximum pressure (and wear) should come on the outside of the tread, rather than next to the flange, where it might tend to produce sharp flanges. By concentrating the brake-shoe wear on the outer side of the tread, the wear on the tread is more nearly equalized, since the rail wears the wheel-tread chiefly near the flange. This same idea is developed still further in the "flange-shoes," which have a curved form to fit the wheel-flange and which bear on the wheel on the flange and on the outside of the tread. It is claimed that by this means the standard form of the tread is better preserved than when the wear is entirely on the tread. The Congdon brake-shoe is one of a type in which wroughtiron pieces are inserted in the face of a cast-iron shoe. It is claimed that these increase the life of the shoe.

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# CHAPTER XVI.

# TRAIN RESISTANCE.

**340.** Classification of the various forms. The various resistances which must be overcome by the power of the locomotive may be classified as follows:

(a) Resistances internal to the locomotive, which include friction of the valve-gear, piston- and connecting-rods, journal friction of the drivers; also all the loss due to radiation, condensation, friction of the steam in the passages, etc. In short, these resistances are the sum-total of the losses by which the power at the circumference of the drivers is less than the power developed by the boiler.

(b) Velocity resistances, which include the atmospheric resistances on the ends and sides; oscillation and concussion resistances, due to uneven track, etc.

(c) Wheel resistances, which include the rolling friction between the wheels and the rails of *all* the wheels (including the drivers); also the journal friction of all the axles, except those of the drivers.

(d) Grade and curve resistances, which include those resistances which are due to grade and to curves, and which are not found on a straight and level track.

(e) Brake resistances. As shown later, brakes consume power and to the extent of their use increase the energy to be developed by the locomotive.

(f) Inertia resistances. The resistance due to inertia is not generally considered as a train resistance because the energy which is stored up in the train as kinetic energy may be utilized in overcoming future resistances. But in a discussion of the demands on the tractive power of the engine, one of the chief items is the energy required to rapidly give to a starting train its normal velocity. This is especially true of suburban trains, which must acquire speed very quickly in order that

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their general average speed between termini may be even reasonably fast.

341. Resistances internal to the locomotive. These are resistances which do not tax the adhesion of the drivers to the rails, and hence are frequently considered as not being a part of the train resistance properly so called. If the engine were considered as lifted from the rails and made to drive a belt placed around the drivers, then all the power that reached the belt would be the power that is ordinarily available for adhesion, while the remainder would be that consumed internally by the engine. The power developed by an engine may be obtained by taking indicator diagrams which show the actual steam pressure in a cylinder at any part of a stroke. From such a diagram the average steam pressure is easily obtained, and this average pressure, multiplied by the length of the stroke and by the net area of the piston, gives the energy developed by one half-stroke of one piston. Four times this product divided by 550 times the time in seconds required for one stroke gives the "indicated horse-power" Even this calculation gives merely the power behind the piston, which is several per cent. greater than the power which reaches the circumference of the drivers, owing to the friction of the piston, piston-rod, cross-head, connecting-rod bearings, and driving-wheel jour-nals. (See § 322, Chapter XV.) By measuring the amount of water used and turned into steam, and by noting the boiler pressure, the energy possessed by the steam used is readily computed. The indicator diagrams will show the amount of steam that has been effective in producing power at the cylinders. The steam accounted for by the diagrams will ordinarily amount to 80 or 85% of the steam developed by the boiler, and the other 15 or 20% represents the loss of energy due to radiation, condensation, ctc. From actual tests it has been found that the power consumed by an engine running light is about 11% of that required by the engine when working hard in express freight service. But since the engine resistances (friction, etc.) are increased when it is pulling a load, it was estimated, after allowing for this fact, that about 15 or 16% of the power developed by the pistons was consumed by the engine, leaving about 84 to 85% for the train. 342. Velocity resistances. (a) Atmospheric. This consists of

342. Velocity resistances. (a) Atmospheric. This consists of the head and tail resistances and the side resistance. The head

and tail resistances are nearly constant for all trains of given velocity, varying but slightly with the varying cross-sections of engines and cars. The side resistance varies with the length of the train and the character of the cars, box-cars or flats, etc. Vestibuling cars has a considerable effect in reducing this side resistance by preventing much of the eddying of air-currents between the cars, although this is one of the least of the ad vantages of vestibuling. Atmospheric resistance is generally assumed to vary as the square of the velocity, and although this may be nearly true, it has been experimentally demon strated to be at least inaccurate. The head resistance is gen erally assumed to vary as the area of the cross-section, but this has been definitely demonstrated to be very far from true. A freight-train composed partly of flat-cars and partly of boxcars will encounter considerably more atmospheric resistance than one made exclusively of either kind, other things being equal. The definite information on this subject is very unsatisfactory, but this is possibly due to the fact that it is of little practical importance to know just how much such resistance amounts to.

(b) Oscillatory and concussive. These resistances are considered to vary as the square of the velocity. Probably this is nearly, if not quite, correct on the general principle that such resistances are a succession of impacts and the force of impacts varies as the square of the velocity. These impacts are due to the defects of the track, and even though it were possible to make a precise determination of the amount of this resistance in any particular case, the value obtained would only be true for that particular piece of track and for the particular degree of excellence or defect which the track then possessed. The general improvement of track maintenance during late years has had a large influence in increasing the possible train-load by decreasing the train resistance. The expenditure of money to improve track will give a road a large advantage over a competing road with a poorer track, by reducing train resistance, and thus reducing the cost of handling traffic.

343. Wheel resistances. (a) Rolling friction of the wheels. To determine experimentally the rolling friction of wheels, apart from all journal friction, is a very difficult matter and has never been satisfactorily accomplished. Theory as well as practice shows that the higher and the more perfect the elasticity of the wheel and the surface, the less will be the rolling friction. But the determination, if made, would be of theoretical interest only.

The combined effect of rolling friction and journal friction is determinable with comparative ease. From the nature of the case no great reduction of the rolling friction by any device is possible. It is only a very insignificant part of the total train resistance.

(b) Journal friction of the axles. This form of resistance has been studied quite extensively by means of the measurement of the force required to turn an axle in its bearings under various conditions of pressure, speed, extent of lubrication, and temperature. The following laws have been fairly well established: (1) The coefficient of friction increases as the pressure diminishes; (2) it is higher at very slow speeds, gradually diminishing to a minimum at a speed corresponding to a train velocity of about 10 miles per hour, then slowly increasing with the speed; it is very dependent on the perfection of the lubrication, it being reduced to one sixth or one tenth, when the axle is lubricated by a bath of oil rather than by a mere pad or wad of waste on one side of the journal; (3) it is much lower at higher temperature, and vice versa. The practical effect of these laws is shown by the observed facts that (1) loaded cars have a less resistance per ton than unloaded cars, the figures being (for speeds of about 10 to 20 miles per hour):

For	passenger- and loaded freight-cars	4	lbs.	$\mathbf{per}$	ton
" "	empty freight-cars.	6	"	"	"
" "	street-cars.	10	"	" "	"
"	freight-trucks without load	14	"	"	" "

(2) When starting a train, the resistances are about 20 lbs. per ton, notwithstanding the fact that the velocity resistances are practically zero; at about 2 miles per hour it will drop to 10 lbs. per ton and above 10 miles per hour it may drop to 4 lbs. per ton if the cars are in good condition. (3) The resistance could probably be materially lowered if some practicable form of journal-box could be devised which would give a more perfect lubrication. (4) It is observed that freight-train loads must be cut down in winter by about 10 or 15% of the loads that the same engine can haul over the same track in summer. This is due partly to the extra roughness and inelasticity of the track in winter, and partly to increased radiation from the engine wasting some energy, but this will not account for all of the loss, and the effect, which is probably due largely to the lower temperature of the journal-boxes, is very marked and costly. It has been suggested that a jacketing of the journalboxes, which would prevent rapid radiation of heat and enable them to retain some of the heat developed by friction, would result in a saving amply repaying the cost of the device.

Roller journals for cars have been frequently suggested, and experiments have been made with them. It is found that they are very effective at low velocities, greatly reducing the starting resistance, which is very high with the ordinary forms of journals. But the advantages disappear as the velocity increases. The advantages also decrease as the load is increased, so that with heavily loaded cars the gain is small. The excess of cost for construction and maintenance has been found to be more than the gain from power saved.

344. Grade resistance. The amount of this may be computed with mathematical exactness. Assume that the ball or cylinder (see Fig. 206) is being drawn up the plane. If W

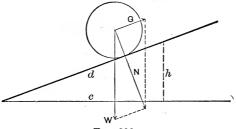


FIG. 206.

is the weight, N the normal pressure against the rail, and G the force required to hold it or to draw it up the plane with uniform velocity, the rolling resistances being considered zero or considered as provided for by other forces, then

$$G:W::h:d$$
, or  $G=\frac{Wh}{d}$ ;

but for all ordinary railroad grades, d=c to within a tenth of 1%, i.e.,  $G = \frac{Wh}{c} = W \times \text{rate of grade}$ . In order that the student may appreciate the exact amount of this approximation the percentage of slope distance to its horizontal projection is given in the following tabular form:

§ 344.

Grade in per cent.	1	2	3	4	5
$\frac{\text{Slope dist.}}{\text{hor. dist.}} \times 100.\dots$	100.005	100.020	100.045	100.080	100.125
Grade in per cent.	6	7	8	9	10
Slope dist. hor. dist.	100.180	100.245	100.319	100.404	100.499

This shows also the error on various grades of measuring with the tape on the ground rather than held horizontally. Since almost all railroad grades are less than 2% (where the error is but .02 of 1%), and anything in excess of 4% is unheard of for normal construction, the error in the approximation is generally too small for practical consideration.

If the rate of grade is 1:100,  $G = W \times \frac{1}{100}$ , i.e., G = 20 lbs. per ton;  $\therefore$  for any per cent. of grade,  $G = (20 \times \text{per cent. of grade})$ pounds per ton. When moving up a grade this force G is to be overcome in addition to all the other resistances. When moving down a grade, the force G assists the motion and may be more than sufficient to move the train at its highest allowable velocity. The force required to move a train on a level track at ordinary freight-train speeds (say 20 miles per hour) is about 7 lbs. per ton. A down grade of  $\frac{7}{20}$  of 1% will furnish the same power; therefore on a down grade of 0.35%, a freight-train would move indefinitely at about 20 miles per hour. If the grade were higher and the train were allowed to gain speed freely, the speed would increase until the resistance at that speed would equal W times the rate of grade, when the velocity would become uniform and remain so as long as the conditions were constant. If this speed was higher than a . safe permissible speed, brakes must be applied and power wasted. The fact that one terminal of a road is considerably higher than the other does not necessarily imply that the extra power needed to overcome the difference of elevation is a total waste of energy, especially if the maximum grades are so low that brakes will never need to be applied to reduce a dangerously high velocity, for although more power must be

used in ascending the grades, there is a considerable saving of power in descending the grades. The amount of this saving will be discussed more fully in Chapter XXIII.

345. Curve resistance. Some of the principal laws will be here given without elaboration. A more detailed discussion will be given in Chapter XXII.

(a) While the total curve resistance increases as the degree of curve increases, the resistance per degree of curve is much greater for easy curves than for sharp curves; e.g., the resistance on the excessively sharp curves (radius 90 feet) of the elevated roads of New York City is very much less per degree of curve than that on curves of 1° to 5°. (b) Curve resistance increases with the velocity. (c) The total resistance on a curve depends on the central angle rather than on the radius; i.e., two curves of the same central angle but of different radius would cause about the same total curve resistance. This is partly explained by the fact that the longitudinal slipping will be the same in each case. (See § 311, Chapter XV.) In each case also the trucks must be twisted around and the wheels slipped laterally on the rails by the same amount  $J^{\circ}$ . (See § 312, Chapter XV.)

346. Brake resistances. If a down grade is excessively steep so that brakes must be applied to prevent the train acquiring a dangerous velocity, the energy consumed is hopelessly lost without any compensation. When trains are required to make frequent stops and yet maintain a high average speed, considerable power is consumed by the application of brakes in stopping. All the energy which is thus turned into heat is hopelessly lost, and in addition a very considerable amount of steam is drawn from the boiler to operate the air-brakes, which consume the power already developed. It can be easily demonstrated that engines drawing trains in suburban service, making frequent stops, and yet developing high speed between stops, will consume a very large proportion of the total power developed by the use of brakes. Note the double loss. The brakes consume power already developed and stored in the train as kinetic or potential energy, while the operation of the brakes requires additional steam power from the engine.

347. Inertia resistance. The two forms of train resistance which under some circumstances are the greatest resistances to be overcome by the engine are the grade and inertia resistances, and fortunately both of these resistances may be computed with mathematical precision. The problem may be stated as follows: What constant force P (in addition to the forces required to overcome the various frictional resistances, etc.) will be required to impart to a body a velocity of v feet per second in a distance of s feet? The required number of foot-pounds of energy is evidently Ps. But this work imparts a kinetic energy which may be expressed by  $\frac{Wv^2}{2g}$ . Equating

these values, we have  $Ps = \frac{Wv^2}{2q}$ , or

 $P = \frac{Wv^2}{2gs}.$  (138)

The force required to increase the velocity from  $v_1$  to  $v_2$  may likewise be stated as  $P = \frac{W}{2gs}(v_2^2 - v_1^2)$ . Substituting in the formula the values W = 2000 lbs. (one ton), g = 32.16, and s =5280 feet (one mile), we have

$$P = .00588(v_2^2 - v_1^2).$$

Multiplying by  $(5280 \div 3600)^2$  to change the unit of velocity to miles per hour, we have

$$P = .01267(V_2^2 - V_1^2).$$

But this formula must be modified on account of the rotative kinetic energy which must be imparted to the wheels of the cars. The precise additional percentage depends on the particular design of the cars and their loading and also on the design of the locomotive. Consider as an example a box-car, 60000 lbs. capacity, weighing 33000 lbs. The wheels have a diameter of 36" and their radius of gyration is about 13". Each wheel weighs 700 lbs. The rotative kinetic energy of each wheel is 4877 ft.-lbs. when the velocity is 20 miles per hour, and for the eight wheels it is 39016 ft.-lbs. For greater precision (really needless) we may add 192 ft.-lbs. as the rotative kinetic energy of the axles. When the car is fully loaded (weight 93000 lbs.) the kinetic energy of translation is 1,244,340 ft.-lbs.; when empty (weight 33000 lbs.) the energy is 441540 ft.-lbs. The rotative kinetic energy thus adds (for this particular car) 3.15% (when the car is loaded) and 8.9% (when the car is empty) to the kinetic energy of translation. The kinetic

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energy which is similarly added, owing to the rotation of the wheels and axles of the locomotive, might be similarly computed. For one type of locomotive it has been figured at about 8%. The variations in design, and particularly the fluctuations of loading, render useless any great precision in these computations. For a train of "empties" the figure would be high, probably 8 to 9%; for a fully loaded train it will not much exceed 3%. Wellington considered that 6% is a good average value to use (actually used 6.14% for "ease of computation"), but considering (a) the increasing proportion of live load to dead load in modern car design, (b) the greater care now used to make up *full* train-loads, and (c) the fact that *full* train-loads are the critical loads, it would appear that 5%is a better average for the conditions of modern practice. Even this figure allows something for the higher percentage for the locomotive and something for a few empties in the train. Therefore, adding 5% to the coefficient in the above equation, we have the true equation

$$P = .0133(V_2^2 - V_1^2), \quad . \quad . \quad . \quad . \quad (139)$$

in which  $V_2$  and  $V_1$  are the higher and lower velocities respectively in *miles per hour*, and P is the force required *per ton* to impart that difference of velocity in a distance of *one mile* If more convenient, the formula may be used thus:

$$P_1 = \frac{70.224}{s} (V_2^2 - V_1^2), \quad \dots \quad (140)$$

in which s is the distance in feet and  $P_1$  is the corresponding force.

As a numerical illustration, the force required per ton to impart a kinetic energy due to a velocity of 20 miles per hour in a distance of 1000 feet will equal

$$P_1 \!=\! \frac{70.224(400\!-\!0)}{1000} =\! 28 \text{ lbs.,}$$

which is the equivalent (see § 344) of a 1.4% grade. Since the velocity enters the formula as  $V^2$ , while the distance enters only in the first power, it follows that it will require *four* times the force to produce twice the velocity in the same distance, or that with the *same* force it will require four times the distance to attain twice the velocity.

As another numerical illustration, if a train is to increase its speed from 15 miles per hour to 60 miles per hour in a distance of 2000 feet, the force required (in addition to all the other resistances) will be

$$P_1 = \frac{70.224(3600 - 225)}{2000} = 118.50$$
 lbs. per ton.

This is equivalent to a 5.9% grade and shows at once that it would be impossible unless there were a very heavy down grade, or that the train was very light and the engine very powerful.

348. Dynamometer tests. These are made by putting a "dynamometer-car" between the engine and the cars to be tested. Suitable mechanism makes an automatic record of the force which is transmitted through the dynamometer at any instant, and also a record of the velocity at any instant. One of the practical difficulties is the accurate determination of the velocity at any instant when the velocity is fluctuating. When the velocity is decreasing, the kinetic energy of the train is being turned into work and the force transmitted through the dynamometer is less than the amount of the resistance which is actually being overcome. On the other hand, when the velocity is increasing, the dynamometer indicates a larger force than that required to overcome the resistances, but the excess force is being stored up in the train as kinetic energy. Grade has a similar effect, and the force indicated by the dynamometer may be greater or less than that required at the given velocity on a level by the force which is derived from. or is turned into, potential energy. Therefore the resistance indicated by the dynamometer of a train will not be that on a level track at uniform velocity, unless the track is actually level and the velocity really uniform.

Dynamometer tests under other circumstances are therefore of no value unless it is possible to determine the true velocity at any instant and its rate of change, and also to determine the grade. Of course, the grade is easily found. An allowance for an increase or decrease of kinetic or potential energy must therefore be made before it is possible to know how much force is being spent on the ordinary resistances.

349. Gravity or "drop" tests. Dynamometer tests require he use of a dynamometer which is capable of measuring a orce of several thousands of pounds, and which therefore cannot determine such values with a close percentage of accuacy, especially if the force is small. A drop test utilizes the orce of gravity which may be measured with mathematical accuracy. The general method is to select a stretch of track which has a uniform grade of about 0.7% and which is preferably straight for two or three miles. On such a grade cars with running gear in good condition may be started by a push. The velocity will gradually increase until at some velocity, lepending on the resistances encountered, the cars will move iniformly. The only work requiring extreme care with this nethod is the determination of the velocity. If the velocity s fluctuating, as it is during the time when it is of the greatest mportance to know the velocity, it is not sufficient to deternine the time required to run some long measured distance, or the average velocity thus obtained would probably differ

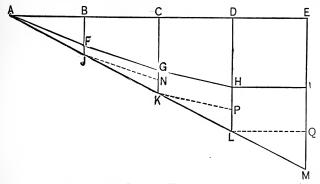


FIG. 207.-Loss in Velocity-head.

considerably from the velocity at the beginning and end of that space. If the train consists of five cars or more, the velocity may be determined electrically (as described by Wellington n his "Economic Location," etc., p. 793 *et seq.*) from the automatic record made on a chronograph of the passage of the irst wheel and the last, the chronograph also recording automatically the ticks of a clock beating seconds. From this the exact time of the passage of the first and last wheels of the train of cars may be determined to the tenth or twentieth of a second.

Velocity-head. From theoretical mechanics we know that if a body descends through any path by the action of gravity, and is unaffected by friction, its velocity at any point in the direction of the path of motion is  $V = \sqrt{2gh}$ . If the body is retarded by resistances, its velocity at any point will be less than this. If AM, Fig. 207, represents any grade (exaggerated of course), then BJ, CK, etc., represent the actual fall at any point. Let BF represent the fall  $h_1$ , determined from  $h_1 = \frac{v_1^2}{2g}$ ,

in which  $v_1$  is the actual observed velocity at J. Then JF = the velocity-head consumed by the resistances between A and J. If the train continues to K, the corresponding  $h_2$  is CG; the remaining fall GK consists of GN (=JF, which is the velocityhead lost back of J) and NK, the velocity-head lost between Jand K. At some velocity  $(V_n)$  on any grade, the velocity will not further increase and the line AFGHI will then be horizontal and at a distance  $(h_n) = EI$  below  $A \dots E$ . The grade AM is the "grade of repose" for that velocity  $(V_n)$ ; i.e., it is the grade that would just permit the train to move indefinitely at the velocity  $V_n$ . The broken line AFGHI should really be a curve, and the grade of repose at any point is the angle between AM and the tangent to that curve at the given point. The "grade of repose" by its definition gives the total resistance of the train at the particular velocity, or multiplying the grade of repose in per cent. by 20 gives the pounds per ton of resistance. Thus being able to determine the total resistance in pounds per ton at any velocity, the variation of total resistance with velocity may be determined, and then by varying the resistances, using different kinds of cars, empty and loaded, box-cars and flats, the resistances of the different kinds at various velocities may be determined.

350. Formulæ for train resistance. These are generally given in one of the forms

in which R is the resistance in pounds per ton, a and b are coefficients to be determined, V is the velocity in miles per hour, and c is a constant, also to be determined. These formulæ disregard grade and curve resistances, inertia resistance and the active resistance (or assistance) of wind, as distinct from mere atmospheric resistance. In short, they are supposed to give the resistance of a train moving at a uniform velocity over a straight and level track, there being no appreciable wind.

The various formulæ are sometimes based directly on experiments made by the proposer of the formula; sometimes they are deduced from a mere study of the results of one or more series of tests made by others. Unfortunately for either method, no one investigator has ever been able to make tests which are so thorough and made under such a wide range of conditions that his results may be considered as conclusive, while a student of the tests of others is handicapped by a lack of knowledge of precise conditions, which, if fully understood, would verhaps permit some reconciliation of the very discordant figures which are reported. As already intimated, the condition of the rolling stock, the unit weight on the axles, the lubrication of the axles, the length of the train in relation to its weight and the condition of the track, which involves the weight of rail, spacing and size of ties, tamping of ties, etc., all have their influence in modifying the apparent resistance. There is also good reason to believe that the effect of grade, curvature, and changing velocity has not been properly allowed for in deducing many of the formulæ. In view of all these considerations, it may be considered as demonstrated that no one formula, and especially a simple formula, will represent the resistance for all conditions. But, since some of the calculations of railroad economics are absolutely dependent on the law of tractive resistance, some law must be deduced with sufficient accuracy for the purpose. Fortunately several of the formulæ are amply accurate for such purposes. A report of a committee of the A. R. E. & M. W. Assoc. (1907) quoted sixty-one different formulæ which have been suggested. Some of these are chiefly of historical value, since they were deduced from tests made many years ago with track and rolling stock very dissimilar from those in use at the present time. Such formulæ will therefore be omitted. For convenience of comparison, all formulæ will be changed (if necessarv) from the original statement of them so that they give the

resistance per ton of 2000 pounds. The coefficients of V and  $V^2$  will be given decimally. Other notation occasionally used is as follows:

t = weight of train in tons of 2000 pounds; L = length of train in feet; n = number of cars in train; A = area of front of train in square feet.

(a) Formulæ of the first class: R = aV + c. Among those most commonly used are the following:

Engineering News,	R = 0.25V + 2.0		•	•	•	(142)
Baldwin locomotive,	R = 0.17V + 3.0	•	•	•	•	<b>(</b> 143)
New York Central,	R = 0.11V + 1.8,					
Henderson,	$R = 0.25V + \frac{50n}{t} + 0.5.$	•	•	•	•	(145)

Although Henderson's formula is in a class by itself, on account of the extra term, and although it is not applicable to general use, when the character of the trains cannot be estimated, it is perhaps more accurate than the others. It is apparently not intended for use at very low velocities.

(b) Formulæ of the second class:  $R = bV^2 + c$ :

Crawfo	ord,	$R = 0.00214 V^2 + 2.5$		•	•		•	(146)
Wolff,		$R = 0.00357 V^2 + 2.7$	•		•	•	•	(147)
Hende	rson,	$R = 0.00461 V^2 + 3.0$	•		•	•	•	(148)
Forney	· ·	$R \!=\! 0.00585 V^2 \!+\! 4.0$	•	•	•		•	(149)
Wel- ling- ton	R = 0.0 R = 0.0	$\frac{1056V^{2} + \frac{.57V^{2}}{t} + 3.9}{t} + 3.9 \text{ (for loade}}$ $1000000000000000000000000000000000000$	d b y fi	oox lat	can can	rs) :s)	},	(150)

Notice in formulæ (150) the additional journal resistance (indicated by the constant term) for unloaded cars. The second

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term evidently indicates the atmospheric resistance. The first term allows for the oscillatory resistances. Assuming the constant term and the coefficients to have been correctly determined, these formulæ should be better than the others, since a choice of formulæ can be made depending on the conditions. 'A train consisting partly of box-cars and partly of flat-cars will have a higher resistance than is shown by any of the above formulæ (and not a mean value), on account of the increased atmospheric resistance acting on the irregular form of the train. (c) Formulæ of the third class:  $R = aV + bV^2 + c$ :

W. N. Smith,	$R = 0.17V + \frac{0.0025AV^2}{t} + 3.0; \dots$	<b>(</b> 151 <b>)</b>
Von Borries,	$R = 0.04V + 0.0016V^2 + 3.0;$	<b>(</b> 152)
Lundie,	$R = 0.24V + \frac{4.8V^2}{t} + 4.0; \dots \dots$	<b>(</b> 153)
Sprague,	$R = 0.17V + \frac{0.333V^2}{t} + 4.0.$	(154)

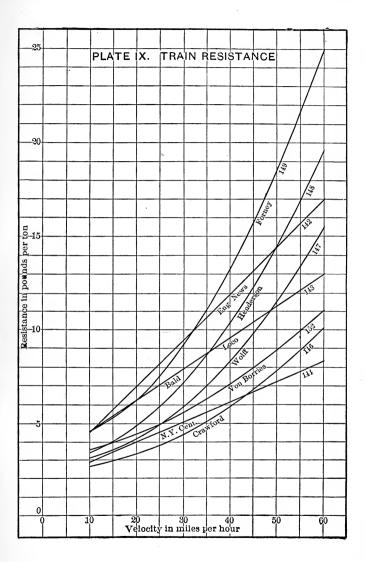
Although several formulæ have been proposed which involve the area of the front of the train in order to allow more definitely for the atmospheric resistance, only one of these (151) has been quoted. In applying this formula, the proper value to choose for A is somewhat indefinite, since the shape of the front of the train will make a considerable difference in the atmospheric resistance encountered. The area will vary from 80 to 100 square feet. In the comparison of the formulæ given below, A will be assumed as 100 square feet. In order to compare these resistances, the values of R for the various speeds of 10, 20, 30, 40, 50, and 60 miles per hour will be computed by these formulæ on the basis of a train of twelve cars, having a length of 480 feet, and a weight of 600 tons. Therefore in applying the formula, t=600, L=480, n=12, and A=100. In order to apply formula (150) to this case, it will be assumed that this train consists of loaded box-cars, and therefore we must apply the second of that group of formulæ. Computing the resistance according to these several formulæ, we may tabulate the results as given below:

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Formula.		v	elocity in r	niles per ho	our.	
	10	20	30	40	50	60
$142 \\ 143 \\ 144 \\ 145$	$2700 \\ 2800 \\ 1747 \\ 2400$	4200 3800 2413 3900	$5700 \\ 4800 \\ 3080 \\ 5400$	7200 5800 3747 6900	$8700 \\ 6800 \\ 4413 \\ 8400$	10200 7800 5080 9900
$146 \\ 147 \\ 148 \\ 149 \\ 150$	$1628 \\ 1834 \\ 2077 \\ 2751 \\ 2854$	$\begin{array}{r} 2014 \\ 2477 \\ 2906 \\ 3804 \\ 4396 \end{array}$	$\begin{array}{r} 2656 \\ 3548 \\ 4289 \\ 5559 \\ 6966 \end{array}$	$3554 \\ 5047 \\ 6226 \\ 8116 \\ 10564$	$\begin{array}{r} 4710\\ 6975\\ 8715\\ 11175\\ 15188\end{array}$	6122 9331 11746 15036 20844
$151 \\ 152 \\ 153 \\ 154$	$2845 \\ 2136 \\ 4320 \\ 3453$	$3940 \\ 2664 \\ 7200 \\ 4573$	$5085 \\ 3384 \\ 11040 \\ 5760$	6280 4296 15840 7013	$7525 \\ 5400 \\ 19440 \\ 8333$	8820 6696 28080 9720

Although there is a fair agreement among the results for ordinary velocities, it should be said, in fairness to the proposers of the various formulæ, that some of them evidently were not designed for use at high velocities such as 60 miles per hour.

Another method of comparing formulæ is to plot them on cross-section paper, using velocities as abscissæ and resistances as ordinates. For general use this method may only be applied to formulæ which do not involve the weight, length or area of the train nor the number of cars. All of the above formulæ have thus been plotted on Plate IX, with the exception of Nos. 145, 150, 151, 153, and 154. TRAIN RESISTANCE.



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### CHAPTER XVII

#### COST OF RAILROADS.

351. General considerations. Although there are many elements in the cost of railroads which are roughly constant per mile of road, yet the published reports of the cost of railroads differ very widely. The variation in the figures is due to several causes. (a) Economy requires that a road shall be operated and placed on an earning basis as soon as possible. Therefore the reported cost of a road during the first few years of its existence is somewhat less than that reported later. This is well illustrated when a long series of consecutive reports from an old-established road is available; nearly every year there will be shown an addition to the previous figures. And this is as it should be. The magnificent road-beds of some old roads cannot be the creation of a single season. It takes many years to produce such settled perfect structures. (b) A large part of the variation is due to a neglect to charge up "permanent improvements" as additions to the cost of the road. For the first few years of the life of a road a great deal of work is done which is in reality a completion of the work of construction, and yet the cost of it is buried under the item "maintenance of way." For example, a long wooden trestle is replaced by an earth embankment and a culvert. Since the original trestle is to be considered a temporary structure, the excess of the cost of the permanent structure over that of the temporary structure should evidently be considered as an addition to the cost of the road. But if the filling-in was done slowly, a few train-loads at a time, and the work scattered over many years, the cost of operating the "mud-train" has perhaps been buried under "maintenance" charges. (c) The reports from which many of the following figures were taken have not always analyzed the items of cost with the same detail as has been here attempted, and to that is probably due many of the variations and apparent discrepancies.

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The various items of cost will be classified as follows:

- 1. Preliminary financiering.
- 2. Surveys and engineering expenses.
- 3. Land and land damages.
- 4. Clearing and grubbing.
- 5. Earthwork.
- 6. Bridges, trestles, and culverts
- 7. Trackwork.
- 8. Buildings and miscellaneous structures.
- 9. Interest on construction.
- 10. Telegraph line.

352. Item I. PRELIMINARY FINANCIERING. The cost of this preliminary work is exceedingly variable. The work includes the clerical and legal work of organization, printing, engraving of stocks and bonds, and (sometimes the most expensive of all) the securing of a charter. This sometimes requires special legislative enactments, or may sometimes be secured from a State railroad commission. It has been estimated that about 2% of the railway capital of Great Britain has been spent in Parliamentary expenses over the charters. These expenses are usually but a small percentage of the total cost of the enterprise, but for important lines the gross cost is large, while the amount of money thus spent by organizations which have never succeeded in constructing their roads is, in the aggregate, an enormous amount, although it is of course not ascertainable by any investigator.

Another occasional feature of the financing of a road must be kept in mind. The promoters of a railroad enterprise frequently endeavor to limit their own personal expenditures to the purely preliminary expenses as mentioned above. The project, after having been surveyed, mapped, and written up in a glowing "prospectus," is submitted to capitalists, in the endeavor to have them furnish money for construction, the money to be secured by bonds. If the project will stand it, the amount of the bond issue is made sufficient to pay the entire cost of the road, even with a discount of perhaps 15%. The bond issue may also provide for a very generous commission to the broker who is the intermediary between the promoters and the capitalists. The bond issue may even provide for repaying the promoters for their preliminary expenses. Frequently a considerable proportion of the capital stock goes to the capitalists who take the bonds, the promoters retaining only such proportion as may be agreed upon. In such a case, the capital stock is "pure velvet," and costs nothing. Its future value, whatever it may be, is so much clear profit. The effect of such a financial policy is to burden the project with a capitalization which is far in excess of the actual cost of constructing the road. Comparatively few projects will stand such over-capitalization. The apparent financial failure of many railroads, which have gone into the hands of receivers is due to their inability to make returns on an over-capitalization rather than because they could not earn enough to pay the legitimate cost of their construction. These features of financiering are really foreign to the engineer's work, but he should know that many projects which would return a handsome profit on an investment amounting only to the legitimate cost, will be rejected by capitalists because it is apparent that there is not enough "velvet" in it.

353. Item 2. SURVEYS AND ENGINEERING EXPENSES. The comparison of a large number of itemized reports on the cost of construction shows that the cost of the "engineering" will average about 2% of the total cost of construction. This includes the cost of surveys and the cost of laying out and super-intending the constructive work. The cost of mere surveying up to the time when construction actually commences has been variously quoted at \$60, \$75, and even \$150 per mile. In exceptional cases the surveying for a few miles through some gorge might cost many times this amount, but \$150 per mile may be considered an ordinary maximum for difficult country. On the other hand, much construction has been done over the western prairies after hasty surveys costing not much over \$10 per mile. In the estimate given at the end of this chapter the cost of "engineering and office expenses" is given at 5% of the cost of the construction work. The item then includes the cost of the very considerable amount of clerical work and superintendence incident to the expenditure of such a large sum of money.

354. Item 3. LAND AND LAND DAMAGES. The cost of this item varies from the extreme, in which not only the land for

right-of-way but also grants of public land adjoining the road are given to the corporation as a subsidy, to the other extreme, where the right-of-way can only be obtained at exorbitant prices. The width required is variable, depending on the width that may be needed for deep cuts or high fills, or the extra land required for yards, stations, etc. A strip of land 1 mile long and 8.25 feet wide contains precisely 1 acre. An average width of 4 rods (66 feet), therefore, requires 8 acres per mile. On the Boston & Albany Railroad the expenditure assigned to "land and land damages" averages over \$25000 per mile. Of course this includes some especially expensive land for terminals and stations in large cities. Less than \$300 per mile was assigned to this item by an unimportant 18-mile road.

355. Item 4. CLEARING AND GRUBBING. The cost of this may vary from zero to 100% for miles at a time, but as an average figure it may be taken as about 3 acres per mile at a cost of say \$50 per acre. The possibility of obtaining valuable timber, which may be utilized for trestles, ties, or otherwise, and the value of which may not only repay the cost of clearing and grubbing, but also some of the cost of the land, should not be forgotten.

356. Item 5. EARTHWORK. This item also includes rockwork. The methods of estimating the cost of earthwork and rockwork have been discussed in Chapter III. The percentage of this item to the total cost is very variable. On a western prairie it might not be more than 5 to 10%. On a road through the mountains it will run up to 20 or 25%, and even more. The item also includes tunneling, which on some roads is a heavy item.

357. Item 6. BRIDGES, TRESTLES, AND CULVERTS. This item will usually amount to 5 or 6% of the total cost of the road. In special cases, where extensive trestling is necessary, or several large bridges are required, the percentage will be much higher. On the other hand, a road whose route avoids the watercourses may have very little except minor culverts. On the Boston & Albany the cost is given as \$5860 per mile; on the Adirondack Railroad, \$2845 per mile. Considering their relative character (double and single track), these figures are relatively what we might expect.

358. Item 7. TRACKWORK. This item will be considered as including everything above subgrade, except as otherwise itemized.

(a) Ballast. With an average width, for single track, of 10 feet and an average depth of 15 inches, 2444 cubic yards of ballast will be required. The Pennsylvania Railroad estimate is 2500 yards of gravel per mile of single track. At an estimate of 60 c. per yard, this costs \$1500 per mile. Broken-stone ballast must be filled out over the ends of the ties and therefore more is required; 2800 cubic yards of broken stone at \$1.25 per yard in place will cost \$3500 per mile.

(b) Ties. Ties cost anywhere from 80 c. down to 35 c. and even 25 c. At an average figure of 50 c., 2640 ties per mile will cost \$1320 per mile of single track. The cheaper ties are usually smaller and more must be used per mile, and this tends to compensate the difference in cost.

The following tabular form is convenient for reference:

Number per 33' rail.	Average spacing center to center.	Number per mile.
22 21 20 19 18 17 16 15 14 13	18.0 inches         18.9 ''         19.8 ''         20.9 ''         22.0 ''         23.3 ''         24.75 ''         26.4 ''         28.3 ''         30.5 ''	$\begin{array}{c} 3520\\ 3360\\ 3200\\ 3040\\ 2880\\ 2720\\ 2560\\ 2400\\ 2240\\ 2080\\ \end{array}$

TABLE XV.---NUMBER OF CROSS TIES PER MILE.

(c) Rails. The total weight of the rails used per mile may best be seen by the tabular form.

A convenient and useful rule to remember is that the number of *long* tons (2240 lbs.) per mile of single track equals the weight of the rail per yard times  $\frac{1}{7}$ . The rule is exact. For example, there are 3520 yards of rail in a mile of single track; at 70 lbs. per yard this equals 246400 lbs., or 110 long tons (exactly); but  $70 \times \frac{1}{7} = 110$ .

Any calculation of the required weight of rail for a given weight of rolling-stock necessarily depends on the assumptions which are made regarding the support which the rails receive from the ties. This depends not only on the width and spacing

#### COST OF RAILROADS.

Weight in lbs. • per yd.	Tons (2240 lb.) per mile of single track.	Cost at \$26 per ton.	Cost at \$30 per ton.	Weight in lbs. per yd.	Tons (2240 lb.) per mile of single track.	Cost at \$26 per ton.	Cost at \$30 per ton.
$ \begin{array}{r}             8 \\             10 \\             12 \\             14 \\             16 \\             20 \\             25 \\             30 \\             35 \\             40 \\             45 \\             40 \\             45 \\             40 \\             45 \\             40 \\             45 \\             40 \\             45 \\             40 \\             45 \\             40 \\             45 \\             40 \\             45 \\             40 \\             45 \\             40 \\             45 \\             40 \\             45 \\             40 \\             45 \\             40 \\             45 \\             40 \\             45 \\             40 \\             45 \\             40 \\             45 \\             40 \\             45 \\             40 \\             45 \\             45 \\           $	$\begin{array}{c} 12.571\\ 15.714\\ 18.857\\ 22.000\\ 25.143\\ 31.429\\ 39.286\\ 47.143\\ 55.000\\ 62.857\\ 70.714\\ 75.490\end{array}$	\$326.86 408.57 490.29 572.00 653.71 817.14 1021.43 1225.71 1430.00 1634.29 1838.57	\$377.14 471.43 365.71 660.00 754.20 942.86 1178.57 1414.29 1650.00 1885.71 2121.43 29269.86	$\begin{array}{c} 65\\ 66\\ 67\\ 68\\ 70\\ 71\\ 72\\ 73\\ 75\\ 78\\ 80\\ 82\\ \end{array}$	$\begin{array}{c} 102.143\\ 103.714\\ 105.286\\ 106.857\\ 110.000\\ 111.571\\ 113.143\\ 114.714\\ 117.857\\ 122.571\\ 125.714\\ 128.857\\ \end{array}$	$\begin{array}{c} \$2655.71\\ 2696.57\\ 2737.43\\ 2778.29\\ 2860.00\\ 2900.86\\ 2941.71\\ 2982.57\\ 3064.29\\ 3186.86\\ 3268.57\\ 2250.90\\ \end{array}$	$\begin{array}{c} 3158.59\\ 3205.79\\ 3300.00\\ 3347.14\\ 3394.29\\ 3441.43\\ 3535.71\\ 3677.14\\ 3771.43\end{array}$
$ \begin{array}{r} 48 \\ 50 \\ 52 \\ 56 \\ 57 \\ 60 \\ 61 \\ 63 \\ \end{array} $	$\begin{array}{c} 75.429\\ 78.571\\ 81.714\\ 88.000\\ 89.571\\ 94.286\\ 95.857\\ 99.000 \end{array}$	$1961.14 \\ 2042.86 \\ 2124.57 \\ 2288.00 \\ 2328.86 \\ 2451.43 \\ 2492.29 \\ 2574.00 \\$	$\begin{array}{c} 2262.86\\ 2357.14\\ 2451.43\\ 2640.00\\ 2687.14\\ 2828.57\\ 2875.71\\ 2970.00\\ \end{array}$	82 85 88 90 92 95 98 100	$\begin{array}{c} 128.837\\ 133.571\\ 138.286\\ 141.429\\ 144.571\\ 149.286\\ 154.000\\ 157.143\\ \end{array}$	$\begin{array}{c} 3350.29\\ 3472.86\\ 3595.43\\ 3677.14\\ 3758.86\\ 3881.43\\ 4004.00\\ 4085.71\\ \end{array}$	$\begin{array}{r} 4007.14\\ 4148.57\\ 4242.86\\ 4337.14\\ 4478.57\end{array}$

TABLE XVI.—TONS PER MILE (WITH COST) OF RAILS OF VARIOUS WEIGHTS.

About two per cent. (2%) extra should be allowed for waste in cutting.

of the ties (which are determinable), but also on the support which the ties receive from the ballast, which is not only very uncertain but variable. No general rule can therefore claim any degree of precision, but the following is given by the Baldwin Locomotive Works: "Each ten pounds weight per yard of ordinary steel rail, properly supported by cross-ties (not less than 14 per 30-foot rail), is capable of sustaining a safe load per wheel of 2240 pounds." For example, a consolidation locomotive with 112600 lbs. on 8 drivers has a load of 14075 lbs. per wheel. This divided by 2240 gives 6.28. According to the rule, the rails for such a locomotive should weigh at least 62.8 lbs. per yard.

(d) Splice-bars, track-bolts, and spikes. These are usually sold by the pound, except the patented forms of rail-joints, which are sold by the pair. In any case they are subject to market fluctuations in price. As an approximate value the following prices are quoted: Splice-bars, 1.35 c. per pound; track-bolts, 2.4 c.; spikes, 1.75 c. The weight of the splicebars will depend on the precise pattern adopted—its crosssection and length.

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In Table XVII are quoted from a catalogue of the Illinois Steel Co. the weights per foot of sections of angle-bars which they recommend for various weights of rail and which are designed to fit standard A. S. C. E. rail sections of those weights. The net weight of the angle-bars may be approximated by subtracting about 2.5% to 4% from the gross weight to allow for the bolt-holes. A deduction of 2.5% is usually about right for the heavier sections. Their recommendations regarding lengths of angle-bars do not include those for rails heavier. than 50 pounds per yard. On the basis of a length of 23 inches for four-hole splices and of 33 inches for six-hole splices, the weights of splice-bars have been computed for the several styles of splices for heavier rails, allowing 2.5% for the holes. The lengths recommended for track bolts are those which will allow about  $\frac{1}{2}$  inch for the nutlock and for margin, except for the lighter rails.

Weight of rail.	Length of angle-bar.	Weight per foot.	Weight of pair.	Proper size of track-bolt.	Proper size of spikes.
30 35 40 45 50 55	21" 21" 21" 21" 21" 21" 21" 23"	$\begin{array}{r} 4.49 \\ 4.7 \\ 5.54 \\ 6.3 \\ 6.97 \\ 7.5 \end{array}$	$     \begin{array}{r}       15.1 \\       15.9 \\       18.8 \\       21.5 \\       23.4 \\       28.0 \\     \end{array} $	$\begin{array}{c} 2^{1''}_{22} \times \\ 2^{1''}_{22} \times \\ 3^{1''}_{22} \times \\ 3^{1'''}_{22} \times \\ 3^{1''''}_{22} \times \\ 3^{1'''''}_{22} \times \\ 3^{1''''''''''''''''''''''''''''''''''''$	$\begin{array}{c} 4'' \times \frac{1}{2}'' \\ 4\frac{1}{2}'' \times \frac{1}{2}'' \\ 5\frac{1}{2}'' \times \frac{1}{2}''' \\ 5\frac{1}{2}'' \times \frac{1}{2}'' \\ 5\frac{1}{2}'' \times \frac{1}{2}''' \\ 5\frac{1}{2}'' \times \frac{1}{2}'' \\ 5\frac{1}{2}'' \times \frac{1}{2}'' \\ 5\frac{1}{2}'' \times \frac{1}{2}''' \\ 5\frac{1}{2}'' \\ 5\frac{1}{2}'' \\ 5\frac{1}{2}'' \\ 5\frac{1}{2}'' \\ 5\frac{1}{2}''' \\ 5\frac{1}{2}''''' \\ 5\frac{1}{2}''''' \\ 5\frac{1}{2}'''' \\ 5\frac{1}{2}''''''''''''' \\ 5\frac{1}{2}''''''''''''''''''''''''''''''''''$
60 65 70	23" { 23" { 33" { 23"	8.4 9.2 9.6 9.0	$31.4 \\ 34.4 \\ 51.5 \\ 33.6 \\ 53.6$	$\begin{vmatrix} 3\frac{4}{4} \\ 4 \\ 4 \\ 4 \\ 4 \\ 4 \\ 4 \\ 4 \\ 4 \\ 4 \\$	$5^{2}$
75 80	33" 23" 33" 23" 33"	$10.0 \\ 10.68 \\ 11.9 \\ 10.61 \\ 14.65$	$39.9 \\ 63.7 \\ 39.7 \\ 78.5$	$4\frac{1}{4}'' \times \frac{3}{4}''$	$\begin{array}{c} 5\frac{1}{2}'' \times \frac{1}{2}\frac{1}{2}''' \\ 5\frac{1}{2}'' \times \frac{1}{2}\frac{1}{$
85 90 95 100	`33" 33" 33" 33"	$12.4 \\ 13.5 \\ 14.7 \\ 15.78$	66.4 72.3 78.7 85.0	**************************************	$5\frac{1}{2}$ , $\times$ $\frac{1}{16}$ , $16$ , $16$ , $5\frac{1}{2}$ , $\times$ $\frac{1}{16}$ , $16$ , $16$ , $5\frac{1}{2}$ , $\times$ $\frac{1}{16}$ , $16$ ,

TABLE XVII.----SPLICE-BARS FOR VARIOUS WEIGHTS OF RAILS.

## COST OF RAILROADS.

Size meas- ured under		Ties 24" be ters, 4 spil number	Suitable weight of rail.	
head.	200 pounds	Pounds.	Kegs.	
$\begin{array}{c} 5\frac{1}{2}'' \times \frac{5}{2}'' \\ 5\frac{1}{2}'' \times \frac{9}{16}'' \\ 5'' \times \frac{9}{16}'' \\ 5'' \times \frac{1}{2}'' \end{array}$	$275 \\ 375 \\ 400$	$7680 \\ 5632 \\ 5280$	$38.40 \\ 28.16 \\ 26.40$	90 to 100 45 <sup>11</sup> 100 40 <sup>11</sup> 56
$4\frac{1}{2}'' \times \frac{1}{2}''$ $4'' \times \frac{1}{2}''$	$     \begin{array}{r}       450 \\       530 \\       600     \end{array} $	$4692 \\ 3984 \\ 3520$	$23.46 \\ 19.92 \\ 17.60$	40 35 30
$\bar{4}_{2}^{1''} \times \bar{1}_{16}^{7''}$	680	3104	15.52	25 to 30

TABLE XVIII.-RAILROAD SPIKES.

# TABLE XIX.---TRACK-BOLTS. Average number in a keg of 200 pounds.

Size of bolt.	Square	Hexagonal	Suitable
	nut.	nut.	rail.
2003 03 03 04 44 03 03 44 44 44	$\begin{array}{r} 366\\ 250\\ 243\\ 236\\ 229\\ 215\\ 170\\ 165\\ 161\\ 157\\ 149\\ \end{array}$	$\begin{array}{r} 395\\ 270\\ 261\\ 253\\ 244\\ 236\\ 228\\ 180\\ 175\\ 170\\ 165\\ 160\\ 156\\ \end{array}$	40 pound 50 55 to 60 65 '' 70 75 80 85 90

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(e) Track-laying. Much depends on the force of men employed and the use of systematic methods; \$528 per mile is the estimate employed by the Pennsylvania Railroad. \$500 per mile is the estimate given in § 362.

359. Item 8. BUILDINGS AND MISCELLANEOUS STRUCTURES. Except for rough and preliminary estimates, these items must be individually estimated according to the circumstances. The subitems include depots, engine-houses, repair-shops, waterstations, section- and tool-houses, besides a large variety of smaller buildings. The structures include turn-tables, cattleguards, fencing, road-crossings, overhead bridges, etc. The detailed estimate, given in § 362, illustrates the cost of these smaller items.

360. Item 9. INTEREST ON CONSTRUCTION. The amount of capital that must be spent on a railroad before it has begun to earn anything is so very large that the interest on the cost during the period of construction is a very considerable item. The amount that must be charged to this head depends on the current rate of money on the time required for construction and on the ability of the capitalists to retain their capital where it will be earning something until it is actually needed to pay the company's obligations. Of course, it is not necessary to have the entire capital needed for construction on hand when construction commences. Assuming money to be worth 6%, that the work of construction will require one year, that the money may be retained where it will earn something for an average period of six months after construction commences, or, in other words, it will be out of circulation six months before the road is opened for traffic and begins to earn its way, then we may charge 3% on the total cost of construction.

361. Item 10. TELEGRAPH LINES. This evidently depends on the scale of the road and the magnitude of the business to be operated. In the following estimate it is given as \$200 per mile, which evidently is intended to apply to the business of a small road.

362. Detailed estimate of the cost of a line of road. The following estimate was given in the *Engineering News* of Dec. 27, 1900, of the cost of the Duluth, St. Cloud, Glencoe & Mankato Railroad, 157.2 miles long.

The estimate is exactly as copied from the Engineering News. There are some numerical discrepancies. Item 26 should evi-

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dently be based on the sum of the first 25 items, and item 27 on the sum of the first 26. The figures in parentheses () are deduced from the figures given.

1.	Right-of-way: 1905.3 acres (12.12 acres per mile) @ \$100 per	
	acre	\$190530
2.	Clearing and grubbing. 144 acres (0.916 acre per mile) @ \$50	
	per acre	7200
3.	Earth excavation. 1907590 cu. yds. (12135 cu. yds. per mile)	
	@ 15 c	286138
4.	Rock excavation. 5100 cu. yds. (32.44 cu. yds. per mile) @ 80 c.	4080
	Wooden-box culverts. 508300 ft. B.M. @ \$30 per M \$15249	
	l Iron-pipe culverts: 879840 lbs. @ 3c. per lb 26395	41644
·	Pile trestling.         4000 lin. ft.         35 c. per lin. ft.         20535           Timber trestling.         5000 ft.         B. C. per lin. ft.         1610	
0.	Timber trestling. 509300 ft. B.M. @ \$30 per M 15279	16889
-	(Bridge masonry: 5520 cu. yds. @ \$8 per cu. yd 44160	
7.	Bridges, iron, 100 spans, 2000000 lbs. @ 4 c. per lb 80000	124160
	Cattle-guards.	8750
9.	Ties (2640 per mile). 419813 (159.02 miles) @ 35 c	146935
	Rails (70 lbs. per yd.): 110 tons per mile, 17492.2 tons (159.02	
	miles @\$26.	384797
11.	Rail sidings (70 lbs. per yd.): 110 tons per mile, 3300 tons	
	(30 miles @ \$26	85800
12.	Switch timbers and ties	3300
13.	Spikes: 5920 lbs. per mile, 1107040 (187 m.) @ 1.75. c. per lb.	19373
14.	Splice-bars. 2635776 lbs. @ 1.35 c. per lb	35583
	Track-bolts (2 to joint (?)): 188458.3 lbs. @ 2.4 c. per lb	4520
	Track-laying 187.2 miles @ \$500 per mile	93600
17.	Ballasting: 2152 cu. yds. per mile, 402854 (187.2 m.) @ 60 c	241712
	Turn-out and switch furnishings	6450
	Road-crossings, 68040 ft. B.M. @ \$30 per M	2041
	Section and tool-houses, 16 @ \$800	12800
	Water-stations	15000
	Turn-tables, 6 @ \$800	4800
	Depots, grounds, and repair-shops	78000
	Terminal grounds and special land damages	150000
	Fencing, 314 miles (\$150 per mile)	47100
	Engineering and office expenses (5% of \$1984458)	99222
	Interest on construction (3% of \$2083680)	62510
	Rolling-stock (\$5000 per mile)	786000
	Telegraph line: 157 miles @ \$200 per mile.	31400
		3060340
	i il and for an atim \$10407	

Average cost per mile ready for operation, \$19467.

Approximate cost of 130 miles from St. Cloud to Duluth, estimated at \$23000 per mile.

Approximate cost of entire line from Albert Lea to Duluth, 287.2 miles, \$6050340 (\$21060 per mile).

# PART II.

## RAILROAD ECONOMICS.

### CHAPTER XVIII.

#### INTRODUCTION.

363. The magnitude of railroad business. The gross earnings of railroads for the year ending June 30, 1910, were \$2,750,667,-435. This is greater than the combined value of all the gold, silver, iron, wheat, and corn produced by the country.

About 1,700,000 persons (over one sixtieth of the population) were directly employed by the roads for a compensation of 1,143,725,306. Probably 5,000,000 to 6,000,000 people were supported by this. Besides all these, probably 8,000,000 employés were kept busy in occupations which are a more or less direct result of railroads, *e.g.*, locomotive- and car-shops, rail-mills, etc. We therefore may estimate that perhaps 25,000,-000 people (or over one fourth of our population) are supported by railroads or by occupations which owe their chief existence to railroads.

The "number of passengers carried 1 mile" was 32,338 millions. Calling the population of the United States 92,000,000 for round numbers, it means an average ride of 351 miles for every man, woman, and child.

The "tons carried 1 mile" were 255,017 millions, or nearly 2773 ton-miles per inhabitant. The payments made to the railroads averaged nearly \$30 per inhabitant.

The actual bona-fide cost of the railroads of the country cannot be accurately computed (as will be shown later), but the capital, as represented by stocks and bonds, aggregated

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in 1910, \$18,417,132,238 or about \$200 per inhabitant. This is roughly about one sixth of the total national wealth.

The above figures may give some idea of the magnitude of the interests involved in the operation of railroads. No single business in the country approaches it in capital involved, earnings, number of people affected, or effect on other business. **364. Cost of transportation.** The importance of railroads

364. Cost of transportation. The importance of railroads may be also indicated by their power of creating cheap transportation. Less than one hundred years ago local famine and overabundant harvests within a radius of a few miles were not unknown. When the transportation of goods depended on actual porterage by human beings, as has been the case but recently in the Klondike, the transportation of 50 lbs. 20 miles might be considered a hard day's labor. At \$2 per day, this equals \$4 per ton-mile. In 1909 the railroads transported freight at an average cost to the public of 0.763 c. per ton per mile, and the feeding of Europe with wheat from Manitoba has become a commercial possibility. In 1909 passengers paid an average charge of 1.928 c. per mile, and a trip of 1000 miles inside of 24 hours is now common.

365. Study of railroad economics-its nature and limitations. The multiplicity of the elements involved in most problems in railroad construction preclude the possibility of a solution which is demonstrably perfect. Barring out the comparatively few cases in this country where it is difficult to obtain any practicable location, it may be said that a comparatively low order of talent will suffice to locate anywhere a railroad over which it is physically possible to run trains. It may be very badly located for obtaining business, the ruling grades may be excessive, the alignment may be very bad, and the road may be a hopeless financial failure, and yet trains can be run. Among the infinite number of possible locations of the road, the engineer must determine the route which will give the best railroad property for the least expenditure of moneythe road whose earning capacity is so great that after paying the operating expenses and interests on the bonds, the surplus available for dividends or improvements is a maximum.

An unfortunate part of the problem is that even the blunders are not always readily apparent nor their magnitude. A defective dam or bridge will give way and every one realizes the failure, but a badly located railroad affects chiefly the finances

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of the enterprise by a series of leaks which are only perceptible and demonstrable by an expert, and even he can only say that certain changes would probably have a certain financial value.

366. Outline of the engineer's duties. The engineer must realize at the outset the nature and value of the conflicting interests which are involved in variable amount in each possible route.

(a) The maximum of business must be obtained, and yet it may happen that some of the business may only be obtained by an extravagant expenditure in building the line or by building a line very expensive to operate.

(b) The ruling grades should be kept low, and yet this may require a sacrifice in business obtained and also may cost more than it is worth.

(c) The alignment should be made as favorable as possible; favorable alignment reduces the future operating expenses, but it may require a very large immediate outlay.

(d) The total cost must be kept within the amount at which the earnings will make it a profitable investment.

(e) The road must be completed and operated until the "normal" traffic is obtained and the road is self-supporting without exhausting the capital obtainable by the projectors; for no matter how valuable the property may ultimately become, the projectors will lose nearly, if not quite, all they have invested if they lose control of the enterprise before it becomes a paying investment.

Each new route suggested makes a new combination of the above conflicting elements. The engineer must select a route by first eliminating all lines which are manifestly impracticable and then gradually narrowing the choice to the best routes whose advantages are so nearly equal that a closer detailed comparison is necessary.

The ruling grade and the details of alignment have a large influence on the operating expenses. A large part of this course of instruction therefore consists of a study of operating expenses under average normal conditions, and then a study of the effect on operating expenses of given changes in the alignment.

367. Justification of such methods of computation. It may be argued that the data on which these computations are based are so unreliable (because variable and to some extent non-

computable) that no dependence can be based on the conclusions. This is true to the extent that it is useless to claim great precision in the computation of the value of any proposed change of alignment. Suppose, for example, it is com-puted that a given improvement in alignment will reduce the operating expenses of 20 trains per day by \$1000 per year. Suppose the change in alignment may be made for \$5000, which may be obtained at 5% interest. Even with large allowances for inaccuracy in the computation of the value, \$1000, it evidently will be better to incur an additional interest charge of \$250 than increase the annual operating expenses by \$1000. Moreover, since traffic is almost sure to increase (and interest charges are generally decreasing), the advantage of the improvement will only increase as time passes. On the other hand, if the improvement cannot be made except by an expenditure of, say, \$50000, the change would evidently be unjustifiable. When the interest on the first cost is practically equal to the annual operating value of the proposed improvement, there is evidently but little choice; no great harm can result from either decision, and the decision frequently will depend on the willingness to increase the total amount invested in the enterprise.

To express the above question more generally, in every computation of the operating value of a proposed improvement, it may always be shown that the true value lies somewhere between some maximum and some minimum. Closer calculations and more reliable data will narrow the range between these extreme values. According as the interest on the cost of the proposed improvement is greater or less than the mean of these limits, we may judge of its advisability. The range of the limits shows the uncertainty. If it lies outside of the limits there is no uncertainty, assuming that the limits have been properly determined. If well within the limits, either decision will answer unless other considerations determine the question. And so, although it is not often possible to obtain precise values, we may generally reach a conclusion which is unquestionable. Even under the most unfavorable circumstances, the computations, when made with the assistance of all the broad common sense and experience that can be brought to bear, will point to a decision which is much better than mere "judgment," which is responsible for very many glaring and

costly railroad blunders. In short, Railroad Economics means the application of systematic methods of work plus experience and judgment, rather than a dependence on judgment unsystematically formed. It makes no pretense to furnishing mechanical rules by which all railroad problems may be solved by any one, but it does give a general method of applying principles by which an engineer of experience and judgment can apply his knowledge to better advantage. To the engineer of limited experience the methods are invaluable; without such methods of work his opinions are practically worthless; with them his conclusions are frequently more sound than the unsystematically formed judgments of a man with a glittering record. But the engineer of great experience may use these methods to form the best opinions which are obtainable, for he can apply his experience to make any necessary local modifications in the method of solution. The dangers lie in the extremes, either recklessly applying a rule on the basis of insufficient data to an unwarrantable extent, or, disgusted with such evident unreliability, neglecting altogether such systematic methods of work

## CHAPTER XIX.

### THE PROMOTION OF RAILROAD PROJECTS.

368. Method of formation of railroad corporations. Manv business enterprises, especially the smaller ones, are financed entirely by the use of money which is put into them directly in the form of stock or mere partnership interest. A railroad enterprise is frequently floated with a comparatively small financial expenditure on the part of the original promoters. The promoters become convinced that a railroad between Aand B, passing through the intermediate towns of C and D, with others of less importance, will be a paying investment. They organize a company, have surveys made, obtain a charter, and then, being still better able (on account of the additional information obtained) to exploit the financial advantages of their scheme, they issue a prospectus and invite subscriptions to bonds. Sometimes a portion of these bonds are guaranteed, principal and interest, or perhaps the principal alone, by townships or by the national government. The cost of this preliminary work, although large in gross amount if the road is extensive, is yet but an insignificant proportion of the total amount involved. The proportionate amount that can be raised by means of bonds varies with the circumstances. Tn the early history of railroad building, when a road was pro-jected into a new country where the traffic possibilities were great and there was absolutely no competition, the financial success of the enterprise would seem so assured that no difficulty would be experienced in raising from the sale of bonds all the money necessary to construct and equip the road. But the promoters (or stockholders) must furnish all money for the preliminary expenses, and must make up all deficiencies be-tween the proceeds of the sale of the bonds and the capital needed for construction.

"In theory, stocks represent the property of the responsible owners of the road, and bonds are an encumbrance on that

property. According to this theory, a railroad enterprise should begin with an issue of stock somewhere near the value of the property to be created and no more bonds should be issued than are absolutely necessary to complete the enterprise. Now it is not denied that there are instances in which this theory is followed out. In New England, for example, as well as in some of the Southern States, there are a few roads represented wholly by stock or very lightly mortgaged. But this theory does not conform to the general history of railway construction in the United States, nor is it supported by the figures that appear in the summary. The truth is, railroads are built on borrowed capital, and the amount of stock that is issued represents in the majority of cases the difference between the actual cost of the undertaking and the confidence of the public expressed by the amount of bonds it is willing to absorb in the ultimate success of the venture." \*

"The same general law obtains and has always obtained throughout the world, that such properties (as railways) are always built on borrowed money up to the limit of what is regarded as the positive and certain minimum value. The risk only—the dubious margin which is dependent upon sagacity, skill, and good management—is assumed and held by the company proper who control and manage the property." †

369. The two classes of financial interests—the security and profits of each. From the above it may be seen that stocks, bonds, car-trust obligations, and even current liabilities represent railroad capital. The issue of the bonds "was one means of collecting the capital necessary to create the property against which the mortgage lies." The variation between these interests lies chiefly in the security and profits of each. The current liabilities are either discharged or, as frequently happens, they accumulate until they are funded and thus become a definite part of the railroad capital.

The growth of this tendency is shown in the following tabular form (see next page):

The bonded interest has greater security than the stock, but less profit. The interest on the bonds must be paid before any money can be disbursed as dividends. If the bond interest

<sup>\*</sup> Henry C. Adams, Statistician, U. S. Int. Con. Commission.

<sup>†</sup> A. M. Wellington, Economic Theory of Railway Location.

Capitalization of Railroads in the United States.	June 30, 1888.		June 30, 1898.		June 30, 1910.	
	Amount, milions.	Per cent.	Amount, millions.	Per cent.	Amount, millions.	Per cent.
Stocks Funded debt Current liabilities, etc	3864 3869 396	$47.5 \\ 47.6 \\ 4.9$	$5311 \\ 5510 \\ 1087$	$\begin{array}{c} 44.6 \\ 46.3 \\ 9.1 \end{array}$	8,113 10,303	44.05 55.95

is not paid, a receivership, and perhaps a foreclosure and sale of the road, is a probability, and in such case the stockholder's interests are frequently wiped out altogether. The bondholder's real profit is frequently very different from his nominal profit. He sometimes buys the bonds at a very considerable discount, which modifies the rate which the interest received bears to the amount really invested. Even the bondholder's security may suffer if his mortgage is a second (or fifth) mortgage, and the foreclosure sale fails to net sufficient to satisfy all previous claims.

On the other hand, the stockholder, who may have paid in but a small proportion of his subscription, may, if the venture is successful, receive a dividend which equals 50 or 100% of the money actually paid in, or, as before stated, his entire holdings may be entirely wiped out by a foreclosure sale. When the road is a great success and the dividends very large, additional issues of stock are generally made, which are distributed to the stockholders in proportion to their holdings, either gratuitously or at rates which give the stockholders a large advantage over outsiders. This is the process known as "watering." While it may sometimes be considered as a legitimate "salting down" of profits, it is frequently a cover for dishonest manipulation of the money market.

For the twelve years between 1887 and 1899 about two thirds of all the railroad stock in the United States paid no dividends, while of those that paid dividends the average rate varied from 4.96 to 5.74%. The year from June 30, 1898, to June 30, 1899, was the most prosperous year of the group, and yet nearly 60% of all railroad stock paid no dividend, and the average rate paid by those which paid at all was 4.96%. The total amount distributed in dividends was greater than ever before, but the average rate is the least of the above group because many roads, which had passed their dividends for many previous

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years, distinguished themselves by declaring a dividend, even though small. During that same period but 13.35% of the stock paid over 6% interest. The total dividends paid amounted to but 2.01% of all the capital stock, while investments ordinarily are expected to yield from 4 to 6% (or more) according to the risk. Of course the effect of "watering" stock is to decrease the nominal rate of dividends, but there is no dodging the fact that, watered or not, even in that year of "good times," about 60% of all the stock paid *no* dividends. Unfortunately there are no accurate statistics showing how much of the stock of railroads represents actual paid-in capital and how much is "water." The great complication of railroad finances and the dishonest manipulation to which the finances of some railroads have been subjected would render such a computation practically worthless and hopelessly unreliable now.

During the year ending June 30, 1898 (which may in general be considered as a sample), 15.82% of the funded debt paid no interest. About one third of the funded debt paid between 4 and 5% interest, which is about the average which is paid.

The income from railroads (both interest on bonds and dividends on stock) may be shown graphically by diagrams, such as are given in the annual reports of the Interstate Commerce Commission. They show that while railroad investments are occasionally very profitable, the average return is less than that of ordinary investments to the investors. The indirect value of railroads in building up a section of country is almost incalculable and is worth many times the cost of the roads. It is a discouraging fact that very few railroads (old enough to have a history) have escaped the experience of a receivership, with the usual financial loss to the then stockholders. But there is probably not a railroad in existence which, however much a financial failure in itself, has not profited the community more than its cost.

370. The small margin between profit and loss to projectors. When a railroad is built entirely from the funds furnished by its promoters (or from the sale of stock) it will generally be a paying investment, although the rate of payment may be very small. The percentage of receipts that is demanded for actual operating expenses is usually about 67%. The remainder will usually pay a reasonable interest on the total capital involved. But the operating expenses are frequently 90 and even 100% of the gross receipts. In such cases even the bondholders do not get their due and the stockholders have absolutely nothing. Therefore the stockholder's interest is very speculative. A comparatively small change in the business done (as is illustrated numerically in § 372) will not only wipe out altogether the dividend—taken from the last small percentage of the total receipts and which may equal 50% or more of the capital stock *actually paid in*—but it may even endanger the bondholders' security and cause them to foreclose their mortgage. In such a case the stockholders' interest is usually entirely lost. It does not alter the essential character of the above-stated relations that the stockholders sometimes protect themselves somewhat by buying bonds. By so doing they simply decrease their risk and also decrease the possible profit that might result from the investment of a given total amount of capital.

371. Extent to which a railroad is a monopoly. It is a popular fallacy that a railroad, when not subject to the direct competition of another road, has an absolute monopoly-that it controls "all the traffic there is" and that its income will be practically independent of the facilities afforded to the public. The growth of railroad traffic, like the use of the so-called necessities or luxuries of life, depends entirely on the supply and the cost (in money or effort) to obtain it. A large part of railroad traffic belongs to the unnecessary class-such as traveling for pleasure. Such traffic is very largely affected by mere matters of convenience, such as well-built stations, • convenient terminals, smooth track, etc. The freight traffic is very largely dependent on the possibility of delivering manufactured articles or produce at the markets so that the *total* cost of production and transportation shall not exceed the total cost in that same market of similar articles obtained elsewhere. The creation of facilities so that a factory or mine may successfully compete with other factories or mines will develop such traffic. The receipts from such a traffic may render it possible to still further develop facilities which will in return encourage further business. On the other hand, even the partial withdrawal of such facilities may render it impossible for the factory or mine to compete successfully with rivals; the traffic furnished by them is completely cut off and the railroad (and indirectly the whole community) suffers correspondingly. The "strictly necessary" traffic is thus so small that few railroads could pay

their operating expenses from it. The dividends of a road come from the last comparatively small percentage of its revenue, and such revenue comes from the "unnecessary" traffic which must be coaxed and which is so easily affected by apparently insignificant "conveniences."

372. Profit resulting from an increase in business done; loss resulting from a decrease. In a subsequent chapter it will be shown that a large portion of the operating expenses are independent of small fluctuations in the business done and that the operating expenses are roughly two thirds of the gross revenue. Assume that by changes in the alignment the business obtained has been increased (or diminished) 10%. Assume for simplicity that the operating expenses on the revised track are the same as on the route originally planned; also that the cost of the track is the same and hence the fixed charges are assumed to be constant for all the cases considered. Assume the fixed charges to be 28%. The additional business, when carried in cars otherwise but partly filled will hardly increase the operating expenses by a measurable amount. When extra cars or extra trains are required, the cost will increase up to about 60% of the average cost per train mile. We may say that 10% increase may in general be carried at a rate of 40% of the average cost of the traffic. A reduction of 10%in traffic may be assumed to reduce expenses a similar amount. The effect of the change in business will therefore be as follows:

•	Business increased $10\%$ .	Business decreased 10%.		
	$67(1+10\% \times 40\%) = 69.68$	$67(1 - 10\% \times 40\%) = 64.32$		
95 Total income100	97.68 Income110.00	92.32 Income		
Available for divi- dends 5	Available for divi- dends 12.32	Deficit		

In the one case the increase in business, which may often be obtained by judicious changes in the alignment or even by, better management without changing the alignment, more than doubles the amount available for dividends. In the other case the profits are gone, and there is an absolute deficit. The above is a numerical illustration of the argument, previously stated, of the small margin between profit and loss to the original projectors.

373. Estimation of probable volume of traffic and of probable growth. Since traffic and traffic facilities are mutually interdependent and since a large part of the normal traffic is merely potential until the road is built, it follows that the traffic of a road will not attain its normal volume until a considerable time after it is opened for operation. But the estimation even of this normal volume is a very uncertain problem. The estimate may be approached in three ways:

1st. The actual gross revenue derived by all the railroads in that section of the country (as determined by State or U. S. Gov. reports) may be divided by the total population of the section and thus the average annual expenditure per head of population may be determined. A determination of this value for each one of a series of years will give an idea of the normal rate of growth of the traffic. Multiplying this annual contribution by the population which may be considered as tributary gives a valuation of the possible traffic. Such an estimate is unreliable (a) because the average annual contribution may not fit that particular locality, (b) because it is very difficult to correctly estimate the number of the true tributary population especially when other railroads encroach more or less into the territory. Since a rough value of this sort may be readily determined, it has its value as a check, if for nothing else.

2d. The actual revenue obtained by some road whose circumstances are as nearly as possible identical with the road to be considered may be computed. The weak point consists in the assumption that the character of the two roads is identical or in incorrectly estimating the allowance to be made for observed differences. The method of course has its value as a check.

3d. A laborious calculation may be made from an actual study of the route—determining the possible output of all factories, mines, etc., the amount of farm produce and of lumber that might be shipped, with an estimate of probable passenger traffic based on that of like towns similarly situated. This method is the best when it is properly done, but there is always the danger of leaving out sources of income—both existent and that to be developed by traffic facilities, or, on the other hand, of overestimating the value of expected traffic. In the

## RAILROAD CONSTRUCTION.

following tabular form are shown the population, gross receipts, receipts per head of population, mileage, earnings per mile of line operated, and mileage per 10,000 of population for the whole United States. It should be noted that the values are only *averages*, that individual variations are large, and that only a very rough dependence may be placed on them as applied to any particular case.

Year.	Population (estimated).	Gross receipts.	Receipts per head of popu- lation.	Mileage†	Earnings per mile of line operated.	Mileage per 10,000 popula- tion.‡
1888 1889 1890 1891	60,100,000 61,450,000 *62,801,571 64,150,000	\$910,621,220 964,816,129 1051,877,632 1096,761,395	\$15.15 15.81 16.75 17.10	$\begin{array}{r} 136,884\\ 153,385\\ 156,404\\ 161,275\end{array}$		$24.94 \\ 25.67 \\ 26.05 \\ 26.28$
1892 1893 1894 1895 1896	65,500,000 68,850,000 68,200,000 69,550,000 70,900,000	$\begin{array}{c} 1171,407,343\\ 1220,751,874\\ 1073,361,797\\ 1075,371,462\\ 1150,169,376\end{array}$	$17.89 \\ 18.26 \\ 15.74 \\ 15.46 \\ 16.22$	$\begin{array}{r} 162,397\\ 169,780\\ 175,691\\ 177,746\\ 181,983 \end{array}$	$7213 \\ 7190 \\ 6109 \\ 6050 \\ 6320$	$\begin{array}{r} 26.19\\ 26.40\\ 26.20\\ 25.97\\ 25.78\end{array}$
1897 1898 1899 1900 1901	$\begin{array}{c} 72,350,000\\73,600,000\\74,950,000\\*76,295,220\\77,863,000\end{array}$	$\begin{array}{r} 1122,089,773\\1247,325,621\\1313,610,118\\1487,044,814\\1588,526,037\end{array}$	$15.53 \\ 16.95 \\ 17.53 \\ 19.49 \\ 20.47$	$183,284 \\184,648 \\187,535 \\192,556 \\195,562$	6122 6755 7005 7722 8123	$\begin{array}{r} 25.53 \\ 25.32 \\ 25.25 \\ 25.44 \\ 25.52 \end{array}$
1902 1903 1904 1905 1906	$\begin{array}{r} 79,431,000\\80,998,000\\82,566,000\\84,134,000\\85,701,000\end{array}$	$\begin{array}{r} 1726,380,267\\ 1900,846,907\\ 1975,174,091\\ 2082,482,406\\ 2325,765,167\\ \end{array}$	$21.88 \\ 23.70 \\ 24.23 \\ 25.15 \\ 27.65$	$\begin{array}{r} 200,155\\ 205,314\\ 212,243\\ 216,974\\ 222,340 \end{array}$	8625 9258 9306 9508 10460	$\begin{array}{r} 25.76 \\ 26.03 \\ 26.34 \\ 26.44 \\ 26.78 \end{array}$
1907 1908 1909 1910	87,279,000 88,837,000 90,405,000 *91,972,266	2589,105,578 2393,805,989 2418,677,538 2750,667,435	$\begin{array}{r} 29.63 \\ 26.95 \\ 26.71 \\ 29.91 \end{array}$	$\begin{array}{r} 227,455\\ 231,540\\ 234,800\\ 238,609 \end{array}$	11383 10338 10301 11528	26.3826.3026.2026.14

\* Actual. † Excludes a small percentage not reporting "gross receipts." ‡ Actual mileage.

The probable growth in traffic, after the traffic has once attained its normal volume, is a small but almost certain quantity. In the above tabular form this is indicated by the gradual growth in "receipts per head of population" from 1897 to 1907. Then the sudden drop due to the panic of 1907 is clearly indicated, and also the gradual growth in the last few years. Even in England, where the population has been nearly stationary for many years, the growth though small is unmistakable. On the other hand the growth in some of the Western States

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has been very large. For example, the gross earnings per head of population in the State of Iowa increased from \$1.42 in 1862 to \$10.00 in 1870, and to \$19.46 in 1884.

There will seldom be any justification in building to accommodate a larger business than what is "in sight." Even if it could be anticipated with certainty that a large increase in business would come in ten years, there are many reasons why it would be unwise to build on a scale larger than that required for the business to be immediately handled. Even though it may cost more in the future to provide the added accommodations (*e.g.* larger terminals, engine-houses, etc.), the extra expense will be nearly if not quite offset by the interest saved by avoiding the larger outlay for a period of years which may often prove much longer than was expected. A still more important reason is the avoidance of uselessly sinking money at a time when every cent may be needed to insure the success of the enterprise as a whole.

374. Probable number of trains per day. Increase with growth of traffic. The number of passenger trains per day cannot be determined by dividing the total number of passengers estimated to be carried per day by the capacity of the cars that can be hauled by one engine. There are many small railroads, running three or four passenger trains per day each way, which do not carry as many passengers all told as are carried on one heavy train of a trunk line. But because the bulk of the passenger traffic, especially on such light-traffic roads, is "unnecessary" traffic (see § 371) and must be encouraged and coaxed, the trains must be run much more frequently than mere capacity requires. The minimum number of passenger trains per day on even the lightest-traffic road should be two. These need not necessarily be passenger trains exclusively. They may be mixed trains.

The number required for freight service may be kept more nearly according to the actual tonnage to be moved. At least one local freight will be required, and this is apt to be considerably within the capacity of the engine. Some very light-traffic roads have little else than local freight to handle, and on such there is less chance of economical management. Roads with heavy traffic can load up each engine quite accurately according to its hauling capacity and the resulting economy is great. Fluctuations in traffic are readily allowed for by adding on or dropping off one or more trains. Passenger trains must be run on regular schedule, full or empty. Freight trains are run by train-despatcher's orders. A few freight trains per day may be run on a nominal schedule, but all others will be run as extras. The criterion for an increase in the number of passenger trains is impossible to define by set rules. Since it should always come before it is absolutely demanded by the train capacity being overtaxed, it may be said in general terms that a train should be added when it is believed that the consequent increase in facilities will cause an increase in traffic the value of which will equal or exceed the added expense of the extra train.

. 375. Effect on traffic of an increase in facilities. The term facilities here includes everything which facilitates the transport of articles from the door of the producer to the door of the consumer. As pointed out before, in many cases of freight transport, the reduction of facilities below a certain point will mean the entire loss of such traffic owing to local inability to successfully compete with more favored localities. Sometimes owing to a lack of facilities a railroad company feels compelled to pay the cartage or to make a corresponding reduction on what would normally be the freight rate. In competitive freight business such a method of procedure is a virtual necessity in order to retain even a respectable share of the business. Even though the railroad has no direct competitor, it must if possible enable its customers to meet their competitors on even terms. In passenger business the effect of facilities is perhaps even more marked. The pleasure travel will be largely cut down if not destroyed.

376. Loss caused by inconvenient terminals and by stations far removed from business centers. This is but a special case of the subject discussed just in the preceding paragraph. The competition once existing between the West Shore and the New York Central was hopeless for the West Shore from the start. The possession of a terminal at the Grand Central Station gave the New York Central an advantage over the West Shore with its inconvenient terminal at Weehawken which could not be compensated by any obtainable advantage by the West Shore. This is especially true of the passenger business. The through freight business passing through or terminating at New York is handled so generally by means of floats that the disadvantage in this respect is not so great. The enormous expenditure (roughly \$10,000,000) made by the Pennsylvania R. R., on the Broad Street Station (and its approaches) in Philadelphia, a large part of which was made in crossing the Schuylkill River and running to City Hall Square, rather than retain their terminal in West Philadelphia, is an illustration of the policy of a great road on such a question. The fact that the original plan and expenditure has been very largely increased since the first construction proves that the management has not only approved the original large outlay, but saw the wisdom of making a very large increase in the expenditure.

The construction of great terminals is comparatively infrequent and seldom concerns the majority of engineers. But an engineer has frequently to consider the question of the location of a way station with reference to the business center of the town. The following points may (or may not) have to be considered, and the real question consists in striking a proper balance between conflicting considerations.

(1) During the early history of a railroad enterprise it is especially needful to avoid or at least postpone all expenditures which are not demonstrably justifiable.

(2) The ideal place for a railroad station is a location immediately contiguous to the business center of the town. The location of the station even one fourth of a mile from this may result in a loss of business. Increase this distance to one mile and the loss is very serious. Increase it to five miles and the loss approaches 100%.

(3) The cost of the ideal location and the necessary right of way may be a very large sum of money for the new enterprise. On the other hand the increase in property values and in the general prosperity of the town, caused by the railroad itself, will so enhance the value of a more convenient location that its cost at some future time will generally be extravagant if not absolutely prohibitory. The original location is therefore under ordinary conditions a finality.

(4) To some extent the railroad will cause a movement of the business center toward it, especially in the establishment of new business, factories, etc., but the disadvantages caused to business already established is permanent.

(5) In any attempt to compute the loss resulting from a location at a given distance from the business center it must be

recognized that each problem is distinct in itself and that any change or growth in the business of the town changes the amount of this loss.

The argument for locating the station at some distance from the center of the town may be based on (a) the cost of right of way, thus involving the question of a large initial outlay, (b) the cost of very expensive construction (e.g. bridges), again involving a large initial outlay. (c) the avoidance of excessive grade into and out of the town. It sometimes happens that a railroad is following a line which would naturally cause it to pass at a considerable elevation above (rarely below) In this case there is to be considered not only the the town. possible greater initial cost, but the even more important increase in operating cost due to the introduction of a very heavy grade. To study such a case, compute the annual increase in operating expenses due to the additional grade, curvature, and distance; add to this the annual interest on the increased initial cost (if any) and compare this sum with the estimated annual loss due to the inconvenient location. The estimation of the increase in operating expenses is discussed in a subsequent chapter. The loss of business due to inconvenient location can only be guessed at. Wellington says that at a distance of one mile the loss would average 25%, with upper and lower limits of 10 and 40%, depending on the keepiness of the competition and other modifying circumstances. For each additional mile reduce 25% of the preceding value. While such estimates are grossly approximate, yet with the aid of sound judgment they are better than nothing and may be used to check gross errors.

377. General principles which should govern the expenditure of money for railroad purposes. It will be shown later that the elimination of grade, curvature, and distance have a positive money value; that the reduction of ruling grade is of far greater value; that the creation of facilities for the handling of a large traffic is of the highest importance and yet the added cost of these improvements is sometimes a large percentage of the cost of *some road* over which it would be physically possible to run trains between the termini.

The subsequent chapters will be largely devoted to a discussion of the value of these details, but the general principles governing the expenditure of money for such purposes may be stated as follows: 1. No money should be spent (beyond the unavoidable minimum) unless it may be shown that the addition is in itself a profitable investment. The additional sum may not wreck the enterprise and it may add something to the value of the road, but unless it adds more than the improvement costs it is not justifiable.

2. If it may be positively demonstrated that an improvement will be more valuable to the road than its cost, it should certainly be made even if the required capital is obtained with difficulty. This is all the more necessary if the neglect to do so will permanently hamper the road with an operating disadvantage which will only grow worse as the traffic increases.

3. This last principle has two exceptions: (a) the cost of the improvement may wreck the whole enterprise and cause a total loss to the original investors. For, unless the original promoters can build the road and operate it until its stock has a market value and the road is beyond immediate danger of a receivership, they are apt to lose the most if not all of their investment; (b) an improvement which is very costly although unquestionably wise may often be postponed by means of a cheap temporary construction. Cases in point are found at many of the changes of alignment of the Pennsylvania R. R., the N. Y., N. H. & H. R. R., and many others. While some of the cases indicate faulty original construction, at many of the places the original construction was wise, considering the then scanty traffic, and now the improvement is wise considering the great traffic.

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## CHAPTER XX.

### OPERATING EXPENSES.

378. Distribution of gross revenue. When a railroad comprises but one single property, owned and operated by itself, the distribution of the gross revenue is a comparatively simple matter. The operating expenses then absorb about two thirds of the gross revenue; the fixed charges (chiefly the interest on the bonds) require about 25 or 30% more, leaving perhaps 3 to 8% (more or less) available for dividends. The report on the Fitchburg R. R. for 1898 shows the following:

Operating expenses.	\$5,083,571	69.1%
Fixed charges	$1,\!567,\!640$	21.3%
Available for dividends, surplus, or per-		
manent improvements	708,259	9.6%
Total revenue	\$7,359,470	100.0%

But the financial statements of a large majority of the railroad corporations are by no means so simple. The great consolidations and reorganizations of recent years have been effected by an exceedingly complicated system of leases and sub-leases, purchases, "mergers," etc., whose forms are various. Railroads in their corporate capacity frequently own stocks and bonds of other corporations (railroad properties and otherwise) and receive, as part of their income, the dividends (or bond interest) from the investments.

In consequence of this complication, the U. S. Interstate Commerce Commission presents a "condensed income account" of which the following is a sample (1910):

Rail operations, operating revenues '' expenses	\$2,750,667,435 1,822,630,433
Net operating revenue Net revenue from outside operations	\$ 928,037,002 2,225,455
Total net revenue Taxes accrued	930,262,457 98,034,593
Operating income Other income (chiefly dividends and interest on	832,227,864
stocks and bonds owned)	252,219,946
Gross corporate income	\$1,084,447,810 454

Deductions from gross corporate income (chiefly in terest on funded debt, rents for lease of other roads and hire of equipment)	567,853,088
Net corporate income. Dividends\$283,411,828 Appropriations for additions, better- ments, new lines, and extensions. 55,061,675	\$ 516,594,722
Appropriations for other reserves 2,640,893	
Total	\$341,114,396
Balance to credit of profit and loss	175,480,326

In the above account an item of *income* (*e.g.*, lease of road) reported by one road will be reported as a "deduction from income" by the road which leases the other.

The above statement may be reduced to an income account of all the railways considered as one system. We then have

Operating revenues Clear income from investments	
Operating expenses\$1,822,630,433 Salaries and maintenance_of leased lines	2,829,109,462
Total	1,822,962,675
Net revenues and income.	1,006,146,787
Total	490,408,265
Available for dividends, adjustments and improve- ments	, ,
Available for adjustments and improvements	221,901,659

Of the balance "available for adjustments and improvements," part was spent in permanent improvements, part was advanced to cover deficits in the operation of weak lines, and more than half was left as "surplus," *i.e.*, working capital.

The percentages of the gross revenue which are devoted to operating expenses, fixed charges, and dividends are not *necessarily* an indication of creditable management or the reverse. Causes utterly beyond the control of the management, such as the local price of coal, may abnormally increase certain items of expense, while ruinous competition may cut down the gross revenue so that little or nothing is left for dividends. A favorable location will sometimes make a road prosperous in spite of bad management. On the other hand, the highest grade of skill will fail to keep some roads out of the hands of a receiver.

379. Fivefold distribution of operating expenses. The distribution of operating expenses here used is copied from the method of the Interstate Commerce Commission. The aim is to divide the expenses into groups which are as mutually independent and distinct as possible—although, as will be seen later, a change in one item of expense will variously affect other items.

Operating expenses.	1908.	1909.	1910.
Maintenance of way and structures Maintenance of equipment Traffic expenses Transportation expenses General expenses	$22.06 \\ 2.89 \\ 52.01$	$     \begin{array}{r}       19.29\% \\       22.75 \\       3.08 \\       50.90 \\       3.98 \\       100.00     \end{array} $	$   \begin{array}{r}     20.22\% \\     22.66 \\     3.07 \\     50.29 \\     3.76 \\     \hline     100.00   \end{array} $

The above percentages represent the averages given by the reports for the three years from 1908 to 1910 inclusive.

380. Operating expenses per train-mile. The reports of the U. S. Interstate Commerce Commission give the average cost per train-mile for every railroad in the United States. Although there are wide variations in these values, it is remarkable that the very large majority of roads give values which agree to within a small range, and that within this range are found not only the great trunk lines with their enormous train mileage, but also roads with very light traffic.

In the following tabular form is shown a statement taken from the reports for 1904 and for 1910 of ten of the longest railroads in the United States and, in comparison with them, a corresponding statement regarding ten more roads selected *at random*, except in the respect that each had a mileage less of than 100 miles. Although the extreme variations are greater, yet there is no very marked difference in the general values for operating expenses per train-mile, or in the ratio of expenses to earnings. The averages for the ten long roads agree fairly well with the averages for the whole country, but there would be no trouble (as is shown by some of the individual cases) in finding another group of ten short roads giving either greater or less average values than those given. And yet the tendency to uniform values, regardless of the mileage, is very striking. For comparison the figures for 1910 have been merely added to the figures for 1904, given in previous editions.

	Mile	eage.	Oper expens train-	ses per	Ratio expenses to earnings per cent.		
	1904.	1910.	1904.	1910.	1904.	1910.	
Whole United States	220,112	240,439	1.314	1.489	67.79	66.29	
Canadian Pacific C., B. & Q Chicago & Northwestern Southern Railway. C., R. I. & P Northern Pacific. A., T. & S. F. Great Northern Illinois Central. Atlantic Coast Line	$\begin{array}{c} & 8,332 \\ 8,326 \\ 7,412 \\ 7,197 \\ 6,761 \\ 5,619 \\ 5,031 \\ 4,489 \\ 4,374 \\ 4,229 \end{array}$	$9,040 \\ 7,629$	$\begin{array}{c} 1.320\\ 1.313\\ 1.136\\ 1.048\\ 1.199\\ 1.392\\ 1.305\\ 1.464\\ 1.107\\ 0.984 \end{array}$	$\begin{array}{c} 1.504\\ 1.710\\ 1.306\\ 1.234\\ 1.344\\ 1.824\\ 1.626\\ 1.808\\ 1.409\\ 1.213 \end{array}$	$\begin{array}{c} 64.35\\ 66.61\\ 70.30\\ 72.90\\ 52.26\\ 60.05\\ 49.72\\ 70.02\\ \end{array}$	$\begin{array}{c} 65.41\\ 71.71\\ 70.31\\ 67.43\\ 73.07\\ 61.71\\ 64.33\\ 60.53\\ 74.84\\ 62.44 \end{array}$	
Average of ten			1.227	1.498	63.39	67.18	
Montpelier & Wells River Somerset Railway Co.* Huntingdon & Broadtop	44 42 66	50 94 70	$1.169 \\ 0.802 \\ 0.950$	$1.430 \\ 1.314 \\ 2.052$	80.73 59.37	75.08 76.65 96.40	
Mountain Lehigh & New England Ligonier Valley Newburgh, Dutchess & Con-	96 11	$170 \\ 16$	$\begin{array}{c} 0.793 \\ 1.427 \end{array}$	$\begin{array}{c} 2.045\\ 1.480 \end{array}$	$69.80 \\ 69.33$	$\begin{array}{c} 62.84 \\ 49.15 \end{array}$	
necticut † Susquehanna & New York Detroit & Charlevoix Harriman & Northeastern * Galveston, Houston & Hen- derson	59 55 51 20 50	80 51 20 50	$\begin{array}{c} 0.922 \\ 1.368 \\ 1.424 \\ 2.162 \\ 1.556 \end{array}$	1.028 1.010 1.733 1.759	85.0978.4767.5279.2647.27	77.81 99.53 63.70 70.37	
Average of ten (or nine)			1.257	1.539	68.89	74.61	

OPERATING	EXPENSES	PER	TRAD	N-MILE	ON	LARGE	AND	SMALL
	ROA	ADS (	1904	AND 1	910)			

\* Subsidiary road since 1904.

† Merged since 1904; separate figures not available.

The fluctuations of the average cost per train-mile for several years past may be noted from the following tabular form:

Year.	Average cost per train-mile in cents.	Year.	Average cost per train-mile in cents.	Year.	Average cost per train-mile in cents.
1890	96.006	1897	92.918	1904	131.375
$\begin{array}{c} 1891 \\ 1892 \end{array}$	95.707 96.580	$     1898 \\     1899 $	$95.635 \\ 98.390$	1905 1906	$132.140 \\ 137.060$
$1893 \\ 1894$	$97.272 \\ 93.478$	1900 1901	$107.288 \\ 112.292$	1907 1908	$146.993 \\ 147.340$
$1895 \\ 1896$	$91.829 \\ 93.838$	1902 1903	$117.960 \\ 126.604$	1909 1910	$143.370 \\ 148.865$
1000	55.000	1000	120.001	1010	110.000

The enforced economies after the panic of 1893 are well shown. The reduction generally took the form of a lowering of the standards of maintenance of way and of maintenance of equipment. The marked advance since 1895 is partly due to the necessity for restoring the roads to proper condition, replenishing worn-out equipment and providing additional equipment to handle the greatly increased volume of business. The recent advance is chiefly due to the increase in wages and the generally increased cost of supplies.

In looking over the list, it may be noted that the cases where the operating expenses per train-mile and the ratio of expenses to earnings vary very greatly from the average are almost invariably those of the very small roads or of "junction roads" where the operating conditions are abnormal. For example, one little road, with a total length of 13 miles and total annual operating expenses of \$5342, spent but 22<sup>1</sup>/<sub>c</sub>, per train-mile, which precisely exhausted its earnings. This precise equality of earnings and expenses suggests jugglery in the bookkeeping. As another abnormal case, a road 44 miles long spent \$3.81 per train-mile, which was nearly *fourteen* times its earnings. In another case a road 13 miles long earned \$7.76 per train-mile and spent \$6.03 (78%) on operating expenses, but the fixed charges were abnormal and the earnings were less than half the sum of the operating expenses and fixed charges. The normal case, even for the small road, is that the cost per train-mile and the ratio of operating expenses to earnings will agree fairly well with the average, and when there is a marked difference it is generally due to some abnormal conditions of expenses or of earning capacity.

381. Reasons for uniformity in expenses per train-mile. The chief reason is that, although on the heavy-traffic road everything is kept up on a finer scale, better roadbed, heavier rails, better rolling stock, more employees, better buildings, stations, and terminals, etc., yet the number of trains is so much greater that the divisor is just enough larger to make the average

cost about constant. This is but a general statement of a fact which will be discussed in detail under the different items of expense.

382. Detailed classification of expenses with ratios to the total expense. The Interstate Commerce Commission now publishes each year a classification with detailed summation for the cost of each item. These summations are made up from reports furnished by railroads which have (in the reports recently made) represented over 99% of the total traffic handled. In the annexed tabular form (Table XX) are shown the percentages which each item bears to the total. The railroads have been divided into two classes, "large" and "small," as indicated below. Large roads report on 116 items which are combined and condensed with 44 items for small roads.

"Large roads" are those with mileage greater than 250 miles, or those with operating revenues greater than \$1,000,000. Roads subsidiary to "large roads" are also included in this class.

"Small roads" are those with mileage less than 250 miles and also with operating revenues less than \$1,000,000.

383. Amounts and percentages of the various items. The I. C. C. report for the year ending June 30, 1909, was the first to include the distribution of expenses according to the present classification. The items as given are reliable and may be utilized, as far as any such computations are to be depended on, in estimating future expenses. The chief purpose of this discussion is to point out those elements of the cost of operating trains which may be affected by such changes of location as an engineer is able to make. There are some items of expense with which the engineer has not the slightest concern, nor will they be altered by any change in alignment or constructive detail which he may make. In the following discussion such items will be passed over with a brief discussion of the sub-items included.

## MAINTENANCE OF WAY AND STRUCTURES.

384. Items 2 to 5. Track material. The relative cost of ballast, ties, rails and other track material, as shown by comparing either the gross amounts or the percentages in Table IX.

is suggestive and instructive. The fact that ties cost considerably more than all other track material combined shows the importance of any possible saving in tie renewals. It is also significant that the relative importance of ties has increased in the last few years, and that the relative increase has not been due to a reduction in the cost of other track material. Apparently the lengthening of the average life of ties, due to preservative processes, the use of tie-plates, and greater care to avoid the premature withdrawal from the track of ties which are still serviceable, has not kept pace with the increase in the average cost per tie. The cost of Bessemer rails per ton has remained almost constant for several years, but the adoption of heavier rails by many roads, necessitated by heavier rolling stock, and also the adoption of open-hearth steel costing about \$2 per ton more for much of the tonnage, have been potent causes in increasing the cost of maintenance.

385. Item 6. Roadway and track. This item is three-eighths of the total cost of maintenance of way and structures. It consists chiefly of the wages of trackmen. There has been an almost steady increase in the daily wages of section foremen and other trackmen since 1900, as shown below:

	1900	1901	1902	1903	1904	1905	1906	1907	1908	1909	1910
Section foremen Other trackmen	$\begin{array}{c} 1.68 \\ 1.22 \end{array}$	$\begin{array}{c} 1.71 \\ 1.23 \end{array}$	1.72 1.25	$\begin{array}{c} 1.78\\ 1.31 \end{array}$	$1.78 \\ 1.33$	$1.79 \\ 1.32$	$\frac{1.80}{1.36}$	1.90 1.46	$1.95 \\ 1.45$	$\begin{array}{c} 1.96 \\ 1.38 \end{array}$	1.99 1.47
No. of trackmen per 100 miles	118	122	140	147	136	143	155	162	130	136	157

The average number of section foremen per 100 miles of line has remained almost constant at 18. Although there have been fluctuations in the number of "other trackmen" required per 100 miles of line, there has been in general a very substantial increase. These two causes combined (increased number and increased wages) have had a great influence in producing the regular and steady increase in the average cost of a train-mile, as shown in § 380. The variations in average daily wages in the various Groups for 1910 are shown herewith:

AVERAGE WAGES OF TRACKMEN IN THE SEVERAL GROUPS.

	Ι.	II.	III.	IV.	v.	VI.	VII.	VIII	IX.	x.	U.S.
Section foremen Other trackmen	$2.38 \\ 1.65$	$2.08 \\ 1.52$	$1.99 \\ 1.57$	$\begin{array}{c} 1.77\\ 1.21 \end{array}$	$\begin{array}{c} 1.83 \\ 1.13 \end{array}$	$1.90 \\ 1.56$	$\begin{array}{c} 2.22 \\ 1.60 \end{array}$	$\begin{array}{c} 1.83\\ 1.37\end{array}$	$1.88 \\ 1.26$	$2.51 \\ 1.52$	1.99 1.47

The classification of expenses for "small roads" combine items 2 to 7. It should be noted that this item (see Table XX A) is over three-fourths of the total for that division, and also that the cost of maintenance of way and structures for "small roads" is nearly 26% of the total operating expenses and that it is about 20% for "large roads." In 1908 and 1909, this difference was even more marked, and the fact should not be neglected when considering the economics of a project which will evidently be, at least for many years, a "small road."

386. Items 8 to 15. Maintenance of track structures. As a matter of economics, the locating engineer has little or no concern with the cost of maintaining track structures. If he is comparing two proposed routes it would be seldom that they would be so different that he would be justified in attempting to compute a train-mile difference in cost of operation, based on differences in these items. Of course, one proposed line might call for one or more tunnels which the alternate line might not have, and the annual cost of maintaining the tunnels would increase the cost of operation. Such a case would justify special consideration. So far as the maintenance of small bridges and culverts are concerned it would usually be sufficiently accurate to consider that a proposed change of line, involving perhaps several miles of road, would require substantially the same number of bridges and culverts, and therefore that the cost of maintaining them would be the same by either line. The error involved in such an assumption would usually be insignificant, unless there was a very large and material difference in the two lines in this respect. Under such conditions special computations should be made. The items total less than 3% for small roads and still less for large roads.

387. Items 16 to 21. The other items of maintenance of way and structures are very small, except No. 16, and under ordinary conditions will not be affected by any changes which the locating engineer may make, except as noted in the chapter on Distance.

#### MAINTENANCE OF EQUIPMENT.

388. Item 24. Superintendence of Equipment. The item averages about two-thirds of one per cent and has so little fluctuation under ordinary conditions that it may almost be considered as a fixed charge. It includes those fixed charges in superintendence which do not fluctuate with small variations in business done. It includes the salaries of superintendent of motive power, master mechanic, master car-builder, foreman, etc., but does not include that of road foreman of engines nor enginemen. Although the item will vary with the general scale of business on the road, it does not fluctuate with it and hence will not usually be influenced by any small changes in alinement which the engineer may be considering.

389. Items 25 to 27. Repairs, renewals, and depreciation of steam locomotives. This subject will be treated at greater length in Chapter XXI, Distance. The item is <sup>4</sup> of interest to the locating engineer because he must appreciate the effect on locomotive repairs and renewals of an addition to distance. A large part of the repairs of locomotives are due to the wear of wheels, which is largely caused by curvature. Therefore the value of any reduction of curvature is a matter of importance, and this will be considered in Chapter XXII. A considerable portion of the deterioration of a locomotive is due to grade, and the economic advantages of reductions of grade will be considered in Chapter XXIII.

This item includes the expenses of work whose effect is supposed to last for an indefinite period. It does not include the expense of cleaning out boilers, packing cylinders, etc., which occurs regularly and which is charged to items 72 or 81. It does include all current repairs, general overhauling, and even the replacement of old and worn-out locomotives by new ones to the extent of keeping up the original standard and number. Of course additions beyond this should be considered as so much increase in the original capital investment. As a locomotive becomes older the annual repair charge becomes a larger percentage on the first cost, and it may become as much as onefourth and even one-third of the first cost. When a locomotive is in this condition it is usually consigned to the scrap-pile; the annual cost for maintenance becomes too large an item for its annual mileage. The effect on expenses of increasing the weight of engines is too complicated a problem to be solved accurately, but certain elements of it may be readily computed. While the cost of repairs is greater for the heavier engines, the increase is only about one-half as fast as the increase in weight-some of the subitems not being increased at all.

390. Items 28 to 30. Repairs, renewals, and depreciation of electric locomotives. The use of electric locomotives as an adjunct to steam railroad service applies to only a small percentage of the roads of the country at present, but the general principles stated in the previous article will apply to these items.

391. Items 31 to 36. Repairs, renewals, and depreciation of passenger-train cars and of freight-cars. Many of the economic features of car construction, especially the effect of modern improvements, such as friction draft-gear, automatic couplers. and air-brakes, have been considered in Chapter XV. Such figures will be utilized in considering the effect on car repairs of additional distance, of variations in curvature, and of grade as discussed later. Although the published figures for these items since 1908 are on a slightly different basis from those published previously, it is evident that these items with respect to passenger-cars have remained fairly constant, while those for freight-cars have substantially increased, not only in gross amount but even in percentage to the total. The fluctuations of these items are largely due to accidents rather than to any line of policy under the control of the engineer. It should be understood that for these items, as well as the previous item, the renewal of rolling stock generally means the construction of higher-grade locomotives and higher-grade cars. When this is done the difference in cost between the higher-grade, and probably more expensive, construction and the former cheap construction should be considered as an addition to the capital account rather than a charge against operating expenses. The enormous increase in the movement of freight during the last few years has required a corresponding increase in freight-car equipment. Some roads have been charging up the full cost of the renewing of their old-fashioned light-weight equipment with more expensive equipment under the head of operating expenses. and it is quite possible that a portion of the increase in these items is due to this policy.

392. Items 37 to 52. Electric equipment; floating equipment; work equipment; shop machinery and tools; power-plant equipment; miscellaneous items. The location of the road along the line has no connection with the maintenance of marine equipment. The maintenance of shop machinery and tools can only be affected as the work of repairs of rolling stock fluctuates, and of course in a much smaller ratio. No change which an engineer can effect will have any appreciable influence on this item.

The other items are too small and have too little connection with location to be here discussed, except as it may be considered that they vary with train-mileage, which an engineer may influence (see Chapter XXIII, Grades).

#### TRAFFIC.

393. Items 53 to 60. These items have exclusive reference to the work of securing business for the road and have no necessary relation to any questions which the locating engineer must answer.

#### TRANSPORTATION.

394. Items 61 to 70. These items cover the superintendence of transportation and many of the yard and station expenses.

They require over one-eighth of the entire operating expenses. Although some of them might be somewhat affected by the details of the design of a yard, they are practically unaffected by any changes of alinement which an engineer may make.

395. Items 71 to 76. Yard-engine expenses. By comparing these items with the corresponding items (80 to 85) for road engines, it may be seen that the total expenses assignable to yard engines are about 20% of those road of engines; the relative fuel charge for 1910 was 15.3%. The number of switching locomotives in the United States in 1910 was 9115 or 15.4% of the total number, 58,947. The relative charge for wages of enginemen was 25.7%. This higher proportionate charge is probably due to the fact that the wages for yard enginemen must necessarily be on a per diem basis, but the wages of road enginemen are generally on a mileage basis, as explained later. On the other hand, the mileage of a yard engine is usually comparatively low, and the coal consumed will be correspondingly, although not proportionately, low. It must also be remembered that these figures are exclusive of the work and equipment of switching and terminal companies.

396. Item 80. Road enginemen. This item requires 6% of the total operating expenses. The enginemen are usually paid on a mileage basis, or by the trip, except on very small railroads.

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On very short roads, where a train crew may make two, three, or even four complete round trips per day, they may readily be paid by the day, so many round trips being considered as a day's work, but on roads of great length, where all trains, and especially freight-trains, are run day and night, weekday and Sunday, all trainmen are necessarily paid by the trip or, as it is more usually expressed, by the "run." It is generally found convenient to divide the road into "divisions" which are approximately 100 miles in length. According as the division is greater or less than 100 miles, it is designated as a  $1\frac{1}{8}$  run,  $1\frac{1}{4}$  run, or perhaps  $\frac{7}{8}$  run. The enginemen will then be paid according to the number of runs made per month. There is a considerable fluctuation in the average wages paid in different sections of the United States, as is shown by the tabular form given below, in which the "groups" refer to the sections into which the country has been divided by the Interstate Commerce Commission. This tabular form may be of some assistance in showing the average daily compensation which must be allowed for in the various sections of the country:

AVERAGE DAILY COMPENSATION BY GROUPS-1910.

	I.	11.	111.	IV.	v.	VI.	VII.	VIII	IX.	x.	U.S.
Enginemen Firemen	\$ 3.97 2.35	\$ 4.53 2.75	\$ 4.34 2.57	\$ 4.34 2.16	\$ 4.81 2.42	\$ 4.58 2.84	\$ 4.72 3.14	\$ 4.75 3.13	\$ 4.87 3.03	\$ 4.84 3.04	\$ 4.55 2.74

The increase in the average wages paid to enginemen and firemen during eleven years is plainly shown by the following figures:

INCREASE IN DAILY WAGES, FROM 1900 TO 1910.

	8	\$	\$	-	e .	•	•			1909 \$	
Enginemen Firemen	$\begin{vmatrix} 3.75 \\ 2.14 \end{vmatrix}$	$3.78 \\ 2.16$	$3.84 \\ 2.20$	$\begin{array}{c} 4.01 \\ 2.28 \end{array}$	$4.10 \\ 2.35$	$\begin{array}{c} 4.12 \\ 2.38 \end{array}$	$\begin{array}{c} 4.12\\ 2.42\end{array}$	$4.30 \\ 2.54$	$4.45 \\ 2.64$	$4.44 \\ 2.67$	$4.55 \\ 2.74$

The fluctuations of this item are of importance to the locating engineer in discussing the economics of differences in distance. This feature will be more fully discussed in Chapter XXI.

307. Item 82. Fuel for road locomotives. This item includes every subitem of the entire cost of the fuel until it is placed in the engine-tender. The cost therefore includes not only the first cost at the point of delivery to the road, but also the expense of hauling it over the road from the point of delivery to the various coaling-stations and the cost of operating the coal-pockets from which it is loaded on to the tenders. Even though the cost may be fairly regular for any one road, the cost for different roads is exceedingly variable. There has been an almost steady increase in the percentage of the cost of this item per train-mile since 1897. Items 73 and 82 amounted to nearly 12% of the total operating expenses in 1910, and required an actual expenditure of nearly \$213,000,000. It is the largest item in the whole cost of railroad operation. Although some roads, which traverse coal-regions and perhaps actually own the coal-mines, are able to obtain their coal for a cost which may be charged up as \$1 per ton or less, there are many roads which are far removed from coal-fields which have to pay \$3 or \$4 per ton, on account of the excessive distance over which the coal must be hauled. Unfortunately the figures published by the Interstate Commerce Commission do not show the variations in the percentage of this item in the different groups. In the succeeding chapters will be shown the effect on fuel consumption of the several variations on location details. The great importance of this item requires that it shall be thoroughly understood and studied by the engineer. It will be shown, contrary to the commonly received opinion, that the fuel consumption is quite largely independent of distance and even of the number of cars hauled.

398. Items 83 to 95. Water, lubricants, and other supplies for road locomotives. These items aggregate about 1.3% of the operating expenses. There seems to be slight tendency for the percentage to increase. Since the consumption of all these supplies will vary nearly as the engine mileage, the engineer is concerned with them directly to the extent to which he may change the engine mileage.

399. Item 88. Road trainmen. This item includes the wages of conductors and "other trainmen." As in the case of all other employees, the average daily wages have advanced since 1900 as shown below: AVERAGE DAILY WAGES OF CONDUCTORS AND OTHER TRAINMEN, 1900 TO 1910.

	1900	1901	1902	1903	1904	1905	1906	1907	1908	1909	1910
Conductors Other trainmen	\$ 3.17 1.96	\$ 3.17 2.00	\$ 3.21 2.04	\$ 3.38 2.17	\$ 3.50 2.27	\$ 3.50 2.31	\$ 3.51 2.35	\$ 3.69 2.54	\$ 3.81 2.60	\$ 3.81 2.59	\$ 3.91 2.69

The following form shows the variation in the daily wages of conductors and trainmen in the several groups for 1910:

AVERAGE DAILY WAGES IN 1910 IN THE SEVERAL GROUPS.

	I.	II.	III.	IV.	v.	VI.	VII.	VIII	IX.	X.	U.S.
Conductors Other trainmen	\$ 3.52 2.49	\$ 3.74 2.71	\$ 3.73 2.72	\$ 3.38 1.89	\$ 3.79 2.18	\$ 4.12 2.81	\$ 4.16 2.86	\$ 4.38 2.84	\$ 4.59 3.00	\$ 4.38 3.04	\$ 3.91 2.69

These figures are of vital importance from an economic standpoint, since they show a constant tendency to increase and thereby raise the average cost of a train mile. And as there is no present indication of any limit to this increase, all economic calculations which attempt to predict future expenses, even for a few years in advance, must allow for these and other increased expenses.

400. Item 89. Train supplies and expenses. These items, which average about 1.8%, include the large list of consumable supplies such as lubricating oil, illuminating-oil or gas, ice, fuel for heating, cleaning materials, etc., which are used on the cars and not on the locomotives. The consumption of some of these articles is chiefly a matter of time. In other cases it is a function of mileage. The effect of changes which an engineer may make on this item will be considered when estimating the effect of the changes.

401. Items 93, 99 to 103. Clearing wrecks, loss, damage and injuries to persons and property. These expenses are fortuitous and bear no absolute relation either to the number of miles of road or the number of train-miles. While they depend largely on the standards of discipline on the road, even the best of roads have to pay some small proportion of their earnings to these items. While we might expect that a road with heavy traffic would have a larger proportion of train accidents than a road of light traffic, it is usually true that on the heavy-traffic roads the precautions taken are such that they are usually freer from accidents than the light-traffic roads. During recent years there has been a very perceptible increase in the percentages of these items, particularly in the compensations paid for "injuries to persons." The increase in this item coincides with the increase already noted in the number of passengers killed during recent years. The possible relation between curvature and accidents has already been discussed, but otherwise the locating engineer has no concern with these items.

402. Items 104, 105. Operating joint tracks and facilities, Dr. and Cr. A large part of these debit and credit charges are those for car per diem and mileage charges. This is a charge paid by one road to another for the use of cars, which are chiefly freight-cars. To save the rehandling of freight at junctions, the policy of running freight-cars from one road to another is very extensively adopted. Since the foreign road receives its mileage proportion of the freight charge, it justly pays to the road owning the car at a rate which is supposed to represent the value of the use of the freight-car for the number of miles traveled. The foreign road then loads up the freight-car with freight consigned to some point on the home road and sends it back, paying mileage for the distance traveled on the foreign road, a proportional freight charge having been received for that service. All of these movements of freight-cars are reported to a car association, which, by a clearing-house arrangement, settles the debit and credit accounts of the various roads with each other. Such is the simple theory. In practice the cars are not sent back to the home road at once, but wander off according to the local demand. As long as a strict account is kept of the movements of every car, and as long as the home road is paid the charge which really covers the value of lost service, no harm is done to the home road, except that sometimes, when business has suddenly increased, the home road cannot get enough cars to handle its own business. The value of the car is then abnormally above its ordinary value, and the home road suffers for lack of the rolling stock which belongs to it. Formerly such charges were paid strictly according to the mileage. This developed the intolerable condition that loaded cars would be

run onto a siding and left there for several days, simply because it was not convenient to the consignee to unload the car immediately. On the mileage basis the car would be earning nothing. and, since the road on which the car then was had no particular interest in the car, the car was allowed to stand to suit the convenience of the consignee. To correct this evil a system of per diem charges has been developed, so that a railroad has to pay a per diem charge for every foreign car on its lines. To reduce this charge as much as possible the railroads compel consignees. under penalty of heavy demurrage charges, to unload cars promptly. The running of freight-cars on foreign lines is now settled almost exclusively on the per diem basis, but the earning of passenger-cars over other lines, as is done on account of the advantages of through-car service, as well as the running of Pullmans and other special cars, is still paid for on the mileage basis. To the extent to which this charge is settled on the mileage basis, any change in distance which the engineer may be able to effect in the length of the road will have its influence on this item, but when the freight-car business, which comprises by far the larger part of the running of cars over foreign lines, is settled on the per diem basis no changes in alinement which the engineer may make will affect the item appreciably.

Switching Charges. Where two or more railroads intersect there will be a considerable amount of shifting of cars, chiefly freight-cars, from one road to the other. This shifting at any one junction may be done entirely by the engines of one road or perhaps by those of both roads. A portion of the expense of this work is charged up against the other road by the road which does the work. The total amount of this work is carefully accounted for by a clearing-house arrangement, and the balance is charged up against the road which has done the least work. The item is very small, is fairly uniform year by year, and is seldom, if ever, affected by changes of alinement.

Other Items. All of the remaining items, as stated in Table IX, are of no concern to the locating engineer. They are either general expenses, such as the salaries of general officers, insurance or law expenses, or are special items, such as advertising or the operation of marine equipment which will not be changed by any variations in distance, curvature, or grades which a locating engineer may make. There is therefore no need for their further discussion here.

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# RAILROAD CONSTRUCTION.

TABLE XX.—SUMMARY SHOWING CLASSIFICATION OF OPERATING EXPENSES FOR THE YEAR ENDING JUNE 30, 1910, AND PRO-PORTION OF EACH CLASS TO THE TOTAL.—LARGE ROADS.

	Operating expenses.	Amount.	Per cent
	MAINTENANCE OF WAY AND STRUCTURES.		
1	Superintendence of way and structures	\$17,058,473	0.957
$\hat{2}$	Ballast.	8,861,334	0.497
3	Ties	55,259,585	3.099
4	Rails	16,435,349	0.922
5	Other track material	20,225,436	1.134
6	Roadway and track Removal of snow, sand, and ice	134,275,440	7.531
7 8	Tuppels	8,297,715 1,147,140	0.465
ŝ	Tunnels         Bridges, trestles, and culverts	30,471,313	1.709
10	Over and under grade crossings	1,086,702	0.061
ĩĭ	Grade crossings, fences, cattle guards, and signs.	6,105,192	0.343
12	Snow and sand fences and snowsheds	385,730	0.022
13	Signals and interlocking plants	8,175,641	0.459
14	Telegraph and telephone lines	3,407,627 367,400	0.191
15	Electric power transmission Buildings, fixtures, and grounds	367,400 32,181,561	$ \begin{array}{c} 0.021 \\ 1.805 \end{array} $
$\frac{16}{17}$	Docks and wharves	3,537,331	0.198
18	Docks and wharves Roadway tools and supplies	5,141,983	0.288
19	Injuries to persons	1,886,865	0.106
20	Stationery and printing	714.637	0.040
21	Other expenses Maintn'g joint tracks, yds., and other facilities, Dr.	333,056	0.018
<b>22</b>	Maintn'g joint tracks, yds., and other facilities, Dr.	12,151,280	0.681
23	Maintn'g joint tracks, yds., and other facilities, Cr.	9,241,467	0.518
-	Total maintenance of way and structures	\$358,265,293	20.093
1	MAINTENANCE OF EQUIPMENT.		
24	Superintendence of equipment	\$11,457,025	0.643
25	Steam locomotives—repairs Steam locomotives—renewals	138,548,039	7.770 0.184
$\frac{26}{27}$	Steam locomotives—renewals	3,272,370 11,755,130	0.184
28	Electric locomotives—repairs	217,182	0.039
29	Electric locomotives—renewals	211,102	0.012
30 ·	Electric locomotives-depreciation	22,341	0.001
31	Passenger-train cars-repairs	30,695,229	1.721
32	Passenger-train cars-renewals	1,608,124	0.090
33	Passenger-train cars—depreciation	5,827,607	0.327
34	Freight-train cars—repairs.	137,846,373	7.731
35 36	Freight-train cars—renewals Freight-train cars—depreciation	12,423,890 30,712,546	1.722
37 37	Electric equipment of cars—repairs	161,624	0.009
38	Electric equipment of cars—renewals	27,000	0.002
39	Electric equipment of cars—renewals Electric equipment of cars—depreciation	42,996	0.003
40	Floating equipment—repairs	924,976	0.052
41	Floating equipment—renewals Floating equipment—depreciation	48,144	0.003
42	Floating equipment—depreciation	381,129	0.021
43 44	Work equipment—repairs	$4,461,503 \\754,536$	$0.250 \\ 0.042$
44 45	Work equipment—renewals Work equipment—depreciation	899,128	0.042
46	Shop machinery and tools	9,439,056	0.529
47	Power plant equipment	167.182	0.010
<b>4</b> 8	Injuries to persons	$\begin{array}{r}1,370,388\\978,744\end{array}$	0.077
<b>1</b> 9	Stationery and printing	978,744	0.055
50	Other expenses Maintaining joint equipment at terminals Dr	841,019	0.047
$51 \\ 52$	Maintaining joint equipment at terminals Dr Maintaining joint equipment at terminals, Cr	$1,392,411 \\ 840,895$	$0.078 \\ 0.047$
	Total maintenance of equipment		22.738

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# OPERATING EXPENSES.

# TABLE XX.-(Continued.)

	Operating expenses.	Amount.	Per cent
	TRAFFIC.		
53	Superintendence of traffic	\$13,960,333	0.783
54	Outside agencies	19,592,049	1.099
55	Advertising	8,347,914	0.468
56	Traffic associations	1,519,215	0.085
57	Fast freight lines	3,984,644	0.224
58	Industrial and immigration bureaus	931,212	0.052
$\frac{59}{60}$	Stationery and printing Other expenses	$6,476,861 \\ 120,052$	0.363
00		·	
	Total traffic expenses	\$54,932,280	3.081
	TRANSPORTATION.		
61	Superintendence of transportation	21,365,630	1.198
62	Dispatching trains	16,250,243 123,062,288	$ \begin{array}{c} 0.911 \\ 6.902 \end{array} $
63 64	Station employees Weighing and car-service associations	2,389,673	0.134
65	Coal and ore docks	2,542,882	0.143
66	Station supplies and expenses.	10,302,118	0.578
67	Yardmasters and their clerks	14,563,707	0.817
68	Yard conductors and brakemen	48,211,995	2.704
69	Yard switch and signal tenders	3,888,708	0.218
70	Yard supplies and expenses	1,249,844 27,890,126	0.070
71 72	Yard enginemen.	8,106,787	1.564 0.454
73	Enginehouse expenses—yard Fuel for yard locomotives	28,306,698	1.587
74	Water for vard locomotives	1,754,359	0.098
75	Lubricants for yard locomotives	576,693	0.032
76	Lubricants for yard locomotives Other supplies for yard locomotives	644,336	0.036
77	Operating joint yards and terminals—Dr Operating joint yards and terminals—Cr	20,875,654	1.171
78 79	Operating joint yards and terminals—Cr	12,998,087 477,404	0.727
80	Motormen	108,471,661	6.083
81	Road enginemen Enginehouse expenses—road	30,580,907	1.715
82	Fuel for road locomotives	184,588,622	10.352
83	Water for road locomotives	11,624,756	0.652
84	Lubricants for road locomotives	3,573,631	0.200
85	Other supplies for road locomotives	$3,708,286 \\726,742$	$0.208 \\ 0.041$
86 87	Operating power plants Purchased power	413,783	0.023
88	Road trainmen	114.122.534	6.400
89	Train supplies and expenses	31,795,761	1.783
90	Road trainmen Train supplies and expenses Interlockers & block & other signals—operation.	8,718,693	0.490
91	Crossing flagmen and gatemen	6,319,183	0.354
92 •93	Drawbridge operation	$897,495 \\ 4,488,082$	$0.050 \\ 0.252$
93	Clearing wrecks	5,820,358	0.326
95	Telegraph and telephone—operation Operating floating equipment	2,876,653	0.161
96	Express service	597	*
97	Stationery and printing	8,113,694	0.455
98	Other expenses	2,060,571	0.117
100	Loss and damage—freight Loss and damage—baggage	$21,756,671 \\ 360,244$	$1.220 \\ 0.020$
100 101	Demage to property	4,791,32 <b>4</b>	0.020 0.269
101	Damage to property Damage to stock on right of way	3,650,544	0.205 0.206
103	Injuries to persons	20,139,285	1.129
104	Operating joint tracks and facilities-Dr	4,625,115	0.259
105	Injuries to persons Operating joint tracks and facilities—Dr Operating joint track and facilitiess—Cr	4,357,256	0.244
	Total transportation expenses	\$899,328,994	50.438

\* Less than 0.0001 per cent.

#### RAILROAD CONSTRUCTION.

## TABLE XX.—(Continued.)

	Operating expenses.	Amount.	Per cent
	GENERAL.		
106	Salaries and expenses of general officers	\$9,206,835	0.516
107	Salaries and expenses of clerks and attendants	25,167,569	1.411
108	General office supplies and expenses	3,295,407	0.185
109	Law expenses	10,845,738	0.608
110	Insurance	7,551,789	0.424
111	Relief department expenses	680,843	0.038
112	Pensions	2,007,818	0.113
113	Stationery and printing	2,853,808	0.160
114	Other expenses	3,006,289	0.169
115 116	General administration, joint tracks, yards, and terminals—Dr General administration, joint tracks, yards,	655,875	0.037
	and terminals—Cr	192,378	0.011
	Total general expenses	\$65,079,593	3.650
	Recapitulation of expenses:		
	I. Maintenance of way and structures	\$358,265,293	20.093
	II. Maintenance of equipment	405,434,797	22.738
	III. Traffic expenses		3.081
	IV. Transportation expenses	899,328,994	50.438
	V. General expenses.	65,079,593	3.650
	Total operating expenses	\$1,783,040,957	100.000

The "Credit items" 23, 52, 78, 105, and 116 represent receipts from other roads, from switching and terminal companies (which are not included in this or the following table) or from other sources. The amounts and percentages must be deducted from the other expenses to obtain the net expenses.

# TABLE XX*a*.—SUMMARY SHOWING CLASSIFICATION OF OPERATING EXPENSES FOR THE YEAR ENDING JUNE 30, 1910, AND PRO-PORTION OF EACH CLASS TO THE TOTAL.—SMALL ROADS.

	Operating expenses.	Per cent	Correspond- ing items in Table XX.
1 2 3 4 5 6 7 8	I. MAINTENANCE OF WAY AND STRUCTURES Superintendence of way and structures Maintenance of roadway and track Maintenance of buildings, docks, and wharves. Injuries to persons Other maintenance of way & structures expenses Maintaining joint tracks, yards, and other fa- cilities—Dr Maintaining joint tracks, yards, and other fa- cilities—Cr Total, maintenance of way and structures.	0.469	1 2-7 8-15 16, 17 19 18, 20, 21 22 23

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TABLE XXa.—SUMMARY SHOWING CLASSIFICATION OF OPERATING EXPENSES FOR THE YEAR ENDING JUNE 30, 1910, AND PRO-PORTION OF EACH CLASS TO THE TOTAL.—SMALL ROADS.— (Continued.)

	· · · · · · · · · · · · · · · · · · ·		
<u>.</u>	Operating expenses.	Per cent.	Correspond- ing items in Table XX.
9 10 11 12 13 14 15 16 17 18 19	II. MAINTENANCE OF EQUIPMENT. Superintendence of equipment Locomotives—repairs Cars—repairs Floating equipment—repairs. Work equipment—repairs. Equipment—renewals Equipment—depreciation Injuries to persons Other maintenance of equipment expenses Maintaining joint equipment at terminals—Dr. Maintaining joint equipment at terminals—Cr. Total, maintenance of equipment	$\begin{array}{c} 0.025 \\ 0.785 \\ 0.026 \\ 0.063 \end{array}$	$\begin{array}{r} 24 \\ 25, 28 \\ 31, 34, 37 \\ 40 \\ 43 \\ 26, 29, 32, 35, \\ 38, 41, 44 \\ 27, 30, 33, 36, \\ 39, 42, 45 \\ 46, 47, 49, 50 \\ 51 \\ 52 \\ \end{array}$
	III. TRAFFIC EXPENSES.	19.508	
20	Traffic expenses	2.418	53-60
	IV. TRANSPORTATION EXPENSES.		
$\begin{array}{c} 21\\ 22\\ 23\\ 24\\ 25\\ 26\\ 27\\ 29\\ 30\\ 31\\ 32\\ 33\\ 45\\ 36\\ 37\\ 39\\ \end{array}$	Superintendence and dispatching trains. Station service. Yard euginemen. Other yard employees. Fuel for yard locomotives. All other yard expenses. Operating joint yards and terminals—Dr. Operating joint yards and terminals—Cr. Road enginemen and motormen. Fuel for road locomotive supplies and expenses. Other road locomotive supplies and expenses. Injuries to persons. Loss and damage. Other transportation expenses. All other transportation expenses. Operating joint tracks and facilities—Dr. Operating joint tracks and facilities—Cr.	$\begin{array}{c} 2.200\\ 6.185\\ 0.823\\ 1.259\\ 1.276\\ 0.743\\ \dots\\ 5.977\\ 11.184\\ 2.850\\ 6.313\\ 0.936\\ 0.619\\ 0.471\\ 0.616\\ 1.916\\ 0.481\\ 0.135\\ \hline 43.472 \end{array}$	
40 41 42 43 44	V. GENERAL EXPENSES. Administration Insurance. Other general expenses. General administration, joint tracks, yards, and terminals—Dr. General administration, joint tracks, yards, and terminals—Cr.	43.472 7.088 0.749 0.968 0.031 0.066 8.770	106–109 110 111–114 115 116

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## CHAPTER XXL

### DISTANCE.

403. Relation of distance to rates and expenses. Rates are usually based on distance traveled, on the apparent hypotheses that each additional mile of distance adds its proportional amount not only to the service rendered but also to the expense of rendering it. Neither hypothesis is true. The value of the service of transporting a passenger or a ton of freight from A to B is a more or less uncertain gross amount depending on the necessities of the case and independent of the exact distance. Except for that very small part of passenger traffic which is undertaken for the mere pleasure of traveling, the general object to be attained in either passenger or freight traffic is the transportation from A to B, however it is attained. A mile greater distance does not improve the service rendered; in fact, it consumes valuable time of the passengers and perhaps deteriorates the freight. From the standpoint of service rendered, the railroad which adopts a more costly construction and thereby saves a mile or more in the route between two places is thereby fairly entitled to additional compensation rather than have it cut down as it would be by a strict mileage rate. The actual value of the service rendered may therefore vary from an insignificant amount which is less than any reasonable charge (which therefore discourages such traffic) and its value in cases of necessity-a value which can hardly be measured in money. If the passenger charge between New York and Philadelphia were raised to \$5, \$10, or even \$20, there would still be some passengers who would pay it and go, because to them it would be worth \$5, \$10, or \$20, or even more. Therefore. when they pay \$2.25 they are not paying what the service is worth to them. The service rendered cannot therefore be made a measure of the charge, nor is the service rendered proportional to the miles of distance.

The idea that the cost of transportation is proportional to

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#### DISTANCE.

the distance is much more prevalent and is in some respects more justifiable, but it is still far from true. This is especially true of passenger service. The extra cost of transporting a single passenger is but little more than the cost of printing his ticket. Once aboard the train, it makes but little difference to the railroad whether he travels one mile or a hundred. Of course there are certain very large expenses due to the passenger traffic which must be paid for by a tariff which is rightfully demanded, but such expenses have but little relation to the cost of an additional mile or so of distance inserted between stations. The same is true to a slightly less degree of the freight traffic. As shown later, the items of expense in the total cost of a trainmile, which are directly affected by a small increase in distance, are but a small proportion of the total cost.

404. The conditions other than distance that affect the cost; reasons why rates are usually based on distance. Curvature and minor grades have a considerable influence on the cost of transportation, as will be shown in detail in succeeding chapters, but they are never considered in making rates. Ruling grades have a very large influence on the cost, but they are likewise disregarded in making rates. An accurate measure of the effect of these elements is difficult and complicated and would not be appreciated by the general public. Mere distance is easily calculated; the public is satisfied with such a method of calculation; and the railroads therefore adopt a tariff which pays expenses and profits even though the charges are not in accordance with the expenses or the service rendered. An addition to the length of the line may (and generally does)

An addition to the length of the line may (and generally does) involve curvature and grade as well as added distance. In this chapter is considered merely the effect of the added distance. The effect of grade and curvature must be considered separately, according to the methods outlined in succeeding chapters. The additional length considered is likewise assumed *not* to affect the business done nor the number of stations, but that it is a mere addition to length of track.

## EFFECT OF DISTANCE ON OPERATING EXPENSES.

405. Effect of changes in distance on maintenance of way. The items of maintenance of way are more nearly affected in proportion to the distance than any other group of items. In fact it will be easier to note the exceptions from a full 100% addition for all increases of distance. The cost of track labor, which is such a large percentage of the total cost of Item 6 (see Table XX in Chapter XX), and also the cost of all track material, will vary almost exactly in accordance with the distance. If the track-labor was so perfectly organized that there were no more laborers than could precisely accomplish the necessary work, working full time, then any additional labor would necessarily require a greater expenditure for laborers. Although a division of a road is divided into sections of such a length that a gang of say six or seven men will be employed as steadily as possible in maintaining the track in proper condition, the addition of a few feet of track would not probably have the effect of increasing the number of sections, nor would it even require the addition of another man to the track-gang. It might require a little harder work in maintaining a section, it might even mean a slight lowering in the standard of work done in order that the whole section should be covered. The fact remains that the cost of track-labor will not inevitably and necessarily be increased in a strict proportion to the increase in distance. On the other hand, it would not be wise to rely on any definite reduction or discount from the full 100% of work required, since to do so implies that, with the lessened distance there would be some loafing on the part of the trackgang, or that with the added distance the men would be overworked or would be compelled to slight their work. The items, renewals of rails and renewals of ties, should certainly be considered as changing in direct proportion to the distance. Therefore it is only safe to allow the full 100% addition for Items 1 to 7.

The repairs and renewals of tunnels, bridges, culverts, fences, road crossings, signs, cattle-guards, buildings and fixtures, docks and wharves, etc. (Items 8 to 17), may perhaps be considered in the same way, although there are some of these items on which the effect is more doubtful. If a proposed change in line does not involve any difference in the number of streams crossed, then the number of the bridges and culverts will not be altered, and although the size may be altered, the effect of the change on the cost for repairs will probably be too insignificant for notice. For small changes of distance it may very readily happen that no bridge or culvert is involved. For

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great changes of distance, especially those which would involve an entire change of route for a distance of many miles, it might be proper to consider Item 9 to be affected fully 100%. Although Items 9 and 10 are small, averaging about 1.8%, the error involved in these items by considering that the change amounts to 100% for great distances and zero for small distances will be almost inappreciable. For Items 11 to 13 the full 100% will be allowed for all changes of distance, for the same reason as previously given for repairs of roadway. Item 16 will usually be absolutely unaffected by a small change in distance, since it does not usually involve any buildings or fixtures. Larger changes of distance will probably require some change in the number of minor buildings required, but such buildings will be the more insignificant buildings, and we are therefore making ample allowance, if, under ordinary conditions, we estimate that 20% of the average cost of all buildings (which include terminals, etc.) is allowed for this item. Under ordinary conditions Item 17 will be absolutely unaffected by any changes in alinement which the engineer may make. An addition to distance will not usually affect the telegraph system, except as it adds to the number of telegraph-poles and to the amount of wiring and pole fixtures. Therefore any addition to distance will not add more than 50% to the average cost of Item 14. Items 18 to 21 are insignificant in amount, and can hardly be said to be affected by any small difference in distance which would ordinarily be measured in feet. Larger differences, which are measured in miles and which may involve, for instance, all the blank forms required for the reports of an additional section-gang, additional pay-rolls, etc., will be increased to practically their full proportion. Therefore there is but little error involved in allowing 100% on these items for changes of distance measured in miles.

406. Effect on maintenance of equipment. The relation between an increase in length of line and the expenses of Items 24, and 46 to 50 are quite indefinite. In some respects they would be unaffected by slight changes of distance, and yet it is difficult to prove that the expenses should not be considered proportionate for the distance. For example, the added trainmileage will increase repairs of rolling-stock, and will therefore hasten the deterioration and increase the cost of "repairs and renewals of shop machinery and tools" (Item 46). Fortunately, all these items are so small, even in the aggregate, that little error will be involved, whatever decision is made. It will therefore be assumed that these items are affected 100% for large additions in distance and 50% for small additions. Items 40 to 42 are evidently unaffected by any change of distance. Electrical equipment, items 28–30 and 37–39, which are used on so few steam railroads, is ignored in this discussion.

There only remain the four groups of items, the repairs, renewals and depreciation of steam locomotives and of passenger and freight-cars and of work equipment. The deterioration of rolling stock, which requires its repair and finally its ultimate abandonment and therefore renewal, is caused by a combination of a large number of causes, of which the mere distance they travel on the road is but one cause. They deteriorate first with age; second, on account of the strains due to stopping and starting; third, on account of the strains and wear of wheels due to curved track; fourth, on account of the additional stresses due to grade and change of grade, and fifth, on account of the work of pulling on a straight level track. In addition to this, locomotives suffer considerable deterioration due to expansion and contraction, especially of the fire-box when the fires are drawn and the fire-box and boiler become cold. and again when the fire is started up. A large part of the expenses of maintaining passenger-cars is the expense of painting. which is a matter of mere time. Considering that the changes of distance, whose economic value the engineer tries to compute, will never make a difference in the number of round trips the engine or car would make in a day or month, the added distance which may be traveled does not add to the exposure of the car to the weather. Therefore, whatever deterioration of the car paint is due to weather, it will be incurred regardless of whether the length of the division of the road is 100 miles or 99 or 101. That element of the cost of car maintenance is absolutely independent of the precise length of that division of the road. On the other hand, the wear of car- and enginewheels, although largely affected by curvature, is certainly affected to some extent by wear on a straight tangent. To determine the proportion of total wear due to these various causes is a matter of estimation and judgment. An approach to accuracy may be made by a compilation of the shop records of rolling-stock, repairs, showing the amount which is spent

#### DISTANCE.

in various kinds of repairs, and estimating as closely as possible what is the cause of each form of deterioration. A check on any such estimate is the consideration that the total deterioration is simply the summation of the deterioration due to all causes combined. It is therefore a question of dividing 100% into as many portions as there are contributing causes, and to assign to each cause its relative importance in per cent, so that the sum total shall reach 100. A. M. Wellington, in his "Economic Theory of Railway Location," distributed the cost of engine repairs to its various contributing causes, as shown in the following tabular form. He did not claim that such an estimate was accurate and applicable to all cases, but he did claim that the error was probably not sufficient to be of importance. A comparison of these percentages, with the data given by shop records on any particular road, would not probably show a very material difference, and the writer will not attempt to claim that any figures he might obtain will be any more accurate in general, although they might be more accurate as applied to some particular conditions.

DISTRIBUTION OF THE COST OF ENGINE REPAIRS TO ITS VARIOUS CONTRIBUTING CAUSES. (Copied from Wellington.)

Contraction of the local design of the local d						
- 1 C - 2 C						
Item.	Total cost of item.	Effect of time, age, and expos- ure, per cent.	starting	Termi- nal: getting up steam making up trains, per cent.	Curva- ture and grades, per cent. (App'x- imate aver- age.)	Dis- tance on tangent between sta- tions, per cent.
Boiler Running gear Machinery	$20.0 \\ 20.0 \\ 30.0$	 . 1	2 4 7	7 2 3	4 7 5	7 7 14
Mountings Lagging and painting Smoke-box, etc Tender:	$\begin{array}{c} 12.0\\ 5.0\end{array}$	4 1		$ \begin{array}{c} 2\\ 1 \end{array} $		6 3
Running gear Body and tank	$\substack{10.0\\3.0}$	····i	2 	1 1	3	4 1
Total	100.0	7	15	17	19	42

It may be noted from the above table that 42% of engine repairs has been assigned to distance on a tangent between stations. If the added distance does not imply an extra stoppage of the train, there is but little, if any, reason to differentiate between the effect on repairs of a large or small addition to distance. We will therefore consider Items 25–27 to be affected in this ratio of 42%.

Wellington similarly distributed the cost of freight-car repairs to its various causes, and by a very similar method estimated that 36% of such repairs was due to distance on a tangent between stations. The considerable transformation in the construction of freight-cars, since the time that Wellington compiled this table, has certainly utterly changed the absolute cost of car repairs, even if it has not changed the relative percentage of the cost of the various items. In the lack of any better figures this same figure will be for Items 34-36. Although there are evidently enormous differences between Items 34-36 and 43-45. Items 43-45 are so small that it is hardly worth the calculation of any more precise figures, and therefore the same ratio, 36%, will be used for Items 43-45. Wellington made no definite calculations for the itemized cost of passenger-car repairs. but contented himself with using the same figure as for freight-cars, 36%. Such a percentage is probably very much too high, since it is estimated that about one-half the cost of passenger-car repairs is due to the work of painting, inside and out, and of maintaining the seats and upholstery in proper condition. Such repairs are chiefly a function of time, and are but little, if any, dependent on mere distance between stations. It is therefore considered that Items 31-33 will not be affected more than 20% by any addition of distance.

Traffic expenses will be unaffected.

407: Effect on conducting transportation. Items 61-78, superintendence and dispatching, all station and yard expenses, and the joint expenses of yards and terminals, may be considered as unaffected. Item 79, motormen's wages, is ignored.

Item 80. Road enginemen. In a previous chapter, §396 the wages of road enginemen were discussed. The discussion showed that the enginemen are rarely, although sometimes, paid on a strict mileage basis. They are usually paid on a trip basis, in accordance with which a slight change in the distance will not affect the classification of the trip, and therefore would make no difference in the wages. We will therefore say that for small changes of distance, especially such as would be measured in feet, this item will be unaffected; but that for larger changes, such as would be measured in miles, this item will be affected by the full amount of the enginemen's wages.

Although there might be some justification for saying that the engine-house expenses for road engines (Item 81) might be somewhat increased by additions to distance, the addition may be considered as already covered by the increase in maintenance charges (Items 25-27), and no further allowance will be made.

Item 82. Fuel. A surprisingly large percentage of the fuel consumed is not utilized in drawing a train along the road. A portion of this percentage is used in firing-up. A portion is wasted when the engine is standing still, which is a considerable proportion of the whole time. The policy of banking fires instead of drawing them reduces the injury resulting from great fluctuations in temperature, but in a general way we may say that there is but little, if any, saving in fuel by banking the fires, and therefore we may consider that almost a fire-box full of coal is wasted whether the fires are banked or drawn. Some tests were made on the Santa Fé, in which some large locomotives consumed from 1200 to 1660 pounds of coal merely in firing-up. But even the amount of coal required to produce the required steam-pressure in the boiler from cold water does not represent the total loss. The train-dispatcher, in his anxiety that engines shall be ready when needed, will sometimes order out the locomotives which remain somewhere in the yard, perhaps exposed to cold weather, and blow off steam for several hours before they make an actual start. Of course the amount thus attributable to firing-up is a very variable one, depending on the management, and therefore no precise figures are obtainable. But it has been estimated that it amounts to from 5 to 10% of the total consumption. A freight-train, especially on a singletrack road, will usually spend several hours during the day on sidings, and when a single-track road is being run to the limit of its capacity, or when the management is not good, the time will be still greater. It has been found that the amount of coal required by an engine merely to keep up steam will amount to from 25 to 50 pounds per hour. If, in addition to this, steam escapes through the safety-valve, the loss is much larger. Τt is estimated that the amount lost through a  $2\frac{1}{2}$ -inch safetyvalve in one minute would represent the consumption of 15 pounds of coal, which would be sufficient to haul 100 tons on a mile of track with easy grades. Again we see that the amount thus lost is exceedingly variable and almost non-computable, although as a rough estimate the amount has been placed at from 3 to 6% of the total. Another very large subitem of loss of useful energy is that occasioned by stopping and starting. A train running 30 miles per hour has enough kinetic energy to move it on a straight level track for more than two miles. Therefore, every time a train running at 30 miles per hour is stopped, enough energy is consumed by the brakes to run it about two miles. There is a double loss, not only due to the fact of the loss of energy, but also because the power of the locomotive has been consumed in operating the brakes. When the train is again started, this kinetic energy must be restored to the train in addition to the ordinary resistances which are even greater, on account of the greater resistance at very low velocities. Of course, the proportion of fuel thus consumed depends on the frequency of the stops. It was demonstrated by some tests on the Manhattan Elevated Road in New York City, where the stops average one in every three-eighths of a mile, that this cause alone would account for the consumption of nearly three-fourths of the fuel. On ordinary railroads the proportion, of course, will not be nearly so great, but there is reason to believe that 10 to 20% is not excessive as an average figure. The amount of fuel which is consumed on account of curvature is, of course, a function of the curvature and will vary with each case. The only possible basis for a calculation of this amount must be somewhat as follows: Since all of the above calculations consider the average cost of a train-mile throughout the country, we must consider what is the average amount of curvature per mile of track throughout the country. By estimating, as will be developed in the next chapter, the proportion of the fuel expenditure which is due to this average amount of curvature and subtracting this, as well as the other subitems enumerated above, from the total average cost of a train-mile, we would then have the desired quantity, the cost of fuel per mile of straight level track. Although it is not easy to obtain reliable statistics showing the average curvature per mile or road throughout the United States, there is reason to believe that it is not far from 35° per mile. According to the

method of calculations given in the next chapter, to determine the additional fuel consumed by the added resistance due to  $35^{\circ}$  of curvature per mile, we obtain the approximate value that about 4% of the fuel consumption will be due to this cause. To obtain an average figure for the resistance due to grade is perhaps even harder, but on the approximate basis that the average amount of rise and fall per mile of track is about 11 feet per mile, it would seem as if 25% of the consumption of fuel were due to grades. Summarizing the above items we would have

Firing Loss by radiation, etc Stopping and starting Average curvature	3 to 10 to	$6\% \\ 20\%$	
Average grade	25 to	25%	
Direct hauling			Average 44%

This gives, as an average figure for the increased consumption of fuel due to one additional mile of straight level track, 44%of the average consumption per mile.

Items 83, 84, and 85. Minor engine-supplies. If water is obtained from municipal supplies and paid for at meter rates, then the cost will be strictly according to the consumption, which will be nearly according to the number of engine-miles. Almost the only waste would be that occasioned by blowing off steam. Under such circumstances the increase in this item would be very nearly 100%, but, on the other hand, where the supply is obtained from the company's own plant, there is hardly any appreciable increase in expense due to the extra draft on the tanks. Of course the cost of pumping would be somewhat affected. Considering that the sum of Items 83, 84, and 85 is only 1.06%, very little error would be involved if we consider as an average figure that this item will be increased the same as fuel, 44%.

Item 88 includes the wages of trainmen other than enginemen. Their wages are paid on very much the same basis as the enginemen, which means usually that small additions of distance will not affect their wages. Large additions will affect them 100%. Item 89. Train-supplies and expenses include a very large matter of small subitems, the consumption of which is partly a matter of mere time and partly a matter of mileage. It is sufficiently precise in this case to say that 50% of these subitems will be affected directly as the mileage.

Items 90, 91. Signals, flagmen, and gatemen. The necessity for flagmen and switchmen may be said in general to increase with the mileage, although it might readily happen that a given change in distance which is under consideration might not effect the slightest change in this item. It is quite unlikely that the number of switchmen would be affected. It is probable that 25% of this item is sufficient as an average figure.

Item 94. Telegraph expenses include the wages of operators at stations (which are unaffected) and the special expenses due to offices and telegraph stations and to operating the line, the maintenance of the line being charged to Item 14. Although it will theoretically require more battery material to transmit telegrams over a longer line, the added expense is so very slight that it may be utterly ignored.

Items 86 and 87, operating power plants and purchased power, which depend on electric traction, are ignored. Item 92, drawbridge operation, and Item 95, operating floating equipment, are considered to be unaffected. Items 96 to 98 are small miscellaneous expenses which are considered unaffected, as are likewise Items 104 and 105, the operation of joint tracks and facilities. This leaves Items 93 and 99 to 103, which are the fortuitous expenses due to wrecks, damage and mishaps. While it cannot be definitely predicted that these will happen with any stated regularity, it is only proper to consider that they will increase with added distance and to charge them as strictly proportional to distance.

The general expenses, Items 106 to 116, are considered to be unaffected.

408. Estimate of total effect on expenses of small changes in distance measured in feet; also estimate for distances measured in miles. Collecting the above percentages for the various items we have Table XXI, which shows that the average cost of operating a small additional distance will be about 33% of the average cost per unit distance. If the additional distance amounts to several miles, the added cost will amount to about 50% of the unit cost. These figures may also be con-

# DISTANCE.

# § 408.

TABLE XXI.	EFFECT ON OPERATING EXPENSES OF GREAT AND	
	SMALL CHANGES IN DISTANCE.	

No. of item.	Normal	Per cent	affected.	Cost per mile, per cent.			
No. of Item.	average.	Great.	Small.	Great.	Small.		
$\begin{array}{c} *1-7\\8\\9,10\\11-13\\14\\15\\16\\17\\18-21\\22,23\end{array}$	$14.61 \\ 0.06 \\ 1.77 \\ 0.82 \\ 0.49 \\ 0.02 \\ 1.81 \\ 0.20 \\ 0.45 \\ 0.16 $	$     \begin{array}{r}       100 \\       0 \\       100 \\       50 \\       0 \\       20 \\       0 \\       100 \\       0     \end{array} $	$     \begin{array}{r}       100 \\       0 \\       0 \\       100 \\       50 \\       0 \\$	14.6101.770.820.1000.3600.450	$14.61 \\ 0 \\ 0.82 \\ 0.10 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\$		
	20.09		· · · · · · · · · · · · · · · · · · ·	18.11	15.53		
$\begin{array}{c} 24\\ 25-27\\ 28-30\\ 31-33\\ 34-36\\ 37-39\\ 40-42\\ 43-45\\ 46-50\\ 51, 52\end{array}$	$\begin{array}{c} 0.64\\ 8.62\\ 0.01\\ 2.14\\ 10.15\\ 0.01\\ 0.08\\ 0.34\\ 0.72\\ 0.03\\ \end{array}$	$100 \\ 42 \\ 0 \\ 20 \\ 36 \\ 0 \\ 0 \\ 36 \\ 100 \\ 0$	$50 \\ 42 \\ 0 \\ 20 \\ 36 \\ 0 \\ 0 \\ 36 \\ 50 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ $	$\begin{array}{c} 0.64\\ 3.62\\ 0\\ 0.43\\ 3.65\\ 0\\ 0\\ 0.12\\ 0.72\\ 0 \end{array}$	$\begin{array}{c} 0.32\\ 3.62\\ 0\\ 0.43\\ 3.65\\ 0\\ 0\\ 0.12\\ 0.36\\ 0\end{array}$		
	22.74			9.18	8.50		
53-60	3.08	0	0	0	0		
61-79 80 81 82-85 86, 87 88 89 90, 91 92 93 94-98 99-103 104, 105	$\begin{array}{c} 17.92 \\ 6.08 \\ 1.72 \\ 11.41 \\ 0.06 \\ 6.40 \\ 1.78 \\ 0.85 \\ 0.05 \\ 0.25 \\ 1.06 \\ 2.84 \\ 0.02 \\ \hline \\ 50.44 \\ \hline \\ 3.65 \\ \hline \end{array}$	$\begin{array}{c} 0 \\ 100 \\ 0 \\ 44 \\ 0 \\ 100 \\ 50 \\ 25 \\ 0 \\ 100 \\ 0 \\ 100 \\ 0 \\ 0 \\ \hline \\ 0 \\ \hline \\ 0 \\ \hline \\ 0 \\ \hline \end{array}$	$ \begin{array}{c} 0 \\ 0 \\ 44 \\ 0 \\ 50 \\ 25 \\ 0 \\ 100 \\ 0 \\ 100 \\ 0 \\ \hline \hline \hline \hline 0 \\ \hline \hline \hline \hline \hline \hline 0 \\ \hline \hline$	$\begin{array}{c} 0\\ 6.08\\ 0\\ 5.02\\ 0\\ 6.40\\ 0.89\\ 0.21\\ 0\\ 0.25\\ 0\\ 2.84\\ 0\\ \hline 21.69\\ \hline 0\\ \hline \end{array}$	$ \begin{array}{c} 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\$		
	100.00			48.98	33.24		

\* For the significance of the items, see Table XX.

sidered as the saving in operating expenses resulting from a shortening of the line, and thus gives a measure of the operating value of reducing the length of the line. The average cost of a train-mile since 1890 has varied between 91.829 c. in 1895 to

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148.865 c. in 1910. The cost has been rising almost steadily since 1897. Whether the cost will continue to rise or whether it will recede during the next few years is of course a matter of pure conjecture. Even if the cost recedes somewhat from the high value of recent years, it is quite certain that it will never again sink to the low value of 1895. If we adopt the round number of \$1.50 as the probable cost of a train-mile during the next few years, we can reduce the above percentages to cents per train-mile, which will come to 50 and 73 c. per train-mile respectively. Some trains run 365 days per year; others run but 313 days. The tendency, however, is toward the larger figure, especially in the case of freight service, which comprises about 52% of the number of train-miles. The added cost per daily train per year for *each foot* of distance would therefore be

 $\frac{50 \times 365 \times 2}{5280} = 6.91 \text{ c.}$ 

When the distance is measured in miles the added cost per daily train per year for *each mile* of distance would be

$$73 \times 365 \times 2 = $533.$$

Of course, if such calculations are made for a light traffic road which only runs trains on week-days, we should use 313 in the above equations instead of 365. It should be noted that the subitems in the above table which are the most uncertain are those whose absolute value is the smallest, and that even if we make very large variations in the most uncertain items, the final result will not be very materially altered. On the other hand, the very largest items are those which are capable of fairly precise calculations.

# EFFECT OF DISTANCE ON RECEIPTS.

409. Classification of traffic. There are various methods of classifying traffic, according to the use it is intended to make of the classification. The method here adopted will have reference to its competitive or non-competitive character and also to the method of division of the receipts on through traffic. Traffic may be classified first as "through" and "local"—

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through traffic being that traveling over two (or [more) lines, no matter how short or non-competitive it may be; "local" traffic is that confined entirely to one road. A fivefold classification is however necessary—which is:

A. Non-competitive local—on one road with no choice of routes.

B. Non-competitive through—on two (or more) roads, but with no choice.

C. Competitive local—a choice of two (or more) routes, but the entire haul may be made on the home road.

D. Competitive through—direct competition between two or more routes each passing over two or more lines.

E. Semi-competitive through—a non-competitive haul on the home road and a competitive haul on foreign roads.

There are other possible combinations, but they all reduce to one of the above forms so far as their essential effect is concerned.

410. Method of division of through rates between the roads run over. Through rates are divided between the roads run over in proportion to the mileage. There may be terminal charges and possibly other more or less arbitrary deductions to be taken from the total amount received, but when the final division is made the remainder is divided according to the mileage. On account of this method of division and also because non-competitive rates are always fixed according to the distance, there results the unusual feature that, unlike curvature and grade, there is a compensating advantage in increased distance, which applies to all the above kinds of traffic except one (competitive local), and that the compensation is sometimes sufficient to make the added distance an actual source of profit. It has just been proved that the cost of hauling a train an additional mile is only 33 to 49% of the average Therefore in all non-competitive business (local or cost. through) where the rate is according to the distance, there is an actual profit in all such added distance. In competitive local business, in which the rate is fixed by competition and has practically no relation to distance, any additional distance is dead loss. In competitive through business the profit or loss depends on the distances involved. This may best be demonstrated by examples.

411. Effect of a change in the length of the home road on its receipts from through competitive traffic. Suppose the Suppose the home road is lengthened 5 miles; then it will receive  $\frac{105}{105+150}$ =41.176% of the through rate. The traffic being competitive, the rate will be a fixed quantity regardless of this change of distance. By the first plan the rate received is 0.4% per mile; adding 5 miles, the rate for the original 100 miles may be considered *the same* as before; and that the additional 5 miles receive 1.176%, or 0.235% per mile. This is 59% of the original rate per mile, and since this is more than the cost per mile for the additional distance (see § 408), the added distance is evidently *in this case* a source of distinct profit. On the other hand, if the line is shortened 5 miles, it may be similarly shown that not only are the receipts lessened, but that the saving in operating expenses by the shorter distance is less than the reduction in receipts.

A second example will be considered to illustrate another phase. Suppose the home road is 200 miles long and the foreign road is 50 miles long. In this case the home road will receive  $\frac{200}{200+50} = 80\%$  of the through rate. Suppose the home road is lengthened 5 miles; then it will receive  $\frac{205}{205+50} = 80.392\%$ of the through rate. By the first plan the rate received is 0.400% per mile; adding 5 miles, there is a surplus of 0.392, or 0.0784 per mile, which is but 19.6% of the original rate. At this rate the extra distance evidently is not profitable, although it is not a dead loss—there is some compensation.

412. The most advantageous conditions for roads forming part of a through competitive route. From the above it may be seen that when a road is but a short link in a long competitive through route, an addition to its length will increase its receipts and increase them more than the addition to the operating expenses.

As the proportionate length of the home road increases the less will this advantage become, until at some proportion an increase in distance will just pay for itself. As the proportionate length grows greater the advantage becomes a disadvantage until, when the competitive haul is entirely on the home road, any increase in distance becomes a net loss without any compensation. It is therefore advantageous for a road to be a short link in a long competitive route; an increase in that link will be financially advantageous; if the total length is less than that of the competing line, the advantage is still greater, for then the rate received per mile will be greater.

413. Effect of the variations in the length of haul and the classes of the business actually done. The above distances refer to particular lengths of haul and are not necessarily the total lengths of the road. Each station on the road has traffic relations with an indefinite number of traffic points all over the country. The traffic between each station on the road and any other station in the country between which traffic may pass therefore furnishes a new combination, the effect of which will be an element in the total effect of a change of distance. In consequence of this, any *exact* solution of such a problem becomes impracticable, but a sufficiently accurate solution for all practical purposes is frequently obtainable. For it frequently happens that the great bulk of a road's business is non-competitive, or, on the other hand, it may be competitive-through, and that the proportion of one or more definite kinds of traffic is so large as to overshadow the other miscellaneous traffic. In such cases an approximate but sufficiently accurate solution is possible.

414. General conclusions regarding a change in distance. (a) In *all* non-competitive business (local and through) the added distance is actually profitable. Sometimes practically all of the business of the road is non-competitive; a considerable proportion of it is always non-competitive.

(b) When the competitive local business is very large and the competitive through business has a very large average home haul compared with the foreign haul, the added distance is a source of loss. Such situations are unusual and are generally confined to trunk lines.

(c) The above may be still further condensed to the general conclusion that there is always *some* compensation for the added cost of operating an added length of line and that it frequently is a source of actual profit.

(d) There is, however, a limitation which should not be lost sight of. The above argument may be carried to the logical

conclusion that, if added distance is profitable, the engineer should purposely lengthen the line. But added distance means added operating expenses. A sufficient tariff to meet these is a tax on the community—a tax which more or less discourages traffic. It is contrary to public policy to burden a community with an avoidable expense. But, on the other hand, a railroad is not a charitable organization, but a money-making enterprise, and cannot be expected to unduly load up its first cost in order that subsequent operating expenses may be unduly cheapened and the tariff unduly lowered. A common reason for increased distance is the saving of the first cost of a very expensive although shorter line.

(e) Finally, although there is a considerable and uncompensated loss resulting from curvature and grade which will justify a considerable expenditure to avoid them, there is by no means as much justification to incur additional expenditure to avoid distance. Of course needless lengthening should be avoided. A moderate expenditure to shorten the line may be justifiable, but large expenditures to decrease distance are never justifiable except when the great bulk of the traffic is exceedingly heavy and is competitive.

415. Justification of decreasing distance to save time. It should be recalled that the changes which an engineer may make which are physically or financially possible will ordinarily have but little effect on the time required for a trip. The time which can thus be saved will have practically no value for the freight business—at least any value which would justify changing the route. When there is a large directly competitive passenger traffic between two cities (e.g. New York to Philadelphia) a difference of even 10 minutes in the time required for a run might have considerable financial importance, but such cases are comparatively rare. It may therefore be concluded that the value of the time saved by shortening distance will not ordinarily be a justification for increased expense to accomplish it.

**416.** Effect of change of distance on the business done. The above discussion is based on the assumption that the business done is unaffected by any proposed change in distance. If a proposed reduction in distance involves a loss of business obtained, it is almost certainly unwise. But if by increasing the distance the original cost of the road is decreased (because the construction is of less expensive character), and if the receipts are greater, and are increased still more by an increase in business done, then the change is probably wise. While it is almost impossible in a subject of such complexity to give a general rule, the following is generally safe: Adopt a route of such length that the annual traffic per mile of line is a maximum. This statement may be improved by allowing the element of original cost to enter and say, adopt a route of such length that the annual traffic per mile of line divided by the average cost per mile is Even in the above the operating cost per mile. a maximum. as affected by the curvature and grades on the various routes, does not enter, but any attempt to formulate a general rule which would allow for variable operating expenses would evidently be too complicated for practical application.

# CHAPTER XXII.

## CURVATURE.

417. General objections to curvature. In the popular mind curvature is one of the most objectionable features of railroad alignment. The cause of this is plain. The objectionable qualities are on the surface, and are apparent to the non-technical mind. They may be itemized as follows:

1. Curvature increases operating expenses by increasing (a) the required tractive force, (b) the wear and tear of roadbed and track, (c) the wear and tear of equipment, and (d) the required number of track-walkers and watchmen.

2. It may affect the operation of trains (a) by limiting the length of trains, and (b) by preventing the use of the heaviest types of engines.

3. It may affect travel (a) by the difficulty of making time, (b) on account of rough riding, and (c) on account of the apprehension of danger.

4. There is actually an increased danger of collision, derailment, or other form of accident.

Some of these objections are quite definite and their true value may be computed. Others are more general and vague and are usually exaggerated. These objections will be discussed in inverse order.

**478.** Financial value of the danger of accident due to curvature. At the outset it should be realized that in general the problem is *not* one of curvature *vs.* no curvature, but simply sharp curvature *vs.* easier curvature (the central angle remaining the same), or a greater or less percentage of elimination of the degrees of central angle. A straight road between termini is in general a financial (if not a physical) impossibility. The practical question is then, how much is the financial value of such diminution of danger that may result from such eliminations of curvature as an engineer is able to make?

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In the year 1898 there were 2228 railroad accidents reported by the Railroad Gazette, whose lists of all accidents worth reporting are very complete. Of these a very large proportion clearly had no relation whatever to curvature. But suppose we assume that 50% (or 1114 accidents) were directly caused by curvature. Since there are approximately 200,000 curves on the railroads of the country, there was on the average an accident for every 179 curves during the year. Therefore we may say, according to the theory of probabilities, that the chances are even that an accident may happen on any particular curve in 179 years. This assumes all curves to be equally dangerous, which is not true, but we may temporarily consider it to be true. If, at the time of the construction of the road, \$1.00 were placed at compound interest at 5% for 179 years, it would produce in that time \$620.89 for each dollar saved, wherewith to pay all damages, while the amount necessary to eliminate that curvature, even if it were possible, would probably be several thousand dollars. The number of passengers carried one mile for one killed in 1898–99 was 61,051,580. If a passenger were to ride continuously at the rate of sixty miles per hour, day and night, year after year, he would need to ride for more than 116 years before he had covered such a mileage, and even then the probabilities of his death being due to curvature or to such a reduction of curvature as an engineer might accomplish are very small. Of course particular curves are often, for special reasons, a source of danger and justify the employment of special watchmen. They would also justify very large expen-ditures for their elimination if possible. But as a general proposition it is evidently impossible to assign a definite money value to the danger of a serious accident happening on a particular curve which has no special elements of danger.

Another element of safety on curved track is that trait of human nature to exercise greater care where the danger is more apparent. Many accidents are on record which have been caused by a carelessness of locomotive engineers on a *straight* track when the extra watchfulness usually observed on a curved track would have avoided them.

419. Effect of curvature on travel. (a) Difficulty in making time. The growing use of transition curves has largely eliminated the necessity for reducing speed on curves, and even when the speed is reduced it is done so easily and quickly by means of air-brakes that but little time is lost. If two parallel lines were competing sharply for passenger traffic, the handicap of sharp curvature on one road and easy curvature on the other might have a considerable financial value, but ordinarily the

mere reduction of time due to sharp curvature will not have any computable financial value.(b) On account of rough riding. Again, this is much reduced

by the use of transition curves. Some roads suffer from a general reputation for crookedness, but in such cases the excessive curvature is practically unavoidable. This cause probably does have some effect in influencing competitive passenger traffic.

(c) On account of the apprehension of danger. This doubtless has its influence in deterring travel. The amount of its influence is hardly computable. When the track is in good condition and transition curves are used so that the riding is smooth, even the apprehension of danger will largely disappear.

Travel is doubtless more or less affected by curvature, but it is impossible to say how much. Nevertheless the engineer should not ordinarily give this item any financial weight whatsoever. Freight traffic (two thirds of the total) is unaffected by it. It chiefly affects that limited class of sharply competitive passenger traffic—a traffic of which most roads have not a trace.

420. Effect on operation of trains. (a) Limiting the length of trains. When curvature actually limits the length of trains, as is sometimes true, the objection is valid and serious. But this can generally be avoided. If a curve occurs on a ruling grade without a reduction of the grade sufficient to compensate for the curvature, then the resistance on that curve will be a maximum and that curve will limit the trains to even a less weight than that which may be hauled on the ruling grade. In such cases the unquestionably correct policy is to "compensate for curvature," as explained later (see §§ 427, 428), and not allow such an objection to exist. It is possible for curvature to limit the length of trains even without the effect of grade. On the Hudson River R. R. the total net fall from Albany to New York is so small that it has practically no influence in determining grade. On the other hand, a considerable portion of the route follows a steep rocky river bank which is so crooked that much curvature is unavoidable and very sharp curvature can only be avoided by very large expenditure. As a consequence sharp curvature has been used and the resistance on the curves is far greater than that of any fluctuations of grade which it was necessary to use. Or, at least, a comparatively small expenditure would suffice to cut down any grade so that its resistance would be less than that of some curve which could not be avoided except at an enormous cost. And as a result, since the length of trains is really limited by curvature, minor grades of 0.3 to 0.5% have been freely introduced which might be removed at comparatively small expense. The above case is very unusual. Low grades are usually associated with generally level country where curvature is easily avoided as in the Camden and Atlantic R. R. Even in the extreme case of the Hudson River road the maximum curvature is only equivalent to a comparatively low ruling grade.

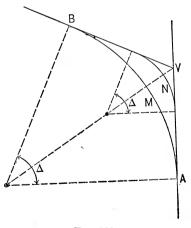
(b) Preventing the use of the heaviest types of engines. The validity of this objection depends somewhat on the degree of curvature and the detailed construction of the engine. While some types of engines might have difficulty on curves of extremely short radius, yet the objection is ordinarily invalid. This will best be appreciated when it is recalled that the "Consolidation" type was originally designed for use on the sharp curvature of the mountain divisions of the Lehigh Valley R. R., and that the type has been found so satisfactory that it has been extensively employed elsewhere. It should also be remembered that during the Civil War an immense traffic daily passed over a hastily constructed trestle near Petersburg, Va., the track having a radius of 50 feet. As a result of a test made at Renovo on the Philadelphia and Erie R. R. by Mr. Isaac Dripps, Gen. Mast. Mech., in 1875,\* it was claimed that a Consolidation engine encountered less resistance per ton than one of the "American" type. Whether the test was strictly reliable or not, it certainly demonstrated that there was no trouble in using these heavy engines on very sharp curvature. and we may therefore consider that, except in the most extreme cases, this objection has no force whatsoever.

\* Seventh An. Rep. Am. Mast. Mech. Assn.

## EFFECT OF CURVATURE ON OPERATING EXPENSES.

421. Relation of radius of curvature and of degrees of central angle to operating expenses. The smallest consideration will show that the sharper the curvature the greater will be the tractive force required, also the greater per unit of track length will be the rail wear and the general wear and tear on roadbed and rolling stock. But it would be inconvenient to use a relation between operating expenses and radius of curvature, because even when such a relation was found there would be two elements to consider in each problem—the radius and the length of the curve. The method which will be here developed cannot claim to be strictly accurate or even strictly logical, but, as will be shown later, the most uncertain elements of the computation have but a small influence on the final result, and the method is in general the only possible method of solution. The outline of the method is as follows:

(1) For reasons given in detail later, it is found that the expenses, wear, etc., on the track from A to B will be substantially the same whether by the route M or N. The wear, etc.,





per foot at N is of course greater, but the length of curve is less. Therefore the effect of the curvature depends on the degrees of central angle  $\varDelta$  and is independent of the radius.

(2) At what degree of curvature is the total train resistance double its value on a tangent? Probably no one figure would be exact for all conditions. Train resistance varies with the velocity and with the various conditions of train loading even on a tangent, and it is by no means certain (or even probable) that the ratio would be exactly the same for all conditions. As an average figure we may say that a train running at average velocity on a 10° curve will encounter a resistance due to curvature which is approximately equal to the average resistance found on a level tangent. On a 10° curve therefore the resistance is doubled.

(3) A train-mile costs about so much—approximately \$1.35. Doubling the tractive resistance will increase certain items of expenditure about so much. Their combined value is so much *per cent* of the cost of a train-mile. A mile of continuous 10° curve contains 528° of central angle. A mile of such track would add so much per cent to the average train-mile expenses, and each degree of central angle is responsible for  $\frac{1}{528}$  of this increase. Since the increase is irrespective of radius and depends only on the degrees of central angle, we therefore say that each degree of central angle of a curve will add so much to the average operating expenses of a train-mile. The "cost per train-mile" considered above should be con-

The "cost per train-mile" considered above should be considered as the cost of a mile of level tangent. If we for a moment consider that all the railroads of the country were made absolutely straight and level, it is apparent that the average cost per train-mile instead of being about \$1.35, would be somewhat less. The percentage should therefore be applied to this reduced value, but the net effect of this change would evidently be small.

422. Effect of curvature on maintenance of way. A very large proportion of the items of expense in a train-mile are absolutely unaffected by curvature. It will therefore simplify matters somewhat if we at once throw out all the unaffected items. Of the items of maintenance of way and structures all but items 2 to 6 may be thrown out. Item 9 will be somewhat affected when bridges or trestles occur on a curve. But when it is considered what a very small percentage of this small item (1.709%) could be ascribed to curvature, since the very large majority of bridges and trestles are purposely made

straight, and since culverts, etc., are not affected, we may evidently ignore any variation in the item.

Item 3. RENEWALS OF TIES. Curvature affects ties by increasing the "rail cutting" and on account of the more frequent respiking, which "spike-kills" the ties even before they have decayed. Wellington estimates that a tie which will last nine years on a tangent will last but six years on a 10° curve. He adds 50% for tie renewals. He considers the decrease in tie life to be proportional to the degree of curve and therefore again verifies the general statement made above regarding the expense of curvature.

Item 4. RENEWALS OF RAILS. The excess wear due to curvature has never been determined with satisfactory conclusiveness. Some tests have been made within the last few years on the Northern Pacific Railroad, which have perhaps followed the only practical method for determining the law of rail wear on curves. Selected rails on several tangents and curves of varying degrees of curvature were annually taken up, cleaned and weighed, and the annual loss due to wear was noted. The results indicated a loss of weight on curves varying nearly according to the degree of curve, and that the excess wear on a curve is 22.6% per degree of curve over that on a tangent. For a 10° curve, this would mean an excess wear of 226%.

Item 6. Repairs of Roadway. A very large proportion of the subitems are absolutely unaffected. The care of embankments and slopes, the ditching, weeding, etc., are evidently unaffected. The track-labor on rails and ties and the work of surfacing will evidently be somewhat increased, and yet it is very seldom that the length of a track section would be decreased simply on account of excessive curvature throughout that section. We are here trying to estimate how much this item, which consists largely of track-labor, will be affected by 528° of central angle per mile. In the previous chapter an approximate estimate was made that the average curvature per mile of road for the whole United States is about 35°. 528° of curvature in a mile probably does not frequently occur. It would mean the equivalent of nearly  $1\frac{1}{2}$  complete circles, and yet it is probably a generous estimate to say that the tracklabor and other expenses belonging to this item would not be increased more than 25% for such an amount of curvature. Items 2 and 5 are also allowed 25%.

423. Effect of curvature on maintenance of equipment. All items except the repairs, renewals and depreciation of steam locomotives, passenger-, freight- and work-cars, and shop machinery and tools, will be considered as unaffected. As before, electric equipment is ignored.

Items 25-27. Repairs and renewals of locomotives. Curvature affects locomotive repairs by increasing very largely the wear on tires and wheels, and also the wear and strain due to the additional power required. Since the resistance due to curvature is very small compared with that due to even a moderate grade, this last cause may be neglected altogether. Referring to the tabulation in § 406, we find an estimate that 19% of the cost of engine repairs is assigned to curvature and grades combined. Of this amount two-thirds, or, say, 13%, should be assigned to curvature alone. On the basis that the average curvature of the roads of the country is about 35° per mile, which is about one-fifteenth of the 528° of curvature per mile which we are considering, then, if  $35^{\circ}$  is responsible for 13%increase in engine repairs, 528° would be responsible for 196%. It must be admitted that the above computation is grossly approximate, and that it contains the unwarrantable assumption that the extra cost of engine repairs which is due to curvature will be strictly in proportion to the degrees of curve. Although it is probably not true that 528° of curvature would increase the cost of engine repairs by 15 times the extra cost of 35° of curvature, yet it is probably true that for ordinary variations from that average of 35° per mile the increased cost of engine repairs will be approximately as the number of degrees of curve, and therefore our final value is not necessarily far out of the way. If  $35^{\circ}$  is responsible for an increase of 13%, 1° would be responsible for about .37 of 1%. In allowing an increase of 196% for  $528^{\circ}$  we are also allowing .37 of 1% per degree of central angle.

Items 31-36, 43-45. By a similar course of reasoning to that above given, the estimates for Items 34-36 and 43-45 will be made 100%, while that for Items 31-33 will be made only 50%, because such a large proportion of the expenses of Items 31-33 are due to painting and maintaining upholstery, which have no relation to variations in alignment.

Item 46. The repairs and renewals of shop machinery and tools will not be increased more than 50% per mile

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for the additional repairs required on the above equipment.

424. Effect of curvature on conducting transportation. An inspection of the items under this general heading will show us that we may at once throw out as unaffected all the items except those which concern engine-supplies for road engines, flagmen, and watchmen, and the group which refers to accidents.

Items 82, 83, 84, and 85. The required quantities in this calculation are the additions to cost resulting from the introduction of  $528^{\circ}$  of central angle into a mile of track. We have assumed that this amount of curvature will exactly double the resistance. We found in Chapter XXI (§ 407) that the average increase in fuel consumption due to direct hauling amounts to about 44%. We have here assumed that the added curvature exactly doubles the work. We will therefore charge 44% of the average cost of a train-mile for this extra curvature. Since the consumption of water and other engine-supplies is roughly proportional to the consumption of coal, there will evidently be no error worth considering in assigning this same percentage to Items 83, 84, and 85.

Flagmen. There are many cases where a dangerous curve justifies and requires the employment of a special flagman to give timely notice of any dangerous condition of the track. Such special cases would, of course, justify a considerable expenditure to eliminate the dangerous features of that particular location, but such a charge should not be made against curvature in general. Ordinarily the elimination or retention of a curve will not involve the question of watchmen and flagmen in any way. We are therefore justified in disregarding this item altogether as a general proposition, if we keep in mind that the item should be included when we are considering the elimination of some particularly dangerous curve.

Items 99, 99–103. This group of items, which refer to accidents and the increased danger of accident due to curvature, and therefore the amount of money which might be justifiably spent to avoid this danger, has already been discussed in § 418. It was there shown that, although there might be special cases which would justify considerable expenditure on account of specific dangers in the situation, we cannot ordinarily give any definite financial value to this item as applied to curvature in general. We therefore must eliminate these items as affecting the cost of curvature in general.

General expenses. Items 106 to 116 will also be unaffected. 425. Estimate of total effect per degree of central angle. Compiling the above estimates we have Table XXII. Accord-

TABLE XXII. EFFECT ON OPERATING EXPENSES OF CHANGES IN CURVATURE.

Item - number.	Item (abbreviated).	Normal average.	Per cent affected.	Cost per mile, per cent.
$\begin{array}{c}2\\3\\4\\5\\6\end{array}$	Ballast. Ties. Rails. Other track material. Roadway and track. (All other items).	$\begin{array}{c} 0.50 \\ 3.10 \\ 0.92 \\ 1.13 \\ 7.53 \\ 6.91 \end{array}$	$25 \\ 50 \\ 226 \\ 25 \\ 25 \\ 25 \\ 0$	$\begin{array}{c} 0.12 \\ 1.55 \\ 2.10 \\ 0.28 \\ 1.88 \\ 0 \end{array}$
	Maintenance of way	20.09		5.93
$\begin{array}{r} 25-27\\ 31-33\\ 34-36\\ 43-45\\ 46\end{array}$	Locomotives. Passenger-cars. Freight-cars. Work-cars. Shop machinery; tools. (All other items).	$\begin{array}{r} 8.61 \\ 2.14 \\ 10.15 \\ 0.34 \\ 0.53 \\ 0.97 \end{array}$	$     \begin{array}{r}       196 \\       50 \\       100 \\       100 \\       50 \\       0 \\       0     \end{array} $	$16.88 \\ 1.07 \\ 10.15 \\ 0.34 \\ 0.26 \\ 0$
	Maintenance of equipment	22.74		28.70
53-60	Traffic	3.08	0	0
82-85	Fuel and other supplies for road engines	$\begin{array}{c} 11.41\\ 39.03 \end{array}$	44 0	5.02 0
	Transportation	50.44		5.02
106-116	General expenses	3.65	0	0
		100.00		39.65

ing to the table 528 of curvature in one link will increase the expenses of each train passing over it by 39.65% of the average cost of a train-mile, and, according to the general principles laid down in § 425, one degree of central angle of any curve, no matter what the radius, will increase the expenses by  $\frac{1}{528}$  of 39.65%, or .0751% per degree. Therefore, the cost per year per daily train each way, at the average rate of \$1.50 per train-mile would be

 $150 \times .0751\% \times 2 \times 365 = 82.23$  c.

For a round number we will call this 82 cents.

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To forestall one kind of objection to the foregoing course of reasoning, it should be remembered that many of the estimates of additional cost, instead of being actually based on the effects of a continuous 10° curve, were based on the observed effects of lighter curvature, which were then multiplied by a factor to obtain the effect of a continuous 10° curve, as if the effects of curvature were strictly proportional to the curvature; but since we afterward divide our final result by 528 to obtain the effect of one degree of curvature, and then multiply this constant by the number of degrees of central angle, as found in ordinary practice, our calculations are not thereby vitiated because the effect of curvature is not strictly proportional to the rate of curvature. It is probably true that within the ordinary limits of variations in rate of curvature the above calculations are substantially true. In extreme cases they are probably in error, although it is likewise probably true that extreme curvature will have a variable effect on the rate of increase of the various items, and that even in extreme cases the error will not be very large.

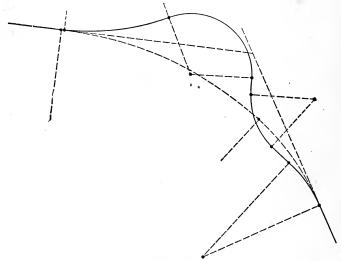


FIG. 209.

As a simple illustration (a more extended one will be given later), suppose that by using greater freedom with regard to earthwork the crooked line sketched may be reduced to the simple curve shown and a curvature of, say, 110° may be reduced to, say, 60°.

Note that since the extreme tangents are identical, the saving in central angle results from the elimination of the reversed curvature and of that part of the direct curvature necessary to balance the reversed curvature. Assume that there are six daily trains each way. Then the annual saving is

# $50 \times .82 \times 6 = $246$ ,

which at 5% would justify an expenditure of \$4920. If the extra cost of construction does not exceed this, the improvement is justifiable, and is made all the more so if the probabilities are great that the future traffic will largely exceed six trains per day. At the same time the warning regarding "discounting the future" with respect to expected traffic should not be neglected. The possible effect of change of distance has not been referred to in the above problem. In any case it is a distinct problem. According to the above sketch, the difference in distance is probably very slight, and considering the compensating character of extra distance, such small differences may usually be disregarded. The possible effect of change of grade will be discussed in the next chapter. Assuming that there is no difference to be considered on account of either grade or distance, the question hinges on the advisability of spending \$4920 for the improvement.

426. Reliability and value of the above estimate. It should be realized at the outset that no extreme accuracy is claimed for the above estimate. The effect of curvature is somewhat variable as well as uncertain, but such estimates have this great value. Vary the estimates of individual items as you please (within reason), and the final result is still about the same and may be used to guide the judgment. As an illustration, suppose that the item of renewals of rails is assumed to be affected 300% rather than 226%, the justifiable expenditure to avoid the curvature in the above case may similarly be computed as \$5017, an increase of about 2%. But, after all, the real question is not whether the improvement is worth \$4800 or \$5017. The extra work involved may perhaps be done for \$500 or it may require \$10000. The above general method furnishes reliance on vague judgment that it should not be ignored.

## COMPENSATION FOR CURVATURE.

427. Reasons for compensation. The effect of curvature on a grade is to increase the resistance by an amount which is equivalent to a material addition to that grade. On minor grades the addition is of little importance, but when the grade is nearly or quite the ruling grade of the road, then the additional resistance induced by a curve will make that curve a place of maximum resistance and the real maximum will be a "virtual grade" somewhat higher than the nominal maximum. If, in Fig. 210,

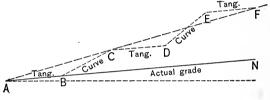


Fig. 210.

AN represents an actual uniform grade consisting of tangents and curves, the "virtual grade" on curves at BC and DE may be represented by BC and DE. If BC and DE are very long, or if a stop becomes necessary on the curve, then the full disadvantage of the curve becomes developed. If the whole grade may be operated without stoppage, then, as elaborated further in the next chapter, the whole grade may be operated as if equal to the average grade, AF, which is better than BC, although much worse than AN. The process of "compensation" consists in reducing the grade on every curve by such an amount that the actual resistance on each curve, due to both curvature and grade, shall precisely equal the resistance on the tangent. The practical effect of such reduction is that the "virtual" grade is kept constant, while the nominal grade fluctuates.

One effect of this is that (see Fig. 211) instead of accomplishing the vertical rise from A to G (i.e., HG) in the horizontal distance AH, it requires the horizontal distance AK. Such an addition to the horizontal distance can usually be obtained by proper development, and it should always be done on a ruling

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### CURVATURE.

grade. Of course it is possible that it will cost more to accomplish this than it is worth, but the engineer should be sure of this before allowing this virtual increase of the grade.

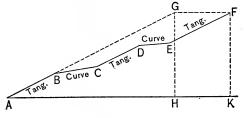


FIG. 211.

European engineers early realized the significance of unreduced curvature and the folly of laying out a uniform ruling grade regardless of the curvature encountered. Curve compensation is now quite generally allowed for in this country, but thousands of miles have been laid out without any compensation. A very common limitation of curvature and grade has been the alliterative figures 6° curvature and 60 feet per mile of grade, either singly or in combination. Assuming that the resistance on a 6° curve is equivalent to a 0.3% grade (15.84 feet per mile), then a 6° curve occurring on a 60-foot grade would develop more resistance than a 75-foot grade on a tangent. The "mountain cut-off" of the Lehigh Valley Railroad near Wilkesbarre is a fine example of a heavy grade compensated for curvature, and yet so laid out that the virtual grade is uniform from bottom to top, a distance of several miles.

428. The proper rate of compensation. This evidently is the rate of grade of which the resistance just equals the resistance due to the curve. But such resistance is variable. It is greater as the velocity is lower; it is generally about 2 lbs. per ton (equivalent to a 0.1% grade) per degree of curve when starting a train. On this account, the compensation for a curve which occurs at a known stopping-place for the heaviest trains should be 0.1% per degree of curve. The resistance is not even strictly proportional to the degree of curvature, although it is usually considered to be so. In fact most formulæ for curve resistance are based on such a relation. But if the experimentally determined resistances for low curvatures are applied to the excessive

curvature of the New York Elevated road, for example, the rules become ridiculous. On this account the compensation per degree of curve may be made less on a sharp curve than on an easy curve. The compensation actually required for very fast trains is less than for slow trains, say 0.02 or 0.03% per degree of curve; but since the comparatively slow and heavy freight trains are the trains which are chiefly limited by ruling grade, the compensation must be made with respect to those trains. From 0.04 to 0.05% per degree is the rate of compensation most usually employed for average conditions. Curves which occur below a known stopping-place for all trains need not be compensated, for the extra resistance of the curve will be simply utilized in place of brakes to stop the train. If a curve occurs just above a stopping-place, it is very serious and should be amply compensated. Of course the down-grade traffic need not be considered.

It sometimes happens that the ordinary rate of compensation will consume so much of the vertical height (especially if the curvature is excessive) that a steeper through grade must be adopted than was first computed, and then the trains might stall on the tangents rather than on the curves. In such cases a slight reduction in the rate of compensation might be justifiable. The proper rate of compensation can therefore be estimated from the following rules:

(1) On the upper side of a stopping-place for the heaviest trains compensate 0.10% per degree of curve.

(2) On the lower side of such a stopping-place do not compensate at all.

(3) Ordinarily compensate about 0.05% per degree of curve.

(4) Reduce this rate to 0.04% or even 0.03% per degree of curve if the grade on tangents must be increased to reach the required summit.

(5) Reduce the rate somewhat for curvature above  $8^{\circ}$  or  $10^{\circ}$ .

(6) Curves on minor grades need not be compensated, unless the minor grade is so heavy that the added resistance of the curve would make the total resistance greater than that of the the ruling grade, or unless there is some ground to believe that the ruling grade may sometime be reduced below that of the minor grade under consideration.

429. The limitations of maximum curvature. What is the maximum degree of curvature which should be allowed on any

road? It has been shown that sharp curvature does not prevent the use of the heaviest types of engines, and although a sharp curve unquestionably increases operating expenses, the increase is but one of degree with hardly any definite limit. The general character of the country and the gross capital available (or the probable earnings) are generally the true criterions. A portion of the road from Denver to Leadville, Col., is an

A portion of the road from Denver to Leadville, Col., is an example of the necessity of considering sharp curvature. The traffic that might be expected on the line was so meagre and yet the general character of the country was so forbidding that a road built according to the usual standards would have cost very much more than the traffic could possibly pay for. The line as adopted cost about \$20,000 per mile, and yet in a stretch of 11.2 miles there are about 127. curves. One is a 25° 20' curve, twenty-four are 24° curves, twenty-five are 20° curves, and seventy-two are sharper than 10°. If 10° had been made the limit (a rather high limit according to usual ideas), it is probable that the line would have been found impracticable (except with prohibitive grades) unless four or five times as much per mile had been spent on it, and this would have ruined the project financially.

For many years the main-line traffic of the Baltimore and Ohio R. R. has passed over a 300-foot curve  $(19^{\circ} 10')$  and a 400-foot curve  $(14^{\circ} 22')$  at Harper's Ferry. A few years ago some reduction was made in this by means of a tunnel, but the fact that such a road thought it wise to construct and operate such curves (and such illustrations on the heaviest-traffic roads are quite common) shows how foolish it is for an engineer to sacrifice money or (which is much more common) sacrifice gradients in order to reduce the *rate* of curvature on a road which at its best is but a second- or third-class road.

Of course such belittling of the effects of curvature may be (and sometimes is) carried to an extreme and cause an engineer to fail to give to curvature its due consideration. Degrees of central angle should always be reduced by all the ingenuity of the engineer, and should only be limited by the general relation between the financial and topographical conditions of the problem. Easy curvature is in general better than sharp curvature and should be adopted when it may be done at a small financial sacrifice, especially since it reduces distance generally and may even cut down the initial cost of that section of the road. But large financial expenditures are rarely, if ever, justifiable where the net result is a mere increase in radius without a reduction in central angle. An analysis of the changes which have been so extensively made during late years on the Penn. R. R. and the N. Y., N. H. & H. R. R. will show invariably a reduction of distance, or of central angle, or both, and perhaps incidentally an increase in radius of curvature. There are but few, if any, cases where the sole object to be attained by the improvement is a mere increase in radius.

The requirements of standard M. C. B. car-couplers have virtually placed a limitation on the radius on account of the corners of adjacent cars striking each other on very sharp curves. This limitation has been crystallized into a rule on the P. R. R. that no.curve, even that of a siding, can have a less radius than 175 feet, which is nearly the radius of a 33° curve. Of course only the most peremptory requirements of yard work would justify the employment of such a radius.

# CHAPTER XXIII.

## GRADE.

430. Two distinct effects of grade. The effects of grade on train expenses are of two distinct kinds; one possible effect is very costly and should be limited even at considerable expenditure; the other is of comparatively little importance, its cost being slight. As long as the length of the train is not limited, the occurrence of a grade on a road simply means that the engine is required to develop so many foot-pounds of work in raising the train so many feet of vertical height. For example, if a freight train weighing 600 tons (1,200,000 lbs.) climbs a hill 50 feet high, the engine performs an additional work of creating 60,000,000 foot-pounds of potential energy. If this height is surmounted in 2 miles and in 6 minutes of actual time (20 miles per hour), the extra work is 10,000,000 foot-pounds per minute, or about 303 horse-power. But the disadvantages of such a rise are always largely compensated. Except for the fact that one terminus of a road is generally higher than the other, every up grade is followed, more or less directly, by a down grade which is operated partly by the potential energy acquired during the previous climb. But when we consider the trains running in both directions even the difference of elevation of the termini is largely neutralized. If we could eliminate frictional resistances and particularly the use of brakes, the net effect of minor grades on the operation of minor grades in both directions would be zero. Whatever was lost on any up grade would be regained on a succeeding down grade, or at any rate on the return trip. On the very lowest grades (the limits of which are defined later) we may consider this to be literally true, viz., that nothing is lost by their presence; whatever is temporarily lost in climbing them is either immediately regained on a subsequent light down grade or is regained on the return trip. If a stop is required at the bottom of a sag, there is a net and uncompensated loss of energy.

On the other hand, if the length of trains is limited by the grade, it will require more trains to handle a given traffic. The receipts from the traffic are a definite sum. The cost of handling it will be nearly in proportion to the number of trains. Anticipating a more complete discussion, it may be said as an example that increasing the ruling grade from 1.20% (63.36 feet per mile) to 1.55% (81.84 feet per mile—an increase of about 18.5 feet per mile) will be sufficient to increase the required number of trains for a given gross traffic about 25%, i.e., five trains will be required to handle the traffic which four trains would have handled before at a cost slightly more than four-fifths as much. The effect of this on dividends may readily be imagined.

431. Application to the movement of trains of the laws of accelerated motion. When a train starts from rest and acquires its normal velocity, it overcomes not only the usual tangent resistances (and perhaps curve and grade resistances), but it also performs work in storing into the train a vast fund of kinetic energy. This work is not lost, for every foot-pound of such energy may later be utilized in overcoming resistances, provided it is not wasted by the action of train-brakes. If for a moment we consider that a train runs without any friction, then, when running at a velocity of v feet per second, it possesses a kinetic energy which would raise it to a height h feet, when  $h = \frac{v^2}{2a}$ , in which g is the acceleration of gravity = 32.16. Assuming that the engine is exerting just enough energy to overcome the frictional resistances, the train would climb a grade until the train was raised h feet above the point where its velocity was  $v_{i}$ When it had climbed a height h' (less than h) it would have velocity  $v_1 = \sqrt{2g(h-h')}$ . As a numerical illustration, assume v = 30 miles per hour = 44 feet per second. Then  $h = \frac{v^2}{2a} = 30.1$  feet, and assuming that the engine was exerting just enough force to overcome the rolling resistances on a level, the kinetic energy in the train would carry it for two miles up a grade of 15 feet per mile, or half a mile up a grade of 60 feet per mile. When the train had climbed 20 feet, there would still be 10.1 feet left and its velocity would be  $v_1 = \sqrt{2g(10.1)} = 25.49$  feet per second =17.4 miles per hour. These figures, however, must be slightly modified on account of the weight and the revolving action of the wheels, which form a considerable percentage of the total weight of the train. When train velocity is being acquired, part of the work done is spent in imparting the energy of rotation to the driving-wheels and various truck-wheels of the train. Since these wheels run on the rails and must turn as the train moves, their rotative kinetic energy is just as effective—as far as it goes—in becoming transformed back into useful work. The proportion of this energy to the total kinetic energy has already been demonstrated (see Chapter XVI, § 347). The value of this correction is variable, but an average value of 5% has been adopted for use in the accompanying tabular form (Table XXIII), in which is given the corrected "velocity head" corresponding to various velocities in miles per hour. The table is computed from the following formula:

Velocity head  $=\frac{v^2 \text{ in ft. per sec.}}{64.32} = \frac{2.151v^2 \text{ in m. per h.}}{64.32} = 0.03344v^2$ adding 5% for the rotative kinetic energy of the wheels,  $0.00167v^2$ The corrected velocity head therefore equals  $0.03511v^2$ 

Part of the figures of Table XXIII were obtained by interpolation and the final *hundredth* may be in error by one unit, but it may readily be shown that the final hundredth is of no practical importance. It is also true that the chief use made of this table is with velocities much less than 50 miles per hour. Corresponding figures may be obtained for higher velocities, if desired, by multiplying the figure for *half* the velocity by *four*.

432. Construction of a virtual profile. The following simple demonstration will be made on the basis that the ordinary tractive resistances and also the tractive force of the locomotive are independent of velocity. For a considerable range of velocity which includes the most common freight-train velocities this assumption is so nearly correct that the method will give an approximately correct result, but for higher velocities and for more accurate results a more complicated method (given later) must be used. The following demonstration will serve well as a preliminary to the more accurate method. It may best be illustrated by considering a simple numerical example.

Assuming that a train is passing A (see Fig. 212), running at 30 miles per hour. Assume that the throttle is not changed or any brakes applied, but that the engine continues to exert the

TABLE	XXIII	-VI	LOCITY	HEAD	(RE	PRESENTII	NG	THE	KINETIC
EN	VERGY)	$\mathbf{OF}$	TRAINS	MOVING	$\mathbf{AT}$	VARIOUS	VE	LOCII	TES.

Vel. mi. hr.	0.0	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9
$10 \\ 11 \\ 12 \\ 13 \\ 14$	3.51 4.25 5.06 5.93 6.88	$3.58 \\ 4.33 \\ 5.15 \\ 6.02 \\ 6.98$	$\begin{array}{r} 3.65 \\ 4.41 \\ 5.23 \\ 6.12 \\ 7.08 \end{array}$	$\begin{array}{c c} 3.72 \\ 4.49 \\ 5.32 \\ 6.21 \\ 7.19 \end{array}$	$\begin{array}{r} 3.79 \\ 4.57 \\ 5.41 \\ 6.31 \\ 7.29 \end{array}$	$\begin{array}{r} 3.87 \\ 4.65 \\ 5.50 \\ 6.40 \\ 7.39 \end{array}$	$\begin{array}{r} 3.95 \\ 4.73 \\ 5.58 \\ 6.50 \\ 7.49 \end{array}$	$\begin{array}{r} 4.02 \\ 4.81 \\ 5.67 \\ 6.59 \\ 7.60 \end{array}$	$\begin{array}{r} 4.10 \\ 4.89 \\ 5.75 \\ 6.69 \\ 7.70 \end{array}$	$\begin{array}{r} 4.17 \\ 4.97 \\ 5.84 \\ 6.78 \\ 7.80 \end{array}$
$15 \\ 16 \\ 17 \\ 18 \\ 19$	$7.90 \\ 8.99 \\ 10.15 \\ 11.38 \\ 12.68$	$8.00 \\ 9.10 \\ 10.27 \\ 11.50 \\ 12.81$	$\begin{array}{r} 8.11 \\ 9.21 \\ 10.39 \\ 11.63 \\ 12.95 \end{array}$	$\begin{array}{r} 8.22 \\ 9.32 \\ 10.51 \\ 11.76 \\ 13.08 \end{array}$	$\begin{array}{r} 8.33 \\ 9.43 \\ 10.63 \\ 11.89 \\ 13.22 \end{array}$	$\begin{array}{r} 8.44 \\ 9.55 \\ 10.75 \\ 12.02 \\ 13.35 \end{array}$	$\begin{array}{r} 8.55 \\ 9.67 \\ 10.87 \\ 12.15 \\ 13.49 \end{array}$	$\begin{array}{r} 8.66\\ 9.79\\ 10.99\\ 12.28\\ 13.63\end{array}$	$\begin{array}{r} 8.77\\ 9.91\\ 11.12\\ 12.41\\ 13.77\end{array}$	$\begin{array}{r} 8.88 \\ 10.03 \\ 11.25 \\ 12.55 \\ 13.91 \end{array}$
$20 \\ 21 \\ 22 \\ 23 \\ 24$	$14.05 \\ 15.49 \\ 17.00 \\ 18.58 \\ 20.23$	$14.19 \\ 15.64 \\ 17.15 \\ 18.74 \\ 20.40$	$14.33 \\ 15.79 \\ 17.30 \\ 18.90 \\ 20.57$	$14.47 \\15.94 \\17.46 \\19.06 \\20.74$	$14.61 \\ 16.09 \\ 17.62 \\ 19.22 \\ 20.91$	$14.75 \\ 16.24 \\ 17.78 \\ 19.38 \\ 21.08$	$14.89 \\ 16.39 \\ 17.94 \\ 19.55 \\ 21.25$	$15.04 \\ 16.54 \\ 18.10 \\ 19.72 \\ 21.42$	$\begin{array}{c} 15.19 \\ 16.69 \\ 18.26 \\ 19.89 \\ 21.59 \end{array}$	$15.34 \\ 16.84 \\ 18.42 \\ 20.06 \\ 21.77$
$25 \\ 26 \\ 27 \\ 28 \\ 29$	$21.95 \\ 23.74 \\ 25.60 \\ 27.53 \\ 29.53$	$\begin{array}{c} 22.12 \\ 23.92 \\ 25.79 \\ 27.73 \\ 29.73 \end{array}$	$22.30 \\ 24.10 \\ 25.98 \\ 27.93 \\ 29.93$	$22.48 \\ 24.28 \\ 26.17 \\ 28.13 \\ 30.13$	$22.66 \\ 24.46 \\ 26.36 \\ 28.33 \\ 30.34$	$22.84 \\ 24.65 \\ 26.55 \\ 28.53 \\ 30.55$	$23.02 \\ 24.84 \\ 26.74 \\ 28.73 \\ 30.76$	$\begin{array}{r} 23.20 \\ 25.03 \\ 26.93 \\ 28.93 \\ 30.97 \end{array}$	$\begin{array}{r} 23.38 \\ 25 \ 22 \\ 27.13 \\ 29.13 \\ 31.18 \end{array}$	$\begin{array}{c} 23.56 \\ 25.41 \\ 27.33 \\ 29.33 \\ 31.39 \end{array}$
$30 \\ 31 \\ 32 \\ 33 \\ 34$	$31.60 \\ 33.74 \\ 35.95 \\ 38.23 \\ 40.58$	$\begin{array}{c} 31.81 \\ 33.96 \\ 36.17 \\ 38.46 \\ 40.82 \end{array}$	$32.02 \\ 34.18 \\ 36.39 \\ 38.69 \\ 41.06$	$32.23 \\ 34.40 \\ 36.62 \\ 38.92 \\ 41.30$	32.44 34.62 36.85 39.15 41.54	32.65 34.84 37.08 39.38 41.78	32.86 35.06 37.31 39.62 42.02	$33.08 \\ 35.28 \\ 37.54 \\ 39.86 \\ 42.26$	$\begin{array}{r} 33.30\\ 35.50\\ 37.77\\ 40.10\\ 42.51\end{array}$	$\begin{array}{r} 33.52 \\ 35.72 \\ 38.00 \\ 40.34 \\ 42.76 \end{array}$
35 36 37 38 39	$\begin{array}{r} 43.01 \\ 45.51 \\ 48.08 \\ 50.72 \\ 53.42 \end{array}$	$\begin{array}{r} 43.26 \\ 45.76 \\ 48.34 \\ 50.99 \\ 53.69 \end{array}$	$\begin{array}{r} 43.51 \\ 46.01 \\ 48.60 \\ 51.26 \\ 53.96 \end{array}$	$\begin{array}{r} 43.76 \\ 46.26 \\ 48.86 \\ 51.53 \\ 54.23 \end{array}$	$\begin{array}{r} 44.01 \\ 46.52 \\ 49.12 \\ 51.80 \\ 54.51 \end{array}$	$\begin{array}{r} 44.26 \\ 46.78 \\ 49.38 \\ 52.07 \\ 54.79 \end{array}$	$\begin{array}{r} 44.51 \\ 47.04 \\ 49.64 \\ 52.34 \\ 55.07 \end{array}$	$\begin{array}{r} 44.76 \\ 47.30 \\ 49.91 \\ 52.61 \\ 55.35 \end{array}$	$\begin{array}{r} 45.01 \\ 47.56 \\ 50.18 \\ 52.88 \\ 55.63 \end{array}$	$\begin{array}{r} 45.26 \\ 47.82 \\ 50.45 \\ 53.15 \\ 55.91 \end{array}$
$ \begin{array}{r} 40 \\ 41 \\ 42 \\ 43 \\ 44 \end{array} $	$\begin{array}{c} 56.19 \\ 59.03 \\ 61.94 \\ 64.92 \\ 67.98 \end{array}$	$\begin{array}{c} 56.47\\ 59.32\\ 62.23\\ 65.22\\ 68.29\end{array}$	$\begin{array}{c} 56.75\\ 59.61\\ 62.52\\ 65.52\\ 68.60\end{array}$	$\begin{array}{c} 57.03 \\ 59.90 \\ 62.82 \\ 65.82 \\ 68.91 \end{array}$	$57.31 \\ 60.19 \\ 63.12 \\ 66.12 \\ 69.22$	$57.59 \\ 60.48 \\ 63.42 \\ 66.43 \\ 69.53$	$57.87 \\ 60.77 \\ 63.72 \\ 66.74 \\ 69.84$	$\begin{array}{c} 58.16 \\ 61.06 \\ 64.02 \\ 67.05 \\ 70.15 \end{array}$	$\begin{array}{c} 58.45 \\ 61.35 \\ 64.32 \\ 67.36 \\ 70.46 \end{array}$	$\begin{array}{c} 58.74 \\ 61.64 \\ 64.62 \\ 67.67 \\ 70.78 \end{array}$
$     \begin{array}{r}       45 \\       46 \\       47 \\       48 \\       49 \\       50     \end{array} $	71.10 74.30 77.57 80.91 84.32 87.79	71.42 74.62 77.90 81.25 84.66 88.14	71.74 74.94 78.23 81.59 85.00 88.49	72.06 75.26 78.56 81.93 85.34 88.85	72.3875.5978.8982.2785.6989.20	72.70 75.92 79.22 82.61 86.04 89.55			73.6676.9180.2383.6387.0990.61	73.98 77.24 80.57 83.97 87.44 90.97

same draw-bar pull. At A its "velocity head" is that due to 30 miles per hour, or 31.60 feet. At B it has gained 40 feet more, and its velocity is that due to a velocity head of 71.60 feet, or slightly over 45 miles per hour. At B' its velocity is again 30 miles per hour and velocity head 31.60 feet. At C the velocity head is but 6.60 feet and the velocity about 13.7 miles per hour.

## GRADE.

As the train runs from C to D its velocity increases to 30 miles at C' and to over 45 miles per hour at D. At E the velocity again becomes 30 miles per hour. Although there will be some slight modifications of the above figures in actual practice, yet the above is not a fanciful theoretical sketch. Thousands of just such undulations of grade are daily operated in such a way, without disturbing the throttle or applying brakes, and the draw-bar pull, if measured by a dynamometer, would be found to be practically constant. Of course the above case assumes that

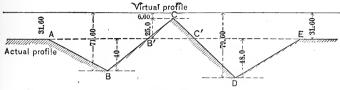
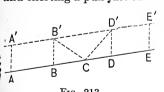


FIG. 212.

there are no stoppages and that the speed through the sags is not so great that safety requires the application of brakes. Observe that the "virtual profile" is here a straight line—as it always is when the draw-bar pull is constant. The virtual profile (in this case as well as in every other case, illustrations of which will follow) is found by adding to the actual profile at any point an ordinate which represents the "velocity head" due to the velocity of the train at that point.

As another case, assume that a train is climbing the grade AEand exerting a pull just sufficient to maintain a constant velocity





up that grade. Then A'B' (parallel to AB) is the virtual profile, AA'representing the velocity head. A stop being required at C, steam is shut off and brakes are applied at B, and the velocity head BB'reduces to zero at C. The train

starts from C, and at D attains a velocity corresponding to the ordinate DD'. At D the throttle may be slightly closed so that the velocity will be uniform and the virtual grade is D'E', parallel to DE.

From the above it may be seen that a virtual profile has the following properties:

(a) When the velocity is *uniform*, the virtual profile is parallel with the actual.

(b) When the velocity is increasing the profiles are separating; when decreasing the profiles are approaching.

(c) When the velocity is zero the profiles coincide.

433. Use, value, and possible misuse. The essential feature respecting grades is the demand on the locomotive. From the foregoing it may readily be seen that the ruling grade of a road is not necessarily the steepest nominal grade. When a grade may be operated by momentum, i.e., when every train has an opportunity to take "a run at the hill," it may become a very harmless grade and not limit the length of trains, while another grade, actually much less, which occurs at a stopping-place for the heaviest trains, will require such extra exertion to get trains started that it may be the worst place on the road. Therefore the true way to consider the value of the grade at any critical place on the road is to construct a virtual profile for that section of the road. The required length of such a profile is variable, but in general may be said to be limited by points on each side of the critical section at which the velocity is definite. as at a stopping-place (velocity zero), or a long heavy grade where it is the minimum permissible, say 10 or 15 miles per hour.

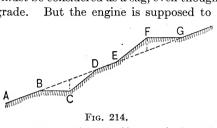
Since the velocities of different trains vary, each train will have its own virtual profile at any particular place. The fast passenger trains are generally unaffected, practically. The requirement of high average speed necessitates the use of powerful engines, and grades which would stall a heavy freight will only cause a momentary and harmless reduction of speed of the fast passenger train.

A possible misuse of virtual profiles lies in the chance that a station or railroad grade crossing may be subsequently located on a heavy grade that was designed to be operated by momentum. But this should not be used as an argument against the employment of a virtual profile. The virtual profile shows the *actual state of the case* and only points out the necessity, if an unexpected requirement for a full stoppage of trains at a critical point has developed, of changing the location (if a station), or of changing the grade by regrading or by using an overhead crossing. Examples of such modifications are given in Chapter XXIV, The Improvement of Old Lines.

434. Undulatory grades. Advantages. Money can generally be saved by adopting an actual profile which is not strictly uniform—the matter of compensation for curvature being here

#### GRADE.

ignored. Its effect on the operation of trains is harmless provided the sag or hump is not too great. In Fig. 214 the undulatory grade may actually be operated as a uniform grade AG. The sag at C must be considered as a sag, even though BC is actually an up grade. But the engine is supposed to be working



hard enough to carry a train at uniform velocity up a grade AG. Therefore it gains in velocity from B to C, and from C to D loses an equal amount. It may even be proven that the *time* required to pass the sag will be slightly less than the time required to run the uniform grade.

Disadvantages. The hump at F is dangerous in that, if the velocity at E is not equal to that corresponding to the extra velocity-head ordinate at F, the train will be stalled before reaching F. In practice there should be considerable margin. Any train should have a velocity of at least 10 miles per hour in passing any summit. This corresponds to a velocity head of 3.51 feet. An extra heavy head wind, slippery rails, etc., may use up any smaller margin and stall the train. If the grade AG is a ruling grade, then *no* hump should be allowed under any circumstances. For the heaviest trains are supposed to be so made up that the engine will *just* haul them up the ruling grades—of course with some margin for safety. Any increase of this grade, however short, would probably stall the train.

Safe limits. It is quite possible to have a sag so deep that it is not safe to allow freight trains to rush through them with-out the use of brakes. The use of brakes of course adds a distinct element of cost. To illustrate: If a freight train is running at a velocity of 20 miles per hour (velocity head 14.05 feet) and encounters a sag of 25 feet, the velocity head at the bottom of the sag will be 39.05 feet, which corresponds to a velocity of 33.3 miles per hour. This approaches the limit of safe speed for freight trains, and certainly passes the limit for trains not equipped with air-brakes and automatic couplers.

# § 434.

The term "safe limits" as used here, refers to the limits within which a freight train may be safely operated without the application of brakes or varying the work of the engine. Of course much greater undulations are frequently necessary and are safely operated, but it should be remembered that they add a distinct element to the cost of operating trains and that they must not be considered as harmless or that they should be introduced unless really necessary.

# MINOR GRADES.

435. Basis of cost of minor grades. The basis of the computation of this least objectionable form of grade is as follows: The resistance encountered by a train on a level straight track is somewhat variable, depending on the velocity and the number and character of the cars, but for average velocities we may consider that 10 lbs. per ton is a reasonable figure. This value agrees fairly well with the results of some dynamometer tests made by Mr. P. H. Dudley, using a passenger train of 313 tons running at about 50 miles per hour. It also agrees with the Engineering News formula (Eq. 143) for the resistance of a train at a velocity of 32 miles per hour. Ten pounds per ton is the grade resistance of a 0.5% grade, or that of 26.4 feet per mile. On the above basis, a 0.5% grade will just double the tractive resistance on a level straight track. We may compute, as in the previous chapter, the cost of doubling the tractive resistance for one mile. But since the extra resistance is due to lifting the train through 26.4 feet of elevation, we may divide the extra cost of a mile of 0.5% grade by 26.4 and we have the cost of one foot of difference of elevation, and then (disregarding the limiting effect of grades) we may say that this cost of one foot of difference of elevation will be independent of the rate of grade. There are, however, limitations to this general proposition which will be developed in the next section.

436. Classification of minor grades. These are classified with reference to their effect on the operation of trains. In the first class are grades which may be operated without changing the work of the engine and which have practically no other effect than a harmless fluctuation of the velocity. But a grade which belongs to this class when considering a fast passenger train will belong to another class when considering a slow but heavy freight train. And since it is the slow heavy freight trains which must be chiefly considered, a grade will usually be classified with respect to them. The limit of class A (the harmless

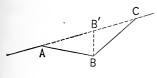


FIG. 215.

class) therefore depends on the maximum allowable speed. The effect of a sag on speed will depend on the vertical feet of drop rather than on the rate of grade, for with the engine working as usual on even a light down grade a train

would soon exceed permissible speed. Assume that a freight train runs at an average speed of 15 miles per hour with a minimum of 10 miles and a permissible maximum of 30 miles per hour. Assume that a train runs up the grade at A with a uniform velocity of 15 miles per hour, i.e., the engine is working so that the velocity would be uniform to C. How much sag (BB') can there be without the speed exceeding 30 miles per hour?

Velocity	head	for	30	miles	$\mathbf{per}$	hour	• • •		•••	 31.60
" "	" "	"	15	"	""	" "	•••	•••	•••	 7.90
The drop	5 <i>BB</i> ′	wil	1 th	nerefor	e be	e		••	•••	 23.70

While each case must be figured by itself, considering the probable velocity of approach and the maximum permissible velocity, we may say that a sag of *about* 24 feet will ordinarily mark the limit of this class. With a higher velocity of approach even this limit will be much reduced.

The classification therefore applies to sags and humps and to the vertical feet of drop or climb which are involved, rather than to grade *per se*. The practical application of these principles is necessarily confined to humps or sags which are possibly removable and does not apply to the long grades which are essential to connect predetermined points of the route---grades which are irreducible except by development and which must be studied as ruling grades (see §§ 440-445).

The application therefore consists in the comparative study of two proposed grades, noting the relative energy required to operate them and the probable cost. The depth in feet saved would be the maximum difference between the grades, and the classification will depend on the necessary method of operating the trains. The next classification (B) applies to drops so deep that steam must be shut off when descending the grade, while the work required of the engine when ascending the opposite grade is correspondingly increased. The loss is not so serious as in the next case, but the inability of the engine to work continuously may result in a failure to accumulate sufficient kinetic energy to carry the train over a succeeding summit.

The third class (C) includes the grades so long that brakes must be applied to prevent excessive velocity. The loss involved is very heavy; the brakes require power for their application, they wear the brake-shoes and wheel-tires, they destroy kinetic or potential energy which had previously been created, while the tax on the locomotive on the corresponding ascending grade is very great. The ascending grade may or may not be a ruling grade.

437. Effect on operating expenses. As in the previous chapter we may at once throw out a large proportion of the items of expense of an average train-mile. In "maintenance of way and structures," Items 2 to 6 will be variously affected according to the classification of grades. The other items are evidently unaffected.

Item 3. Renewals of ties. The extra wear of ties on grades is considered by Wellington as being somewhat compensated by the improved drainage of the roadbed which is found on a track which is not quite level, the better drainage tending to increase the life of the ties. On this account Wellington made an allowance of 5% increase for class C and no increase for the other classes.

Item 4. Renewals of rails. Observations of rail wear on heavy grades show that the wear is much greater than on level tangents. The heavy grades of a mountain division of a road are usually operated with shorter trains or with the help of pusherengines, and in such cases the proportion of engine tonnage to the total is much greater than on minor grades, and, since the engine has much greater effect on rail wear than an equal total tonnage of cars, partly on account of the use of sand and excess of engine tonnage, the grade will have a marked effect on rail wear. But such circumstances apply to ruling grades and very little, if at all, to minor grades. The use of sand on up-grades and the possible skidding of wheels on downgrades will wear the rails considerably. Even the slipping of the drivers, although sand is not used, will wear the rails. Wellington allows 10% increase for class C and 5% for class B.

Item 6. Roadway and track. It is very plain that a large proportion of the subitems are absolutely unaffected by minor grades. In fact it is a little difficult to ascribe any definite increase to any subitem. Rail wear is somewhat increased and this will have some effect in increasing the track-work. Wellington allows 5% increase as a liberal estimate for class C, and makes no allowance for classes A and B. Items 2 and 5 are allowed the same.

Maintenance of equipment. It is evident that none of these items will be affected except repairs and renewals and depreciation of road engines and cars. The chief effect on these items will evidently be the repairs and renewals of wheels and brakeshoes. The draw-bars are also apt to suffer somewhat, on account of the increased work which they are required to do. It would appear that the extra stress on the locomotive mechanism will have some effect on locomotive repairs, and the expense of boiler repairs may be increased on account of the greater range of the demands on it. It would seem as if such effects would be quite large, but if the records of engine and car repairs on mountain divisions and on comparatively level divisions of the same road are examined and compared, there appears to be no such difference as might be expected. Considering the very small proportion of locomotive and car repairs which are affected at all by such circumstances, and also the very small percentage of these subitems which can be said to be affected by these two classes of minor grades, Wellington allows only an increase of 4% on each of these four items for class C and 1%for class B. This is reasonable in view of the 19% allowed for grades and curvature (see § 406) of which 13% was estimated for curves, leaving only 6% for all grades.

Conducting transportation. It is apparent that the only items in conducting transportation which will be affected will be the four items of engine supplies (82 to 85). As in Chapter XXII, since we are considering that the resistance is doubled, we will assume that there is an increase of 44% as the cost of the extra fuel used in climbing 26.4 feet, but the total cost of both rise and fall is to be considered. In class *B*, although steam is shut off, fuel will be wasted by mere radiation. On this account we will add 5%. For class *C* we must allow in

addition the energy spent in applying the brakes, which we may assume as 5% more. Therefore we will allow 49% for class *B* and 54% for class *C*. The other small items of supplies, 83, 84, and 85, will be estimated similarly. The items of general

438. Estimate of cost of one foot of change of elevation. Collecting the above estimates we have Table XXIV, showing

expense are evidently unaffected.

TABLE XXIV.—EFFECT ON OPERATING EXPENSES OF 26.4 FEET OF RISE AND FALL.

			Clas	s B.	Class C.		
Item number	Item (abbreviated).	Normal average			Per cent affected	Cost per mile per cent.	
$\begin{array}{c}2\\3\\4\\5\\6\end{array}$	Ballast Ties Rails. Other track material. Roadway and track (All other items)	$\begin{array}{r} 0.50 \\ 3.10 \\ 0.92 \\ 1.13 \\ 7.53 \\ 6.91 \end{array}$	0 0 5 0 0 0	0 0.05 0 0 0	5 5 10 5 5 0	$\begin{array}{c} 0.02 \\ 0.15 \\ 0.09 \\ 0.06 \\ 0.38 \\ 0 \end{array}$	
	Maintenance of way	20.09		0.05		0.70	
25-27, 31-36, 43-45	{ Locomotives, passen- ger cars, freigh -cars and work-cars (All othe items)	$21.^{4}$ 1.50	10	0.21	<b>4</b> 0	0.85 0	
•	Maintenance of equip- ment	22.74		0.21		0.85	
53-60	Traffic	3.08	0	0	0	0	
82-85	Fuel and other supplies for road engines (All other items)	$\begin{array}{c}11.41\\39.03\end{array}$	49 0	5.59 0	$ \begin{array}{c} 54\\0 \end{array} $	6.16 0	
	Transportation	50.44		5.59		6.16	
106-116	General expenses	3.65	0	0	0	0	
		100.00		5.85		7.71	

that the percentage of *increase* for operating grades of classes B or C will be 5.85% and 7.71% respectively on the average cost of a train-mile. On the basis of an average cost of \$1.50 per train-mile, the additional cost for the 26.4 feet of rise and fall in one mile would be 8.77 c. and 11.56 c., or 0.33 c. and 0.44 c.

520

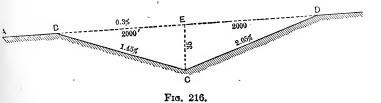
#### GRADE.

per foot for the two classes respectively. For each train per day each way per year the value per foot of difference of elevation is

> For class B:  $2 \times 365 \times \$0.0033 = \$2.41$ . For class C:  $2 \times 365 \times \$0.0044 = \$3.21$ .

In assuming the number of trains running over a given grade the character of the trains must be carefully considered, since it will quite frequently happen that a hump or sag must be classified as belonging to class C, so far as heavy freight-trains are concerned, but may be classified as B or perhaps even A, the harmless class, for passenger-trains. The above values should likewise be modified when the trains are run only 313 days per year instead of 365.

439. Operating value of the filling of a sag in a grade. Assume that the sag is 4000 feet long and that its depth in the center is 35 feet, as sketched in Fig. 216. Assume that a freight train is approaching the sag from the right-hand side (running to the left), the speed of passing D being 25 miles per hour. The 0.3% grade to the left will furnish a gravity pull of 6 pounds per ton, which may be more than half the force required to pull the train, and the locomotive would have but little to do, even if there were no sag, to maintain the speed of 25 miles per hour. Assuming that the locomotive is doing just this amount of work in running to the left through the sag, it will gain in velocity. Its velocity head at D is that corresponding to 25 miles per hour, or 21.95 feet. Adding 35 feet, the depth of the sag, we have 56.95 feet, which is the velocity head at C, which



means that the velocity of the train would be 40.3 miles per hour. For passenger trains this will not be an objectionably high velocity, and even freight trains, which are provided with air-brakes and standard M. C. B. couplers, which are now nearly universal, may be safely run at this velocity. Therefore for all trains which may run at a speed of over 40 miles per hour, this sag will belong to class A, or the harmless class, so far as trains moving to the left are concerned. The effect on trains moving to the right will depend partly on the rate of ruling grade on that section of the road. The conditions of class A pre-suppose that the draw-bar pull is *constant*, but horsepower is measured by the product of pull times velocity. Assume that AB is a ruling grade—0.3% has recently been adopted as ruling grade for revision work on the Erie R. R. Then, if 20 miles per hour were the speed of approach (running to the right) the speed at C would have to be 37.4 miles per hour. But since the draw-bar pull is to be constant, the horse-power

developed would have to be nearly doubled  $\left(\frac{37.4}{20}\right)$ . Since

this would be impossible, it would mean that such a sag would not only be a serious matter but would be prohibitive on a ruling grade. For ordinary roads, 0.3% will not be a ruling grade, and the possibility of temporarily increasing the horsepower developed by the locomotive while running through the sag, so that the draw-bar pull will remain constant, will be far greater. The ability to develop such horse-power is very apt to be the criterion as to whether a sag belongs to class A rather than the danger that the speed may be prohibitive. The criterion as to whether the grade belongs to class B or C for trains moving to the left, depends on whether brakes must be applied before reaching the bottom of the sag. A sharp curve at or near C might require the use of brakes to prevent a dangerous velocity. For trains moving to the right, there is no definite criterion between classes B and C, but a 2.05% grade is a very severe tax on a locomotive, especially when the assistance of momentum has been wasted by shutting off steam or by the Ignoring the possible limiting effect of application of brakes. a ruling grade (which is a separate matter) the value of the 35foot sag is evidently

 $35 \times \$2.41 = \$84.35$  per daily round-trip train for class B and

 $35 \times \$3.21 = \$112.35$  per daily round-trip train for class C.

Assume that there are six daily trains each way, for which the grade would be classified as grade B, and four others, for

#### GRADE.

which the sag would be classified as involving class C grade. Then on the above basis, the total annual cost would be

> $6 \times \$84.35 = \$506.10$  $4 \times \$112.35 = \$449.40$

# \$955.50

This annual cost capitalized at 5% equals \$19,110, which is the justifiable expenditure to fill up the sag. The amount of fill in such a sag, roughly calculated, is 125,000 cubic yards. Assuming that it would cost 30 c. per cubic yard to make the fill, this would require an expenditure of \$37,500, which apparently would not be justifiable.

But another solution may be considered. It has been shown above that a sag may be made harmless for all classes of trains provided the depth is not greater than some uncertain limit, which depends on the particular circumstances of the case. The volume of earth in this fill is great on account of the great depth in the center. It may be readily computed that by filling up the lower part of the sag so that its maximum depth below the grade line, BED, is about one-half of CE, or about 17 feet, that the amount of earthwork required will be only about 25,000 yards rather than 125,000 yards. This would make the cost of such a fill practically \$7500 rather than \$37,500. If it could be shown that a sag of about 18 feet could be operated on the class A basis by all trains, then it would certainly be justifiable to expend \$7500 in order to secure a reduction in the operating expenses, whose capitalized value according to the above calculation, is \$19,110.

#### RULING GRADES.

440. Definition. Ruling grades are those which limit the weight of the train of cars which may be hauled by one engine. The subject of "pusher grades" will be considered later. For the present it will suffice to say that on all well-designed roads the large majority of the grades on any one division are kept below some limit which is considered the ruling grade. If a heavier grade is absolutely necessary no special expense will be made to keep it below a rate where the resistance is twice

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(or possibly three times) the resistance on the ruling grade, and then the trains can be hauled unbroken up these few special grades with the help of one (or two) pusher engines. So far as limitation of train length is concerned, these pusher grades are no worse than the regular ruling grades and, except for the expense of operating the pusher engines (which is a separate matter), they are not appreciably more expensive than any ruling grade. As before stated, the engineer cannot alter very greatly the ruling grade of the road when the general route has been decided on. He may remove sags or humps, or he may lower the natural grade of the route by development in order to bring the grade within the adopted limit of ruling grade. The financial value of removing sags and humps has been considered. It now remains to determine the financial relation between the lowest permissible ruling grade and the morey which may profitably be spent to secure it.

441. Choice of ruling grade. It is of course impracticable for an engine to drop off or pick up cars according to the grades which may be encountered along the line. A train load is made up at one terminus of a division and must run to the other terminus. Excluding from consideration any short but steep grades which may *always* be operated by momentum, and also all pusher grades, the maximum grade on that division is the ruling grade.

It will evidently be economy to reduce the few grades which naturally would be a little higher than the great majority of others until such a large amount of grade is at some uniform limit that a reduction at all these places would cost more than it is worth. The precise determination of this limit is practically impossible, but an approximate value may be at once determined from a general survey of the route. The distance apart of the termini of the division into their difference of elevation is a first trial figure for the rate of the grade. If a grade even approximately uniform is impossible owing to the elevations of predetermined intermediate points, the worst place may be selected and the natural grade of that part of the route determined. If this grade is much steeper than the general run of the natural grades, it may be policy to reduce it by development or to boldly plan to operate that place as a pusher grade. The choice of possible grades thus has large limitations, and it justifies very close study to determine the best

combination of grades and pusher grades. When the choice has narrowed down to two limits, the lower of which may be obtained by the expenditure of a definite extra sum, the choice may be readily computed, as will be developed.

442. Maximum train load on any grade. The tractive power of a locomotive has been discussed in Chap. XV, § 322. The net train load which may be placed behind any engine is the difference between the weight of the engine itself and the gross load which can be handled under the given circumstances, with a given weight on the drivers. Since the design of locomotives is so variable, it is impracticable to show in tabular form the power of all kinds of locomotives on all grades. In Table XXV are given the tractive powers of locomotives of a wide range of types and weights and with various ratios of adhesion. They may be accepted as typical figures and will serve to compute the effect of variations of grade on train load. In Table XXVI is given the total train resistance in pounds per ton for various grades and for various values of track resistances. By a combination

TABLE XXV.---TRACTIVE POWER OF VARIOUS TYPES OF STANDARD-GAUGE LOCOMOTIVES AT VARIOUS RATES OF ADHESION.

Type of locomotive.	Total weight of engine and tender.		Weight of engine	Weight on the drivers.	Tractive power when ratio of adhesion is			
	Lbs.	Tons.	only.	unvers.	ł	<u>9</u> 40	1 B	
Atlantic, 4–4–2 Atlantic, 4–4–2, four	340,000	170.0	199,400	105,540	26,385	23,740	21,100	
cylinder compound Pacific, 4-6-2	$368,800 \\ 343,600$		$206,000 \\ 218,000$	$115,000 \\ 142,000$				
Pacific, $4-6-2$ Ten-wheel, $4-6-0$	$   \begin{array}{r}     403,780 \\     321,000   \end{array} $						$30,380 \\ 30,800$	
Prairie, 2–6–2 Consolidation, 2–8–0		107.0	120,000	106,000	26,500	23,850		
Consolidation, 2–8–0 Mikado, 2–8–2	366,700 405,500		221,500 259,000				39,500 39,200	

of these two tables the net train load on any grade under given conditions may be quickly determined For example, an ordinary consolidation engine having a weight of 106000 pounds on the drivers (see Table XXV) will have a tractive force of 26500 pounds under fair conditions of track, when the adhesion ratio is  $\frac{1}{4}$ . When climbing slowly up a grade of 1.30% the tractive resistance will be about 32 pounds per ton if the rolling-stock and track are fair—assuming a tractive resistance on a level of 6 pounds per ton. Dividing 26500 by 32 we have 828 tons, the gross train load. Subtracting 107 tons, the weight of the engine and tender in working order, we have 721 tons, the *net* load. Incidentally we may note that, cutting down the grade to 0.90% (a reduction of only 21.12 feet per mile), the resistance per ton is reduced to 24 pounds and the gross train load is increased to 1104 tons and the net load to 997 tons—an increase of about 38%.

As another numerical example, consider a contractor's locomotive (not referred to in Table XXV), a light four-wheel-connected-tank narrow-gauge engine, with a total weight of 12000 pounds, all on the drivers. On the rough temporary track used by contractors the tractive ratio may be as low as  $\frac{1}{5}$ . The tractive adhesion should therefore be taken as 2400 pounds. Assume that the grade when hauling "empties" is 4.7% and that the tractive resistance on such a track on a level is 10 pounds per ton. By Table XXVI, the total train resistance is therefore (by interpolation) 104 pounds per ton. 2400÷104=23 tons; subtracting the weight of the engine we have 17 tons, the net load of empty cars—perhaps twenty cars weighing 1700 pounds per car.

In general, and to compute accurately the train load under conditions not exactly given in the tables, the maximum train load at slow speed may be computed according to the following rule:

The maximum load behind an engine on any grade may be found by multiplying the weight on the drivers by the ratio of adhesion and dividing this by the sum of the grade and tractive resistances per ton; this gives the gross load, from which the weight of the engine and tender must be subtracted to find the net load.

443. Proportion of the traffic affected by the ruling grade. Some very light traffic roads are not so fortunate as to have a traffic which will be largely affected by the rate of the ruling grade. When passenger traffic is light, and when, for the sake of encouraging traffic, more frequent trains are run than are required from the standpoint of engine capacity, it may happen that no passenger trains are really limited by any grade on the road—i.e., an extra passenger car *could* be added if needed. The maximum grade then has no worse effect (for passenger trains) than to cause a harmless reduction of speed at a few points.

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Grade.		When tractive re- sistance on a level in pounds per ton is			Grade.		When tractive re- sistance on a level in pounds per ton is						
Rate per cent.	Feet per mile.	6	7	8	9	10	Rate per cent.	Feet per mile.	6	7.	8	9	10
$\begin{array}{r} \textbf{0.00} \\ .05 \\ .10 \\ .15 \\ .20 \\ \textbf{0.25} \end{array}$	$\begin{array}{r} 0.00 \\ 2.61 \\ 5.28 \\ 7.92 \\ 10.56 \\ 13.20 \end{array}$	6 7 8 9 10 11	$7 \\ 8 \\ 9 \\ 10 \\ 11 \\ 12$		$9 \\ 10 \\ 11 \\ 12 \\ 13 \\ 14$	$10 \\ 11 \\ 12 \\ 13 \\ 14 \\ 15$	$2.00 \\ .05 \\ .10 \\ .15 \\ .20 \\ 2.25$	$\begin{array}{c} 105.60 \\ 108.24 \\ 110.88 \\ 113.52 \\ 116.16 \\ 118.80 \end{array}$	$46 \\ 47 \\ 48 \\ 49 \\ 50 \\ 51$	$47 \\ 48 \\ 49 \\ 50 \\ 51 \\ 52$	$48 \\ 49 \\ 50 \\ 51 \\ 52 \\ 53$	49 50 51 52 53 54	$50 \\ 51 \\ 52 \\ 53 \\ 54 \\ 55$
$.30 \\ .35 \\ .40 \\ .45 \\ 0.50$	$15.84 \\ 18.48 \\ 21.12 \\ 23.76 \\ 26.40$	$12 \\ 13 \\ 14 \\ 15 \\ 16$	$13 \\ 14 \\ 15 \\ 16 \\ 17$	$14 \\ 15 \\ 16 \\ 17 \\ 18$	$15 \\ 16 \\ 17 \\ 18 \\ 19$	$16 \\ 17 \\ 18 \\ 19 \\ 20$	$\begin{array}{r} .30\\ .35\\ .40\\ .45\\ 2.50\end{array}$	$121.44 \\ 124.08 \\ 126.72 \\ 129.36 \\ 132.00$	$52 \\ 53 \\ 54 \\ 55 \\ 56$	$53 \\ 54 \\ 55 \\ 56 \\ 57 \\ 57 \\ $	54 55 56 57 58	55 56 57 58 59	56 57 58 59 60
.55 .60 .65 .70 0.75	$\begin{array}{r} 29.04 \\ 31.68 \\ 34.32 \\ 36.96 \\ 39.60 \end{array}$	$17 \\ 18 \\ 19 \\ 20 \\ 21$	$18 \\ 19 \\ 20 \\ 21 \\ 22$	$19 \\ 20 \\ 21 \\ 22 \\ 23$	$20 \\ 21 \\ 22 \\ 23 \\ 24$	$21 \\ 22 \\ 23 \\ 24 \\ 25$	.55 .60 .65 .70 2.75	$134.64 \\ 137.28 \\ 139.92 \\ 142.56 \\ 145.20$	$57 \\ 58 \\ 59 \\ 60 \\ 61$	$58 \\ 59 \\ 60 \\ 61 \\ 62$	$59 \\ 60 \\ 61 \\ 62 \\ 63$	$\begin{array}{c} 60 \\ 61 \\ 62 \\ 63 \\ 64 \end{array}$	$\begin{array}{c} 61 \\ 62 \\ 63 \\ 64 \\ 65 \end{array}$
$.80 \\ .85 \\ .90 \\ 0.95 \\ 1.00$	$\begin{array}{r} 42.24 \\ 44.88 \\ 47.52 \\ 50.16 \\ 52.80 \end{array}$	$22 \\ 23 \\ 24 \\ 25 \\ 26$	$23 \\ 24 \\ 25 \\ 26 \\ 27$	$24 \\ 25 \\ 26 \\ 27 \\ 28$	25 26 27 28 29	$26 \\ 27 \\ 28 \\ 29 \\ 30$	.80 .85 .90 .95 3.00	$^{\prime}147.84$ 150.48 153.12 155.76 158.40	$\begin{array}{c} 62 \\ 63 \\ 64 \\ 65 \\ 66 \end{array}$	$     \begin{array}{r}       63 \\       64 \\       65 \\       66 \\       67 \\     \end{array} $	$     \begin{array}{r}       64 \\       65 \\       66 \\       67 \\       68 \\     \end{array} $	$     \begin{array}{r}       65 \\       66 \\       67 \\       68 \\       69 \\     \end{array} $	66 67 68 69 70
$.05 \\ .10 \\ .15 \\ .20 \\ 1.25$	$\begin{array}{r} 55.44 \\ 58.08 \\ 60.72 \\ 63.36 \\ 65.00 \end{array}$	27 23 29 30 31	$28 \\ 29 \\ 30 \\ 31 \\ 32$	$29 \\ 30 \\ 31 \\ 32 \\ 33$	$30 \\ 31 \\ 32 \\ 33 \\ 34$	$31 \\ 32 \\ 33 \\ 34 \\ 35$	$.05 \\ .10 \\ .15 \\ .20 \\ 3.25$	$\begin{array}{r} 161.04 \\ 163.68 \\ 166.32 \\ 168.96 \\ 171.60 \end{array}$	$67 \\ 68 \\ 69 \\ 70 \\ 71$	$68 \\ 69 \\ 70 \\ 71 \\ 72$	69 70 71 72 73	$70 \\ 71 \\ 72 \\ 73 \\ 74$	$71 \\ 72 \\ 73 \\ 74 \\ 75$
$     \begin{array}{r}       .30 \\       .35 \\       .40 \\       .45 \\       1.50     \end{array} $	$\begin{array}{c} 68.64 \\ 71.28 \\ 73.92 \\ 76.56 \\ 79.20 \end{array}$	$32 \\ 33 \\ 34 \\ 35 \\ 36 \\ 36 \\ 36 \\ 31 \\ 32 \\ 30 \\ 30 \\ 30 \\ 30 \\ 30 \\ 30 \\ 30$	33 34 35 36 37	$34 \\ 35 \\ 36 \\ 37 \\ 38$	35 36 37 38 39	$36 \\ 37 \\ 38 \\ 39 \\ 40$	$ \begin{array}{r} .30\\.35\\.40\\.45\\3.50\end{array} $	$\begin{array}{r} 174.24 \\ 176.88 \\ 179.52 \\ 182.16 \\ 184.80 \end{array}$	$72 \\ 73 \\ 74 \\ 75 \\ 76$	73 74 75 76 77	74 75 76 77 78	75 76 77 78 79	76 77 78 79 80
.55 .60 .65 .70 1.75	$\begin{array}{r} 81.84\\ 84.48\\ 87.12\\ 89.76\\ 92.40\end{array}$	$37 \\ 38 \\ 39 \\ 40 \\ 41$	$38 \\ 39 \\ 40 \\ 41 \\ 42$	$39 \\ 40 \\ 41 \\ 42 \\ 43$	${ 40 \\ 41 \\ 42 \\ 43 \\ 44 }$	$     \begin{array}{r}       41 \\       42 \\       43 \\       44 \\       45     \end{array} $	$\begin{array}{r} 4.00 \\ 4.50 \\ 5.00 \\ 5.50 \\ 6.00 \end{array}$	$\begin{array}{c} 211.20\\ 237.60\\ 264.00\\ 290.40\\ 316.80\end{array}$	116	117	88 98 108 118 128	$\frac{109}{119}$	120
$     \begin{array}{r}       .80 \\       .85 \\       .90 \\       1.95 \\       2.00     \end{array} $	$\begin{array}{r} 95.04\\ 97.68\\ 100.32\\ 102.96\\ 105.60\end{array}$	$42 \\ 43 \\ 44 \\ 45 \\ 46$	$43 \\ 44 \\ 45 \\ 46 \\ 47$	$     \begin{array}{r}       44 \\       45 \\       46 \\       47 \\       48 \\     \end{array} $	$45 \\ 46 \\ 47 \\ 48 \\ 49$	$46 \\ 47 \\ 48 \\ 49 \\ 50$	$\begin{array}{c} 6.50 \\ 7.00 \\ 8.00 \\ 9.00 \\ 10.00 \end{array}$	$\begin{array}{r} 343.20\\ 369.60\\ 422.40\\ 475.20\\ 528.00\end{array}$	$146 \\ 166 \\ 186$	$\begin{array}{c} 167 \\ 187 \end{array}$	$138 \\ 148 \\ 168 \\ 188 \\ 208$	149 169 189	150 170 190

# TABLE XXVI.—TOTAL TRAIN RESISTANCE PER TON (OF 2000 POUNDS) ON VARICUS GRADES.

The local freight business is frequently affected in practically the same way. All coal, mineral, or timber roads are affected by the rate of ruling grade as far as such traffic is concerned. Likewise the through business in general merchandise, especially of the heavy traffic roads, will generally be affected by the rate of ruling grade. Therefore in computing the effect of ruling grade, the total number of trains on the road should not ordinarily be considered, but only the trains to which cars are added, until the limit of the hauling power of the engine on the ruling grades is reached.

444. Financial value of increasing the train load. The gross receipts for transporting a given amount of freight is a definite sum regardless of the number of train loads. The cost of a train mile is nearly constant. If it were exactly so, the saving in operating expenses would be strictly proportional to the number of trains saved. How will the cost per train mile vary when by a reduction in ruling grade more cars are handled in one train than before? First, compute the effect of increasing the train load so that one less engine will handle the traffic, or, for example, that an engine can haul 11 cars instead of 10 or 44 instead of 40-that 10 engines will do the work for which 11 engines would be required with the steeper grade. What will be the relative cost of running 10 heavy trains rather than 11 lighter trains, or, rather, what will be the extra cost of the extra engine?

We will estimate as before the difference in the cost of operating, say, four light trains on heavy grades, or three heavier trains on the lighter grades. In either case the gross tonnage of cars, with their contents, is supposed to be the same. The difference consists in the cost of operating the extra engine and also the extra cost for train service, etc., which is a function of the number of trains on the road rather than of their tonnage. The additional cost of maintenance of way is confined to the effect of the extra engine, and this will evidently effect only Items 2 to 6 and 9. On the basis that an engine produces one-half of the track deterioration, we may allow 50% of those items as the total effect on maintenance of way.

Maintenance of equipment. The effect on maintenance of equipment will be practically confined to the repairs, renewals, and depreciation of steam locomotives (Items 25 to 27) and the same items for freight-cars (Items 34 to 36). Very few roads have a passenger traffic which is affected by the rate of the ruling grade, since, for the encouragement of traffic, passenger-

trains are usually added to the schedule in advance of the physical capacity of a locomotive to haul one or more additional cars. Therefore, in general, no allowance need be made for any effect on passenger-trains, or on the maintenance of the passenger-cars. But the cost of maintaining the freight-cars is actually reduced by having more trains and less cars per train. This means that, although the maximum draw-bar pullwill be the same in both cases, and will equal the maximum capacity of the locomotive, while on the ruling grades, the draw-bar pull while on the light grades, level track and down grades, which may mean 90% of the length of the road, will average very much less. It is impossible to make an accurate estimate of the amount of this saving which would be generally applicable. Wellington estimated it at 10%. Considering the very large proportion of freight-car maintenance charges which are evidently independent of draw-bar pull, the estimate is probably large enough and the error in adopting that figure is not very great.

Although, for either system of grades, the locomotive is supposed to work to its full capacity while on the ruling grades. there is also some saving for each locomotive when hauling a lighter train over the light grades, level sections and down grades. If, on account of the reduction in average draw-bar pull, the repairs of each of four locomotives were reduced 5%below the repairs of the three locomotives which could haul the same number of cars over lower ruling grades, then the repairs of the four locomotives would cost  $4 \times 95$ , or 380 compared with  $3 \times 100$ , or 300 for the three locomotives. This would mean that the additional locomotive should be assigned an added expenditure of 80% of the average cost for one. Tf the saving by the reduction of grade was only half as much, or one train in eight, so that seven trains were required to do the work of eight on the steeper grade, then the saving per engine would be correspondingly less. If it were 2.5% instead of 5, we would have, for the cost of eight engines,  $8 \times 97.5$ , or 780 compared with  $7 \times 100$ , or 700 for the seven engines. Again, we would have 80% as the additional net cost of the repairs on the additional engine. Of course the above estimates of 5% and 2.5%, as the saving on one engine, are merely guesswork, but the above demonstration shows that if the saving in repairs is proportional to the reduction in number of trains which is

made possible by the reduction of grade, as is quite probable, then the cost of repairs of the extra engine is the same, whether it is one engine out of four, or one engine out of eight, or one engine out of any other number. Therefore, although the estimate of 5% per engine as made above is a guess, it is probably near enough to the truth, so that there is a comparatively little error in using the figure of 80% for the additional cost of repairs of the additional engine.

Conducting transportation. Items 61-79, chiefly yard work, will be practically unaffected. Items 80 and 81 will be given their full value. The additional cost for the fuel for the added engine may be computed somewhat on the same basis as the cost of engine repairs. The fuel used by four engines will average somewhat less than that used by three engines, since the four engines will do far less work on the level and on very light grades, while on the heavier grades the engines are working to the limit of their capacity in either case. The loss of heat, due to radiation and the other causes, which are independent of the direct work done by the engine in hauling, will be the same in either case. These causes have already been discussed in \$407. It is impossible to make any general calculations as to the relative consumption of fuel in the two cases, since so much depends on the proportion of track which is level or which has a very light grade. If the four engines operating lighter trains each burn 5% less fuel than three engines operating heavier trains, we will find, by the same method as before, that the extra engine may be charged with 80% of the average fuel consumption of the other three engines. If, as before, we assume that this variation in fuel consumption is proportional to the variation in the number of trains required to handle a given traffic, then the extra engine would be responsible for 80% of the average fuel consumption, regardless of whether the number of trains saved was one in four or one in ten. Although it is true that the value 80% is a mere guess, that no general value is obtainable, and that the value for any particular and special case could only be computed with great difficulty, it is evident that the error is not very great, and we will therefore assume 80% as the fuel consumption assignable to the extra engine. The consumption of other engine supplies, water, oil, waste, etc., is not strictly proportional to the con-

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sumption of fuel, but we will assume it to be so in this case, and that 80% of Items 83-85 are allowable for the extra engine.

Items 88 to 94, which concern train-service, will be considered as varying according to the number of train-miles, and we will therefore add 100% for all these items. Items 97 and 98 will be allowed 50%. Items 99, 101 to 103, which refer to damages, might be considered from one standpoint to be unaffected, while from other standpoints the effect might be considered as 100%. The risk of train operations varies very largely with the number of trains, and yet in some respects the danger is independent of whether there are 15 or 20 cars in a train. There will be little error in assigning 50% extra for this item. Items . 104 and 105 will be allowed 100% of their net value. The general expenses are evidently unaffected. Collecting these various items we have Table XXVII.

If we assume that the average cost of a train-mile is \$1.50, then the operating value per mile of saving the use of the additional engine equals 41.63% of \$1.50, or 62.45 c.

445. Operating value of a reduction in the rate of the ruling grade. As a practical application of the above figures, assume that on a constructed and operated road the ruling grade on a 100-mile division is 1.6%; the actual traffic affected by ruling grade is 8 daily trains with a net load of 552 tons or 4416 tons. It is found that with an expenditure of \$400,000 the ruling grade may be reduced to 1.2%. Will it pay? At 1.2% grade the net load behind an 80-ton consolidation engine, with 48 tons on the drivers, adhesion  $\frac{1}{4}$ , and 6 pounds per ton normal resistance, is 720 tons. The traffic (4416 tons) may therefore be hauled by 6 engines, the balance, less than 100 tons, being taken care of by lighter trains not affected by the ruling grade. There is therefore the saving due to not operating two engines. Since the additional cost of the two engines drawing lighter trains is 62.45 c. per mile, the annual saving is therefore  $2 \times \$0.6245 \times 100$  $\times 365 = $45,588.50$ , which capitalized at 5% = \$911,770. This shows that if the improvement can be accomplished for \$400,000 it is worth while.

As in other similar problems, it must be reiterated that although there are some more or less uncertain elements in the above estimates, yet with a considerable margin for error in

## RAILROAD CONSTRUCTION.

# TABLE XXVII. ADDITIONAL COST OF OPERATING A GIVEN FREIGHT TONNAGE WITH (n+1) ENGINES ON HEAVY RULING GRADES INSTEAD OF WITH n ENGINES ON LIGHTER GRADES.

Item number.	Item (abbreviated).	Normal average.	Per cent affected.	Cost per mile, per cent.
2 3 4 5 6 9	Ballast, Ties, Rails, Other track material, Roadway and track, Bridges, trestles and culverts	14.89	50	7.45
v	(All other items)	5.20	0	0
	Maintenance of way	20.09		7.45
25–27 34–36	Steam locomotives Freight cars	$8.61 \\ 10.15 \\ 3.98$		$-{}^{6.89}_{-1.01}_{0}$
	Maintenance of equipment	22.74		5.88
53-60	Traffic	3.08	0	0
80 81 82-85	Road enginemen Enginehouse expenses, road Fuel, and other supplies for road	$\begin{array}{r} 6.08 \\ 1.72 \end{array}$	100 100	$\begin{array}{c} 6.08 \\ 1.72 \end{array}$
88–94 97, 98 99, 101,	engines Train service, etc Stationery, printing, etc	${\begin{array}{r}11.41\\9.66\\0.57\end{array}}$	80 100 50	$9.13 \\ 9.66 \\ 0.28$
103 104, 105	Loss, damage, etc Operating joint tracks, <i>net</i> (All other items)	$2.82 \\ 0.02 \\ 18.16$	$\begin{smallmatrix} 50\\100\\0\end{smallmatrix}$	$\begin{array}{c} 1.41\\ 0.02\\ 0 \end{array}$
	Transportation	50.44		28.30
<b>1</b> 06–116	General expenses	3.65	0	0
		100.00		41.63

individual items the value of the whole improvement will not be very greatly altered and the estimate will be infinitely better than an indefinite reliance on vague "judgment." Of course certain items in the above estimates are somewhat variable and should be altered to fit the particular case to be computed.

#### PUSHER GRADES.

446. General principles underlying the use of pusher engines. On nearly all roads there are some grades which are greatly in excess of the general average rate of grade and these heavy

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grades cannot usually be materially reduced without an expenditure which is excessive and beyond the financial capacity of the road. If no pusher engines are used, the length of all heavy trains is limited by these grades. The financial value of the reduction of such ruling grades has already been shown. But in the operation of pusher grades there is incurred the additional cost of pusher-engine service, for a pusher engine must run twice over the grade for each train which is assisted. It is possible for this additional expense to equal or even exceed the advantage to be gained. In any case it means the adoption of the lesser of two evils, or the adoption of the more economical method. A simple example will illustrate the point. Assume that at one point on the road there is a grade of 1.9% which is five miles long. Assume that all other grades are less than 0.92%. If pushers are not to be used the net capacity of a 107-ton consolidation engine with 53 tons on the drivers, assuming  $\frac{9}{40}$  adhesion and 6 pounds per ton for normal resistance, will be 435 tons, and that will be the maximum weight of train allowable. By using pusher engines on this one 5-mile grade the train load is at once doubled and the number of trains cut down one half. This double load, 870 tons, can easily be hauled by one engine up the 0.92% grades. As a rough comparison, free from details and allowances, we may say:

(a) 10 trains per day over a 100-mile division, 435 tons net per train, will require 1000 engine miles daily.

(b) 5 trains per day handling the same traffic, 870 tons net per train, with  $2 \times 5 \times 5$  pusher-engine miles, will require  $(5 \times 100) + (2 \times 5 \times 5) = 550$  engine miles daily. There is thus a large saving in the number of engine miles and also in the number of the engines required for the work. Moreover, the engines are working to the limit of their capacity for a much larger proportion of the time, and their work is therefore more economically done. The work of overcoming the normal resistances of so many loaded cars over so many miles of track and of lifting so many tons up the gross differences of elevation of predetermined points of the line is approximately the same whatever the exact route, and if the grades are sc made that fewer engines working more constantly can accomplish the work as well as more engines which are not hard worked for a considerable proportion of the time, the economy is very apparent and unquestionable. Wellington expresses it concisely: "It is a truth of the first importance that the objection to high gradients is not the work which the engines have to do on them, but it is the work which they do *not* do when they thunder over the track with a light train behind them, from end to end of a division, in order that the needed power may be at hand at a few scattered points where alone it is needed."

447. Balance of grades for pusher service. In the above illustration the "through" grade and the "pusher" grade are "balanced" for the use of one equal pusher. It is therefore evident that if some intermediate grade (such as 1.4%) were permitted, it could only be operated by (a) making it the ruling grade and cutting down all train loads from 870 tons to 594 tons. or (b) operating it as a pusher grade, although with a loss of economy, since two engines would have much more power than necessary. The proper plan in such a case would be to strive to reduce the 1.4% grade to 0.92%, or, if that seemed impracticable, to attempt to get an operating advantage at the expense of an increase of the 1.4% grade to anything short of 1.9%. For the increase in rate of grade would cost almost nothing, and some advantage might be obtained which would practically compensate for the introduction of a pusher grade. Another possible solution would be to operate the 1.9% with two pushers. adopt a corresponding grade for use with one pusher and a corresponding ruling grade for through trains. With the above data these three grades would be 1.90% 1.27%, and 0.54%, obtained as follows:

Tractive power of three engines =  $106000 \times \frac{9}{40} \times 3 = 71550$  pounds.

Resistance on 1.9% grade =  $6 + (20 \times 1.9) = 44$  lbs. per ton.  $71550 \div 44 = 1626 = \text{gross load in tons.}$ 

 $1626 - (3 \times 107) = 1305 = \text{net load in tons.}$ 

 $1305 + (2 \times 107) = 1519 =$ gross load on the one-pusher grade. Tractive power of two engines = 47700 lbs.

 $47700 \div 1519 = 31.40 =$  possible tractive force in lbs. per ton.  $(31.40-6) \div 20 = 1.27\% =$  permissible grade for one pusher.

1305 + 107 = 1412 = gross load on the through grade.

Tractive power of one engine = 23850 lbs.

 $23850 \div 1412 = 16.89 = \text{possible tractive force in lbs. per ton.}$  $(16.89-6) \div 20 = 0.54\% = \text{permissible through grade.}$ 

#### GRADE.

It should be realized that, assuming the accuracy of the normal resistance (6 lbs.) and the normal adhesion  $\binom{9}{4^{7}0}$  and with the use of 107-ton locomotives with 53 tons on the drivers, the above figures are *precisely* what is required for hauling with one, two, and three engines. Other types of engines, other values for resistance and adhesion will vary considerably the gross load in tons which may be hauled up those grades, but starting with 0.54% as a through grade, the corresponding values for one and for two pushers would vary but slightly from those given. To show the tendency of these variations, the corresponding values have been computed as follows:

Adhesion.	Resistance per ton.	Load on drivers.	Through grade.	One-pusher grade.	Two-pusher grade.
90 40 40 40	$\begin{array}{c} 6 \ \text{lbs.} \\ 7 \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \$	53 tons. 53 '' 53 '' 53 '' 53 ''	$0.54\% \\ .54\% \\ .54\% \\ .54\% \\ .54\% \\ .54\% \\ .54\%$	$1.27\% \\ 1.31\% \\ 1.28\% \\ 1.26\% \\ 1.29\% $	$1.90\% \\ 1.96\% \\ 1.93\% \\ 1.86\% \\ 1.92\% \\ 1.92\%$

The above form shows that *increasing* the resistance per ton and *decreasing* the adhesion have opposite effects on altering the ratio of these grades, and as a storm, for example, would increase the resistance and decrease the adhesion, the changes in the ratio would be compensating although the absolute reduction in train load might be considerable.

In Table XXVIII is shown a series of "balanced" grades on which a given *net* train load may be operated by means of one or two pusher engines. For example, assuming a track resistance of 6 pounds per ton, a consolidation engine of the type shown in the table can haul a train weighing 977 tons (exclusive of the engine) up a grade of 0.80%. If this is the maximum *through* grade, pusher grades as high as 1.70% for one pusher, or 2.46% for two pushers, may be introduced and the same *net* load may be hauled up these grades.

The ratios of pusher grade to through grade, as given in Table XXVIII, are exactly true only for the conditions named as to weight and type of engine, ratio of adhesion, and norma track resistance. But a little comparative study of the two

# § 447.

# TABLE XXVIII.—BALANCED GRADES FOR ONE, TWO, AND THREE ENGINES.

Basis.—Through and pusher engines alike; consolidation type; total weight, 107 tons; weight on drivers, 53 tons; adhesion,  $\frac{2}{30}$ , giving a tractive force for each engine of 23850 lbs.; normal track resistance, 6 (also 8) lbs. per ton.

	Track r	esistance,	6 lbs.	Track r	Track resistance, 8 lbs.			
Through grade.	<i>Net</i> load for one engine in	ne same net load.		Net load for one engine in	Corresponding pusher grade for same net load.			
	tons (2000 lbs.).	One pusher.			One pusher.	Two pushers.		
Level. 0.10% 0.20% 0.30% 0.40%	$\begin{array}{c} 3868 \ {\rm tons} \\ 2874 \ \ {}^{\prime\prime} \\ 2278 \ \ {}^{\prime\prime} \\ 1880 \ \ {}^{\prime\prime} \\ 1596 \ \ {}^{\prime\prime} \end{array}$	$\begin{array}{c} 0.28\% \\ 0.47\% \\ 0.66\% \\ 0.84\% \\ 1.02\% \end{array}$	$0.55\% \\ 0.82\% \\ 1.08\% \\ 1.33\% \\ 1.57\%$	2874 tons 2278 '' 1880 '' 1596 '' 1384 ''	$\begin{array}{c} 0.37\% \\ 0.56\% \\ 0.74\% \\ 0.92\% \\ 1.09\% \end{array}$	$\begin{array}{c} 0.72\%\\ 0.98\%\\ 1.23\%\\ 1.47\%\\ 1.70\%\end{array}$		
$\begin{array}{c} 0.50\% \\ 0.60\% \\ 0.70\% \\ 0.80\% \\ 0.90\% \end{array}$	1384 '' 1218 '' 1085 '' 977 '' 887 ''	$1.19\% \\ 1.37\% \\ 1.54\% \\ 1.70\% \\ 1.87\% \\ 1.87\% \\$	$1.80\% \\ 2.02\% \\ 2.24\% \\ 2.46\% \\ 2.66\%$	1218 '' 1085 '' 977 '' 887 '' 810 ''	$1.27\% \\ 1.44\% \\ 1.60\% \\ 1.77\% \\ 1.93\%$	$1.92\% \\ 2.14\% \\ 2.36\% \\ 2.56\% \\ 2.76\%$		
$\begin{array}{c} 1.00\% \\ 1.10\% \\ 1.20\% \\ 1.30\% \\ 1.40\% \end{array}$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	2.03% 2.19% 2.34% 2.50% 2.65%	$\begin{array}{r} 2.86\% \\ 3.06\% \\ 3.25\% \\ 3.43\% \\ 3.61\% \end{array}$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{r} 2.09\% \\ 2.24\% \\ 2.40\% \\ 2.55\% \\ 2.70\% \end{array}$	$\begin{array}{r} 2.96\% \\ 3.15\% \\ 3.33\% \\ 3.51\% \\ 3.68\% \end{array}$		
$\begin{array}{c} 1.50\% \\ 1.60\% \\ 1.70\% \\ 1.80\% \\ 1.90\% \end{array}$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{r} 2.80\% \\ 2.95\% \\ 3.09\% \\ 3.23\% \\ 3.37\% \end{array}$	$\begin{array}{r} 3.78\%\\ 3.95\%\\ 4.12\%\\ 4.27\%\\ 4.43\%\end{array}$	$\begin{array}{c} 521 & ``\\ 489 & ``\\ 461 & ``\\ 435 & ``\\ 411 & ``\end{array}$	$\begin{array}{c} 2.85\% \\ 2.99\% \\ 3.13\% \\ 3.27\% \\ 3.42\% \end{array}$	$\begin{array}{r} 3.85\% \\ 4.02\% \\ 4.17\% \\ 4.33\% \\ 4.49\% \end{array}$		
$\begin{array}{c} 2.00\% \\ 2.10\% \\ 2.20\% \\ 2.30\% \\ 2.40\% \\ 2.50\% \end{array}$	411 '' 390 '' 370 '' 352 '' 335 '' 319 ''	$\begin{array}{c} 3.52\%\\ 3.65\%\\ 3.78\%\\ 3.91\%\\ 4.04\%\\ 4.17\%\end{array}$	$\begin{array}{r} 4.59\% \\ 4.73\% \\ 4.88\% \\ 5.02\% \\ 5.15\% \\ 5.29\% \end{array}$	390 '' 370 '' 352 '' 335 '' 319 '' 304 ''	3.55% 3.68% 3.81% 3.94% 4.07% 4.20%	$\begin{array}{r} 4.63\% \\ 4.78\% \\ 4.92\% \\ 5.05\% \\ 5.19\% \\ 5.32\% \end{array}$		

halves of Table XXVIII and of the tabular form given on page 535 will show that although the net load which can be hauled on any grade varies considerably with the normal track resistance and also with the ratio of adhesion, yet the *ratios* of through to pusher grade, for either one or two pushers, varies but slightly with ordinary changes in these conditions. Therefore when the precise conditions are unknown or variable, the

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figures of Table XXVIII may be considered as applicable to any ordinary practice, especially for preliminary computations. For final calculations on any proposed ruling grade and pusher grade, the whole problem should be worked out on the principles outlined above and on the basis of the best data obtainable.

**Problem:** If the through ruling grade for the road has been established at 1.12%, what pusher grades are permissible? Answer: Interpolating in Table XXVIII, we may employ a grade of 2.22% if the track and road-bed are to be such that a tractive resistance of 6 pounds per ton can be expected. With a poorer track, the normal resistance assumed as 8 pounds per ton, the rate is raised to 2.27%. The *increase* in rate of pusher grade with increase of resistance is due to the fact that the net load hauled is less—so much less that on the pusher grade a larger part of the adhesion is available to overcome a grade resistance.

448. Operation of pusher engines. The maximum efficiency in operating pusher engines is obtained when the pusher engine is kept constantly at work, and this is facilitated when the pusher grade is as long as possible, i.e., when the heavy grades and the great bulk of the difference of elevation to be surmounted is at one place. For example, a pusher grade of three miles followed by a comparatively level stretch of three miles and then by another pusher grade of two miles cannot all be operated as cheaply as a continuous pusher grade of five miles. Either the two grades must be operated as a continuous grade of eight miles (sixteen pusher miles per trip) or else as two short pusher grades, in which case there would be a very great loss of time and a difficulty in so arranging the schedules that a train need not wait for a pusher or the pushers need not waste too much time in idleness waiting for trains. If the level stretch were imperative, the two grades would probably be operated as one, but an effort should be made to bring the grades together. Tt is not necessary to bring the trains to a stop to uncouple the pusher engine, but a stop is generally made for coupling on, and the actual cost in loss of energy and in wear and tear of stopping and starting a heavy train is as great as the cost of running an engine light for several miles.

There are two ways in which it is *possible* to economize in the use of pusher engines. (a) When the traffic of a road is so very light that a pusher engine will not be kept reasonably busy on the pusher grade it may be worth while to place a siding long enough for the longest trains both at top and bottom of the pusher grade and then take up the train in sections. Perhaps the worst objection to this method is the time lost while the engine runs the extra mileage, but with such very light traffic roads a little time more or less is of small consequence. On light traffic roads this method of surmounting a heavy grade will be occasionally adopted even if pushers are never used. If the traffic is fluctuating, the method has the advantage of only requiring such operation when it is needed and avoiding the purchase and operation of a pusher engine which has but little to do and which might be idle for a considerable proportion of the year. (b) The second possible method of economizing is only practicable when a pusher grade begins or ends at or near a station yard where switching-engines are required. In such cases there is a possible economy in utilizing the switchingengines as pushers, especially when the work in each class is small, and thus obtain a greater useful mileage. But such cases are special and generally imply small traffic.

A telegraph-station at top and bottom of a pusher grade is generally indispensable to effective and safe operation.

449. Length of a pusher grade. The virtual length of the pusher grade, as indicated by the mileage of the pusher engine, is always somewhat in excess of the true length of the grade as shown on the profile, and sometimes the excess length is very great. If a station is located on a lower grade within a mile or so of the top or bottom of a pusher grade, it will ordinarily be advisable to couple or uncouple at or near the station, since the telegraph-station, switching, and signaling may be more economically operated at a regular station. If the extra engine is coupled on ahead of the through engine (as is sometimes required by law for passenger trains) the uncoupling at the top of the grade may be accomplished by running the assistant engine ahead at greater speed after it is uncoupled, and, after running it on a siding, clearing the track for the train. But this requires considerable extra track at the top of the grade. Therefore, when estimating the length of the pusher grade, the most desirable position for the terminal sidings must be studied and the length determined accordingly rather than by measuring the mere length of the grade on the profile. Of course these odd distances are always *excess*; the coupling or uncoupling should not be done while on the grade.

450. The cost of pusher-engine service. When we analyze the elements of cost, we will find that many of them are dependent only on time, while others are dependent upon mileage. Still others are dependent on both. Very much will depend on the constancy of the service, and this in turn depends on the train schedule and on a variety of local conditions which must be considered for each particular case. The effect of a pusherengine on maintenance of way may be considered to be the same as the cost of an additional engine to handle a given traffic, as developed in § 198. The same total allowance for the expenses of maintenance of way (7.45%) will therefore be made. Although the cost of repairs and renewals of engines is evidently a function of the mileage, and would therefore be somewhat less for a pusher-engine which did little work than for an engine which was worked to the limit of its capacity, yet it is only safe to make the same allowance as for other engines. Other items of maintenance of equipment are evidently to be ignored. The item of wages of enginemen will evidently depend upon the system employed on the particular road. Whatever the precise system the general result is to pay the enginemen as much in wages as the average payment for regular service, and therefore the full allowance for Item 80 will be made. Similarly we must allow the full cost of the items for engine supplies. While the engine is doing its heavy work in climbing up the grade, the consumption of fuel and water is certainly greater than the average; but, on the other hand, on the return trip, when the engine is running light, it probably runs for a considerable portion of the distance actually without steam, and therefore the consumption of fuel and water will nearly, if not quite, average the consumption for an engine running up and down grade along the whole line. That portion of fuel consumption which is due to radiation, blowing-off steam, and the many other causes previously enumerated, will be the same regardless of the work done. We therefore allow 100% for all of these items of engine supplies. In general we must add 100% for Items 90, 91, and 94, the cost of switchmen and telegraphic service. While there might be cases where there would be no actual addition

Item number.	Item (abbreviated).	Normal average.	Per cent affected.	Cost per engine mile, per cent.
2-6, 9 25-27 80, 81	Track material, labor, bridges Steam locomotives	$14.89\%\ 8.61$	$\begin{array}{c} 50\\100\end{array}$	$\begin{array}{c} 7.45 \\ 8.61 \end{array}$
82-85 90, 91,	house expenses Fuel and other engine supplies Signaling, flagmen, and tele-	$\begin{array}{c} 7.80 \\ 11.41 \end{array}$	$\begin{array}{c} 100 \\ 100 \end{array}$	$\begin{array}{c} 7.80\\11.41\end{array}$
194	graph	1.17	100	1.17
		•••••		45.05

## TABLE XXIX.—COST FOR EACH MILE OF PUSHER-ENGINE SERVICE.

to the pay-rolls or the operating expenses on account of these items, we are not justified in general in neglecting to add the full quota for such service. Collecting these items we will have 45.05% of the average cost of a train-mile for the cost of each mile run by the pusher engine. Using the same figure as before, \$1.50, for the cost of one train mile, we have 67.57 c. for each mile run.

451. Numerical comparison of pusher and through grades. In § 445 the computation was made of the desirability of reducing a 1.6% ruling grade to a 1.2% grade. Suppose it is found that by keeping the 1.6% grades as pusher grades having a total length of 20 miles on a 100-mile division, the other grades may be reduced to a grade not exceeding 0.713% (the corresponding through grade) for an expenditure of \$200,000. Will it pay? The saving by cutting down trains from 8 to 4, computed as before, would be (see § 445),  $4 \times \$0.6245 \times 100 \times 365 = \$91,177$ . But this saving is only accomplished by the employment of pushers making four round trips over 20 miles of pusher grades at a cost of  $4 \times 20 \times 2 \times 365 \times \$0.6757 = \$39,461$ .

The net annual saving is therefore \$51,716, which when capitalized at 5% = \$1,034,320.

The above estimate probably has this defect. The total daily pusher-engine mileage is but  $2 \times 4 \times 20 = 160$ , scarcely work enough for two pushers. Unless the pusher grades were bunched into two groups of about 10 miles each, two pusher engines could not do the work. If the number of trains was

much larger, then the above method of calculation would be more exact even though the 20 miles of pusher grade was divided among four or five different grades. Therefore with the above data the annual cost of the pusher service would probably be much more, say, \$60,000, and the annual saving about \$30,000, which would justify an expenditure of \$600,000. But even this would very amply justify the assumed expenditure of \$200,000 which would accomplish this result.

The above computation is but an illustration of the general truth which has been previously stated. In spite of the uncertainties and the variations of many items in the above estimates it will generally be possible to make a computation which will show unquestionably, as in the above instance, what is the best and the most economical method of procedure. When the capitalized valuations of both methods are so nearly equal that a proper choice is more difficult, the question will frequently be determined by the relative ease of raising additional capital.

#### BALANCE OF GRADES FOR UNEQUAL TRAFFIC.

452. Nature of the subject. It sometimes happens, as when a road runs into a mountainous country for the purpose of hauling therefrom the natural products of lumber or minerals, that the heavy grades are all in one direction-that the whole line consists of a more or less unbroken climb having perhaps a few comparatively level stretches, but no down grade (except possibly a slight sag) in the direction of the general up grade. With such lines this present topic has no concern. But the majority of railroads have termini at nearly the same level (500 feet in 500 miles has no practical effect on grade) and consist of up and down grades in nearly equal amounts and rates. The general rate of ruling grade is determined by the character of the country and the character and financial backing of the road to be built. It is always possible to reduce the grade at some point by "development" or in general by the expenditure of more money. It has been tacitly assumed in the previous discussions that when the ruling grade has been determined all grades in either direction are cut down to that If the traffic in both directions were the same this would limit. be the proper policy and sometimes is so. But it has developed.

especially on the great east and west trunk lines, that the weight of the eastbound freight traffic is enormously greater than that of the westbound-that westbound trains consist very largely of "empties" and that an engine which could haul twenty loaded cars up a given grade in eastbound traffic could haul the same cars empty up a much higher grade when running west. As an illustration of the large disproportion which may exist, the eastbound ton-mileage on the P. R. R. between the years 1851 and 1885 was 3.7 times the westbound ton-mileage. Between the years 1876 and 1880 the ratio rose to more than 4.5 to 1. On such a basis it is as important and necessary to obtain, say, a 0.6% ruling grade against the eastbound traffic as to have, say, a 1.0% grade against the westbound traffic. This is the basis of the following discussion. It now remains to estimate the probable ratio of the traffic in the two directions and from that to determine the proper "balance" of the opposite ruling grades.

453. Computation of the theoretical balance. Assume first, for simplicity, that the exact business in either direction is accurately known. A little thought will show the truth of the following statements.

1. The locomotive and passenger-car traffic in both directions is equal.

2. Except as a road may carry emigrants, the passenger traffic in both directions is equal. Of course there are innumerable individual instances in which the return trip is made by another route, but it is seldom if ever that there is any marked tendency to uniformity in this. Considering that a car load of, say, 50 passengers at 150 pounds apiece weigh but 7500 pounds, which is  $\frac{1}{6}$  of the 45000 pounds which the car may weigh, even a considerable variation in the number of passengers will not appreciably affect the hauling of cars on grades. On parlor-cars and sleepers the ratio of live load to dead load (say 20 passengers, 3000 pounds, and the car, 75000 pounds) is even more insignificant. The effect of passenger traffic on balance of grades may therefore be disregarded.

3. Empty cars have a greater resistance *per ton* than loaded cars. Therefore in computing the hauling capacity of a locomotive hauling so many tons of "empties," a larger figure must be used for the ordinary tractive resistances—say four pounds per ton greater.

4. Owing to greater or less imperfections of management a small percentage of cars will run empty or but partly full in the direction of greatest traffic.

5. Freight having great bulk and weight (such as grain, lumber, coal, etc.) is run from the rural districts toward the cities and manufacturing districts.

6. The return traffic—manufactured products—although worth as much or more, do not weigh as much.

As a simple numerical illustration assume that the weight of the cars is  $\frac{1}{3}$  and the live load  $\frac{2}{3}$  of the total load when the cars are "full"-although not loaded to their absolute limit of capacity. Assume that the relative weight of live load to be hauled in the other direction is but  $\frac{1}{3}$ ; assume that the grade against the heaviest traffic is 0.9%. Since the tractive resistance per ton is considerably greater in the case of unloaded cars than it is in the case of loaded cars, allowance must be made for this in calculating the train resistance. Mr. A. C. Dennis, of the Canadian Pacific Railway Company, has made some elaborate tests of train resistance for trains which were alternately loaded and empty, and found that the tractive resistance of loaded cars was very uniform at 4.7 pounds per ton, when the weight of the empty cars was  $\frac{1}{2}$  of the total weight. He also found that the tractive resistance of empty cars was very uniform at 8.9 pounds per ton. Although the live load capacity of a box-car is usually considerably more than twice the weight of the empty car, it will probably coincide more nearly with actual running conditions to consider that the live load is just twice the dead load. Assume that these loads are being hauled by a consolidation engine with a total weight, including engine and tender, of 107 tons, of which 106000 pounds is on the drivers. We will assume that the tractive resistance of the locomotive is likewise 4.7 pounds per ton. On the 0.9%grade, the grade resistance will be 18 pounds per ton, and therefore the total resistance is 22.7 pounds per ton. Assume that this engine is working with a tractive adhesion of  $\frac{1}{4}$ ; the tractive power at the circumference of the drivers will be 1 of 106000 pounds, or 26500 pounds. Dividing this by 22.7, we obtain 1167 as the gross load of the train in tons. Subtracting the weight of the locomotive, 107 tons, we have 1060 tons as the weight of the loaded cars which could be hauled by this locomotive up a 0.9% grade, assuming an adhesion of 1. Since

the traffic in the other direction is but  $\frac{1}{3}$ , we will assume that 3 of the return cars are empty. We then have 353 tons of loaded cars with a locomotive weighing 107 tons, and 236 tons of empty cars in the return train. The loaded cars with the locomotive will weigh 460 tons, and their tractive resistance will be 4.7 pounds per ton, or 2162 pounds. The 236 tons of empty cars will have a resistance of 8.9 pounds per ton, or a total tractive resistance of 2100 pounds. This makes a total of 4262 pounds of tractive resistance. Subtracting this from the 26500 of total adhesion of the drivers, we have left 22238 as the amount of pull available for grade. But the return train weighs 696 tons. Dividing this into 22238, we find that 32 pounds per ton is available for grade, which is the resistance on a 1.60% grade. Therefore, under the above conditions, a 0.9% grade against the heaviest traffic will correspond with a 1.60% grade against the lighter traffic.

Of course these figures will be slightly modified by variations in the assumptions as to the tractive resistance of loaded and unloaded cars, and more especially by variations in the ratio of live load to dead load in the two directions. Therefore no great accuracy can be claimed for the ratio of these two grades in opposite directions, nevertheless the above calculation shows unmistakably that under the given conditions, a very considerable variation in the rate of grade in opposite directions is not only justifiable, but a neglect to allow for it would be a great economic error.

454. Computation of relative traffic. Some of the principal elements have already been referred to, but in addition the following facts should be considered.

(a) The greatest disparity in traffic occurs through the handling of large amounts of coal, lumber, iron ore, grain, etc. On roads which handle but little of these articles or on which for local reasons coal is hauled one way and large shipments of grain the other way the disparity will be less and will perhaps be insignificant.

(b) A marked change in the development of the country may, and often does, cause a marked difference in the disparity of traffic. The heaviest traffic (in mere weight) is always toward manufacturing regions and away from agricultural regions. But when a region, from being purely agricultural or mineral, becomes largely manufacturing, or when a manufacturing region develops an industry which will cause a growth of heavy freight traffic from it, a marked change in the relative freight movement will be the result.

(c) Very great fluctuations in the relative traffic may be expected for prolonged intervals.

(d) An estimate of the relative traffic may be formed by the same general method used in computing the total traffic of the road (see § 373, Chap. XIX) or by noting the relative traffic on existing roads which may be assumed to have practically the same traffic as the proposed road will obtain.

# CHAPTER XXIV.

## THE IMPROVEMENT OF OLD LINES.

455. Classification of improvements. The improvements here considered are only those of alignment—horizontal and vertical. Strictly there is no definite limit, either in kind or magnitude, to the improvements which may be made. But since a railroad cannot ordinarily obtain money, even for improvements, to an amount greater than some small proportion of the previously invested capital, it becomes doubly necessary to expend such money to the greatest possible advantage. It has been previously shown that securing additional business and increasing the train load are the two most important factors in increasing dividends. After these, and of far less importance, come reductions of curvature, reductions of distance (frequently of doubtful policy, see Chap. XXI, § 414), and elimination of sags and humps. These various improvements will be briefly discussed.

(a) Securing additional business. It is not often possible by any small modification of alignment to materially increase the business of a road. The cases which do occur are usually those in which a gross error of judgment was committed during the original construction. For instance, in the early history of railroad construction many roads were largely aided by the towns through which the road passed, part of the money necessary for construction being raised by the sale of bonds, which were assumed or guaranteed and subsequently paid by the Such aid was often demanded and exacted by the towns promoters. Instances are not unknown where a failure to come to an agreement has caused the promoters to deliberately pass by the town at a distance of some miles, to the mutual disadvantage of the road and the town. If the town subsequently grew in spite of this disadvantage, the annual loss of business might readily amount to more than the original sum in dispute.

Such an instance would be a legitimate opportunity for study of the advisability of a re-location.

As another instance (the original location being justifiable) a railroad might have been located along the bank of a considerable river too wide to be crossed except at considerable expense. When originally constructed the enterprise would not justify the two extra bridges needed to reach the town. A growth in prosperity and in the business obtainable might subsequently make such extra expense a profitable investment.

(b) Increasing the train load. On account of its importance this will be separately considered in § 458 et seq.

(c) Reductions in curvature and distance and the elimination of sags and humps. The financial value of these improvements has already been discussed in Chapters XXI, XXII, and XXIII. Such improvements are constantly being made by all progressive roads. The need for such changes occurs in some cases because the original location was very faulty, the revised location being no more expensive than the original, and in other cases because the original location was the best that was then financially possible and because the present expanded business will justify a change.

(d) Changing the location of stations or of passing sidings. The station may sometimes be re-located so as to bring it nearer to the business center and thus increase the business done. But the principal reasons for re-locating stations or passing sidings is that starting trains may have an easier grade on which to overcome the additional resistances of starting. Such changes will be discussed in detail in § 460.

456. Advantages of re-locations. There are certain undoubted advantages possessed by the engineer who is endeavoring to improve an old line.

(a) The gross traffic to be handled is definitely known.

(b) The actual cost per train-mile for that road (which may differ very greatly from the average) is also known, and therefore the value of the proposed improvement can be more accurately determined.

. (c) The actual performance of such locomotives as are used on the road may be studied at leisure and more reliable data may be obtained for the computations.

457. Disadvantages of re-locations. The disadvantages are. generally more apparent and frequently appear practically insuperable—more so than they prove to be on closer inspection. (a) It frequently means the abandonment of a greater or less length of old line and the construction of new line. At first thought it might seem as if a change of line such as would permit an increase of train-load of 50 or perhaps 100% could never be obtained, or at least that it could not be done except at an impracticable expense. On the contrary a change of 10%of the old line is frequently all that is necessary to reduce the grades so that the train-loads hauled by one engine may be nearly if not quite doubled. And when it is considered that the cost of a road to sub-grade is generally not more than onethird of the total cost of construction and equipment per mile, it becomes plain that an expenditure of but a small percentage of the original outlay, expended where it will do the most good, will often suffice to increase enormously the earning capacity.

(b) One of the most difficult matters is to convince the financial backers of the road that the proposed improvement will be justifiable. The cause is simple. The disadvantages of the original construction lie in the large increase of certain items of expense which are necessary to handle a given traffic. And yet the fact that the expenditures are larger than they need be are only apparent to the expert, and the fact that a saving may be made is considered to be largely a matter of opinion until it is demonstrated by actual trial. On the other hand the cost of the proposed changes is definite, and the very fact that the road has been uneconomically worked and is in a poor financial condition makes it difficult to obtain money for improvements.

(c) The legal right to abandon a section of operated line and thus reduce the value of some adjoining property has sometimes been successfully attacked. A common instance would be that of a factory which was located adjoining the right of way for convenience of transportation facilities. The abandonment of that section of the right of way would probably be fatal to the successful operation of the factory. The objection may be largely eliminated by the maintenance of the old right of way as a long siding (although the business of the factory might not be worth it), but it is not always so easy of solution, and this phase of the question must always be considered.

#### REDUCTION OF VIRTUAL GRADE.

458. Obtaining data for computations. As developed in the last chapter (§§ 432-434) the real object to be attained is the reduction of the virtual grade. The method of comparing grades under various assumed conditions was there discussed. When the road is still "on paper" some such method is all that is possible; but when the road is in actual operation the virtual grade of the road at various critical points, with the rolling stock actually in use, may be determined by a simple test and the effect of a proposed change may be reliably computed. Bearing in mind the general principle that the virtual grade line is the locus of points determined by adding to the actual grade profile ordinates equal to the velocity head of the train. it only becomes necessary to measure the velocity at various points. Since the velocity is not usually uniform, its precise determination at any instant is almost impossible, but it will generally be found to be sufficiently precise to assume the velocity to be uniform for a short distance, and then observe the time required to pass that short space. Suppose that an ordinary watch is used and the time taken to the nearest second. At 30 miles per hour, the velocity is 44 feet per second. To obtain the time to within 1%, the time would need to be 100 seconds and the space 4400 feet. But with variable velocity there would be too great error in assuming the velocity as uniform for 4400 feet or for the time of 100 seconds. Using a stopwatch registering fifths of a second, a 1% accuracy would require but 20 seconds and a space of 880 feet, at 30 miles per hour. Wellington suggests that the space be made 293 feet 4 inches, or  $\frac{1}{18}$  of a mile; then the speed in miles per hour equals  $200 \div s$ , in which s is the time in seconds required to traverse the 293' 4". For instance, suppose the time required to pass the interval is 12.5 seconds.  $\frac{1}{18}$  mile in 12.5 seconds = one mile in 225 seconds, or 16 miles per hour. But likewise  $200 \div 12.5 = 16$ , the required velocity. The following features should be noted when obtaining data for the computations:

(a) All critical grades on the road should be located and their profiles obtained—by a survey if necessary.

(b) At the bottom and top of all long grades (and perhaps at intermediate points if the grades are very long) spaces of known

length (preferably  $293\frac{1}{3}$  feet) should be measured off and marked by flags, painted boards, or any other serviceable targets.

(c) Provided with a stop-watch marking fifths of seconds the observer should ride on the trains affected by these grades and note the exact interval of time required to pass these spaces. If the space is  $293\frac{1}{3}$  feet, the velocity in miles per hour  $=200 \div$  interval in seconds. In general,

# $V = \frac{\text{distance in feet} \times 3600}{\text{time in seconds} \times 5280}.$

(d) Since these critical grades are those which require the greatest tax on the power of the locomotive, the conditions under which the locomotive is working must be known-i.e., the steam pressure, point of cut-off, and position of the throttle. Economy of coal consumption as well as efficient working at high speeds requires that steam be used expansively (using an early cut-off), and even that the throttle be partly closed; but when an engine is slowly climbing up a maximum grade with a full load it is not exerting its maximum tractive power unless it has its maximum steam pressure, wide-open throttle, and is cutting off nearly at full stroke. These data must therefore be obtained so as to know whether the engine is developing at a critical place all the tractive force of which it is capable. The condition of the track (wet and slippery or dry) and the approximate direction and force of the wind should be noted with sufficient accuracy to judge whether the test has been made under ordinary conditions rather than under conditions which are exceptionally favorable or unfavorable.

(e) The train-loading should be obtained as closely as possible. Of course the dead weight of the cars is easily found, and the records of the freight department will usually give the live load with all sufficient accuracy.

459. Use of the data obtained. A very brief inspection of the results, freed from refined calculations or uncertainties, will demonstrate the following truths:

(a) If, on a uniform grade, the velocity increases, it shows that, under those conditions of engine working, the load is less than the engine can handle on that grade

(b) If the velocity decreases, it shows that the load is greater than the engine can handle on an indefinite length of such

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grade. It shows that such a grade is being operated by momentum. From the rate of decrease of velocity the maximum practicable length of such a grade (starting with a given velocity) may be easily computed.

(c) By combining results under different conditions of grade but with practically the same engine working, the tractive power of the engine may be determined (according to the principles previously demonstrated) for any grade and velocity. For example: On an examination of the profile of a division of a road the maximum grade was found to be 1.62% (85.54 feet per mile). At the bottom and near the top of this grade two lengths of 293' 4" are laid off. The distance between the centers of these lengths is 6000 feet. A freight train moving up the grade is timed at  $9\frac{2}{5}$  seconds on the lower stretch and  $7\frac{3}{5}$ seconds on the upper. These times correspond to  $\frac{200}{9.4}$  and  $\frac{200}{7.6}$ or 21.3 and 26.3 miles per hour respectively. It is at once observed that the velocity has increased and that the engine could draw even a heavier load up such a grade for an indefinite How much heavier might the load be? distance.

For simplicity we will assume that the conditions were normal, neither exceptionally favorable nor unfavorable, and that the engine was worked to its maximum capacity. The engine is a "consolidation" weighing 128700 pounds, with 112600 pounds on the drivers. The train-load behind the engine consists of ten loaded cars weighing 465 tons and eleven empties weighing 183 tons, thus making a total train-weight of 712 tons. Applying Eq. 140, we find that the *additional* force which the engine has actually exerted per ton in increasing the velocity from 21.3 to 26.3 miles per hour in a distance of 6000 feet is

$$P = \frac{70.224}{6000} (26.3^2 - 21.3^2) = 2.78 \text{ pounds per ton}$$

The grade resistance on a 1.62% grade is 32.4 pounds per ton. The average train resistance may be computed similarly to the method adopted in § 439:

465	tona	~ t	4 7				. 0.400	,
				pounds				
183	66	"	8.9	" "	"	"	=1629	" "
	"							
712							4115	" "

The average tractive resistance is therefore  $4115 \div 712 = 5.78$ pounds per ton. Adding the grade resistance (32.4) we have a total train resistance of 38.18 pounds per ton. But, computing from the increase in velocity, the locomotive is evidently exerting a pull of 2.78 pounds per ton in excess of the computed required pull on that grade, or a total pull of 40.96 pounds per ton. Therefore the train load might have been increased proportionately and might have been made

$$712 \times \frac{2.78 + 38.18}{38.18} = 764$$
 tons.

This shows that 52 tons additional might have been loaded on to the train, or say, three more empties or one additional loaded car.

A pull of 40.96 pounds per ton means a total adhesion at the drivers of 29164 pounds, which is about 26% of the weight on the drivers—112600 pounds. This indicates average conditions as to traction, although better conditions than can be depended on for regular service.

The above calculation should of course be considered simply as a "single observation." The performance of the same engine on the same grade (as well as on many other grades) on succeeding days should also be noted. It may readily happen that variations in the condition of the track or of the handling of the engine may make considerable variation in the results of the several calculations, but when the work is properly done it is always possible to draw definite and very positive deductions.

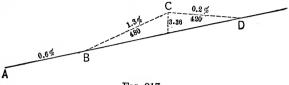
460. Reducing the starting grade at stations. The resistance to starting a train is augmented from two causes: (a) the tractive resistances are usually about 20 pounds per ton instead of, say, 6 pounds, and (b) the inertia resistance must be overcome. The inertia resistance of a freight train (see § 347) which is expected to attain a velocity of 15 miles per hour in a distance of 1000 feet is (see Eq. 140)

 $P = \frac{70.224}{1000}(15^2 - 0) = 15.8$  pounds per ton, which is the equiva-

lent of a 0.79% grade. Adding this to a grade which nearly or quite equals the ruling grade, it virtually creates a new and higher ruling grade. Of course that additional force can be greatly reduced at the expense of slower acceleration, but even

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this cannot be done indefinitely, and an acceleration to only 15 miles per hour in 1000 feet is as slow as should be allowed for. With perhaps 14 pounds per ton additional tractive resistance, we have about 30 pounds per ton additional—equiva-



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lent to a 1.5% grade. Instances are known where it has proven wise to create a hump (in what was otherwise a uniform grade) at a station. The effect of this on high-speed passenger trains moving up the grade would be merely to reduce their speed very slightly. No harm is done to trains moving down the grade. Freight trains moving up the grade and intending to stop at the station will merely have their velocity reduced as they approach the station and will actually save part of the wear and tear otherwise resulting from applying brakes. When the trains start they are assisted by the short down grade, just where they need assistance most. Even if the grade CDis still an up grade, the pull required at starting is less than that required on the uniform grade by an amount equal to 20 times the difference of the grade in per cent.

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# APPENDIX.

# THE ADJUSTMENTS OF INSTRUMENTS.

THE accuracy of instrumental work may be vitiated by any one of a large number of inaccuracies in the geometrical relations of the parts of the instruments. Some of these relations are so apt to be altered by ordinary usage of the instrument that the makers have provided adjusting-screws so that the inaccuracies may be readily corrected. There are other possible defects, which, however, will seldom be found to exist, provided the instrument was properly made and has never been subjected to treatment sufficiently rough to distort it. Such defects, when found, can only be corrected by a competent instrument-maker or repairer.

A WARNING is necessary to those who would test the accuracy of instruments, and especially to those whose experience in such work is small. Lack of skill in handling an instrument will often indicate an apparent error of adjustment when the real error is very different or perhaps non-existent. It is always a safe plan when testing an adjustment to note the amount of the apparent error; then, beginning anew, make another independent determination of the amount of the error. When two or more perfectly independent determinations of such an error are made it will generally be found that they differ by an appreciable The differences may be due in variable measure to amount. careless inaccurate manipulation and to instrumental defects which are wholly independent of the particular test being made. Such careful determinations of the amounts of the errors are generally advisable in view of the next paragraph.

Do NOT DISTURB THE ADJUSTING-SCREWS ANY MORE THAN NECESSARY. Although metals are apparently rigid, they are really elastic and yielding. If some parts of a complicated mechanism, which is held together largely by friction, are subjected to greater internal stresses than other parts of the mechanism, the jarring resulting from handling will frequently cause a slight readjustment in the parts which will tend to more nearly equalize the internal stresses. Such action frequently occurs with the adjusting mechanism of instruments. One screw may be strained more than others. The friction of parts may prevent the opposing screw from *immediately* taking up an equal Perhaps the adjustment appears perfect under these stress. conditions Jarring diminishes the friction between the parts. and the unequal stresses tend to equalize. A motion takes place which, although microscopically minute, is sufficient to indicate an error of adjustment. A readjustment made by unskillful hands may not make the final adjustment any more perfect. The frequent shifting of adjusting-screws wears them badly. and when the screws are worn it is still more difficult to keep them from moving enough to vitiate the adjustments. It is therefore preferable in many cases to refrain from disturbing the adjusting-screws, especially as the accuracy of the work done is not necessarily affected by errors of adjustment, as may be illustrated:

(a) Certain operations are *absolutely* unaffected by certain errors of adjustment.

(b) Certain operations are so slightly affected by certain *small* errors of adjustment that their effect may properly be neglected.

(c) Certain errors of adjustment may be readily allowed for and neutralized so that no error results from the use of the unadjusted instrument. Illustrations of all these cases will be given under their proper heads.

#### ADJUSTMENTS OF THE TRANSIT.

1. To have the plate-bubbles in the center of the tubes when the axis is vertical. Clamp the upper plate and, with the lower clamp loose, swing the instrument so that the plate-bubbles are parallel to the lines of opposite leveling-screws. Level up until both bubbles are central. Swing the instrument  $180^{\circ}$ . If the bubbles again settle at the center, the adjustment is perfect. If either bubble does not settle in the center, move the leveling-screws until the bubble is *half-way* back to the center. Then, before touching the adjusting-screws, note carefully the position of the bubbles and observe whether the bubbles always settle at the same place in the tube, no matter to what position the in-

strument may be rotated. When the instrument is so leveled, the axis is truly vertical and the discrepancies between this constant position of the bubbles and the centers of the tubes measure the errors of adjustment. By means of the adjustingscrews bring each bubble to the center of the tube. If this is done so skillfully that the true level of the instrument is not disturbed, the bubbles should settle in the center for all positions of the instrument. Under unskillful hands, two or more such trials may be necessary.

When the plates are not horizontal, the measured angle is greater than the true horizontal angle by the difference between the measured angle and its projection on a horizontal plane. When this angle of inclination is small, the difference is insignificant. Therefore when the plate-bubbles are very nearly in adjustment, the error of measurement of horizontal angles may be far within the lowest unit of measurement used. A small error of adjustment of the plate-bubble perpendicular to the telescope will affect the horizontal angles by only a small proportion of the error, which will be perhaps imperceptible. Vertical angles will be affected by the same insignificant amount. A small error of adjustment of the platebubble parallel to the telescope will affect horizontal angles very slightly, but will affect vertical angles by the full amount of the error.

All error due to unadjusted plate-bubbles may be avoided by noting in what positions in the tubes the bubbles will remain fixed for all positions of azimuth and then keeping the bubbles adjusted to these positions, for the axis is then truly vertical. It will often save time to work in this way temporarily rather than to stop to make the adjustments. This should especially be done when accurate vertical angles are required.

When the bubbles are truly adjusted, they should remain stationary regardless of whether the telescope is revolved with the upper plate loose and the lower plate clamped or whether the whole instrument is revolved, the plates being clamped together. If there is any appreciable difference, it shows that the two vertical axes or "centers" of the plates are not concentric. This may be due to cheap and faulty construction or to the excessive wear that may be sometimes observed in an old instrument originally well made. In either case it can only be corrected by a maker.

2. To make the revolving axis of the telescope perpendicular to the vertical axis of the instrument. This is best tested by using a long plumb-line, so placed that the telescope must be pointed upward at an angle of about  $45^{\circ}$  to sight at the top of the plumbline and downward about the same amount, if possible, to sight at the lower end. The vertical axis of the transit must be made truly vertical. Sight at the upper part of the line clamping the horizontal plates. Swing the telescope down and see if the cross-wire again bisects the cord. If so, the adjustment is probably perfect (a conceivable exception will be noted later); if not, raise or lower one end of the axis by means of the adjusting-screws, placed at the top of one of the standards, until the cross-wire will bisect the cord both at top and bottom. The plumb-bob may be steadied, if necessary, by hanging it in a pail of water. As many telescopes cannot be focused on an object nearer than 6 or 8 feet from the telescope, this method requires a long plumb-line swung from a high point, which may be inconvenient.

Another method is to set up the instrument about 10 feet from a high wall. After leveling, sight at some convenient mark high up on the wall. Swing the telescope down and make a mark (when working alone some convenient natural mark may generally be found) low down on the wall. Plunge the telescope and revolve the instrument about its vertical axis and again sight at the upper fnark. Swing down to the lower mark. If the wire again bisects it, the adjustment is perfect. If not, fix a point *half-way* between the two positions of the lower mark. The plane of this point, the upper point, and the center of the instrument is truly vertical. Adjust the axis to these upper and lower points as when using the plumb-line.

3. To make the line of collimation perpendicular to the revolving axis of the telescope. With the instrument level and the telescope nearly horizontal point at some well-defined point at a distance of 200 feet or more. Plunge the telescope and establish a point in the opposite direction. Turn the whole instrument about the vertical axis until it again points at the first mark. Again plunge to "direct position" (i.e., with the level-tube under the telescope). If the vertical cross-wire again points at the second mark, the adjustment is perfect. If not, the error is one-fourth of the distance between the two positions of the second mark. Loosen the capstan screw on one side of the telescope and tighten it on the other side until the vertical wire is set at the one-fourth mark. Turn the whole instrument by means of the tangent screw until the vertical wire is *midway* between the two positions of the second mark. Plunge the telescope. If the adjusting has been skillfully done, the crosswire should come exactly to the first mark. As an "erecting eyepiece" reinverts an image already inverted, the ring carrying the cross-wires must be moved in the same direction as the apparent error in order to correct that error.

The necessity for the third adjustment lies principally in the practice of producing a line by plunging the telescope, but when this is required to be done with great accuracy it is always better to obtain the forward point by reversion (as described above for making the test) and take the *mean* of the two forward points. Horizontal and vertical angles are practically unaffected by *small* errors of this adjustment, unless, in the case of horizontal angles, the vertical angles to the points observed are very different.

Unnecessary motion of the adjusting-screws may sometimes be avoided by carefully establishing the forward point on line by repeated reversions of the instrument, and thus determining by repeated trials the exact amount of the error. *Differences* in the amount of error determined would be evidence of inaccuracy in manipulating the instrument, and would show that an adjustment based on the first trial would *probably* prove unsatisfactory.

The 2d and 3d adjustments are mutually dependent. If either adjustment is badly out, the other adjustment cannot be made except as follows:

(a) The second adjustment can be made regardless of the third when the lines to the high point and the low point make equal angles with the horizontal.

(b) The third adjustment can be made regardless of the second when the front and rear points are on a level with the instrument.

When both of these requirements are *nearly* fulfilled, and especially when the error of either adjustment is small, no trouble will be found in perfecting either adjustment on account of a small error in the other adjustment.

If the test for the second adjustment is made by means of the plumbline and the vertical cross-wire intersects the line at all points as the telescope is raised or lowered, it not only demonstrates at once the accuracy of that adjustment, but also shows that the third adjustment is either perfect or has so small an error that it does not affect the second.

4. To have the bubble of the telescope-level in the center of the tube when the line of collimation is horizontal. The line of collimation should coincide with the optical axis of the telescope. If the object-glass and eyepiece have been properly centered, the previous adjustment will have brought the vertical cross-wire to the center of the field of view. The horizontal cross-wire should also be brought to the center of the field of view, and the bubble should be adjusted to it.

a. Peg method. Set up the transit at one end of a nearly level stretch of about 300 feet. Clamp the telescope with its bubble in the center. Drive a stake vertically under the eyepiece of the transit, and another about 300 feet away. Observe the height of the center of the eyepiece (the telescope being level) above the stake (calling it a); observe the reading of the rod when held on the other stake (calling it b); take the instrument to the other stake and set it up so that the eyepiece is vertically over the stake, observing the height, c; take a reading on the first stake, calling it d. If this adjustment is perfect, then

$$a-d=b-c,$$
  
or  $(a-d)-(b-c)=0.$   
Call  $(a-d)-(b-c)=2m.$   
When m is positive, the line points downward;  
" m " negative." " upward.

To adjust: if the line points up, sight the horizontal crosswire (by moving the vertical tangent screw) at a point which is m lower, then adjust the bubble so that it is in the center.

By taking several independent values for a, b, c, and d, a mean value for m is obtained, which is more reliable and which may save much unnecessary working of the adjusting-screws.

b. Using an auxiliary level. When a carefully adjusted level is at hand, this adjustment may sometimes be more easily made by setting up the transit and level, so that their lines of collimation are as nearly as possible at the same height. If a point may be found which is half a mile or more away and which is on the horizontal cross-wire of the level, the horizontal cross-wire of the transit may be pointed directly at it, and the bubble adjusted accordingly. Any slight difference in the heights of the lines of collimation of the transit and level (say  $\frac{1}{4}$  may almost be disregarded at a distance of  $\frac{1}{2}$  mile or more, or, if the difference of level would have an appreciable effect, even this may be practically eliminated by making an estimated allowance when sighting at the distant point. Or, if a distant point is not available, a level-rod with target may be used at a distance of (say) 300 feet, making allowance for the carefully determined difference of elevation of the two lines of collimation.

5. Zero of vertical circle. When the line of collimation is truly horizontal and the vertical axis is truly vertical, the reading of the vertical circle should be  $0^{\circ}$ . If the arc is adjustable, it should be brought to  $0^{\circ}$ . If it is not adjustable, the *index* error should be observed, so that it may be applied to all readings of vertical angles.

#### ADJUSTMENTS OF THE WYE LEVEL.

1. To make the line of collimation coincide with the center of the rings. Point the intersection of the cross-wires at some

well-defined point which is at a considerable distance. The instrument need not be level, which allows much greater liberty in choosing a convenient point. The vertical axis should be clamped, and the clips over the wyes should be loosened and raised. Rotate the telescope in the wyes. The intersection of the cross-wires should be continually on the point. If it is not, it requires adjustment. Rotate the telescope 180° and adjust one-half of the error by means of the capstan-headed screws that move the cross-wire ring. It should be remembered that, with an erecting telescope, on account of the inversion of the image, the ring should be moved in the direction of the apparent error. Adjust the other half of the error with the leveling-screws. Then rotate the telescope 90° from its usual position, sight accurately at the point, and then rotate 180° from that position and adjust any error as before. It may require several trials. but it is necessary to adjust the ring until the intersection of the cross-wires will remain on the point for any position of rotation.

If such a test is made on a very distant point and again on a point only 10 or 15 feet from the instrument, the adjustment may be found correct for one point and incorrect for the other. This indicates that the objectslide is improperly centered. Usually this defect can only be corrected by an instrument-maker. If the difference is very small it may be ignored, but the adjustment should then be made on a point which is at about the mean distance for usual practice—say 150 feet.

If the whole image appears to shift as the telescope is rotated, it indicates that the eyepiece is improperly adjusted. This defect is likewise usually corrected only by the maker. It does not interfere with instrumental accuracy, but it usually causes the intersection of the cross-wires to be eccentric with the field of view.

2. To make the axis of the level-tube parallel to the line of collimation. Raise the clips as far as possible. Swing the level so that it is parallel to a pair of opposite leveling-screws and clamp it. Bring the bubble to the middle of the tube by means of the leveling-screws. Take the telescope out of the wyes and replace it end for end, using *extreme care* that the wyes are not jarred by the action. If the bubble does not come to the center, correct one-half of the error by the vertical adjusting-screws at one end of the bubble. Correct the other half by the levelingscrews. Test the work by again changing the telescope end for end in the wyes.

Care should be taken while making this adjustment to see

that the level-tube is vertically under the telescope. With the bubble in the center of the tube, rotate the telescope in the wyes for a considerable angle each side of the vertical. If the first half of the adjustment has been made and the bubble moves, it shows that the axis of the wyes and the axis of the level-tube are not in the same vertical plane although both have been made horizontal. By moving one end of the level-tube *sidewise* by means of the horizontal screws at one end of the tube, the two axes may be brought into the same plane. As this adjustment is liable to disturb the other, both should be alternately tested until both requirements are complied with.

By these methods the axis of the bubble is made parallel to the axis of the wyes; and as this has been made parallel to the lines of collimation by means of the previous adjustment, the axis of the bubble is therefore parallel to the line of collimation.

3. To make the line of collimation perpendicular to the vertical axis. Level up so that the instrument is approximately level over both sets of leveling-screws. Then, after leveling carefully over one pair of screws, revolve the telescope 180° If it is not level, adjust half of the error by means of the capstan-headed screw under one of the wyes, and the other half by the leveling-screws. Reverse again as a test.

When the first two adjustments have been accurately made, good leveling may always be done by bringing the bubble to the center by means of the leveling-screws, at every sight if necessary, even if the third adjustment is not made. Of course this third adjustment should be made as a matter of convenience, so that the line of collimation may be always level no matter in what direction it may be pointed, but it is not necessary to stop work to make this adjustment every time it is found to be defective.

#### ADJUSTMENTS OF THE DUMPY LEVEL.

1. To make the axis of the level-tube perpendicular to the vertical axis. Level up so that the instrument is approximately level over both sets of leveling-screws. Then, after leveling carefully over one pair of screws, revolve the telescope 180°. If it is not level, adjust one-half of the error by means of the adjust-ing-screws at one end of the bubble, and the other half by means of the leveling-screws. Reverse again as a test.

2. To make the line of collimation perpendicular to the vertical axis. The method of adjustment is identical with that for the transit (No. 4, p. 505) except that the cross-wire must be

adjusted to agree with the level-bubble rather than vice versa, as is the case with the corresponding adjustment of the transit; i.e., with the level-bubble in the center, raise or lower the horizontal cross-wire until it points at the mark known to be on a level with the center of the instrument.

If the instrument has been well made and has not been distorted by rough usage, the cross-wires will intersect at the center of the field of view when adjusted as described. If they do not, it indicates an error which ordinarily can only be corrected by an instrument-maker. The error may be due to any one of several causes, which are

(a) faulty centering of object-slide;

(b) faulty centering of eyepiece;

(c) distortion of instrument so that the geometric axis of the telescope is not perpendicular to the vertical axis. If the error is only just perceptible, it will not probably cause any error in the work.

### EXPLANATORY NOTE ON THE USE OF THE TABLES,

The logarithms here given are "five-place," but the last figure sometimes has a special mark over it  $(e.g., \overline{6})$  which indicates that one-half a unit in the last place should be *added*. For example

the value .69586 .69586 .69586 .69586 .6958625000 + and .6958624999...

The maximum error in any one value therefore does not exceed one-quarter of a fifth-place unit.

When adding or subtracting such logarithms allow a half-unit for such a sign. For example

<b>•69586</b>	·69586	<b>•6958</b> 6
.10841	•1084 <b>Ī</b>	<b>.</b> 1084Ī
·12947	·12947	·12947
<b>.</b> 9337 <b>4</b>	-93375	·93375

All other logarithmic operations are performed as usual and are supposed to be understood by the student.

## TABLE I.-RADII OF CURVES.

	1		1		2° 3°					
Deg		0°		1°		2°		Deg		
Min	Radius.	Log R	Radius,	Log R	Radius,	Log R	Radius.	Log R	Min	
0 1 2 3 4 5	$\infty$ 343775 171887 114592 85944 68755	$ \begin{array}{c} \infty \\ 5.5362\overline{7} \\ 5.23524 \\ 5.0591\overline{5} \\ 4.9342\overline{1} \\ 4.8373\overline{0} \end{array} $	5729.6 5635.7 5544.8 5456.8 5371.6 5288.9	3.75813 .75095 .74389 .73694 .73010 .72336	2864.9 2841.3 2818.0 2795.1 2772.5 2750.4	$\begin{array}{r} 3.4571\overline{1}\\.4535\underline{1}\\.4499\overline{3}\\.44639\\.44639\\.4428\overline{7}\\.43939\end{array}$	1910.1 1899.5 1889.1 1878.8 1868.6 1858.5	$\begin{array}{r} 3 \cdot 28105 \\ \cdot 27864 \\ \cdot 27625 \\ \cdot 27387 \\ \cdot 27151 \\ \cdot 26915 \end{array}$	0 1 2 3 4 5	
6 7 8 9 10	57296 49111 42972 38197 34377	$\begin{array}{r} 4.7581\overline{2} \\ .6911\overline{7} \\ .63318 \\ .58203 \\ .5362\overline{7} \end{array}$	5208.85131.05055.64982.34911.2	3.7167 <u>3</u> .71020 .70377 .6974 <u>3</u> .69118	$\begin{array}{r} 2728.5 \\ 2707.0 \\ 2685.9 \\ 2665.1 \\ \underline{2644.6} \\ \end{array}$	$\begin{array}{r} 3.43593 \\ .43249 \\ .42909 \\ .42571 \\ .42235 \end{array}$	1848.5     1838.6     1828.8     1819.1     1809.6     1809.1     1809.1     1809.1     1809.5     1809.5     1809.5     1809.5     1809.5     1809.5     1809.5     1809.5     1809.5     1809.5     1809.5     1809.5     1809.5     1809.5     1809.5     1800	3.2668 2644 .26217 .2598 .25757	6 7 8 9 10	
$     \begin{array}{r}       11 \\       12 \\       13 \\       14 \\       15 \\       16 \\$	31252 28648 26444 24555 22918	4.49488 .45709 .42233 .39014 .36018	$\begin{array}{r} 4842.0 \\ 4774.7 \\ 4709.3 \\ 4645.7 \\ 4583.8 \\ 4522.4 \end{array}$	3.68502 .67895 .67296 .66705 .66122	$ \begin{array}{r} 2624.4 \\ 2604.5 \\ 2584.9 \\ 2565.6 \\ 2546.6 \\ \hline 25267.0 \\ \hline 2507.0 \\ 2$	$ \begin{array}{r} 3.41903\\.41572\\.41245\\.40919\\.40597\\\end{array} $	$   \begin{array}{r}     1800.1 \\     1790.7 \\     1781.5 \\     1772.3 \\     1763.2 \\     1754.2   \end{array} $	$ \begin{array}{r} 3 \cdot 25529 \\ \cdot 25303 \\ \cdot 25077 \\ \cdot 24853 \\ \cdot 24629 \\ \hline 2 \cdot 24629 $	$     \begin{array}{r}       11 \\       12 \\       13 \\       14 \\       15 \\       10     \end{array} $	
16 17 18 19 20	21486 20222 19099 18093 17189	4.33215 .30582 .28100 .25752 .23524	$\begin{array}{r} 4523.4 \\ 4464.7 \\ 4407.5 \\ 4351.7 \\ 4297.3 \\ \end{array}$	3.65547 .64979 .64419 .63865 .63319	$\begin{array}{r} 2527.9\\ 2509.5\\ 2491.3\\ 2473.4\\ 2455.7\\ \end{array}$	3.40276 .39958 .39642 .39329 .39017	$   \begin{array}{r} 1754.2 \\    1745.3 \\    1736.5 \\    1727.8 \\    1719.1 \\    1710.6 \\   \end{array} $	3.24407 .24186 .23967 .23748 .23530 .23530	16 17 18 19 20	
$21 \\ 22 \\ 23 \\ 24 \\ 25 \\ 20 \\ 20 \\ 20 \\ 20 \\ 20 \\ 20 \\ 20$	16370 15626 14947 14324 13751	$\begin{array}{r} 4 \cdot 2140\overline{5} \\ \cdot 19385 \\ \cdot 17454 \\ \cdot 1560\overline{6} \\ \cdot 1383\overline{3} \end{array}$	$ \begin{array}{r} 4244.2 \\ 4192.5 \\ 4142.0 \\ 4092.7 \\ 4044.5 \\ \hline 2205 \\ \hline 7 \end{array} $	$\begin{array}{r} 3.62780 \\ .62247 \\ .61720 \\ .61200 \\ .60686 \\ \hline 2.00170 \\ \hline \end{array}$	2438.32421.12404.22387.52371.0	$   \begin{array}{r}     3 \cdot 3870\overline{8} \\     \cdot 3840\overline{1} \\     \cdot 38097 \\     \cdot 37794 \\     \cdot 37494 \\     \hline     2 37494 \\     \hline   \end{array} $	1702.11693.71685.41677.2	3.23314 .23098 .22884 .22670 .22458 .22458	21 22 23 24 25	
26 27 28 29 30	13222 12732 12278 11854 11459	$\begin{array}{r} 4.12130 \\ .10491 \\ .08911 \\ .07387 \\ .05915 \end{array}$	3997.5 3951.5 3906.6 3862.7 <u>3819.8</u>	$   \begin{array}{r}     3 \cdot 6017\overline{8} \\     \cdot 5967\overline{6} \\     \cdot 5918\overline{0} \\     \cdot 5868\overline{9} \\     \cdot 5820\overline{4} \\   \end{array} $	2354.82338.82323.02307.42292.0	$3.3719\overline{5}$ .36899 .36604 .36312 .36021	$   \begin{array}{r}     1669 \cdot 1 \\     1661 \cdot 0 \\     1653 \cdot 0 \\     1645 \cdot 1 \\     1637 \cdot 3 \\   \end{array} $	$\begin{array}{r} 3.22247 \\ .22037 \\ .21827 \\ .21619 \\ .21412 \end{array}$	26 27 28 29 30	
31 32 33 34 35	11090 10743 10417 10111 9822.2	$\begin{array}{r} 4.0449\overline{1} \\ .0311\overline{2} \\ .01776 \\ 4.00479 \\ \underline{3.99221} \end{array}$	3777.9 3736.8 3696.6 3657.3 3618.8	3.57724 .57250 .56780 .56316 .55856	$\begin{array}{r} 2276 \cdot 8 \\ 2261 \cdot 9 \\ 2247 \cdot 1 \\ 2232 \cdot 5 \\ 2218 \cdot 1 \end{array}$	3.35733 .35446 .35162 .34879 .34598	1629.51621.81614.21606.71599.2	$\begin{array}{r} 3.21206\\ .21000\\ .20796\\ .20593\\ .20390\end{array}$	31 32 33 34 35	
36 37 38 39 40	9549.3 9291.3 9046.7 8814.8 8594.4	3.97997 .96807 .95649 .94521 .93421	$\begin{array}{r} 3581 \cdot 1 \\ 3544 \cdot 2 \\ 3508 \cdot 0 \\ 3472 \cdot 6 \\ 3437 \cdot 9 \end{array}$	$\begin{array}{r} 3.5540\overline{1} \\ .5495\overline{1} \\ .5450\overline{6} \\ .54065 \\ .53629 \end{array}$	$\begin{array}{r} 2203.9\\ 2189.8\\ 2176.0\\ 2162.3\\ 2148.8 \end{array}$	$\begin{array}{r} 3.3431\overline{8} \\ .34041 \\ .3376\overline{5} \\ .33491 \\ .33219 \end{array}$	$\begin{array}{r} 1591 \cdot 8 \\ 1584 \cdot 5 \\ 1577 \cdot 2 \\ 1570 \cdot 0 \\ 1562 \cdot 9 \end{array}$	$\begin{array}{r}3.20189\\.19988\\.19789\\.19590\\.19392\end{array}$	36 37 38 39 40	
41 42 43 44 45	8384.8 8185.2 7994.8 7813.1 7639.5	3.9234 <u>9</u> .91302 .9028 <u>1</u> .8928 <u>2</u> .88306	$\begin{array}{r} 3403 \cdot 8 \\ 3370 \cdot 5 \\ 3337 \cdot 7 \\ 3305 \cdot 7 \\ 3274 \cdot 2 \end{array}$	$\begin{array}{r} 3.53197\\ .52769\\ .52345\\ .51925\\ .51510\end{array}$	2135.42122.32109.22096.42083.7	$\begin{array}{r} 3.32949 \\ .32680 \\ .32412 \\ .32147 \\ .31883 \end{array}$	$\begin{array}{r} 1555 \cdot 8 \\ 1548 \cdot 8 \\ 1541 \cdot 9 \\ 1535 \cdot 0 \\ 1528 \cdot 2 \end{array}$	$3.1919\overline{5}$ .18999 .18804 .18610 .18417	41 42 43 44 45	
46 47 48 49 50	$\begin{array}{r} 7473.4 \\ 7314.4 \\ 7162.0 \\ 7015.9 \\ 6875.6 \end{array}$	3 · 87352 · 86418 · 85503 · 84608 · 83731	$\begin{array}{r} 3243 \cdot 3 \\ 3213 \cdot 0 \\ 3183 \cdot 2 \\ 3154 \cdot 0 \\ 3125 \cdot 4 \end{array}$	$3.5109\overline{8}$ .50691 .50287 .49883 .49490	$\begin{array}{c} 2071 \cdot 1 \\ 2058 \cdot 7 \\ 2046 \cdot 5 \\ 2034 \cdot 4 \\ 2022 \cdot 4 \end{array}$	3.31621 .31360 .31101 .30843 .30587	1521.41514.71508.11501.51495.0	$\begin{array}{r} 3.1822\bar{4} \\ .1803\bar{2} \\ .17842 \\ .17652 \\ .1746\bar{2} \end{array}$	46 47 48 49 50	
51 52 53 54 55	6740.7 6611.1 6486.4 6366.3 6250.5	3.82871 .82027 .81200 .80388 .79591	$\begin{array}{r} 3097 \cdot 2 \\ 3069 \cdot 6 \\ 3042 \cdot 4 \\ 3015 \cdot 7 \\ 2989 \cdot 5 \end{array}$	$\begin{array}{r} 3.49097\\.48707\\.48321\\.47939\\.47559\end{array}$	2010.6 1998.9 1987.3 1975.9 1964.6	3.30332 .30079 .29827 .29577 .29328	1488.51482.11475.71469.41463.2	$\begin{array}{r} 3.1727\bar{4} \\ .17087 \\ .16900 \\ .16714 \\ .16529 \end{array}$	51 52 53 54 55	
56 57 58 59 60	$\begin{array}{c} 6138 \cdot 9 \\ 6031 \cdot 2 \\ 5927 \cdot 2 \\ 5826 \cdot 8 \\ 5729 \cdot 6 \end{array}$	8.78809 .78040 .77285 .76542 .75813	2963.7 2938.4 2913.5 2889.0 2864.9	$   \begin{array}{r}     3.4718\overline{3} \\     .46811 \\     .46441 \\     .46075 \\     .45711 \\   \end{array} $	1953.51942.41931.51920.71910.1	3.29081 .28835 .28590 .28347 .28105	1457.01450.81444.71438.71432.7	3.16344 .16161 .15978 .15796 .15615	56 57 58 59 60	

#### TABLE I.—RADII OF CURVES.

	1	 4°	[	-0		6°		Dem	
Deg Min	Radius.			5° Radius.   Log R			Radius,	7° Log R	Deg Min
0 1 2 3 4	1432.7 1426.7 1420.8 1415.0 1409.2	$\begin{array}{r} 109 \\ \hline 3.15615 \\ .15434 \\ .15255 \\ .15076 \\ .14897 \end{array}$	1146.3 1142.5 1138.7 1134.9 1131.2	$\begin{array}{r} 109 \\ \hline 3.05929 \\ .05784 \\ .05640 \\ .05497 \\ .05354 \end{array}$	Radius, 955.37 952.72 950.09 947.48 944.88	2.98017 .97896 .97776 .97657 .97537	819.02 817.08 815.14 813.22 811.30	2.91329 .91226 .91123 .91021 .90918	0
5 6 7 8 9	$\frac{1403.2}{1403.5}$ $\frac{1403.5}{1397.8}$ $1392.1$ $1386.5$ $1380.9$ $1375.4$	$\begin{array}{r} .14720 \\ \hline 3.14543 \\ .14367 \\ .14191 \\ .14017 \\ .13843 \end{array}$	$\frac{1131 \cdot 2}{1127 \cdot 5}$ $\frac{1123 \cdot 8}{1120 \cdot 2}$ $\frac{1116 \cdot 5}{1112 \cdot 9}$ $1109 \cdot 3$	$     \begin{array}{r} 0.0331 \\                                   $	$\begin{array}{r} 942.29\\ 939.72\\ 937.16\\ 934.62\\ 932.09\\ 929.57\end{array}$	<u>.97418</u> 2.97300 .97181 .97063 .96945 .96828	809.40 807.50 805.61 803.73 801.86 800.00	<u>90816</u> 2.9071 <u>4</u> .90612 .90511 .90410 .90309	2 3 4 5 6 7 8 9 10
11 12 13 14 15	1369.91364.51359.11353.81348.4	$\begin{array}{r} 3.1366\bar{9} \\ .13497 \\ .13325 \\ .13154 \\ .12983 \end{array}$	1105.8 1102.2 1098.7 1095.2 1091.7	3.04366 .04227 .04088 .03949 .03811	$\begin{array}{r} 927.07\\ 924.58\\ 922.10\\ 919.64\\ 917.19\end{array}$	$\begin{array}{r} 2.96711 \\ .96594 \\ .96478 \\ .96361 \\ .96246 \end{array}$	798.14 796.30 794.46 792.63 790.81	2.90208 .90107 .90007 .89907 .89807	11 12 13 14 15
16 17 18 19 20	1343.21338.01332.81327.61322.5	$3.1281\overline{3}$ .12644 $.1247\overline{5}$ $.1230\overline{7}$ $.1214\overline{0}$	1088.3 1084.8 1081.4 1078.1 1074.7	3-03674 -03537 -03400 -03264 -03128	914.75912.33909.92907.52905.13	2.96130 .96015 .95900 .95785 .95671	789.00 787.20 785.41 783.62 781.84	2.89708 .89608 .89509 .89410 .89312	16 17 18 19 20
21 22 23 24 25	$   \begin{array}{r}     1317.5 \\     1312.4 \\     1307.4 \\     1302.5 \\     1297.6 \\   \end{array} $	3.11974 .11808 .11642 .11477 .11313	$   \begin{array}{r}     1071 \cdot 3 \\     1068 \cdot 0 \\     1064 \cdot 7 \\     1061 \cdot 4 \\     1058 \cdot 2   \end{array} $	3-02992 -02857 -02723 -02589 -02455	$\begin{array}{r} 902.76 \\ 900.40 \\ 898.05 \\ 895.71 \\ 893.39 \end{array}$	2.95557 .95443 .95330 .95217 .95104	780.07 778.31 776.55 774.81 773.07	2.89213 .89115 .89017 .88919 .88821	21 22 23 24 25
26 27 28 29 30	1292.71287.91283.11278.31273.6	3.11150 .10987 .10825 .10663 .10502	$\begin{array}{c} 1054 \cdot 9 \\ 1051 \cdot 7 \\ 1048 \cdot 5 \\ 1045 \cdot 3 \\ 1042 \cdot 1 \end{array}$	3-02322 -02189 -02056 -01924 -01792	891.08 888.78 886.49 884.21 881.95	2.94991 .94879 .94767 .94655 .94655	771.34 769.61 767.90 766.19 764.49	2-88724 -88627 -88530 -88433 -88337	26 27 28 29 30
31 32 33 34 35	1268.91264.21259.61255.01250.4	3.10341 .10182 .10022 .09864 .09705	1039.0 1035.9 1032.8 1029.7 1026.6	3-0166 <u>1</u> .01530 .01400 .01270 .01140	879.69 877.45 875.22 873.00 870.80	$\begin{array}{r} 2 \cdot 94433 \\ \cdot 94322 \\ \cdot 94212 \\ \cdot 94101 \\ \cdot 93991 \end{array}$	762.80 761.11 759.43 757.76 756.10	2.88241 .88145 .88049 .87953 .87858	31 32 33 34 35
36 37 38 39 <u>40</u>	1245.91241.41236.91232.51228.1	$\begin{array}{r} 3.09548 \\ .09391 \\ .09234 \\ .09079 \\ .08923 \end{array}$	$\begin{array}{c} 1023.5\\ 1020.5\\ 1017.5\\ 1014.5\\ 1011.5\end{array}$	$3.0101\overline{0}$ .00882 .00753 .00625 .00497	$\begin{array}{r} 868.60\\ 866.41\\ 864.24\\ 862.07\\ 859.92 \end{array}$	293882 93772 93663 93554 93446	754.44 752.80 751.16 749.52 747.89	2.87762 .87668 .8757 <u>3</u> .87478 .87384	36 37 38 39 40
41 42 43 44 45	1223.71219.41215.11210.81206.6	3.08769 .08614 .08461 .08308 .08155	1008.6 1005.6 1002.7 999.76 996.87	$\begin{array}{r} 3.\ 00370\\ .\ 00242\\ 3.\ 00116\\ 2.\ 99989\\ .\ 99863\end{array}$	857.78 855.65 853.53 851.42 849.32	$2.9333\overline{7} \\ .9322\overline{9} \\ .93122 \\ .93014 \\ .92907$	$\begin{array}{r} 746.27 \\ 744.66 \\ 743.06 \\ 741.46 \\ 739.86 \end{array}$	2.87290 .87196 .87102 .87008 .86915	41 42 43 44 45
46 47 48 49 50	1202.41198.21194.01189.91185.8	3.08003 .07852 .07701 .07550 .07400	993.99991.13988.28985.45982.64	2.99738 .99613 .99488 .99363 .99239	847.23845.15843.08841.02838.97	$\begin{array}{r} 2.92800\\ .92693\\ .92587\\ .92480\\ .92374\end{array}$	738.28736.70735.13733.56732.01	2.86822 .86729 .86636 .86544 .86451	46 47 48 49 50
51 52 53 54 55	$     \begin{array}{r}       1181 \cdot 7 \\       1177 \cdot 7 \\       1173 \cdot 6 \\       1169 \cdot 7 \\       1165 \cdot 7 \\       \hline     \end{array} $	3.07251 .07102 .06954 .06806 .06658	979.84 977.06 974.29 971.54 968.81	2.99115 .98992 .98869 .98746 .98624	836.93 834.90 832.89 830.88 828.88	2.9226 <u>9</u> .9216 <u>3</u> .9205 <u>8</u> .91953 .91849	730.45728.91727.37725.84724.31	2 · 86359 ·86267 ·86175 ·86084 ·85992	51 52 53 54 55
56 57 58 59 60	1161.81157.91154.01150.11146.3	3.0651 <u>1</u> .0636 <u>5</u> .06219 .06074 .05929	966.09 963.39 960.70 958.03 955.37	2.98501 -98380 -98258 -98137 -98017	826.89 824.91 822.93 820.97 819.02	$\left \begin{array}{c} 2.9174\bar{4}\\.9164\bar{0}\\.91536\\.91433\\(.91433\\(.91329\end{array}\right.$	722.79 721.28 719.77 718.27 716.78	2.85901 .85810 .85719 .85629 .85538	58 59

#### TABLE I.-RADII OF CURVES.

Deg.		8°		9°	1	.0°	1	Deg	
Min.	Radius.	Log R	Radius.	Log R	Radius,	Log R	Radius.	Log R	Min
0 1 2 3 4 5	716.78715.29713.81712.34710.87709.40	$\begin{array}{r} 2\cdot 8553\overline{8} \\ \cdot 8544\overline{8} \\ \cdot 8535\overline{8} \\ \cdot 8526\overline{8} \\ \cdot 8517\overline{8} \\ \cdot 85089 \end{array}$	$\begin{array}{r} 637 \cdot 27 \\ 636 \cdot 10 \\ 634 \cdot 93 \\ 633 \cdot 76 \\ 632 \cdot 60 \\ 631 \cdot 44 \end{array}$	2.80432 .80352 .80272 .80192 .80113 .80033	573.69 572.73 571.78 570.84 569.90 568.96	2.75867 .75795 .75723 .75651 .75579 .75508	521.67520.88520.10519.32518.54517.76	$\begin{array}{r} 2\cdot 7173\bar{9} \\ \cdot 71674 \\ \cdot 7160\bar{8} \\ \cdot 7154\bar{3} \\ \cdot 71478 \\ \cdot 71413 \end{array}$	0 1 2 3 4 5 6 7
6 7 8 9 10	707.95 706.49 705.05 703.61 702.17	2.85000 .84911 .84822 .84733 .84644	630.29 629.14 627.99 626.85 625.71	2.7995 <u>4</u> .7987 <u>4</u> .7979 <u>5</u> .7971 <u>6</u> .79637	$\begin{array}{r} 568.02 \\ 567.09 \\ 566.16 \\ 565.23 \\ 564.31 \end{array}$	2.75436 .75365 .75293 .75222 .75151	516.99516.21515.44514.68513.91	$\begin{array}{r} 2.71348 \\ .71283 \\ .71218 \\ .71153 \\ .71088 \end{array}$	8 9 10
11 12 13 14 15	700.75 699.33 697.91 696.50 695.09	2.84556 .84468 .84380 .84292 .84204	$\begin{array}{r} 624\cdot 58\\ 623\cdot 45\\ 622\cdot 32\\ 621\cdot 20\\ 620\cdot 09\end{array}$	2.79558 .79480 .79401 .79323 .79245	$\begin{array}{r} 563.38\\ 562.47\\ 561.55\\ 560.64\\ 559.73\end{array}$	2.75080 .75009 .74939 .74868 .74798	513.15512.38511.63510.87510.11	2.71024 .70959 .70895 .70831 .70767	11 12 13 14 15
16 17 18 19 20	693.70 692.30 690.91 689.53 688.16	2.84117 .84029 .83942 .83855 .83768	$\begin{array}{c} 618.97 \\ 617.87 \\ 616.76 \\ 615.66 \\ 614.56^{\circ} \end{array}$	2.79167 .79089 .79011 .78934 .78856	558.82 557.92 557.02 556.12 555.23	2.74727 .74657 .74587 .74517 .74447	509.36508.61507.86507.12506.38	2.70702 .70638 .70575 .70511 .70447	16 17 18 19 20
21 22 23 24 25	686.78 685.42 684.06 682.70 681.35	2.83682 .83595 .83509 .83423 .83337	613.47 612.38 611.30 610.21 609.14	2.78779 .78702 .78625 .78548 .78471	$\begin{array}{r} 554.34\\ 553.45\\ 552.56\\ 551.68\\ 550.80\end{array}$	$2.7437\overline{7}$ .7430 $\overline{7}$ .74238 .74168 .74099	505.64504.90504.16503.42502.69	2.70383 .70320 .70257 .70193 .70130	21 22 23 24 25
26 27 28 29 30	680.01 678.67 677.34 676.01 674.69	2.83251 .83166 .83080 .82995 .82910	$\begin{array}{c} 608.06 \\ 606.99 \\ 605.93 \\ 604.86 \\ 603.80 \end{array}$	2.78395 .78318 .78242 .78165 .78089	549.92 549.05 548.17 547.30 546.44	2.74030 .73961 .73892 .73823 .73754	501.96501.23500.51499.78499.06	2.70067 .70004 .69941 .69878 .69815	26 27 28 29 30
31 32 33 34 35	$\begin{array}{r} 673.37 \\ 672.06 \\ 670.75 \\ 669.45 \\ 668.15 \end{array}$	2 · 82825 · 82740 · 82656 · 82571 · 82487	602.75 601.70 600.65 599.61 598.57	2.78013 .77938 .77862 .77786 .77711	545.57544.71543.86543.00542.15	2-73685 -73617 -73548 -73480 -73412	498.34 497.62 496.91 496.19 495.48	2.69752 .69690 .69627 .69565 .69565 .69508	31 32 33 34 35
36 37 38 39 40	$\begin{array}{r} 666 \cdot 86 \\ 665 \cdot 57 \\ 664 \cdot 29 \\ 663 \cdot 01 \\ 661 \cdot 74 \end{array}$	2 · 82403 · 82319 · 82235 · 82152 · 82068	597.53596.50595.47594.44593.42	2.77636 .77561 .77486 .77411 .77336	$541.30 \\ 540.45 \\ 539.61 \\ 538.76 \\ 537.92$	2 · 7334 <u>3</u> · 73275 · 73207 · 73140 · 73072	$\begin{array}{r} 494.77\\ 494.07\\ 493.36\\ 492.66\\ 491.96\end{array}$	2.69440 .69378 .69316 .69254 .69192	36 37 38 39 40
41 42 43 44 45	$\begin{array}{r} 660.47\\ 659.21\\ 657.95\\ 656.69\\ 655.45\end{array}$	2.81985 .81902 .81819 .81736 .81653	592.40 591.38 590.37 589.36 588.36	2.77261 .77187 .77112 .77038 .76964	537.09536.25535.42534.59533.77	2 · 73004 · 72937 · 72869 · 72802 · 72735	491.26 490.56 489.86 489.17 488.48	2.69131 .69069 .69007 .68946 .68884	41 42 43 44 45
46 47 48 49 50	$\begin{array}{c} 654 \cdot 20 \\ 652 \cdot 96 \\ 651 \cdot 73 \\ 650 \cdot 50 \\ 649 \cdot 27 \end{array}$	$\begin{array}{r} 2.81571 \\ .81489 \\ .81406 \\ .81324 \\ .81243 \end{array}$	587.36 586.36 585.36 584.37 583.38	$\begin{array}{r} 2.76890 \\ .76816 \\ .76742 \\ .76669 \\ .76595 \end{array}$	532.94 532.12 531.30 530.49 529.67	2.72668 .72601 .72534 .72467 .72401	$\begin{array}{r} 487.79\\ 487.10\\ 486.42\\ 485.73\\ 485.05 \end{array}$	2.68823 .68762 .68701 .68640 .68579	46 47 48 49 50
51 52 53 54 55	$\begin{array}{r} 648.05 \\ 646.84 \\ 645.63 \\ 644.42 \\ 643.22 \end{array}$	2.8116 <u>1</u> .81079 .80998 .80917 .80836	$582.40 \\ 581.42 \\ 580.44 \\ 579.47 \\ 578.49 \\$	2 · 76522 · 76449 · 76376 · 76303 · 76230	528.86528.05527.25526.44525.64	2 · 72334 · 72267 · 72201 · 72135 · 72069	484.37 483.69 483.02 482.34 481.67	2.68518 .68457 .68396 .68335 .68275	51 52 53 54 55
56 57 58 59 60	$\begin{array}{r} 642\cdot 02 \\ 640\cdot 83 \\ 639\cdot 64 \\ 638\cdot 45 \\ 637\cdot 27 \end{array}$	2.80755 .8067 <u>4</u> .80593 .80513 .80432	577.53 576.56 575.60 574.64 573.69	2.76157 .76084 .76012 .75939 .75867	$524 \cdot 84 \\524 \cdot 05 \\523 \cdot 25 \\522 \cdot 46 \\521 \cdot 67$	2.72003 .71937 .7187 <u>1</u> .7180 <u>5</u> .71739	481.00 480.33 479.67 479.00 478.34	2.68214 .68154 .6809 <u>4</u> .6803 <u>3</u> .67973	56 57 58 59 60

#### TABLE I.-RADII OF CURVES.

				ADLE	1			V 1265.			
Deg.	Radius.	Log R	Deg.	Radius.	Log R	Deg.	Radius.	Log R	Deg.	Radius	Log R
12° 2 4 6 8	$\begin{array}{r} 478.34\\ 477.02\\ 475.71\\ 474.40\\ 473.10\end{array}$	$\begin{array}{r} 2.6797\overline{3} \\ .6785\overline{3} \\ .67734 \\ .6761\overline{4} \\ .6749\overline{5} \end{array}$	14° 2 4 6 8	$\begin{array}{r} 410.28\\ 409.31\\ 408.34\\ 407.38\\ 406.42 \end{array}$	$\begin{array}{r} 2.6130\overline{7} \\ .61205 \\ .6110\overline{2} \\ .61000 \\ .60898 \end{array}$	16° 5 10 15 20	$359 \cdot 26$ $357 \cdot 42$ $355 \cdot 59$ $353 \cdot 77$ $351 \cdot 98$	$\begin{array}{r} 2.5554\overline{1} \\ .5531\overline{7} \\ .5509\overline{4} \\ .5487\overline{2} \\ .54652 \end{array}$	21° 10 20 30 40	274.37272.23270.13268.06266.02	$\begin{array}{r} 2 \cdot 4383\overline{3} \\ \cdot 4349\overline{4} \\ \cdot 4315\overline{7} \\ \cdot 4282\overline{3} \\ \cdot 42492 \end{array}$
10 12 14 16 18 20	$\begin{array}{r} 471.81\\ 470.53\\ 469.25\\ 467.98\\ 466.72\\ 465.46\end{array}$	$2.6737\overline{6} \\ .67258 \\ .67140 \\ .67022 \\ .66905 \\ \hline 2.66788$		$\begin{array}{r} 405 \cdot 47 \\ 404 \cdot 53 \\ 403 \cdot 58 \\ 402 \cdot 65 \\ 401 \cdot 71 \\ 400 \cdot 78 \end{array}$	$2 \cdot 60796 \\ \cdot 60694 \\ \cdot 60593 \\ \cdot 60492 \\ \cdot 60391 \\ 2 \cdot 60391 \\ \hline 2 \cdot 60291 \\ \hline$	35	$\begin{array}{r} 350.21\\ 348.45\\ 346.71\\ 344.99\\ 343.29\\ 341.60\\ \end{array}$	$\begin{array}{r} \underline{\cdot 54432} \\ 2 \cdot 54214 \\ \cdot 53997 \\ \cdot 53780 \\ \cdot 53565 \\ \cdot 53351 \end{array}$	$22^{\circ}$ 10 20 30	$\frac{264.02}{262.04}$ $\frac{260.10}{258.18}$ $\frac{256.29}{254.43}$	$     \begin{array}{r} \cdot 4216\overline{3} \\     2 \cdot 41837 \\     \cdot 4151\overline{3} \\     \cdot 41192 \\     \cdot 40873 \\     \cdot 40557   \end{array} $
22 24 26	464.21	2.00700 .66671 .66555 .66439 .66323 2.66207	22 24 26 28	$ \frac{400.78}{399.86} $ $ \frac{398.94}{398.02} $ $ \frac{397.11}{396.20} $			339.93 338.27 336.64 335.01 333.41	$\begin{array}{r} \cdot 5313\overline{8} \\ \hline 2 \cdot 52927 \\ \cdot 52716 \\ \cdot 52506 \\ \cdot 52297 \end{array}$		$\begin{array}{r} \underline{252.60}\\ 250.79\\ 249.01\\ 247.26\\ 245.53 \end{array}$	$     \underbrace{\begin{array}{r} \cdot 40243 \\ 2 \cdot 39931 \\ \cdot 39622 \\ \cdot 39315 \\ \cdot 39010 \end{array}} $
32 34 36 38 40	$\begin{array}{r} 458.06\\ 456.85\\ 455.65\\ 454.45\\ 453.26\end{array}$	.66092 .65977 .65863 .65748 2.65634	32 34 36 38 40	395.30 394.40 393.50 392.61 391.72	.59692 .59593 .59494 .59398 2.59398	30 35 40	$331 \cdot 82$ $330 \cdot 24$ $328 \cdot 68$ $327 \cdot 13$ $325 \cdot 60$ $324 \cdot 09$		$     \begin{array}{r}       50 \\       24^{\circ} \\       10 \\       20     \end{array} $	$\begin{array}{r} 243 & 82 \\ \underline{242 \cdot 14} \\ 240 \cdot 49 \\ 238 \cdot 85 \\ 237 \cdot 24 \\ 235 \cdot 65 \end{array}$	$\begin{array}{r} \cdot 3870\overline{7} \\ 3840\overline{7} \\ \hline 2 \cdot 38109 \\ \cdot 37813 \\ \cdot 37519 \\ \cdot 37227 \end{array}$
50	$\begin{array}{r} 452.07\\ 450.89\\ 449.72\\ 448.56\\ 447.40\\ \end{array}$		$     \begin{array}{r}       44 \\       46 \\       48 \\       50     \end{array} $	390.84 389.96 389.08 388.21 387.34	.59199 .59102 .59004 .58907 2.58809	50 55 18° 5	$322.59 \\ 321.10$	.50864 .50663 2.50464 .50265 .50067	$\begin{array}{r} 40 \\ 50 \\ \hline 25^{\circ} \end{array}$	$234.08 \\ 232.54$	·36937 ·36649 2·36363 ·35517 ·34688
52 54 56 58 13° 2	$\begin{array}{r} 446 \cdot 24 \\ 445 \cdot 09 \\ 443 \cdot 95 \\ 442 \cdot 81 \\ 441 \cdot 68 \\ 440 \cdot 56 \end{array}$	$     \begin{array}{r}                                     $	54 56 58 15°	$386 \cdot 48$ $385 \cdot 62$ $384 \cdot 77$ $383 \cdot 91$ $383 \cdot 06$ $382 \cdot 22$	58713 58616 58519 58423 2.58327 58231	15 20 25 30	$     \begin{array}{r}       315.28 \\       313.86 \\       312.45     \end{array} $	·49869 ·49673 ·49478 2·49284 ·49090	$     \begin{array}{r}       30 \\       \overline{27^{\circ}} \\       30 \\       28^{\circ}     \end{array}   $	218.15	<u>.33875</u> 2.33078 .32296 .31529 .30776
4 6 8 10 12	440.30 439.44 438.33 437.22 436.12 435.02	64290 64290 64180 64070 $2 \cdot 6396\overline{0}$ 63851	4 6 8 10	382.22 381.38 380.54 <u>379.7</u> 1 378.88 378.05	.58231 .58135 .58040 .57945 2.57850 .57755	40 45 50	$308 \cdot 30$ $306 \cdot 95$ $305 \cdot 60$ $304 \cdot 27$ $302 \cdot 94$	.48898     .48706     .48515     .48325     2.48136	$29^{\circ}$ 30 $30^{\circ}$ 30	199.70 196.38 193.19 190.09	2.30037 .29310 .28597 .27896 2.27207
14 16 18 20 22	$\begin{array}{r} 433 \cdot 93 \\ 432 \cdot 84 \\ 431 \cdot 76 \\ 430 \cdot 69 \\ 429 \cdot 62 \end{array}$	63742 63633 63524 2.63416 63308	14     16     18     1	$377 \cdot 23$ $376 \cdot 41$ $375 \cdot 60$ $374 \cdot 79$ $373 \cdot 98$	.57661 .57566 .57472 2.57378 .57284	5 10 15 20 25	$     \begin{array}{r}       301 \cdot 63 \\       300 \cdot 33 \\       299 \cdot 04 \\       297 \cdot 77 \\       296 \cdot 50 \\       \hline     \end{array} $	.47948 .47760 .47573 .47388 .47203	$32 \\ 33 \\ 34 \\ 35$	181.40176.05171.02166.28	25863 24563 23303 22083 $2 \cdot 20899$
24 26 28 30 32	$425.40 \\ 424.35$		26 28 30 32	373.17 372.37 371.57 370.78 369.99	57191 57097 57004 $2 \cdot 56911$ 56819	35 40 45	$295 \cdot 25$ $294 \cdot 00$ $292 \cdot 77$ $291 \cdot 55$ $290 \cdot 33$ $289 \cdot 13$	2.47018 .46835 .46652 .46471 .46289 .46109	$     \begin{array}{r}       37 \\       38 \\       39 \\       40 \\       41     \end{array} $	$   \begin{array}{r}     157 \cdot 58 \\     153 \cdot 58 \\     149 \cdot 79 \\     146 \cdot 19 \\     142 \cdot 77   \end{array} $	$\begin{array}{r} \cdot 1974\bar{9} \\ \cdot 18633 \\ \cdot 17547 \\ \underline{\cdot 16492} \\ \hline 2 \cdot 1546\bar{4} \end{array}$
34 36 38 40 42	$\begin{array}{r} 422\cdot 28\\ \underline{421\cdot 26}\\ 420\cdot 23\\ 419\cdot 22\end{array}$	$62666 \\ 62560 \\ 62454 \\ 2.62349 \\ 62243 \\ 62243 \\ 62123 \\ 62$	$     \begin{array}{r}       34 \\       36 \\       38 \\       40 \\       42 \\       44     \end{array} $	$369 \cdot 20$ $368 \cdot 42$ $367 \cdot 64$ $366 \cdot 86$ $366 \cdot 09$ $365 \cdot 31$	.56726 .56634 .56542 2.56450 .56358	20° 5 10 15 20	287.94 286.76 285.58 284.42 283.27	2.45930 .45751 .45573 .45396 .45219	$\begin{array}{r} 43\\ 44\\ \underline{45}\\ 46 \end{array}$	139.52 136.43 133.47 130.66 127.97 105.90	$ \begin{array}{r} .14464\\.13489\\.12539\\.11613\\\hline 2.10709\\00007 \end{array} $
44 46 48 50 52 54	415.19	·62138 ·62034 ·61929 2·61825 ·61721 ·61617	44 46 48 50 52 54	$363 \cdot 31$ $364 \cdot 55$ $363 \cdot 78$ $363 \cdot 02$ $362 \cdot 26$ $361 \cdot 51$	-56266 -56175 -56084 2-55993 -55902 -55812	35 40 45	$\begin{array}{r} 282.12\\ 280.99\\ 279.86\\ 278.75\\ 277.64\\ 276.54 \end{array}$	<u>.45044</u> 2.44869 .44694 .44521 .44348 .44176	$     \begin{array}{r}       47 \\       48 \\       49 \\       50 \\       52 \\       54     \end{array} $	125.39122.93120.57118.31114.06110.13	$\begin{array}{r} .09827\\ .08965\\ .08124\\ .07302\\ \hline 2.05713\\ .04192 \end{array}$
56 58 14°	$412.23 \\ 411.25$	·61514 ·61410 2·61307	56 58	$360.76 \\ 360.01 \\ 359.26$	55721 55631 2.55541	50 55 21°	276.54 275.45 274.37		56 58 60	$106.50 \\ 103.13$	·02736 ·01340 2·00000

#### TABLE II.—TANGENTS, EXTERNAL DISTANCES, AND LONG CHORDS FOR A 1° CURVE.

Δ	Tang. T.	Ext. Dist. E.	Long Chord LC.	Δ	Tang. T.	Ext. Dist. <i>E</i> .	Long Chord LC.	Δ	Tang. T.	Ext. Dist. Æ.	Long Chord LC.	
1° 10' 20 30 40 50	50.0058.3466.6775.0183.3491.68	$\begin{array}{c} 0.218 \\ 0.297 \\ 0.388 \\ 0.491 \\ 0.606 \\ 0.733 \end{array}$	100.00116.67133.33150.00166.66183.33	11° 10 20 30 40 50	585.36 593.79	$27 \cdot 313$ $28 \cdot 137$ $28 \cdot 9.74$ $29 \cdot 824$ $30 \cdot 686$	1114.9 1131.5 1148.1 1164.7 1181.2	$21^{\circ}$ 10 20 30 40 50	$1096.4 \\ 1105.1$	97.58 99.15 100.75 102.35 103.97 105.60		
2° 10 20 30 40 50	100.01108.35116.68125.02133.36141.70	$\begin{array}{r} 0.873 \\ 1.024 \\ 1.188 \\ 1.364 \\ 1.552 \\ 1.752 \end{array}$	199.99216.66233.32249.98266.65283.31	$12^{\circ}$ 10 20 30 40 50	$\begin{array}{r} 619.07 \\ 627.50 \\ 635.93 \\ 644.37 \end{array}$	$34.259 \\ 35.183 \\ 36.120$	$   \begin{array}{r}     1197 \cdot 8 \\     1214 \cdot 4 \\     1231 \cdot 0 \\     1247 \cdot 5 \\     1264 \cdot 1 \\     1280 \cdot 7 \\   \end{array} $	$22^{\circ}$ 10 20 30 40 50 $20^{\circ}$	$\frac{1131.0}{1139.7}\\ 1148.4\\ 1157.0$	$107.24 \\ 108.90 \\ 110.57 \\ 112.25 \\ 113.95 \\ 115.66 \\ 115.66 \\ 100.000 \\ 1$	2186.5 2202.9 2219.2 2235.6 2251.9 2268.3	
3° 10 20 30 40 50	150.04 158.38 166.72 175.06 183.40 191.74	$   \begin{array}{r}     1.964 \\     2.188 \\     2.425 \\     2.674 \\     2.934 \\     3.207 \\     \hline   \end{array} $	$\begin{array}{r} 299.97\\ 316.63\\ 333.29\\ 349.95\\ 366.61\\ 383.27\\ \hline \end{array}$	$     \begin{array}{r}       13^{\circ} \\       10 \\       20 \\       30 \\       40 \\       50 \\       14^{\circ}     \end{array} $	$     \begin{array}{r}       669.70 \\       678.15 \\       686.60 \\       695.06     \end{array} $	$\begin{array}{r} 40.992\\ \underline{42.004}\end{array}$	$   \begin{array}{r}     1297 \cdot 2 \\     1313 \cdot 8 \\     1330 \cdot 3 \\     1346 \cdot 9 \\     1363 \cdot 4 \\     1380 \cdot 0 \\   \end{array} $	$23^{\circ}$ 10 20 30 40 50 $24^{\circ}$	1174.4 1183.1 1191.8 1200.5 1209.2	117.38119.12120.87122.63124.41126.20		
4° 10 20 30 40 50	200.08208.43216.77225.12233.47241.81	3.492 3.790 4.099 4.421 4.755 5.100	$ \begin{array}{r} 399.92\\ 416.58\\ 433.24\\ 449.89\\ 466.54\\ 483.20\\ \hline 400.85\\ $	10 20 30 40 50	$\begin{array}{r} 728.90 \\ 737.37 \\ 745.85 \end{array}$	$\begin{array}{r} 44.066\\ 45.116\\ 46.178\\ 47.253\\ 48.341 \end{array}$	1396.51413.11429.61446.21462.71462.71479.21495.7	$24^{\circ}$ 10 20 30 40 50 $25^{\circ}$	$\begin{array}{r} 1235.3 \\ 1244.0 \\ 1252.8 \\ 1261.5 \end{array}$	128.00129.82131.65133.50135.36137.23	2447.7 2464.0	
$5^{\circ}$ 10 20 30 40 50	250.16 258.51 266.86 275.21 283.57 291.92	5.459 5.829 6.211 6.606 7.013 7.432	$ \begin{array}{r} 499.85\\516.50\\533.15\\549.80\\566.44\\583.09\\\hline500\\500\\500\\500\\500\\500\\500\\500\\500\\50$	$15^{\circ}$ 10 20 30 40 50 $10^{\circ}$	779.77 788.26 796.75	$51.679 \\ 52.818 \\ 53.969 \\ 55.132$	1512.3 1528.8 1545.3 1561.8 1578.3	$25^{\circ}$ 10 20 30 40 50 $20^{\circ}$	1287.71296.51305.31314.0	139.11141.01142.93144.85146.79148.75	2529.0 2545.3 2561.5	
6° 10 20 30 40 50		$7 \cdot 863 \\ 8 \cdot 307 \\ 8 \cdot 762 \\ 9 \cdot 230 \\ 9 \cdot 710 \\ 10 \cdot 202 \\ \hline$	599.73616.38633.02649.66666.30682.94	$16^{\circ}$ 10 20 30 40 50 $10^{\circ}$	805.25 813.75 822.25 830.76 839.27 847.78		$1594 \cdot 8$ $1611 \cdot 3$ $1627 \cdot 8$ $1644 \cdot 3$ $1660 \cdot 8$ $1677 \cdot 3$	$26^{\circ}$ 10 20 30 40 50 $20^{\circ}$	$1340.4 \\ 1349.2 \\ 1358.0 \\ 1366.8 \\$		2577.8 2594.0 2610.3 2626.5 2642.7 2658.9	
7° 10 20 30 40 50	$     358.81 \\     367.17 \\     375.54 \\     383.91 \\     392.28 $	$   \begin{array}{r}     11.753 \\     12.294 \\     12.847 \\     13.413   \end{array} $	$\begin{array}{r} 699.57\\ 716.21\\ 732.84\\ 749.47\\ 766.10\\ 782.73\end{array}$	$17^{\circ}$ 10 20 30 40 50		$\begin{array}{r} 66 \cdot 178 \\ 67 \cdot 470 \\ 68 \cdot 774 \\ 70 \cdot 091 \end{array}$	$1693 \cdot 8$ $1710 \cdot 3$ $1726 \cdot 8$ $1743 \cdot 2$ $1759 \cdot 7$ $1776 \cdot 2$	$27^{\circ}$ 10 20 30 40 50	1384.41393.21402.01410.91419.7	$169.04 \\ 171.15 \\ 173.27$	2675.1 2691.3 2707.5 2723.7 2739.9 2756.1	
8° 10 20 30 40 50	$\begin{array}{r} 409.03\\ 417.41\\ 425.79\\ 434.17\\ 442.55\end{array}$	$13.991 \\ 14.582 \\ 15.184 \\ 15.799 \\ 16.426 \\ 17.066 \\ 17.066 \\ 17.066 \\ 10.000 \\ 1$	799.36815.99832.61849.23865.85882.47	$     18^{\circ} \\     10 \\     20 \\     30 \\     40 \\     50     $	$933.13 \\ 941.69 \\ 950.25$	74.11975.48876.86978.264	1792.61809.11825.51842.01858.41874.9	$28^{\circ}$ 10 20 30 40 50	$1437.4 \\ 1446.3 \\ 1455.1 \\ 1464.0 \\ 1472.9$	179.72181.89184.08186.29	2772.3 2788.4 2804.6 2820.7 2836.9 2853.0	
9° 10 20 30 40 50	459.32 467.71 476.10 484.49 492.88	$\begin{array}{r} 19.746 \\ 20.447 \\ 21.161 \end{array}$	$\begin{array}{r} 899 \cdot 09 \\ 915 \cdot 70 \\ 932 \cdot 31 \\ 948 \cdot 92 \\ 965 \cdot 53 \\ 982 \cdot 14 \end{array}$	19° 10 20 30 40 50	993.12 1001.70	81.092 82.525 83.972 85.431 86.904	1891.3 1907.8 1924.2 1940.6 1957.1 1973.5	$29^{\circ}$ 10 20 30 40 50	1490.71499.61508.51517.41526.3	190.74 192.99 195.25 197.53 199.82	2869.2 2885.3 2901.4 2917.6 2933.7 2949.8	
10° 10 20 30 40 50	509.68 518.08 526.48 534.89 543.29	23.375 24.138 24.913 25.700	$\begin{array}{r} 998.74 \\ 1015.35 \\ 1031.95 \\ 1048.54 \\ 1065.14 \\ 1081.73 \end{array}$	$20^{\circ}$ $10^{20}$ $30^{40}$ $50^{-10}$	1018.89 1027.49 1036.09 1044.70 1053.31	$\begin{array}{r} 91.399 \\ 92.924 \\ 94.462 \\ 96.013 \end{array}$	2055.5 2071.9	$     \begin{array}{r}       30^{\circ} \\       10 \\       20 \\       30 \\       40 \\       50 \\       \hline     \end{array} $	$\begin{array}{r} 1544.2 \\ 1553.1 \\ 1562.1 \\ 1571.0 \\ 1580.0 \end{array}$	204.44 206.77 209.12 211.48 213.86	2965.9 2982.0 2998.1 3014.2 3030.2 3046.3	
11°	551.70	26.500	1098.33	$21^{\circ}$	1061.93	97.577	2088.8	<u>31°</u>	1589.0	216.25	3062.4	

# TABLE II.—TANGENTS, EXTERNAL DISTANCES, AND LONG CHORDSFOR A 1° CURVE.

, Δ	Tang.	Ext. Dist. <i>E</i> .	Long Chord LC.	Δ	Tang.	Ext. Dist. E.	Long Chord L.C.	Δ	Tang. T.	Ext. Dist. Æ.	Long Chord LC.
31° 10' 20 30 40 50	1606.9 1615.9 1624.9 1633.9	218.66221.08223.51225.96228.42	3094.5 3110.5 3126.6 3142.6	${\begin{array}{*{20}c} {41}^{\circ} \\ {10} \\ {20} \\ {30} \\ {40} \\ {50} \end{array}}$	$\begin{array}{c} 2151.7\\ 2161.2\\ 2170.8\\ 2180.3\\ 2189.9 \end{array}$	$\begin{array}{r} 394.06\\ 397.43\\ 400.82\\ 404.22 \end{array}$	$\begin{array}{r} 4028.7\\ 4044.3\\ 4059.9\\ 4075.5\\ 4091.1 \end{array}$	$51^{\circ}\ 10\ 20\ 30\ 40\ 50$	$\begin{array}{r} 2732.9\\ 2743.1\\ 2753.4\\ 2763.7\\ 2773.9\\ 2784.2\end{array}$	$\begin{array}{r} 622 \cdot 81 \\ 627 \cdot 24 \\ 631 \cdot 69 \\ 636 \cdot 16 \\ 640 \cdot 66 \end{array}$	4933.4 4948.4 4963.4 4978.4 4993.4 5008.4
$32^{\circ}$ 10 20 30 40 50	$1670.0 \\ 1679.1 \\ 1688.1$	233.39235.90238.43240.96243.52	3206.6 3222.6 3238.6		2199.42209.02218.62228.12237.72247.3	$\begin{array}{r} 411 \cdot 07 \\ 414 \cdot 52 \\ 417 \cdot 99 \\ 421 \cdot 48 \\ 424 \cdot 98 \end{array}$	$\begin{array}{r} 4153 \cdot 3 \\ 4168 \cdot 8 \\ 4184 \cdot 3 \end{array}$	$\overline{52^{\circ}}_{10}$ 20 30 40 50	2794.5 2804.9 2815.2 2825.6 2835.9 2846.3		5038.45053.45068.35083.35098.2
$     \begin{array}{r}       33^{\circ} \\       10 \\       20 \\       30 \\       40 \\       50 \\       \overline{34^{\circ}}     \end{array} $	$1724 \cdot 4$ $1733 \cdot 5$ $1742 \cdot 6$	246.08 248.66 251.26 253.87 256.50 259.14	3334.4		$2295.6 \\ 2305.2$	$\begin{array}{r} 432\cdot04\\ 435\cdot59\\ 439\cdot16\\ 442\cdot75\\ 446\cdot35\end{array}$	$4230.8 \\ 4246.3$		2888.0 2898.4 2908.9	696.13	5128.0 5142.9 5157.8 5172.7 5187.6
$     \begin{array}{r}       34 \\       10 \\       20 \\       30 \\       40 \\       50 \\       \overline{35^{\circ}}     \end{array} $	1760.8 1770.0 1779.1 1788.2	$261 \cdot 80  264 \cdot 47  267 \cdot 16  269 \cdot 86  272 \cdot 58  275 \cdot 31  278 \cdot 05 $	3350.4 3366.3 3382.2 3398.2 3414.1 3430.0 3445.9	$     \begin{array}{r}             44^{\circ} \\             10 \\             20 \\             30 \\             40 \\             50 \\             45^{\circ}         \end{array}     $	$\begin{array}{r} 2314.9\\ 2324.6\\ 2334.3\\ 2344.1\\ 2353.8\\ \underline{2363.5}\\ 2373.3\end{array}$	$\begin{array}{r} 449.98\\ 453.62\\ 457.27\\ 460.95\\ 464.64\\ 468.35\\ 472.08\\ \end{array}$	$\begin{array}{r} 4292.7\\ 4308.2\\ 4323.6\\ 4339.0\\ 4354.5\\ \underline{4369.9}\\ 4385.3\end{array}$		2919.42929.92940.42951.02961.52972.12982.7	700.89705.66710.46715.28720.11724.97729.85	5217.3 5232.1
$     \begin{array}{r}       10 \\       20 \\       30 \\       40 \\       50 \\       36^{\circ}     \end{array} $	1815.71824.91834.11843.31852.5	278.03 280.82 283.60 286.39 289.20 292.02 294.86	$\begin{array}{r} 3461\cdot 8\\ 3477\cdot 7\\ 3493\cdot 5\\ 3509\cdot 4\\ 3525\cdot 3\end{array}$	10 20 30 40 50	2383.12392.82402.62412.42422.3	475.82 479.59 483.37 487.16 490.98	$\begin{array}{r} 4400.7 \\ 4416.1 \\ 4431.4 \\ 4446.8 \\ 4462.2 \end{array}$	$     \begin{array}{r}       55 \\       10 \\       20 \\       30 \\       40 \\       50 \\       56^{\circ}     \end{array} $	2993.3 3003.9 3014.5 3025.2 3035.8	734.76739.68744.62749.59754.57	$5306 \cdot 1  5320 \cdot 9  5335 \cdot 6  5350 \cdot 4  5365 \cdot 1 $
10 20 30 40 50	1880.1 1889.4 1898.6 1907.9	297.72 300.59 303.47 306.37 309.29	3557.0 3572.8 3588.6 3604.5 3620.3	$     \begin{array}{r}             46^{\circ} \\             10 \\             20 \\             30 \\             40 \\             50 \\             \hline             10 \\             20 \\             30 \\             40 \\             50 \\             \hline             10 \\             20 \\             30 \\             40 \\             50 \\             \hline         $	2432.12441.92451.82461.72471.52481.4	502.54506.42510.33 $514.25$	$\begin{array}{r} 4523 \cdot 5 \\ 4538 \cdot 8 \\ 4554 \cdot 1 \end{array}$	10 20 30 40 50	3046.5 3057.2 3067.9 3078.7 3089.4 3100.2	774.73779.83784.94	5409.2 5423.9 5438.6 5453.3
$37^{\circ}$ 10 20 30 40 50	$1954.3 \\ 1963.6$	$324.11 \\ 327.12$	$3636 \cdot 1$ $3651 \cdot 9$ $3667 \cdot 7$ $3683 \cdot 5$ $3699 \cdot 3$ $3715 \cdot 0$	$     47^{\circ} \\     10 \\     20 \\     30 \\     40 \\     50     $	2491.3 2501.2 2511.2 2521.1 2531.1 2541.0	538.18	$\begin{array}{r} 4584.7\\ 4599.9\\ 4615.2\\ 4630.4\\ 4645.7\end{array}$	$57^{\circ}$ 10 20 30 40 50	$3143.4 \\ 3154.2 \\ 3165.1$	816.10	
$38^{\circ}$ 10 20 30 40 50 	1972.9 1982 2 1991 5 2000.9 2010.2 2019.6	$\frac{342 \cdot 41}{345 \cdot 52}$	$3730 \cdot 8$ $3746 \cdot 5$ $3762 \cdot 3$ $3778 \cdot 0$ $3793 \cdot 8$ $3809 \cdot 5$	$     48^{\circ} \\     10 \\     20 \\     30 \\     40 \\     50 \\     \hline     70^{\circ}     $	2551.02561.02571.02581.02591.12601.1	550.39554.50558.63562.77	$\begin{array}{r} 4660 \cdot 9 \\ 4676 \cdot 1 \\ 4691 \cdot 3 \\ 4706 \cdot 5 \\ 4721 \cdot 7 \\ 4736 \cdot 9 \end{array}$	$58^{\circ}$ 10 20 30 40 50	$3176 \cdot 0$ $3186 \cdot 9$ $3197 \cdot 8$ $3208 \cdot 8$ $3219 \cdot 7$ $3230 \cdot 7$ $3230 \cdot 7$	821.37826.66831.98837.31842.67848.06	5555.6 5570.2 5584.7 5599.3 5613.8 5628.3
	$2029 \cdot 0$ $2038 \cdot 4$ $2047 \cdot 8$ $2057 \cdot 2$ $2066 \cdot 6$ $2076 \cdot 0$	348.64 351.78 354.94 358.11 361.29 364.50	3825 · 2 3840 · 9 3856 · 6 3872 · 3 3888 · 0 <u>3903 · 6</u>	$     \begin{array}{r}             49^{\circ} \\             10 \\             20 \\             30 \\             40 \\             50 \\             \hline             70^{\circ}         $	$\begin{array}{r} 2611 \cdot 2 \\ 2621 \cdot 2 \\ 2631 \cdot 3 \\ 2641 \cdot 4 \\ 2651 \cdot 5 \\ \underline{2661 \cdot 6} \\ \end{array}$	566.94 571.12 575.32 579.54 583.78 588.04	4752.1 4767.3 4782.4 4797.5 4812.7 4827.8	$59^{\circ}$ 10 20 30 40 50	$\begin{array}{r} 3241 \cdot 7 \\ 3252 \cdot 7 \\ 3263 \cdot 7 \\ 3274 \cdot 8 \\ 3285 \cdot 8 \\ 3296 \cdot 9 \\ \hline \end{array}$	853.46 858.89 864.34 869.82 875.32 880.84	$5671 \cdot 8$ $5686 \cdot 3$ $5700 \cdot 8$ $5715 \cdot 2$
$     \begin{array}{r}         \overline{40^{\circ}} \\             10 \\             20 \\             30 \\             40 \\             50 \\             \overline{10^{\circ}} \\             10 \\             20 \\             30 \\             40 \\             50 \\             \overline{10^{\circ}} \\             10 \\             20 \\             30 \\             40 \\             50 \\             \overline{10^{\circ}} \\        $	$\begin{array}{r} 2123 \cdot 3 \\ 2132 \cdot 7 \end{array}$	$367 \cdot 72$ $370 \cdot 95$ $374 \cdot 20$ $377 \cdot 47$ $380 \cdot 76$ $384 \cdot 06$		$50^{\circ}$ 10 20 30 40 50 $50^{\circ}$	2671.8 2681.9 2692.1 2702.3 2712.5 2722.7	609.62 614.00	4888.2 4903.2 4918.3		3352.6 3363.8	903.15 908.79 914.45	5758.5 5772.9 5787.3 5801.7
41°	2142.2	387.38	4013.1	<b>51°</b>	12732.9	618.39	14933.4	101.	13375-0	1920-14	5816.0

# TABLE II.—TANGENTS, EXTERNAL DISTANCES, AND LONG CHORDS FOR A 1° CURVE. Ext. Long A Tang. Ext. Long A Tang. Ext. Long Chord A Tang. Tang. (

Δ	Tang,	Dist. E.	Chord LC.	Δ	Tang. I.	Dist. E.	Chord LC.	Δ	Tang. T.	Dist. E.	Chord L.C.
$ \begin{array}{c}     \hline             61^{\circ} \\             10' \\             20 \\             30 \\             40 \\             50 \\             50 \\           $	3375.03386.33397.53408.83420.13431.43442.73454.13465.4	$925 \cdot 85931 \cdot 58937 \cdot 34943 \cdot 12948 \cdot 92954 \cdot 75$	5844.75859.15873.45887.75902.05916.3	$71^{\circ} \\ 10 \\ 20 \\ 30 \\ 40 \\ 50 \\ 72^{\circ} \\ 10 \\ 20$	$\begin{array}{r} 4099 \cdot 5 \\ 4112 \cdot 1 \\ 4124 \cdot 8 \\ 4137 \cdot 4 \\ \underline{4150 \cdot 1} \\ 4162 \cdot 8 \\ 4175 \cdot 6 \end{array}$	$1322 \cdot 9 \\ 1330 \cdot 3 \\ 1337 \cdot 7 \\ 1345 \cdot 1 \\ 1352 \cdot 6$	$\begin{array}{c} 6668.0\\ 6681.6\\ 6695.1\\ 6708.6\\ 6722.1\\ 6735.6\\ 6749.1 \end{array}$	$     \begin{array}{r}             81^{\circ} \\             10 \\             20 \\             30 \\             40 \\             50 \\             82^{\circ} \\             10 \\             20         $	$\begin{array}{r} 4908\cdot 0\\ 4922\cdot 5\\ 4937\cdot 0\\ 4951\cdot 5\\ 4966\cdot 1\\ 4980\cdot 7\\ 4995\cdot 4\end{array}$	1805.31814.71824.11833.61843.11852.61862.21871.81881.5	7442.2 7454.9 7467.5 7480.2 7492.8 7505.4 7518.0 7530.5 7543.1
30 40 50	3476.8 3488.2 3499.7	972.39		30 40 50	$4201.2 \\ 4214.0$		6776.0 6789.4 6802.8	30 40 50	5024.8 5039.5	1891.2 1900.9 1910.7	7555.6 7568.2 7580.7
63° 10 20 30 40 50	$\begin{array}{r} 3511 \cdot 1 \\ 3522 \cdot 6 \\ 3534 \cdot 1 \\ 3545 \cdot 6 \\ 3557 \cdot 2 \\ 3568 \cdot 7 \end{array}$	$\frac{1008.3}{1014.4}\\ \underline{1020.5}$	5987.56001.76015.96030.06044.26058.4	$73^{\circ}$ 10 20 30 40 50	$\begin{array}{r} 4265\cdot 6\\ 4278\cdot 5\\ 4291\cdot 5\\ 4304\cdot 6\end{array}$	$\begin{array}{r} 1413.5\\ 1421.2\\ 1429.0\\ \underline{1436.8}\end{array}$	6856-4 6869-7	$83^{\circ}$ 10 20 30 40 50	$5084.0 \\ 5099.0 \\ 5113.9 \\ 5128.9 \\ 5143.9 \\ 5143.9 \\ $	1960.2 1970.3	7593.2 7605.6 7618.1 7630.5 7643.0 7655.4
$ \begin{array}{c} 64^{\circ} \\ 10 \\ 20 \\ 30 \\ 40 \\ 50 \end{array} $	$\begin{array}{r} 3591.9\\ 3603.5\\ 3615.1\\ 3626.8\\ 3638.5 \end{array}$		$\begin{array}{c} 6072 \cdot 5 \\ 6086 \cdot 6 \\ 6100 \cdot 7 \\ 6114 \cdot 8 \\ 6128 \cdot 9 \\ 6143 \cdot 0 \end{array}$	$74^{\circ}$ 10 20 30 40 50	$\begin{array}{r} 4330\cdot 7\\ 4343\cdot 8\\ 4356\cdot 9\\ 4370\cdot 1\\ \underline{4383}\cdot 3\end{array}$	$1468.4 \\ 1476.4 \\ 1484.4$	6923.0 6936.2 6949.5 6962.8	$     \begin{array}{r}       10 \\       20 \\       30 \\       40 \\       50     \end{array} $	5174.1 5189.3 5204.4 5219.7 5234.9	$\tfrac{2021.1}{2031.4}$	7704.9 7717.2 7729.5
65° 10 20 30 40 50	3685.4 3697.2 3709.0	$   \begin{array}{r}     1070 \cdot 2 \\     1076 \cdot 6 \\     1082 \cdot 9 \\     1089 \cdot 3 \\     1095 \cdot 7   \end{array} $	$\begin{array}{c} 6157\cdot 1\\ 6171\cdot 1\\ 6185\cdot 2\\ 6199\cdot 2\\ 6213\cdot 2\\ 6227\cdot 2\end{array}$	_50	$\begin{array}{r} 4423.1 \\ 4436.4 \\ 4449.7 \\ \underline{4463.1} \end{array}$	1500.5 1508.6 1516.7 1524.9 1533.1	7002.4 7015.6 7028.8 7041.9	10 20 30 40 50	$5281.0 \\ 5296.4 \\ 5311.9 \\ 5327.4$	$\begin{array}{r} 2052.1 \\ 2062.5 \\ 2073.0 \\ 2083.5 \\ 2094.1 \end{array}$	7778-6 7790-8 7803-0
66° 10 20 30 40 50	3732.7 3744.6 3756.5 3768.5 3768.5 3780.4	1102.21108.61115.11121.71128.21134.8	$\begin{array}{c} 6241 \cdot 2 \\ 6255 \cdot 2 \\ 6269 \cdot 1 \\ 6283 \cdot 1 \\ 6297 \cdot 0 \\ 6310 \cdot 9 \end{array}$	$10 \\ 20 \\ 30 \\ 40 \\ 50$	$\begin{array}{r} 4489 \cdot 9 \\ 4503 \cdot 4 \\ 4516 \cdot 9 \\ 4530 \cdot 4 \\ 4544 \cdot 0 \end{array}$	$1541 \cdot 4 \\ 1549 \cdot 7 \\ 1558 \cdot 0 \\ 1566 \cdot 3 \\ 1574 \cdot 7 \\ 1583 \cdot 1 $	7068.2 7081.3 7094.4 7107.5 7120.5	$     \begin{array}{r}       10 \\       20 \\       30 \\       40 \\       50 \\     \end{array} $	$5405.6 \\ 5421.4$	2115.32126.02136.72147.52158.4	
67° 10 20 30 40 50	$     3804.4 \\     3816.4 \\     3828.4 \\     3840.5 $	1141.41148.01154.71161.31168.11174.8	$\begin{array}{r} 6324 \cdot 8 \\ 6338 \cdot 7 \\ 6352 \cdot 6 \\ 6366 \cdot 4 \\ 6380 \cdot 3 \\ \underline{6394 \cdot 1} \end{array}$	10 20 30 40 50	4571 · 2 4584 · 8	1608 · 6 1617 · 1 1625 · 7	7146.6 7159.6 7172.6	$     \begin{array}{c}       10 \\       20 \\       30 \\       40 \\       50 \\     \end{array} $	5453.1 5469.0 5484.9	$2180 \cdot 2$ $2191 \cdot 1$ $2202 \cdot 2$ $2213 \cdot 2$ $2224 \cdot 3$	7912.2 7924.3 7936.3 7948.3
68° 10 20 30 40 50	3876.8 3889.0 3901.2 3913.4 3925.6	1181.61188.41195.21202.01208.91215.8	$\begin{array}{r} 6408 \cdot 0 \\ 6421 \cdot 8 \\ 6435 \cdot 6 \\ 6449 \cdot 4 \\ 6463 \cdot 1 \\ 6476 \cdot 9 \end{array}$	$     \begin{array}{r}       10 \\       20 \\       30 \\       40 \\       50     \end{array} $	4653 · 6 4667 · 4		7224 - 5 7237 - 4 7250 - 4 7263 - 3	$     \begin{array}{c}       10 \\       20 \\       30 \\       40 \\       50 \\     \end{array} $	5597.8 5614.2	2246 · 7 2258 · 0 2269 · 3 2280 · 6 2292 · 0	7984.2 7996.2 8008.1 8020.0
69° 10 20 30 40 50	3950.2 3962.5 3974.8 3987.2 3999.5	$   \begin{array}{r}     1236.7 \\     1243.7 \\     1250.8 \\     1257.9   \end{array} $	$\begin{array}{r} 6490 \cdot 6\\ 6504 \cdot 4\\ 6518 \cdot 1\\ 6531 \cdot 8\\ 6545 \cdot 5\\ 6559 \cdot 1\end{array}$	$     \begin{array}{r}       10 \\       20 \\       30 \\       40 \\       50     \end{array} $	4779.4 4793.6	1704 - 7 1713 - 7 1722 - 7 1731 - 7 1740 - 8	7301.9 7314.7 7327.5 7340.3 7353.1	$     \begin{array}{c}       10 \\       20 \\       30 \\       40 \\       50     \end{array} $	5646.9 5663.4 5679.9 5696.4 5713.0	$\begin{array}{r} 2315 \cdot 0 \\ 2326 \cdot 6 \\ 2338 \cdot 2 \\ 2349 \cdot 8 \\ 2361 \cdot 5 \end{array}$	8079.3 8091.2
70° 10 20 30 40 50	$\begin{array}{r} 4024.4\\ 4036.8\\ 4049.3\\ 4061.8\\ 4074.4\end{array}$	1265.01272.11279.31286.51293.71300.9	$6572 \cdot 8$ $6586 \cdot 4$ $6600 \cdot 1$ $6613 \cdot 7$ $6627 \cdot 3$ $6640 \cdot 9$	$10 \\ 20 \\ 30 \\ 40 \\ 50$	4822.0 4836.2 4850.5 4864.8 4879.2	$1749 \cdot 9 \\ 1759 \cdot 0 \\ 1768 \cdot 2 \\ 1777 \cdot 4 \\ 1786 \cdot 7 \\ 1796 \cdot 0 $	7378.7 7391.4 7404.1 7416.8 7429.5	10 20 30 40 50	5796.7 5813.6	$2385 \cdot 1 \\ 2397 \cdot 0 \\ 2408 \cdot 9 \\ 2420 \cdot 9 \\ 2432 \cdot 9 \\ 2432 \cdot 9 \\ 3 \\ 2432 \cdot 9 \\ 3 \\ 3 \\ 3 \\ 3 \\ 3 \\ 3 \\ 4 \\ 3 \\ 3 \\ 4 \\ 3 \\ 3$	8103.0 8114.7 8126.5 8138.2 8150.0 8161.7
71°	4086-9	1308.2	6654.4	<b>81°</b>	4893.6	1805.3	7442.2	<u>191.°</u>	5830.5	2444.9	8173.4

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#### TABLE III .--- SWITCH-LEADS AND DISTANCES.

LEAD-RAILS CIRCULAR THROUGHOUT; GAUGE 4'81/. Sec § 262.

Frog No. (n)	$\begin{array}{c} \operatorname{Frog}\operatorname{Angle}\\ (F). \end{array}$	Lead (L) (Eq. <b>7</b> 9)	$\begin{array}{c} \text{Chord} \\ (QT) \\ (\text{Eq. 77}). \end{array}$	Radius of Lead-rails (r, Eq.78).	Log r.	Length of Switch- rails (QK, Eq. 81).	Frog No. (n)
4 5 6 7	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	37.67 47.08 56.50 65.92	37.38 46.85 56.30 65.75	150.67235.42339.00461.42	$\begin{array}{r} 2.1780\overline{1}\\.37183\\.53020\\.66409\end{array}$	$\begin{array}{c} 11.73 \\ 14.65 \\ 17.62 \\ 20.53 \end{array}$	4 5 6 7
$     \begin{array}{r}             8 \\             9 \\           $	$\begin{array}{cccc} 7^{\circ} & 09' & 10 \\ 6 & 21 & 35 \\ 6 & 01 & 32 \\ 5 & 43 & 29 \end{array}$	75.3384.7589.4694.17	75.1984.6289.3394.05	602.67 762.75 849.85 941.67	$.7800\overline{7}$ .88238 .92934 2.97389	$23.48 \\ 26.43 \\ 27.97 \\ 29.37$	$     \begin{array}{c}       8 \\       9 \\       9^{\frac{1}{2}} \\       10     \end{array}   $
$11 \\ 12 \\ 15 \\ 16$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$103.58 \\ 113.00 \\ 141.25 \\ 150.67$	$103.47 \\ 112.90 \\ 141.17 \\ 150.59$	$1139.42 \\ 1356.00 \\ 2118.75 \\ 2410.67$	$3.0566^{\overline{p}}$ .13226 .32608 .38213	$35.25 \\ 44.06$	$11 \\ 12 \\ 15 \\ 16$
18 20 24	$3^{\circ} 10' 56'' 2 51 51 2^{\circ} 23' 13''$	169.50 188.33 226.00	$169.43 \\ 188.27 \\ 225.95$	$3051.00 \\ 3766.67 \\ 5424.00$	$.48444 \\ .57595 \\ 3.73432$	$52.87 \\ 58.76 \\ 70.52$	18 20 24

TURNOUTS WITH STRAIGHT POINT-RAILS AND STRAIGHT FROG RAILS; GAUGE 4' 8<sup>1</sup>/<sub>2</sub>". See §§ 265 and 276.

	s.		Fr	og.			Switch.			Switch Dimensions.										
g No.	Frog Bluntness.	<i>ଆ</i> ପ	ail.	Total	ngth.	oth.	0	A	lng	le.	Rad	ius.		egr of Lead		L'e	th.		Clos	sure.
(n) Frog	ы. Н Н		r f)	Ê) (H		D. Lenoth			(α	)	(r	)		urv (D)	e.	(1	2)	Str' Ra		Curv'd Rail.
	ft.	ft.	in.				in.	0	,	"	ft		0	,	"	ft		ft		ft.
4 5 6 7	$0.17 \\ 0.21 \\ 0.25 \\ 0.29$	3 3 4 4	2 7 0 5	8 10 11 12	6 0 0 6	$     \begin{array}{c}       11 \\       11 \\       11 \\       16     \end{array} $	0 0 0 6	2 2 2 1	36 36 36 44	$19\\19\\19\\19\\11$	$112 \\ 183 \\ 273 \\ 364$	·22 ·95	$\frac{31}{21}$	53 40 01 47	$56 \\ 24 \\ 58 \\ 19$	42 48	·22 ·98 ·36 ·23	22 28 33 41	. 19 . 11	$23.29 \\ 28.55 \\ 33.38 \\ 41.24$
	$0.33 \\ 0.37 \\ 0.40 \\ 0.42$		9 0 0 0	$13 \\ 16 \\ 16 \\ 16 \\ 16 \\ 16 \\ 16 \\ 16 \\ $	6 0 0 6	16 16 16 16	6 6 6	1 1 1 1	44 44 44 44	11 11 11 11 11	$488 \\ 616 \\ 699 \\ 790$	·27 ·97		44 18 11 15	40 27 33 18	72 75	· 80 · 61 · 30 · 93	46 49 52 55	.74 .40	$\begin{array}{r} 46.42 \\ 49.92 \\ 52.58 \\ 55.17 \end{array}$
$11 \\ 12 \\ 15 \\ 16$	$0.46 \\ 0.50 \\ 0.62 \\ 0.67$		0 5 8 0	17 18 22 24	6 6 6 0	22 22 33 33	0 0 0 0	$1 \\ 1 \\ 0 \\ 0 \\ 0$	18 18 52 52	05	$940 \\ 1136 \\ 1744 \\ 2005$	·34 ·38	3	05 02 17 51					83 36	64.20 68.96 92.46 95.05
18 20 24	$0.75 \\ 0.83 \\ 1.00$	8 9 11	10 8 4	29	6 0 6	33 33 33	0 0 0	0 0 0	52 52 52	05	$2587 \\ 3262 \\ 4932$	.98	1	12 45 09	22	157	.18	$104 \\ 113 \\ 130$	68	$104.61 \\ 113.76 \\ 130.77$

#### TABLE III. SWITCH LEAD AND DISTANCES .- Continued.

TRIGONOMETRICAL FUNCTIONS OF THE FROG ANGLES.

Frog No. (n)	Frog Angle (F).	Nat. $\sin F$ .	Nat. $\cos F$ .	Log sin F.	Log cos F.	$\begin{array}{c} \operatorname{Log}\\ \operatorname{cot} F. \end{array}$	Log vers F.	Frog No. (n)
4 5 6 7	$\begin{array}{ccccccc} 14^\circ \ 15' \ 00'' \\ 11 \ \ 25 \ \ 16 \\ 9 \ \ 31 \ \ 38 \\ 8 \ \ 10 \ \ 16 \end{array}$	$\begin{array}{r} .24615 \\ .19802 \\ .16552 \\ .14213 \end{array}$	.96923 .98020 .98621 .98985	$\begin{array}{r} 9.3912\overline{0} \\ .29670 \\ .21884 \\ .15268 \end{array}$	.99131 .99397	.69461 .77513	·29670	4 5 6 7
	$\begin{array}{ccccccc} 7 & 09 & 10 \\ 6 & 21 & 35 \\ 6 & 01 & 32 \\ 5 & 43 & 29 \end{array}$	.12452 .11077 .10497 .09975	.99222 .99385 .99448 .99501	$0952\overline{2}$ $0444\overline{2}$ 9.02107 8.99891	.99660 .9973 <u>2</u> .99759 .99783	$\begin{array}{r} \cdot & 9013\overline{8} \\ \cdot & 95289 \\ \cdot & 97652 \\ 10 \cdot 99892 \end{array}$	7.89110.78915.74232.69787	8 9 9 <sup>1</sup> / <sub>2</sub> 10
$     \begin{array}{c}       11 \\       12 \\       15 \\       16     \end{array} $	$\begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	09072 08319 06659 06244	.99588 .99653 .99778 .99805	.95770 .92007 .82343 .79543	.99820 .99849 .99903 .99915		·53986 ·34631	$11 \\ 12 \\ 15 \\ 16$
18 20 24	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	.05551 .04997 .04165	.99846 .99875 .99913	$.7443\overline{8} \\ .69869 \\ 8.61959$	.99933 .99945 9.99962		$.1880\overline{7}$ 7.0966 <u>3</u> 6.93834	18 20 24

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#### TABLE IV.-ELEMENTS OF TRANSITION CURVES.

Point.	-1010041000-8000			10	8' 10'' 2 30 37 45 5 00 37 30 5 00 5 00 5 00 7 80 7 80
	0000 0000 0000 0000 0000 0000 0000 0000 0000			-	0     33     33     28       1     1     46     28       1     1     2     16       1     1     16     16       0     37     13     13
n	25.0 55.0 55.0 124.9 124.9 124.9 124.9 224.7 2224.7 2224.7 2224.7		Ì		45 <sup>//</sup> 330 15 15 30 30 30 30 30 30
	000000			6	38 24 38 07 33 00 33 33 33 33 33 33 33 33 33 33 33
8	6611760030000000000000000000000000000000		at-		
Log	43568 134668 581815 581815 58181 17602 39467 58171 58171 58171 58171 58171 58171 58171 58164 58164 58164 58164 58164 58164 58164 58166 58171 58171 58171 58175 581		is a	æ	22 <sup>1</sup> 22 <sup>1</sup>
	80000000H		nent		20°54 29°54 28°54
	000000000000		at the point occupied when the instrument is		00/ 52 337 15 15 15 15
8	$\begin{array}{c} 0.027\\ 0.136\\ 0.136\\ 0.818\\ 0.818\\ 2.481\\ 7.792\\ 0.489\\ 0.489\end{array}$		e in	r	15 03 112 112 00 01 30 30 30 31 31 31 31 31 31 31 31 31 31 31 31 31
			n th		<u>инноооонн</u>
4	202010100000000000000000000000000000000	¥.	whe	9	<pre>/ 37'/ 00 07 07 07 07 07 07 07 07 00 00 00 00</pre>
Log vers	$\begin{array}{c} 4\cdot 37654\\ 5\cdot 33078\\ 5\cdot 33078\\ 6\cdot 33078\\ 6\cdot 37653\\ 6\cdot 72869\\ 6\cdot 72869\\ 7\cdot 28699\\ 7\cdot 68289\\ 7\cdot 68289\\ 7\cdot 82675\\ 7\cdot 82675\\ 7\cdot 85675\end{array}$	Равт	pied	-	$\begin{array}{c} 1^{\circ} \pm 0^{\prime} \\ 1^{\circ} \pm 0^{\prime} \\ 1^{\circ} \pm 0^{\prime} \\ 1^{\circ} \pm 0^{\circ} \\ 0 \pm 3 \\ 0 \pm 3 \\ 0 \pm 3 \\ 0 \pm 4 \\ 0 \pm 5 \\ 1 \pm 5 \\$
Log	4444488888		nooc		115/115/115/115/115/115/115/115/115/115
÷	<b>O</b> 010101014 0 01010	iral	int	10	111' 1 01 7 01 7 00 7 18 6 18 6 18 6 18 6 18 6 18 6 113 6 113 6 113 6 113 6 113 6 113 6 113 6 113 6 113 6 111' 1 111' 1 11' 11'
g cos	$\begin{array}{c} 10 . 0 000 0\\ 9 . 9 9 9 9 9 9 9\\ 9 . 9 9 9 9 9 9 9 9 9 9 9 9 9$	t sp	le pc		<u>8 1 1 0 0 0 0 0 0 1 1 0 1 0 1 0 0 0 0 0 </u>
Log		-fee	at th		$\begin{array}{c} 52^{\prime\prime} \\ 45 \\ 00 \\ 00 \\ 00 \\ 00 \\ 01 \\ 15 \\ 52 \\ 52 \\ 52 \\ 52 \\ 52 \\ 7 \\ 52 \\ 52$
-0-	100010100100000000000000000000000000000	-85	ent	4	$\begin{array}{c} 0^{\circ} \ 46'\\ 0 \ 38\\ 0 \ 38\\ 0 \ 38\\ 0 \ 39\\ 0 \ 39\\ 1 \ 28\\ 2 \ 6\ 6\\ 2 \ 6\\ 2 \ 6\ 6\ 6\ 6\ 6\ 6\ 6\ 6\ 6\ 6\ 6\ 6\ 6$
-us	.33878 116920 53878 53875 53875 5608	30'-per-25-feet spiral.	tang		837 000 000 000 000 000 000 000 000 000 0
Log	<b>⊳⊳∞∞∞∞∞∞∞</b> ∞		the	e	227'3 2203 2203 2000 2000 2315 2315 2315 2315 2323 233 2334 2334 2334 2334 2334 2334
-0-	a ta	õ	Deflections from the tangent		
Nat, cos	000 000 000 000 000 000 00 00 00 00 00		ns f		07'' 00 15 15 15 15 15 00 07 07 37 37 37
Nat			ectic	R	113 00 58 58 118 118 118 118 118 118 118 118 1
-0-			Defl		$\begin{array}{c} \begin{array}{c} & & & \\ & & & & & \\ & & & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & & \\ & $
sin	$\begin{array}{c} 0.022\\ 0.0065\\ 0.0131\\ 0.0218\\ 0.0218\\ 0.0218\\ 0.0327\\ 0.0810\\ 0.0810\\ 0.0980\\ 0.0980\\ 0.0980\\ 0.0980\\ 0.0980\\ 0.0980\\ 0.0980\\ 0.0980\\ 0.0980\\ 0.0980\\ 0.0980\\ 0.0980\\ 0.0980\\ 0.0980\\ 0.0980\\ 0.0980\\ 0.0080\\ $			-	
Nat.				_	
e	2			-	0, 115 115 115 115 115 115 115 115 115 11
Ang	8888888888			Q	3 3 3 3 3 5 6 7 6 1 5 8 5 8 5 8 5 8 5 8 5 8 5 8 5 8 5 8 5
Total Central Angle	024000 023004000 023004000			ы. 1	<u> 000000000000000000000000000000000000</u>
				sighting at	0 - 8 8 4 6 9 2 8 6 0
Point.	1008400-800			ata	

#### TABLE IV .- ELEMENTS OF TRANSITION CURVES.

Dimensions of various 0° 30'-per-25-feet spirals.-Part B.

Deg. of	L'gth of	ZK	QK	A'N	NQ	A' t	o Z.	Deg.
curve.	spiral	21	QA	A N		Defl.	Dist.	curve.
1° 00′ 10 20 30 40 50	25 50 50 50 75 75	$\begin{array}{c} 0.03 \\ 0.14 \\ 0.14 \\ 0.14 \\ 0.38 \\ 0.38 \\ 0.38 \end{array}$	$\begin{array}{r} 25.00 \\ 50.00 \\ 50.00 \\ 50.00 \\ 75.00 \\ 75.00 \\ 75.00 \end{array}$	$\begin{array}{c} 0.01 \\ 0.03 \\ 0.04 \\ 0.05 \\ 0.09 \\ 0.11 \end{array}$	$12.50 \\ 17.86 \\ 21.88 \\ 25.00 \\ 30.00 \\ 43.09$	$\begin{array}{cccc} 0^{\circ} & 04' \\ 0 & 11 \\ 0 & 11 \\ 0 & 11 \\ 0 & 22\frac{1}{2} \\ 0 & 22\frac{1}{2} \end{array}$	12.5032.1428.1325.0045.0040.91	1° 00' 10 20 30 40 50
2° 00' 10 20 30 40 50	75 100 100 100 125 125	0.38 0.82 0.82 0.82 1.50 1.50	$\begin{array}{r} 75.00 \\ 100.00 \\ 100.00 \\ 100.00 \\ 124.99 \\ 124.99 \\ 124.99 \end{array}$	0.14 0.19 0.23 0.27 0.35 0.42	37.50 42.30 46.43 50.00 54.68 58.81	$\begin{array}{cccc} 0^{\circ} & 22\frac{1}{2}' \\ 0 & 37\frac{1}{2} \\ 0 & 37\frac{1}{2} \\ 0 & 37\frac{1}{2} \\ 0 & 56 \\ 0 & 56 \end{array}$	37.50 57.69 53.57 50.00 7C.31 66.18	2° 00' 10 20 30 40 50
8° 00' 10 20 30 40 50	125 150 150 150 175 175	1.50 2.48 2.48 2.48 3.82 3.82	124.99 149.97 149.97 149.97 149.97 174.93 174.93	0.48 0.58 0.68 0.76 0.90 1.03	62.49 67.09 71.24 74.98 79.52 83.67	0° 56' 1 19 1 19 1 19 1 45 1 45	62.50 82.59 78.75 75.00 95.45 91.30	3° 00' 10 20 30 40 50
4° 00' 10 20 30 40 50	175 200 200 200 225 225	3.82 5.56 5.56 5.56 7.79 7.79	174.93 199.87 199.87 199.87 224.77 224.77	1.15 1.32 1.48 1.63 1.88 2.08	$\begin{array}{r} 87.47\\91.96\\96.11\\99.95\\104.40\\108.55\end{array}$	$\begin{array}{cccc} 1^{\circ} & 45' \\ 2 & 15 \\ 2 & 15 \\ 2 & 15 \\ 2 & 49 \\ 2 & 49 \\ 2 & 49 \end{array}$	87.50 108.00 103.85 100.00 120.54 116.38	4° 00' 10 20 30 40 50
5° 00' 10 20 30	225 250 250 250	7.79 10.49 10.49 10.49 10.49	224.77 249.62 249.62 249.62 249.62	2.27 2.51 2.76 3.00	$112.42 \\ 116.83 \\ 120.98 \\ 124.88$	2° 49' 3 26 3 26 3 26 3 26	112.50 133.06 128.91 125.00	5° 00' 10 20 80

# TABLE IV. -ELEMENTS OF TRANSITION CURVES.

Dimensions of various 0° 30'-per-25-feet spirals.—Part C. VALUES OF AN.

Δ.	Degree of curve.										
2	1°	2°	3°	4°	5°	5° 30'					
2° 4 6 8 10	0.00 0.00 0.00 0.00 0.00	0.00 0.01 0.01 0.01 0.01 0.01	$\begin{array}{c} 0.01 \\ 0.02 \\ 0.03 \\ 0.03 \\ 0.04 \end{array}$	0.02 0.04 0.06 0.08 0.10	0.04 0.08 0.12 0.16 0.20	0.05 0.10 0.18 0.21 0.28					
12° 14 16 18 20	0.00 0.00 0.00 0.00 0.00	0.01 0.02 0.02 0.02 0.02	0.05 0.06 0.07 0.08 0.08	$\begin{array}{c} 0.12 \\ 0.14 \\ 0.16 \\ 0.18 \\ 0.20 \end{array}$	0.24 0.28 0.32 0.36 0.40	0.32 0.37 0.42 0.47 0.53					
22° 24 26 28 30	0.00 0.00 0.00 0.00 0.00	0.03 0.03 0.03 0.03 0.04	0.09 0.10 0.11 0.12 0.13	0.22 0.24 0.26 0.29 0.31	0.44 0.48 0.52 0.57 0.61	0.58 0.64 0.69 0.75 0.80					
82° 84 86 88 40	0.00 0.00 0.00 0.00 0.00	0.04 0.04 0.04 0.05 0.05	0.14 0.15 0.16 0.16 0.17	0.33 0.35 0.37 0.39 0.42	0.65 0.69 0.74 0.78 0.83	0.86 0.92 0.97 1.03 1.C9					
42° 44 46 48 50	0.00 0.00 0.00 0.00 0.00	0.05 0.06 0.06 0.06 0.06 0.06	0.18 0.19 0.20 0.21 -0.22	0.44 0.46 0.49 0.51 0.53	0.87 0.92 0.96 1.01 1.06	1.15 1.21 1.27 1.84 1.40					
52° 54 56 58 60	0.00 0.01 0.01 0.01 0.01 0.01	0.07 0.07 0.07 0.08 0.08	0.23 0.24 0.25 0.26 0.28	$\begin{array}{c} 0.56 \\ 0.58 \\ 0.61 \\ 0.64 \\ 0.66 \end{array}$	1.11 1.16 1.21 1.26 1.31	1.46 1.53 1.59 1.66 1.73					
62° 64 66 68 <b>70</b>	0.01 0.01 0.01 0.01 0.01 0.01	0.08 0.09 0.09 0.09 0.10	0.29 0.30 0.31 0.32 0.33	0.69 0.72 0.74 0.77 0.80	1.36 1.42 1.47 1.53 1.59	1.80 1.87 1.95 2.02 2.10					
72° 74 76 78 80	0.01 0.01 0.01 0.01 0.01	0.10 0.10 0.11 0.11 0.11	$\begin{array}{c} 0.35 \\ 0.36 \\ 0.37 \\ 0.39 \\ 0.40 \end{array}$	0.83 0.83 0.90 0.93 0.96	1.65 1.71 1.77 1.84 1.91	2.18 2.26 2.34 2.43 2.51					
82° 84 86 88 90	0.01 0.01 0.01 0.01 0.01 0.01	0.12 0.12 0.13 0.13 0.14	$\begin{array}{c} 0.42 \\ 0.43 \\ 0.45 \\ 0.46 \\ 0.48 \end{array}$	1.00 1.03 1.07 1.10 1.15	1.97 2.04 2.12 2.19 2.27	2.60 2.70 2.79 2.89 3.00					
92° 94 96 98 100	0.01 0.01 0.01 0.01 0.01 0.01	0.14 0.15 0.15 0.16 0.16	$\begin{array}{c} 0.49 \\ 0.51 \\ 0.53 \\ 0.55 \\ 0.57 \end{array}$	1.19 1.23 1.27 1.32 1.37	$2.35 \\ 2.44 \\ 2.52 \\ 2.61 \\ 2.71$	8.10 3.21 3.33 3.45 3.57					

# TABLE IV.-ELEMENTS OF TRANSITION CURVES.

Point.	1008400 <b>2</b> 800	1		10	8' 22'' 5 05	8 49 7 32		9 00 8 45				8
	0000 0000 0000 0000 0000 0000 0000 0000 0000				8°56' 825	7 48 7 07		5 30 4 33		2 28	- 1	8
s	$\begin{array}{c} 25\cdot000\\ 49\cdot999\\ 74\cdot994\\ 99\cdot979\\ 124\cdot942\\ 174\cdot722\\ 1949\cdot722\\ 199\cdot479\\ 224\cdot049\\ 224\cdot049\\ 224\cdot497\\ 248\cdot497\\ \end{array}$			•	34'' 47	02	8:	42 00	15	80	8	8
				6	7°17′ 648	6 15 5 36		10		-	8	12
8 20	73672 43616 88252 88252 69548 69548 69544 88241 08241 08241 08241 19059 19059 19059 19059 19059		at-		47" 7 30 6			30 4 15 3	80	8	8	45
Log	8000004111 24804080118		Deflections from the tangent at the point occupied when the instrument is	œ	48 22			56	8			18
			ume		ດ ດິ (	4		<u>n 1</u>	<u></u>	0		N]
8	.055 .273 .273 .273 .273 .273 .273 .273 .273		instı	~	) 00'	7 30 8 45		2 T D	00 (			8
	20117421 20117421		the		4°30′ 406	3 37 3 03		L 41 0 52	00 0			3 12
<b>Ф</b>			vhen		15,	45		38	30	45		12
Vers c	97860 937860 937888 97858 97858 87234 87238 87238 28363 1 28363 1 28363 1	<b>1</b> °-	ied v	9	21 <sup>′</sup>	33		45 00	52	48	20	28
Log \	4.9 5.9 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0 8.0	per-	cup		° 00 00	01 0	1	0	0			00
		35-	nt oc	10	45	15		38				8
cos 🕁	9999999 9999999 9999999999999999999999	feet	poi	•	2°22' 2 03	1 40		0 45	L 33			4 30
Log	6.0.0.0.0.0.0.0.0.0.0 0.0.0.0.0.0.0.0.0.	1°-per-35-feet spiral.	t the		45'' 30	00	1 1	45 45	8			43
		ral.	nt al	4	33′	56 30		37	02			23
sin <b>þ</b>	$\begin{array}{c} 63981 \\ 63981 \\ 63981 \\ 63969 \\ 63969 \\ 61792 \\$	P/	ange	<del></del>	<u>е</u> н	00		ъч	01	C1 (		4
Log	7.63 8.11 8.41 8.63 9.08 9.19 9.19 9.29 9.29 9.29	PART .	het	e	, 13 0	88		45 30	15			28
		<b>A</b>	on t		0°55′ 041	0 22	30	42	2 26			5 07
<b>4</b> so	7072188000 70772188000		is fro		15, 0	1 1	45	15 1	30			
Nat, cos	000 000 000 000 000 000 000 000 000 00		ctior	2	26' 1 15 C			20 28 1	37 3			
~			Jeffe		00				67		4	2
sin 🕁			Г	_,	,00 00	00 45	30	15	45	30		55
Nat, s	$\begin{array}{c} .0043\\ .0131\\ .0131\\ .0262\\ .0262\\ .0436\\ .0654\\ .0915\\ .1218\\ .1264\\ .1264\\ .1951\\ .2377\end{array}$			-	00 00 0 00	15 33		28	38	22		. 04
					0 30 30	42		30 I 45 2	00 2			38 2
al Angle				ø	0 07 3			22 3 53 4	30 0			48 3
Total ral A	41000145 41000145 41000155				000				23			4
Central <b>b</b>	131049337100°		1	11 11 11 11 11 11 11 11			· ·	~ ~	~	~	•	
Point.	10984004900			at		0.05	י דדי (	6	r	00	6	9
Po	R				I							1

#### TABLE IV .- ELEMENTS OF TRANSITION CURVES.

1

Dimensions of various 1°-per-25-feet spirals.-Part B.

Deg.	L'gth	77	OF	A'N	NQ	A' t	o Z.	Deg.
of curve.	of spiral	ZK	QK	A' N	110	Defl.	Dist.	of curve.
2° 00′ 10 20 30 40 50	25 50 50 50 50 50	0.06 0.27 0.27 0.27 0.27 0.27 0.27	25.00 50.00 50.00 50.00 50.00 50.00 50.00	$\begin{array}{c} 0.03 \\ 0.05 \\ 0.06 \\ 0.08 \\ 0.09 \\ 0.10 \end{array}$	$12.50 \\ 15.38 \\ 17.86 \\ 20.00 \\ 21.87 \\ 23.53$	$\begin{array}{c} 0^{\circ} & 07\frac{1}{2}\\ 0 & 22\frac{1}{2}\\ 0 & 22\frac{1}{2} \end{array}$	$12.50 \\ 34.62 \\ 32.14 \\ 30.00 \\ 28.13 \\ 26.17$	2° 00' 10 20 30 40 50
8° 00' 10 20 30 40 50	50 75 75 75 75 75	0.27 0.76 0.76 0.76 0.76 0.76	50.00 74.99 74.99 74.99 74.99 74.99 74.99 74.99	$\begin{array}{c} 0.11 \\ 0.14 \\ 0.17 \\ 0.20 \\ 0.23 \\ 0.25 \end{array}$	25.00 27.63 29.99 32.13 34.08 35.86	$\begin{array}{cccc} 0^{\circ} & 22\frac{1}{2}' \\ 0 & 45 \\ 0 & 45 \\ 0 & 45 \\ 0 & 45 \\ 0 & 45 \\ 0 & 45 \end{array}$	25.00 47.37 45.00 42.86 40.19 39.13	3° 00' 10 20 30 40 50
4° 00' 10 20 30 40 50	75 100 100 100 100 100	0.76 1.64 1.64 1.64 1.64 1.64	74.99 99.98 99.98 99.98 99.98 99.98 99.98	0.27 0.33 0.38 0.42 0.47 0.51	$\begin{array}{r} 37.49\\ 39.98\\ 42.29\\ 44.43\\ 46.41\\ 48.26\end{array}$	$\begin{array}{ccc} 0^{\circ} & 45' \\ 1 & 15 \\ 1 & 15 \\ 1 & 15 \\ 1 & 15 \\ 1 & 15 \\ 1 & 15 \end{array}$	37.50 60.00 57.69 55.56 53.57 51.72	4° 00' 10 20 30 40 50
5° 00' 10 20 30 40 50	100 125 125 125 125 125 125	1.64 3.00 3.00 3.00 3.00 3.00	99.98 124.94 124.94 124.94 124.94 124.94 124.94	0.55 0.62 0.70 0.77 0.83 0.90	49.98 52.39 54.65 56.78 58.79 60.67	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	50.00 72.58 70.31 68.18 66.18 64.29	5° 00' 10 20 30 40 50
6° 00' 10 20 30 40 50	125 150 150 150 150 150	3.00 4.96 4.96 4.96 4.96 4.96	124.94 149.87 149.87 149.87 149.87 149.87 149.87	$\begin{array}{c} 0.95 \\ 1.06 \\ 1.16 \\ 1.26 \\ 1.35 \\ 1.44 \end{array}$	62.46 64.81 67.04 69.17 71.18 73.10	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	62.50 85.14 82.89 80.77 78.75 76.83	6° 00' 10 20 30 40 50
7° 00' 10 20 30 40 50	150 175 175 175 175 175 175	4.96 7.63 7.63 7.63 7.63 <b>7.63</b>	$149.87 \\ 174.72 \\ 1$	$1.52 \\ 1.67 \\ 1.80 \\ 1.93 \\ 2.05 \\ 2.17$	74.92 77.23 79.44 81.55 83.58 85.51	$\begin{array}{cccc} 2^{\circ} & 37\frac{1}{2}' \\ 3 & 30 \\ 3 & 30 \\ 3 & 30 \\ 3 & 30 \\ 3 & 30 \\ 3 & 30 \end{array}$	75.00 97.67 95.45 93.33 91.30 89.36	7° 00' 10 20 30 40 50
8° 00' 10 20 30 40 50	175 200 200 200 200 200 200	7.63 11.11 11.11 11.11 11.11 11.11 11.11	174.72 199.48 199.48 199.48 199.48 199.48 199.48	2.29 2.46 2.64 2.80 2.96 3.10	87.37 89.64 91.83 93.94 95.96 97.91	3° 30' 4 30 4 30 4 30 4 30 4 30 4 30	87.50 110.20 108.00 105.88 103.85 101.89	8° 00′ 10 20 30 40 50
9° 00' 10 20 30 40 50	200 225 225 225 225 225 225 225	$11.11 \\ 15.50 \\ 15.5$	$199.48 \\ 224.09 \\ 2$	3.26 3.48 3.69 3.90 4.10 4.29	99.79 102.03 104.20 106.29 108.32 110.28	$\begin{array}{cccc} 4^{\circ} & 30' \\ 5 & 37\frac{1}{2} \end{array}$	$100.00 \\ 122.73 \\ 120.54 \\ 118.42 \\ 116.38 \\ 114.41$	9° 00' 10 20 30 40 50
10° 00' 10 20 30 40 11° 00'	225 250 250 250 250 250 250	15.50 20.91 20.91 20.91 20.91 20.91 20.91 20.91	$\begin{array}{c} 224.09\\ 248.50\\ 248.50\\ 248.50\\ 248.50\\ 248.50\\ 248.50\\ 248.50\\ 248.50\\ \end{array}$	$\begin{array}{r} 4.48\\ 4.74\\ 5.00\\ 5.25\\ 5.50\\ 5.73\\ 5.96\end{array}$	112.17114.37116.53118.62120.64122.60124.50	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	112.50 135.25 133.06 130.95 128.91 126.92 125.00	10° 00' 10 20 30 40 50 11° 00'

#### TABLE IV.—ELEMENTS OF TRANSITION CURVES. Dimensions of various 1°-per-25-feet spirals.—Part C. VALUES OF AN.

$\wedge$	Degree of curve.												
	2°	3°	4°	5°	6°	7°	8°	90	10°	11°			
2 4 6 8 10	$\begin{array}{c} 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00\\ 0.00 \end{array}$	$\begin{array}{c} 0.00\\ 0.00\\ 0.01\\ 0.01\\ 0.01\\ 0.01 \end{array}$	$\begin{array}{c} 0.00 \\ 0.01 \\ 0.01 \\ 0.02 \\ 0.02 \\ 0.02 \end{array}$	$\begin{array}{c} 0.01 \\ 0.02 \\ 0.03 \\ 0.04 \\ 0.05 \end{array}$	$\begin{array}{c} 0.02 \\ 0.03 \\ 0.05 \\ 0.07 \\ 0.08 \end{array}$	0.03 0.05 0.08 0.11 0.13	0.04 0.08 0.12 0.16 0.20	$\begin{array}{c} 0.06 \\ 0.11 \\ 0.17 \\ 0.23 \\ 0.29 \end{array}$	0.08 0.16 0.23 0.31 0.39	$\begin{array}{c} 0.11 \\ 0.21 \\ 0.31 \\ 0.42 \\ 0.52 \end{array}$			
12 14 16 18 20	$\begin{array}{c} 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \end{array}$	$\begin{array}{c} 0.01 \\ 0.01 \\ 0.02 \\ 0.02 \\ 0.02 \\ 0.02 \end{array}$	$\begin{array}{c} 0.03 \\ 0.03 \\ 0.04 \\ 0.04 \\ 0.05 \end{array}$	0.06 0.07 0.08 0.09 0.10	0.10 0.12 0.13 0.15 0.17	0.16 0.19 0.21 0.24 0.27	$\begin{array}{c} 0.24 \\ 0.28 \\ 0.32 \\ 0.36 \\ 0.40 \end{array}$	0.34 0.40 0.46 0.52 0.57	0.47 0.55 0.63 0.71 0.79	$\begin{array}{c} 0.63 \\ 0.73 \\ 0.84 \\ 0.94 \\ 1.05 \end{array}$			
22 24 26 28 30	0.01 0.01 0.01 0.01 0.01	$\begin{array}{c} 0.02 \\ 0.02 \\ 0.03 \\ 0.03 \\ 0.03 \\ 0.03 \end{array}$	0.05 0.06 0.06 0.07 0.07	$\begin{array}{c} 0.11 \\ 0.12 \\ 0.13 \\ 0.14 \\ 0.15 \end{array}$	0.19 0.20 0.22 0.24 0.26	$\begin{array}{c} 0.30 \\ 0.32 \\ 0.35 \\ 0.38 \\ 0.41 \end{array}$	0.44 0.49 0.53 0.57 0.61	0.63 0.69 0.75 0.81 0.87	0.87 0.95 1.03 1.11 1.20	1.16 1.27 1.38 1.49 1.60			
82 34 36 38 40	$\begin{array}{c} 0.01 \\ 0.01 \\ 0.01 \\ 0.01 \\ 0.01 \\ 0.01 \\ 0.01 \end{array}$	$\begin{array}{c} 0.03 \\ 0.03 \\ 0.04 \\ 0.04 \\ 0.04 \\ 0.04 \end{array}$	$\begin{array}{c} 0.08 \\ 0.08 \\ 0.09 \\ 0.09 \\ 0.09 \\ 0.10 \end{array}$	$\begin{array}{c} 0.16 \\ 0.17 \\ 0.18 \\ 0.19 \\ 0.20 \end{array}$	$\begin{array}{c} 0.27 \\ 0.29 \\ 0.31 \\ 0.33 \\ 0.35 \end{array}$	$\begin{array}{c} 0.44 \\ 0.47 \\ 0.49 \\ 0.52 \\ 0.55 \end{array}$	$\begin{array}{c} 0.65 \\ 0.70 \\ 0.74 \\ 0.79 \\ 0.83 \end{array}$	0.93 1.00 1.06 1.12 1.19	$1.28 \\ 1.37 \\ 1.45 \\ 1.54 \\ 1.63$	1.71 1.82 1.94 2.05 2.17			
42 44 46 48 50	0.01 0.01 0.01 0.01 0.01 0.01	$\begin{array}{c} 0.04 \\ 0.04 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \end{array}$	0.10 0.11 0.12 0.12 0.13	$\begin{array}{c} 0.21 \\ 0.22 \\ 0.23 \\ 0.24 \\ 0.25 \end{array}$	$\begin{array}{c} 0.37 \\ 0.38 \\ 0.40 \\ 0.42 \\ 0.44 \end{array}$	0.58 0.62 0.65 0.68 0.71	0.88 0.92 0.97 1.02 1.07	$1.25 \\ 1.32 \\ 1.38 \\ 1.45 \\ 1.52$	1.72 1.81 1.90 1.99 2.09	2.28 2.41 2.53 2.65 2.78			
52 54 56 58 60	0.01 0.01 0.01 0.02 0.02	$\begin{array}{c} 0.05 \\ 0.06 \\ 0.06 \\ 0.06 \\ 0.06 \\ 0.06 \end{array}$	$\begin{array}{c} 0.13 \\ 0.14 \\ 0.14 \\ 0.15 \\ 0.16 \end{array}$	$\begin{array}{c} 0.27 \\ 0.28 \\ 0.29 \\ 0.30 \\ 0.31 \end{array}$	$\begin{array}{c} 0.46 \\ 0.49 \\ 0.51 \\ 0.53 \\ 0.55 \end{array}$	0.74 0.78 0.81 0.85 0.88	1.11 1.16 1.21 1.27 1.32	1.59 1.66 1.74 1.81 1.88	$\begin{array}{r} 2.18 \\ 2.28 \\ 2.38 \\ 2.48 \\ 2.58 \end{array}$	2.91 3.04 3.17 3.31 3.44			
62 64 66 68 70	0.02 0.02 0.02 0.02 0.02 0.02	0.07 0.07 0.07 0.07 0.07 0.08	0.16 0.17 0.18 0.18 0.19	0.33 0.34 0.35 0.37 0.38	$\begin{array}{c} 0.57 \\ 0.60 \\ 0.62 \\ 0.64 \\ 0.67 \end{array}$	0.92 0.95 0.99 1.03 1.07	$ \begin{array}{c} 1.37\\ 1.43\\ 1.48\\ 1.54\\ 1.60 \end{array} $	1.96 2.04 2.12 2.20 2.28	2.69 2.80 2.91 3.02 3.13	3.58 3.73 3.87 4.02 4.18			
72 74 76 78 80	$\begin{array}{c} 0.02 \\ 0.02 \\ 0.02 \\ 0.02 \\ 0.02 \\ 0.02 \\ 0.02 \end{array}$	0.08 0.08 0.09 0.09 0.09	0.20 0.20 0.21 0.22 0.23	$\begin{array}{c} 0.40 \\ 0.41 \\ 0.43 \\ 0.44 \\ 0.46 \end{array}$	0.69 0.72 0.74 0.77 0.80	$\begin{array}{c c} 1.11 \\ 1.15 \\ 1.19 \\ 1.23 \\ 1.28 \end{array}$	1.66 1.72 1.79 1.85 1.92	$\begin{array}{c} 2.37 \\ 2.46 \\ 2.55 \\ 2.64 \\ 2.74 \end{array}$	3.25 3.38 3.50 3.63 3.76	$\begin{array}{r} 4.33 \\ 4.49 \\ 4.66 \\ 4.83 \\ 5.00 \end{array}$			
82 84 86 88 90	0.02 0.03 0.03 0.03 0.03	0.09 0.10 0.10 0.11 0.11	0.24 0.24 0.25 0.26 0.27	$\begin{array}{c} 0.47 \\ 0.49 \\ 0.51 \\ 0.53 \\ 0.55 \end{array}$	0.83 0.86 0.89 0.92 0.95	$\begin{array}{c c} 1.32 \\ 1.37 \\ 1.42 \\ 1.47 \\ 1.52 \end{array}$	1.99 2.06 2.13 2.21 2.29	2.83 2.94 3.04 3.15 3.26	$\begin{array}{r} 3.89 \\ 4.03 \\ 4.18 \\ 4.33 \\ 4.48 \end{array}$	5.18 5.37 5.56 5.76 5.96			
92 94 96 98 100	$\begin{array}{c} 0.03 \\ 0.03 \\ 0.03 \\ 0.03 \\ 0.03 \\ 0.03 \end{array}$	0.13	0.28 0.29 0.30 0.31 0.32	$\begin{array}{c} 0.56 \\ 0.58 \\ 0.61 \\ 0.63 \\ 0.65 \end{array}$	0.99 1.02 1.06 1.10 1.13	$1.58 \\ 1.63 \\ 1.69 \\ 1.75 \\ 1.82$	2.372.452.542.632.72	3.38 3.50 3.62 3.75 3.89	$\begin{array}{r} 4.64 \\ 4.80 \\ 4.97 \\ 5.15 \\ 5.34 \end{array}$	6.17 6.39 6.62 6.86 7.11			

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TABLE IV .- ELEMENTS OF TRANSITION CURVES.

Point.	1098465420	'		10	3' 25' 42 25' 2 42 20 2 42 30 2 30 2 30 00 00 00
6				T	11° 53'           16         50           16         53           15         38           12         42           11         00           11         00           12         45           2         30           2         30           0         00
	255.0 249.5 299.5 299.5 299.5 299.5 221.2 22			6	35'30'' 35'30'' 30 15 30 15 39 15 07 30 22 30 22 30 30 00 30 00
8	$\begin{array}{c} 0.0377\overline{4}\\ 0.0377\overline{4}\\ 0.183670\\ 0.183680\\ 0.51468\\ 0.51468\\ 0.51468\\ 0.51468\\ 0.51468\\ 0.51468\\ 1.18207\\ 1.34437\\ 1.34437\\ 1.34437\\ 1.34437\\ 1.34437\\ 1.34437\\ 1.51613\\ 1.51613\\ 1.51613\\ 1.51613\\ 1.51613\\ 1.51613\\ 1.5162$		ļ		20240801234
Log	0.0000000000000000000000000000000000000		nt is at	œ	37' 45''       45     10       45     10       42     36       42     36       33     04       35     00       35     00       15     00       37     30
	109 5545 527 271 271 2903 203 203 317 317 317 203		Deflections from the tangent at the point occupied when the instrument is		110 10 10 10 10 10 10 10 10 10
8	400210200000		he ins	~	00' 05'' 12 34 15 02 07 30 07 30 22 30 22 30 00 00 00 00 07 30 25 00
-0		~ ~	ent		<u>0∞≻∞4∞⊣004∞</u>
	553050 53200 53200 53000 53000 53000 53000 53000 53000 53000 53000 53000 53000 53000 53000 53000 500000000	¥.	l wh	9	2, 30, 30, 30, 30, 30, 30, 30, 30, 30, 30
Log vers	988877710 9888877710 98888	PART.	upiec		6° 42′ 5 07 5 07 5 40 0 00 1 45 5 40 7 52 7 52 7 52
- <del>0</del> -			000		00 00 00 00 00 00 00 00 00 00
cos	999999 999999 9999999 998340 998340 998690 998800 94793 94793	oira	oint	10	45' 45' 15 22 22 22 30 00 55 55 55 55
Log		t s	the I		122300000000000000000000000000000000000
- <del>0</del> -		2°-per-35-feet spiral.	at	4	07'30'35 52300000 1500000 150015 100000 150000 150000 150000 15337 44555 44555 44555 44718
-is	$\begin{array}{c}$	r-3	gen		0707707070700
Log	047010000000000000000000000000000000000	-be	tan		00 30 00 00 00 21 23 21 21
		શ્	the	ຕ	22 22 00 07 07 07 07 07 07 07 07 07 07 07 07
<b>\$</b> so	2000231 <b>₩</b> 120000 231 <b>₩</b> 120000		from		001004000 ,
Nat. cos	00000000000000000000000000000000000000		suc		$\begin{smallmatrix} & & & & & \\ & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & & \\ & & & & & & & \\ & & & & & & & \\ & & & & & & & \\ & & & & & & & \\ & & & & & & & \\ & & & & & & & \\ & & & & & & & \\ & & & & & & & \\ & & & & & & & \\ & & & & & & & \\ & & & & & $
		Ì	ecti	8	0°52' 0 30 0 30 0 45 0 45 1 37 5 14 8 29 8 29 0 22
- <del>•</del>	12 0 0 0 0 0 0 0 0 0 0 0		Defl		P-1
Nat. sin	.0087 .0262 .0523 .0523 .0871 .1305 .1305 .1305 .1322 .1322 .2419 .3827 .3827 .3827				00/ 00/ 00/ 00/ 00/ 00/ 00/ 00/ 00/ 00/
N				-	0°15/ 0000 1551 1551 1551 1551 1551 1551 1
gle	`				
Total ral An				a	00' 00' 15 00 37 30 10 00 10 00 110 00 45 00 54 30 55 53 54 30 36 35
Central Angl	222840 <b>45</b> 310°				0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
			-sight- ing	φ	Ø H & @ 4 6 9 5 8 6 0 0
Point.	10 <b>08400</b> 4201		-8-	at	Ø1884697860 1

#### TABLE IV.—ELEMENTS OF TRANSITION CURVES. Dimensions of various 2°-per-25-feet spirals.—Part B.

And the second se			or various	= por .		All cards a	art D.	
Deg. of	L'gth of	ZK	QK	A'N	NQ	A' t	o Z.	Deg. of
curve.	spiral	DI	ΨΠ		21.62	Defl.	Dist.	curve.
4° 00' 20 40 5° 00' 20 40	25 50 50 50 50 50 50	0.11 0.55 0.55 0.55 0.55 0.55	$\begin{array}{r} 25.00 \\ 50.00 \\ 50.00 \\ 50.00 \\ 50.00 \\ 50.00 \\ 50.00 \\ 50.00 \end{array}$	0.05 0.09 0.12 0.15 0.18 0.20	$12.50 \\ 15.38 \\ 17.85 \\ 19.99 \\ 21.86 \\ 23.52$	$\begin{array}{cccc} 0^{\circ} & 15' \\ 0 & 45 \\ 0 & 45 \\ 0 & 45 \\ 0 & 45 \\ 0 & 45 \end{array}$	12.5034.6232.1430.0028.1326.47	4° 00' 20 40 5° 00' 20 40
6° 00' 20 40 7° 00' 20 40	50 75 75 75 75 75 75	$0.55 \\ 1.52 \\ $	50.00 74.98 74.98 74.98 74.98 74.98 74.98	$\begin{array}{c} 0.22 \\ 0.29 \\ 0.35 \\ 0.40 \\ 0.46 \\ 0.50 \end{array}$	$\begin{array}{r} 24.99\\ 27.61\\ 29.97\\ 32.11\\ 34.06\\ 35.84 \end{array}$	0° 45' 1 30 1 30 1 30 1 30 1 30 1 30	25.0 <b>0</b> 47.37 45.00 42.86 40.91 39.13	6° 00' 20 40 7° 00' 20 40
8° 00' 20 40 9° 00' 20 40	75 100 100 100 100 100	1.52 3.27 3.27 3.27 3.27 3.27 3.27	74.98 99.92 99.92 99.92 99.92 99.92 99.92	$\begin{array}{c} 0.54 \\ 0.65 \\ 0.75 \\ 0.85 \\ 0.93 \\ 1.01 \end{array}$	37.46 39.94 42.24 44.37 46.35 48.20	1° 30' 2 30 2 30 2 30 2 30 2 30 2 30	37.50 60.00 57.69 55.56 53.57 51.72	8° 00' 20 40 9° 00' 20 40
10° 00' 20 40 11° 00' 20 40	100 125 125 125 125 125 125	3.27 5.99 5.99 5.99 5.99 5.99 5.99	99.92 124.77 124.77 124.77 124.77 124.77 124.77	1.09 1.24 1.39 1.53 1.66 1.78	49.92 52.30 54.55 56.68 58.67 60.55	2° 30' 3 45 3 45 3 45 3 45 3 45 3 45	$\begin{array}{c} 50.00 \\ 72.58 \\ 70.31 \\ 68.18 \\ 66.18 \\ 64.29 \end{array}$	10° 00' 20 40 11° 00' 20 40
12° 00' 20 40 13° 00' 20 40	125 150 150 150 150 150	5.99 9.90 9.90 9.90 9.90 9.90 9.90	124.77149.46149.46149.46149.46149.46149.46	1.90 2.11 2.31 2.51 2.69 2.87	62.33 64.68 66.86 68.97 70.97 72.88	$\begin{array}{cccc} 3^{\circ} & 45' \\ 5 & 15 \\ 5 & 15 \\ 5 & 15 \\ 5 & 15 \\ 5 & 15 \\ 5 & 15 \end{array}$	62.50 85.14 82.89 80.77 78.75 76.83	12° 00' 20 40 13° 00' 20 40
14° 00' 20 40 15° 00' 20 40	150 175 175 175 175 175	9.90 15.21 15.21 15.21 15.21 15.21 15.21	149.46 173.89 173.89 173.89 173.89 173.89 173.89	3.03 3.30 3.57 3.83 4.08 4.31	74.69 76.93 79.12 81.22 83.22 85.14	5° 15' 7 00 7 00 7 00 7 00 7 00 7 00	75.00 97.67 95.45 93.33 91.30 89.36	14° 00' 20 40 15° 00' 20 40
16° 00' 20 40 17° 00' 20 40	175 200 200 200 200 200 200	$15.21 \\ 22.10 \\ 22.1$	173.89 197.92 197.92 197.92 197.92 197.92 197.92	4.54 4.87 5.21 5.54 5.86 6.16	86.98 89.15 91.31 93.39 95.38 97.30	7° 00' 9 00 9 00 9 00 9 00 9 00 9 00	87.50 110.20 108.00 105.88 103.85 101.89	16° 00' 20 40 17° 00' 20 40
18° 00' 20 40 19° 00' 20 40	200 225 225 225 225 225 225 225	22.10 30.75 30.75 30.75 30.75 30.75 <b>30.75</b>	197.92 221.38 221.38 221.38 221.38 221.38 221.38	6.45 6.86 7.28 7.69 8.09 8.47	99.15 101.27 103.39 105.45 107.43 109.34	9°00' 11 15 11 15 11 15 11 15 11 15 11 15	100.00 122.73 120.54 118.42 116.38 114.41	18° 00' 20 40 19° 00' 20 40
20° 00' 20 40 21° 00' 20 40 22° 00'	225 250 250 250 250 250 250 250	$\begin{array}{r} \textbf{30.75} \\ \textbf{41.32} \end{array}$	$\begin{array}{r} 221.38\\ 244.03\\ 244.03\\ 244.03\\ 244.03\\ 244.03\\ 244.03\\ 244.03\\ 244.03\end{array}$	8.83 9.31 9.82 10.32 10.80 11.26 11.71	111.19 113.23 115.32 117.35 119.30 121.20 123.04	11° 15' 13 45 13 45 13 45 13 45 13 45 13 45 13° 45'	112.50 135.25 133.06 130.95 128.91 126.92 125.00	20° 00' 20 21° 00' 20 22° 00'

# TABLE IV.-ELEMENTS OF TRANSITION CURVES.

Dimensions of various 2°-per-25-feet spirals.-Part C.

VALUES OF AN.

$\triangle$	Degree of curve,											
77	4°	6°	8°	10°	· 12°	14°	16°	18°	20°	22°		
4° 6 8 10	$\begin{array}{c} 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \\ 0.00 \end{array}$	${ \begin{smallmatrix} 0.01 \\ 0.01 \\ 0.02 \\ 0.02 \\ 0.02 \\ \end{smallmatrix} }$	$\begin{array}{c} 0.02 \\ 0.03 \\ 0.04 \\ 0.05 \end{array}$	$\begin{array}{c} 0.04 \\ 0.06 \\ 0.08 \\ 0.10 \end{array}$	0.07 0.10 0.13 0.17	$\begin{array}{c} 0.11 \\ 0.16 \\ 0.21 \\ 0.27 \end{array}$	${ \begin{smallmatrix} 0.16 \\ 0.24 \\ 0.32 \\ 0.40 \end{smallmatrix} }$	$\begin{array}{c} 0.23 \\ 0.34 \\ 0.45 \\ 0.56 \end{array}$	$\begin{array}{c} 0.31 \\ 0.46 \\ 0.62 \\ 0.77 \end{array}$	${ \begin{smallmatrix} 0.41 \\ 0.61 \\ 0.82 \\ 1.02 \end{smallmatrix} }$		
12 14 16 18 20	0.01 0.01 0.01 0.01 0.01	$\begin{array}{c} 0.02 \\ 0.03 \\ 0.03 \\ 0.03 \\ 0.04 \end{array}$	$\begin{array}{c} 0.06 \\ 0.07 \\ 0.08 \\ 0.09 \\ 0.10 \end{array}$	0.11 0.13 0.15 0.17 0.19	$\begin{array}{c} 0.20 \\ 0.23 \\ 0.27 \\ 0.30 \\ 0.34 \end{array}$	$\begin{array}{c} 0.32 \\ 0.37 \\ 0.43 \\ 0.48 \\ 0.53 \end{array}$	$\begin{array}{c} 0.48 \\ 0.56 \\ 0.64 \\ 0.72 \\ 0.80 \end{array}$	0.68 0.79 0.91 1.02 1.14	$\begin{array}{c} 0.93 \\ 1.08 \\ 1.24 \\ 1.40 \\ 1.56 \end{array}$	$1.23 \\ 1.44 \\ 1.65 \\ 1.85 \\ 2.06$		
22 24 26 28 30	0.01 0.01 0.01 0.01 0.01 0.01	$\begin{array}{c} 0.04 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.05 \\ 0.06 \end{array}$	0.11 0.12 0.13 0.14 0.15	$\begin{array}{c} 0.21 \\ 0.23 \\ 0.25 \\ 0.27 \\ 0.29 \end{array}$	$\begin{array}{c} 0.37 \\ 0.40 \\ 0.44 \\ 0.47 \\ 0.51 \end{array}$	0.59 0.64 0.70 0.76 0.81	$\begin{array}{c} 0.88 \\ 0.96 \\ 1.05 \\ 1.13 \\ 1.22 \end{array}$	1.25 1.37 1.49 1.61 1.73	1.72 1.88 2.04 2.20 2.37	2.28 2.49 2.70 2.92 3.14		
32 34 36 38 40	0.02 0.02 0.02 0.02 0.02 0.02	0.06 0.07 0.07 0.08 0.08	0.16 0.17 0.18 0.19 0.20	$\begin{array}{c} 0.31 \\ 0.33 \\ 0.35 \\ 0.37 \\ 0.40 \end{array}$	0.54 0.58 0.62 0.65 0.69	0.87 0.93 0.99 1.04 1.10	$1.30 \\ 1.39 \\ 1.47 \\ 1.56 \\ 1.65$	1.851.972.102.222.35	2.53 2.70 2.87 3.04 3.22	3.36 3.58 3.80 4.03 4.26		
42 44 46 48 50	0.02 0.02 0.02 0.02 0.02 0.03	0.08 0.09 0.09 0.10 0.10	0.21 0.22 0.23 0.24 0.25	$\begin{array}{c} 0.42 \\ 0.44 \\ 0.46 \\ 0.48 \\ 0.51 \end{array}$	0.73 0.77 0.81 0.85 0.89	$1.16 \\ 1.23 \\ 1.29 \\ 1.35 \\ 1.41$	$1.74 \\ 1.83 \\ 1.93 \\ 2.02 \\ 2.11$	$\begin{array}{c} 2.48 \\ 2.61 \\ 2.74 \\ 2.87 \\ 3.01 \end{array}$	3.39 3.57 3.75 3.93 4.12	4.49 4.73 4.97 5.21 5.46		
52 54 56 58 60	0.03 0.03 0.03 0.03 0.03 0.03	0.11 0.11 0.12 0.12 0.13	0.27 0.28 0.29 0.30 0.31	$\begin{array}{c} 0.53 \\ 0.55 \\ 0.58 \\ 0.60 \\ 0.63 \end{array}$	0.93 0.97 1.01 1.05 1.10	$1.48 \\ 1.54 \\ 1.61 \\ 1.68 \\ 1.75$	$\begin{array}{c} 2.21 \\ 2.31 \\ 2.41 \\ 2.51 \\ 2.62 \end{array}$	3.15 3.29 3.43 3.58 3.73	$\begin{array}{c} 4.31 \\ 4.50 \\ 4.70 \\ 4.90 \\ 5.10 \end{array}$	5.71 5.97 6.23 6.49 6.76		
62 64 66 68 70	0.03 0.03 0.03 0.04 0.04	0.13 0.14 0.14 0.15 0.15	0.33 0.34 0.35 0.37 0.38	0.65 0.68 0.71 0.73 0.76	$1.14 \\ 1.19 \\ 1.23 \\ 1.28 \\ 1.33$	1.82 1.90 1.97 2.05 2.12	2.73 2.83 2.95 3.06 3.18	$\begin{array}{r} 3.88 \\ 4.03 \\ 4.19 \\ 4.35 \\ 4.52 \end{array}$	5.31 5.52 5.74 5.96 6.19	7.04 7.32 7.60 7.90 8.20		
72 74 76 78 <sup>.</sup> 80	$\begin{array}{c} 0.04 \\ 0.04 \\ 0.04 \\ 0.04 \\ 0.05 \end{array}$	0.16	$\begin{array}{c} 0.40 \\ 0.41 \\ 0.43 \\ 0.44 \\ 0.46 \end{array}$	0.78 0.81 0.84 0.88 0.91	$ \begin{array}{c} 1.38\\ 1.43\\ 1.48\\ 1.54\\ 1.59 \end{array} $	2.20 2.28 2.37 2.46 2.54	3.30 3.42 3.54 3.67 3.81	4.69 4.86 5.04 5.22 5.41	$\begin{array}{c} 6.42 \\ 6.66 \\ 6.90 \\ 7.15 \\ 7.41 \end{array}$	8.51 8.82 9.15 9.48 9.82		
82 84 86 88 90	0.05 0.05 0.05 0.05 0.05	0.19 0.20 0.20 0.21 0.22	$\begin{array}{c} 0.47 \\ 0.49 \\ 0.51 \\ 0.53 \\ 0.55 \end{array}$	0.94 0.98 1.02 1.05 1.09	1.65 1.71 1.77 1.83 1.90	2.64 2.73 2.83 2.93 3.03	$\begin{array}{r} 3.94 \\ 4.08 \\ 4.23 \\ 4.38 \\ 4.54 \end{array}$	$\begin{array}{c} 5.61 \\ 5.81 \\ 6.02 \\ 6.23 \\ 6.45 \end{array}$	7.68 7.95 8.24 8.53 8.83	$10.18 \\ 10.54 \\ 10.92 \\ 11.31 \\ 11.71$		
92 94 96 98 100	0.06 0.06 0.06 0.06 0.06	$\begin{array}{c} 0.23 \\ 0.23 \\ 0.24 \\ 0.25 \\ 0.26 \end{array}$	$\begin{array}{c} 0.56 \\ 0.58 \\ 0.61 \\ 0.63 \\ 0.65 \end{array}$	$1.13 \\ 1.17 \\ 1.21 \\ 1.25 \\ 1.30$	1.972.042.112.192.26	3.14 3.25 3.37 3.49 3.61	$\begin{array}{r} 4.70 \\ 4.86 \\ 5.04 \\ 5.22 \\ 5.41 \end{array}$	$\begin{array}{c} 6.68 \\ 6.92 \\ 7.17 \\ 7.42 \\ 7.69 \end{array}$	9.159.479.8110.1610.53	$12.12 \\ 12.56 \\ 13.00 \\ 13.47 \\ 13.95$		

TABLE V.S-LOGARITHMS OF NUMBERS.

	TABLE V.S-LOGARTIHMS OF NUMBERS.											
N.		0	1	2	3	4	5	6	7	8	9	P. P.
100	00	000	043	087	130	173	21ē	260	303	346	389	45 49 49 41
101 102 103 104 105 106 107 108 109	01 02 03	432 860 28 <u>3</u> 703 119 530 938 342 742	475 902 326 745 160 571 979 382 782	518 945 368 787 201 612 *019 422 822	561 987 410 828 243 653 *060 463 862	604 *030 452 870 284 69 <u>4</u> *100 503 901	64 <u>6</u> *072 494 911 325 735 *141 543 941	689 *114 536 953 366 775 *181 583 981	732 *157 57 <u>8</u> 99 <u>4</u> 407 816 *221 623 *020	77 <u>5</u> *199 619 *03 <u>6</u> 448 857 *262 663 *060	703	834.834.433.632.8
110	04	139	178	218	257	297	336	375	415	454	493	10 10 00 00
111 112 113 114 115 116 117 118 119	05 06 07	532 922 308 690 070 446 818 188 554	57 <u>1</u> 96 <u>0</u> 34 <u>6</u> 728 107 483 855 225 591	610 999 384 766 145 520 893 261 627	649 *038 423 804 183 558 930 298 664	688 *076 461 220 595 967 335 700	727 *115 499 880 258 632 *004 372 737	766 *154 538 918 296 670 *040 408 773	*192 576 956 333 707 *077	614	*269 652 *032 408 781 *151 518	$\begin{array}{c} \cdot 2 & 8 \cdot 1 & 8 \cdot 0 & 7 \cdot 8 & 7 \cdot 6 \\ \cdot 3 & 12 \cdot \overline{1} & 12 \cdot 0 & 11 \cdot 7 & 11 \cdot 4 \\ \cdot 4 & 16 \cdot 2 & 16 \cdot 0 & 15 \cdot 6 & 15 \cdot 2 \\ \cdot 5 & 20 \cdot 2 & 20 \cdot 0 & 19 \cdot 5 & 19 \cdot 0 \\ \cdot 6 & 24 \cdot 3 & 24 \cdot 0 & 23 \cdot 4 & 22 \cdot 8 \\ \cdot 7 & 28 \cdot 3 & 28 \cdot 0 & 27 \cdot 3 & 26 \cdot 6 \\ \cdot 8 & 32 \cdot 4 & 32 \cdot 0 & 31 \cdot 2 & 30 \cdot 4 \end{array}$
120		918	954	99ō	*02ē	*062	*098	*134	*17ō	*206	*242	
121 122 123 124 125 126 127 128 129	08 09 10 11	278 636 990 342 691 037 380 721 059	314 671 *026 377 725 071 414 755 092	350 707 *061 412 760 106 448 789 126	386 742 *096 447 795 140 483 822 160	422 778 *131 482 830 174 517 856 193	457 813 *166 517 864 209 551 890 227	493 849 *202 552 899 243 585 924 260	529 884 *237 586 933 277 619 958 294	564 920 *272 621 968 312 653 991 327	656	$\begin{array}{c} \cdot 3 & 11 \cdot \overline{2} & 11 \cdot 1 & 10 \cdot 8 & 10 \cdot 5 \\ \cdot 4 & 15 \cdot 0 & 14 \cdot 8 & 14 \cdot 4 & 14 \cdot 0 \\ \cdot 5 & 18 \cdot \overline{7} & 18 \cdot 5 & 18 \cdot 0 & 17 \cdot 5 \\ \cdot 6 & 22 \cdot 5 & 22 \cdot 2 & 21 \cdot 6 & 21 \cdot 0 \end{array}$
130		394	427	461	494	528	561	594	627	661	694	1
131 132 133 134 135 136 137 138 139	12 13 14	727 057 385 710 033 354 672 988 301	760 090 418 743 065 386 703 *019 332	793 123 450 775 097 417 735 *051 364	826 156 483 807 130 449 767 *082 395	859 189 515 840 162 481 798 *113 426	892 221 548 872 194 513 830 *145 457	925 254 580 904 226 545 862 *176 488	958 287 613 937 258 577 893 \$93 \$19	991 320 645 969 290 608 925 *239 550	*02 <u>4</u> 352 678 *001 322 640 956 *270 582	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
140		613	644	675	706	736	767	798	829	860	891	31 31 30 29
141 142 143 144 145 146 147 148 149 <b>150</b>	15 16 17	922 229 533 836 137 435 731 026 318 609	952 259 564 866 166 465 761 055 348 638	983 290 594 896 196 494 791 085 377 667	*01 <u>4</u> 320 624 926 524 820 114 406 696	*045 351 655 956 554 143 435 725	*07 <u>5</u> 381 685 987 286 584 879 172 464 753	*106 412 715 *017 316 613 908 202 493 782	*137 442 745 *047 346 643 938 231 522 811	*167 473 776 *077 376 672 967 260 551 840	*198 503 806 *107 405 702 997 289 580 869	$\begin{array}{c} .1 & 3.1 & 3.1 & 3.0 & 2.9 \\ .2 & 6.3 & 6.2 & 6.0 & 5.8 \\ .3 & 9.4 & 9.3 & 9.0 & 8.7 \\ .412.612.412.011.6 \\ .515.715.515.014.5 \\ .618.918.618.017.4 \\ .722.021.721.022.3 \\ .825.224.824.0223.2 \\ .928.3127.9127.026.1 \end{array}$
N.		0	1	2	3	4	5	6	7	8	9	<b>P. P.</b>

#### TABLE V.-LOGARITHMS OF NUMBERS.

_				TAB	LEV	.—L	OGA	RITH	IMS	OF 1	NUME	BERS.
N.		0	1	2	3	4	5	6	7	8	9	Р. Р.
150	17	609	638	667	696	725	753	782	811	840	869	<u></u>
151 152 153 154 155 156 157 158 159	18 19 20	897 184 469 752 033 312 590 865 139	926 213 497 780 061 340 617 893 167	955241526808089368645920194	984 270 55 <u>4</u> 836 117 396 673 948 221	*012 298 582 864 145 423 700 975 249	*041 327 611 893 173 451 728 *003 276	*070 355 639 921 201 479 755 *030 303	*098 384 667 949 229 507 783 *057 330	*127 412 695 977 256 534 810 *085 357	*156 440 724 *005 284 562 838 *112 385	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
160		412	439	<b>46</b> ō	<b>4</b> 93	520	547	574	601	628	655	26 26
$161 \\ 162 \\ 163 \\ 164 \\ 165 \\ 166 \\ 167 \\ 168 \\ 169 \\ 169 \\ 169 \\ 169 \\ 169 \\ 160 \\ 100 $	21 22	682 951 219 484 748 011 271 531 788	709 978 245 511 774 037 297 557 814	736 272 537 801 063 323 582 840	763 298 564 827 089 349 608 865	790 *058 325 590 855 115 375 634 891	817 *085 352 616 880 141 401 660 917	844 *112 378 643 906 167 427 686 942	871 *139 40 <u>5</u> 66 <u>9</u> 93 <u>2</u> 19 <u>3</u> 45 <u>3</u> 711 968	898 *165 431 695 958 219 479 737 994	924 *192 458 722 984 245 505 763 *019	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
170	23	045	07ō	096	121	147	172	198	223	249	274	0F 0F 04
171 172 173 174 175 176 177 178 179	24 25	299 5534 0554 551 304 551 797 042 285	325 578 829 080 328 576 822 066 309	350 603 855 105 353 600 846 091 334	37 <u>5</u> 628 880 129 378 625 871 115 358	401 653 905 154 403 650 895 139 382	426 679 930 179 427 674 920 164 406	451 704 955 204 452 699 944 188 430	477 729 980 229 477 723 968 212 455	502 754 *005 254 502 748 993 237 479	527 779 *030 279 526 773 *017 261 503	$\begin{array}{cccccccccccccccccccccccccccccccccccc$
180		527	551	575	599	62 <del>3</del>	647	672	696	720	744	02 00
181 182 183 184 185 186 187 188 189	26 27	768 007 245 482 717 951 184 416 646	792 031 269 505 740 974 207 439 669	816 055 292 529 764 998 230 462 692	840 078 316 552 787 *021 254 485 715	86 <u>3</u> 102 340 576 811 *044 277 508 738	887 126 363 599 834 *068 300 531 761	911 150 387 623 858 *091 323 554 784	935 174 411 646 881 *114 346 577 806	959 197 434 6704 904 *137 369 600 829	98 <u>3</u> 221 45 <u>8</u> 693 928 *161 392 623 852	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
190		875	898	921	944	96 <u>6</u>	98 <u>9</u>	*012	*035	*058	*080	<u>00 00 01</u>
192 193 194	28 29	$   \begin{array}{r}     10\overline{3} \\     330 \\     555 \\     780 \\     225 \\     446 \\     885 \\   \end{array} $	$126 \\ 352 \\ 578 \\ 802 \\ 025 \\ 248 \\ 468 \\ 688 \\ 907 \\$	149 375 600 825 048 270 490 710 929	171 398 623 847 070 292 512 732 950	194 420 645 869 092 314 534 754 972	$\begin{array}{r} 217\\ 443\\ 668\\ 892\\ 114\\ 336\\ 556\\ 776\\ 994 \end{array}$	239 4690 914 137 358 578 798 *016	262 488 713 936 159 380 600 820 *038	285 510 735 959 181 402 622 841 *059	307 533 758 981 203 424 644 863 *081	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
200	30	103	124	146	168	190	211	233	254	276	298	
N.		0	1	2	3	4	5	6	7	8	9	P. P.

TABLE V.-LOGARITHMS OF NUMBERS.

-	TABLE V.—LOGARITHMS OF NUMBERS.											
N.		0	1	2	3	4	5	6	7	8	9	P. P.
200	30	103	124	146	168	190	21Ī	233	$25\overline{4}$	276	298	00 01
201 202 203 204 205 206 207 208 209	31 32	319 535 749 963 175 386 597 806 014	341 556 771 984 196 408 618 827 035	363 578 792 217 429 639 848 056	384 599 813 *027 239 450 660 869 077	406 621 835 *048 260 471 681 890 097	427 642 856 281 492 702 910 118	449 664 878 302 513 722 931 139	470 685 899 *112 323 534 534 743 952 160	492 707 920 *13 <u>3</u> 344 55 <u>5</u> 764 97 <u>3</u> 180	513 728 941 *154 365 576 785 994 201	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
210		222	$24\overline{2}$	263	284	304	325	346	<b>3</b> 66	387	407	97 99
211 212 213 214 215 216 217 218 219	33 34	428 633 838 041 244 445 646 845 044	$\begin{array}{r} 449\\ 654\\ 858\\ 061\\ 264\\ 465\\ 666\\ 865\\ 064 \end{array}$	469 674 878 082 284 485 686 885 084	490 695 899 102 304 505 706 905 104	510 715 919 122 324 525 726 925 925 123	$\begin{array}{r} 531 \\ 736 \\ 940 \\ 142 \\ 344 \\ 546 \\ 746 \\ 945 \\ 143 \end{array}$	$\begin{array}{r} 55\overline{1} \\ 756 \\ 960 \\ 163 \\ 365 \\ 566 \\ 766 \\ 965 \\ 163 \end{array}$	572 776 980 183 385 586 786 985 183	592 797 *001 203 405 606 806 *004 203	613 817 *021 425 626 825 825 *024 222	714 314 0
220		$24\overline{2}$	262	281	30ī	321	341	36Ō	380	400	419	19 19
221 222 223 224 225 226 227 228 229	35	439 635 830 025 218 411 602 793 983	459 655 850 044 237 430 621 812 *002	47 <u>8</u> 67 <u>4</u> 86 <u>9</u> 063 257 449 64 <u>1</u> 83 <u>1</u> *021	498 694 889 083 27 <u>6</u> 468 660 85 <u>0</u> *040	518 713 908 102 295 487 679 869 *059	537 733 928 121 314 507 698 888 *078	526 526 71 <u>7</u> 907	576 772 966 160 353 545 736 926 *116	791 986 179 372 564 755 945	774 964	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
230	36	173	191	210	229	248	267	286	305	323	342	
231 232 233 234 235 236 237 238 239	37	361 54 <u>9</u> 73 <u>5</u> 921 107 291 47 <u>5</u> 657 840	380 567 754 940 125 309 493 676 858	399 586 77 <u>3</u> 95 <u>8</u> 143 328 511 694 876	417 605 791 977 162 346 530 712 894	810 996 180 364 548	828 *014	661 847 *033 217 401 584 767	679 866 *051 236 420	698 884 *070 254 438 621 803	903 *088 273 456 639 821	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
240	38	021	039	057	075	093	111	129	147	165	183	17_ 17
241 242 243 244 245 246 247 248 249 <b>250</b>	39	201 381 560 739 916 093 269 445 620 794	219 399 578 757 934 111 287 462 637 811	237 417 596 774 952 129 305 480 655 828	25 <u>5</u> 435 614 792 970 14 <u>6</u> 322 497 672 846	273 453 632 810 987 164 340 515 689 863	291 471 650 828 *005 181 357 532 707 881	30 489 667 845 *023 199 375 550 724 898	327 507 685 803 *040 217 392 567 742 915	525 703 881 *058	363 543 721 899 *076 252 427 602 776 950	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
N.		0	1	2	3	4	5	6	7	8	9	P. P.

## TABLE V.-LOGARITHMS OF NUMBERS.

-				IAD							Child	E11.5.
N.		0	1	2	3	4	5	6	7	8	9	P. P.
250	39	794	811	828	846	86 <del>3</del>	881	898	915	933	950	
251 252 253 254 255 256 257 258 259	40 41	967 140 312 483 654 824 993 162 330	984 157 329 500 671 841 *010 179 346	*002 174 346 517 688 858 *027 195 363	*019 191 36 <u>3</u> 534 705 875 *044 212 380	*036 209 380 551 722 892 *061 229 397	*054 226 398 569 73 <u>9</u> 908 *077 24 <u>6</u> 413	*07 <u>1</u> 243 415 586 75 <u>6</u> 92 <u>5</u> *094 263 430	*08 260 432 603 773 942 *111 279 447	*10 <u>5</u> 277 449 620 790 95 <u>9</u> *128 296 464	*123 295 466 637 807 976 *145 31 <u>3</u> 480	$\begin{array}{cccccccccccccccccccccccccccccccccccc$
<b>26</b> 0		497	514	530	547	564	581	597	614	631	647	
261 262 263 264 265 266 267 268 269	42	664 830 99 <u>5</u> 160 324 488 651 813 975	680 846 *012 177 341 504 667 829 991	697 863 1937 521 683 846 *007	714 880 *04 <u>5</u> 20 <u>9</u> 373 537 700 862 *023	730 896 226 390 553 716 878 *040	747 913 242 406 569 732 894 *056	764 929 259 423 586 748 910 *072	780 946 *111 275 439 602 765 927 *088	797 962 292 455 618 781 943 *104	813 979 *144 308 472 635 797 959 *120	$\begin{array}{cccccccccccccccccccccccccccccccccccc$
270	43	136	152	168	184	200	216	233	249	265	281	$\begin{array}{c ccccc} \cdot 5 & 8 \cdot 2 & 8 \cdot 0 \\ \cdot 6 & 9 \cdot 9 & 9 \cdot 6 \\ \cdot 7 & 11 \cdot 5 & 11 \cdot 2 \end{array}$
271 272 273 274 275 276 277 278 279	44	297 457 616 775 933 091 248 404 560	313 473 632 791 949 10 <u>6</u> 263 420 576	329 489 648 8065 122 279 435 591	345 505 664 822 980 138 295 451 607	361 520 680 838 996 154 310 467 622	377 536 695 854 *012 169 326 326 482 638	393 552 711 870 *028 185 342 498 653	409 568 727 886 8043 201 357 513 669	4254 584 9019 *0556 3739 529 685	441 600 759 917 *075 232 389 545 700	$\begin{array}{c} .8 \\ .9 \\ 14 \cdot 8 \\ 14 \cdot 8 \\ 14 \cdot 4 \\ 15 \\ .1 \\ 1 \cdot 5 \\ $
280		716	731	747	762	778	793	809	824	839	855	$\begin{array}{cccccccccccccccccccccccccccccccccccc$
281 282 283 284 285 286 287 288 289	45 46	870 025 178 332 484 636 788 939 090	886 040 194 347 499 652 803 954 105	901 055 209 362 515 667 818 969 120	917 071 224 377 530 682 833 984 135	932 086 240 393 545 697 848 999 150	948 102 255 408 560 712 864 *014 165	963 117 270 423 576 727 879 *029 180	978 132 286 438 591 743 894 894 195	994 148 301 454 606 758 909 *059 210	*00 <u>9</u> 163 316 469 621 773 924 *075 225	$\begin{array}{c} .4 & 6.2 \\ .5 & 7.7 \\ .6 & 9.3 \\ 9.0 \\ .7 & 10.8 \\ 12.4 \\ 12.0 \\ .9 \\ 13.9 \\ 13.5 \end{array}$
290		240	255	269	284	299	314	329	344	359	374	$1\overline{4}$ 14 .1 1.4 1.4
291 292 293 294 295 296 297 298 299	47	389 538 687 834 982 129 275 421 567	404 553 701 849 997 144 290 436 581	419 568 716 864 *011 158 305 451 596	434 583 731 879 *026 173 319 465 610 755	449 597 746 894 *041 188 334 480 625 770	464 612 905 2028 494 639 784	479 627 923 *070 217 363 509 654 799	49 <u>3</u> 642 790 938 *085 232 378 523 668 813	508 657 952 *100 246 392 538 683 828	523 672 967 *114 261 407 552 697 842	$\begin{array}{c} 1 & 1 & 2 & 4 \\ 2 & 2 & 9 \\ 3 & 4 & 3 \\ 4 & 5 & 8 \\ 5 & 8 & 5 & 6 \\ 5 & 7 & 2 & 7 & 0 \\ 6 & 8 & 7 \\ 8 & 4 & 7 & 10 & 1 \\ 9 & 10 & 1 & 9 & 8 \\ 8 & 11 & 6 & 11 & 2 \\ 9 & 13 & 0 & 12 & 6 \end{array}$
300	-	712	726	741	/00		/04		-013 	026	042 	
N.		0	1	2	3	4	5	6	7	8	9	P. P.

#### TABLE V.-LOGARITHMS OF NUMBERS.

-	TABLE V.—LOGARITHMS OF NUMBERS.											
N.		0	1	2	3	4	5	6	7	8	9	P. P.
300	47	712	<b>7</b> 2ē	741	755	770	784	799	813	828	842	
301 302 303 304 305 306 307 308 309	48	85 <u>6</u> 00 <u>0</u> 14 <u>4</u> 287 430 572 714 855 996	871 015 158 301 444 586 728 869 *010	173 316 458 600 742 883	900 044 187 330 472 614 756 897 *038	058 201 344 487 629 770 911	928 072 216 358 501 643 784 925 *066	087 230 373 515 657 798 939	101 244 387 529 671 812 953	115 259 401 543 685 827 967	130 273 415 558 699 841 982	$\begin{array}{cccccccccccccccccccccccccccccccccccc$
310	49	136	150	164	178	192	206	220	234	248	262	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$
311 312 313 314 315 316 317 318 319	50	276 415 554 693 831 968 106 242 379	290 429 568 707 845 982 119 256 392	30 <u>4</u> 443 582 720 858 996 133 270 406	318 457 596 734 872 *010 147 283 420	471 610 748 886	346 485 624 762 900 *037 174 311 447	359 499 637 776 913 *051 188 324 460	373 513 651 789 927 *065 201 338 474	52 <u>6</u> 665 803 941 *078 215	540 679 817 955 *092 229	
320		515	528	542	555	569	583	596	610	623	637	
321 322 323 324 325 326 327 328 329	51	650 785 920 054 188 322 455 587 719	664 799 933 068 201 335 468 600 733	677 812 947 081 215 348 481 614 746	691 826 960 228 361 494 627 759	704 839 974 108 242 375 508 640 772	718 853 987 121 255 388 521 653 785	731 866 *001 135 268 401 534 667 798	745 880 148 282 415 547 680 812	758 893 *027 161 295 428 561 693 825	772 907 *041 175 308 441 574 574 838	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
330		851	864	877	891	904	917	93Ō	943	956	969	
331 332 333 334 335 336 337 338 339	52 53	983 114 244 374 504 634 763 891 020	996 127 257 387 517 647 776 904 033	*009 140 270 400 530 660 789 917 045	*022 153 283 413 543 672 801 930 058	*035 166 296 426 556 685 814 943 071	*048 179 3099 5698 698 827 956 084	*061 1922 3222 582 711 840 968 097	*07 <u>4</u> 20 <u>5</u> 335 <u>5</u> 595 <u>5</u> 724 853 98 <u>1</u> 109	*087 218 348 478 608 737 866 994 122	*10 <u>0</u> 231 36 <u>1</u> 621 750 879 *007 135	$\begin{array}{cccccccccccccccccccccccccccccccccccc$
340		148	160	173	186	199	211	$22\overline{4}$	237	250	262	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$
341 342 343 344 345 346 347 348 349	54	275 402 529 656 782 907 033 158 282 	288 415 542 668 794 920 045 170 295	301 428 554 681 807 932 058 183 307	313 440 567 693 819 945 070 195 320	326 453 580 706 832 958 083 208 332 450	339 466 592 719 845 970 095 220 344	352 478 605 731 857 983 108 232 357	364 491 618 744 870 995 120 245 369	377 504 630 756 882 *008 133 257 382	390 516 643 769 895 *020 145 270 394	- 6 7.5 7.2 -7 8.7 8.4 -8 10.0 9.6 -9 11.2 10.8
350 —		407	419	431	444	45ē	469	481	493 	506	518	
N.		0	1	2	3	4	5	6	7	8	9	Р. Р.

TABLE V.-LOGARITHMS OF NUMBERS.

	TABLE VLOGARITIMS OF NUMBERS.											
N.		0	1	2	3	4	5	6	7	8	9	P. P.
350	54	407	419	431	444	456	469	481	<b>49</b> 3	506	518	10
351 352 353 354 355 356 356 357 358 359	55	530 654 777 900 023 145 267 388 509	54 <u>3</u> 666 790 912 035 157 279 400 521	$55\overline{5} \\ 679 \\ 802 \\ 925 \\ 04\overline{7} \\ 169 \\ 291 \\ 41\overline{2} \\ 53\overline{3} \\ \end{array}$	568 691 814 937 059 181 303 424 545	580 703 826 949 071 194 315 437 558	592 716 839 961 084 206 327 449 570	605 728 851 974 096 218 340 461 582	617 740 863 986 108 230 352 473 594	629 753 876 998 120 242 364 485 606	642 765 888 *010 133 254 376 497 618	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
360		63Ō	642	654	666	678	69Ō	702	714	726	738	12
361 362 363 365 365 366 367 368 369	56	750 871 990 110 229 348 466 585 702	762 883 122 241 360 478 596 714	775 895 *014 134 253 372 490 608 726	787 907 *026 146 265 383 502 620 738	799 919 *038 158 277 395 514 632 749	811 931 *050 170 288 407 525 643 761	823 943 *062 181 300 419 537 655 773	835 955 193 312 431 549 667 785	847 966 205 205 324 443 561 679 796	859 978 217 336 455 573 691 808	.1 1.2 .2 2.4 .3 3.6 .4 4.8 .5 6.0 .6 7.2 .7 8.4 .8 9.6 .9 10.8
370		820	832	843	855	867	879	89Ō	902	914	925	11
371 372 373 374 375 376 376 377 378 378	57	937 054 171 287 403 519 634 749 864	949 066 182 299 414 530 645 760 875	961 077 194 310 426 542 657 772 887	9729 089 206 322 4333 6683 6683 898	984 101 217 333 449 565 680 795 909	996 112 229 345 461 576 691 806 921	*007 124 240 357 472 588 703 818 932	*019 136 252 368 484 599 714 829 944	*031 147 264 380 495 611 726 841 955	*042 159 275 391 507 622 737 852 967	.1 1.1 .2 2.3 .3 3.4 .4 4.6 .5 5.7 .6 6.9 .7 8.0 .8 9.2 .9 10.3
380		978	990	*001	*012	*024	*035	*047	*058	*069	*081	11
381 382 383 384 385 386 387 388 389	58	092 206 320 433 546 658 771 883 995	104 217 331 444 557 670 782 894 *006	115 229 345 568 681 793 905 *017	126 240 354 467 580 692 804 916 *028	138 252 365 478 591 703 816 928 *039	149 263 376 489 602 715 827 939 *050	161 274 388 501 613 726 838 950 *062	172 286 399 512 625 737 849 961 *073	183 297 410 523 636 748 861 972 *084	195 308 422 535 647 760 872 984 *095	1 1. 2 2.2 8 3.3 4 4.4 5 5.5 6 6 6 8 7 7.7 8 8.8 .9 9.9
390	59	106	117	128	140	151	162	173	184	195	206	10
<ul> <li>391</li> <li>392</li> <li>393</li> <li>394</li> <li>395</li> <li>396</li> <li>397</li> <li>398</li> <li>399</li> <li>400</li> </ul>	60_	217 328 439 549 549 769 879 988 097 206	229 339 450 560 670 780 890 999 108 217	240 351 461 571 681 791 901 *010 119 227	251 362 472 582 692 802 912 *021 130 238	262 373 483 593 703 813 923 *032 141 249	$\begin{array}{c} 273\\ 384\\ 494\\ 604\\ 714\\ 824\\ 933\\ *043\\ 151\\ 260\\ \end{array}$	284 395 505 615 725 835 944 *053 162 271	295 406 516 626 736 846 955 5 5 5 5 5 7 3 6 4 173 282	306 417 527 637 747 857 966 *075 184 293	317 428 538 648 758 868 977 *086 195 303	.1 1.0 .2 2 1 .3 4 2.2 .4 5 5 3 .6 6 7 7 3 .8 8 4 .9 9 .4
N.		0	1	2	3	4	5	6	7	8	9	P. P.

TABLE V.-LOGARITHMS OF NUMBERS.

-	TABLE VLOGARITHMS OF NUMBERS.											
N.		0	1	2	3	4	5	6	7	8	9	P, P.
400	60	206	217	227	238	249	26 <b>0</b>	271	282	293	30 <u>3</u>	
401 402 403 404 405 406 407 408 409	61	31 <u>4</u> 422 530 638 74 <u>5</u> 852 959 06 <u>6</u> 172	32 <u>5</u> 433 541 649 756 863 970 076 183	336 444 552 659 767 874 981 087 193	347 455 563 670 777 884 991 098 204	357 466 573 681 788 895 *002 108 215	36 <u>8</u> 47 <u>6</u> 584 692 799 906 *013 119 225	37 <u>9</u> 487 595 702 810 916 *023 130 236	390 498 606 713 820 927 *034 140 246	401 509 616 724 831 938 *044 151 257	412 519 627 735 842 949 *055 161 268	$\begin{array}{c} 11\\ .1 & 1.1\\ .2 & 2.2\\ .3 & 3.3\\ .4 & 4.4\\ .5 & 5.5\\ .6 & 6.6\\ .7 & 7.7\end{array}$
410		278	289	299	310	320	331	342	352	363	373	·8 8·8 ·9 9·9
411 412 413 414 415 416 417 418 419	62 ,	384 489 595 700 805 909 013 117 221	$\begin{array}{r} 39\overline{4} \\ 50\overline{0} \\ 60\overline{5} \\ 71\overline{0} \\ 81\overline{5} \\ 920 \\ 024 \\ 128 \\ 232 \end{array}$	$\begin{array}{r} 40\overline{5} \\ 511 \\ 616 \\ 721 \\ 82\overline{5} \\ 930 \\ 034 \\ 13\overline{8} \\ 242 \end{array}$	$\begin{array}{r} 416\\ 521\\ 626\\ 731\\ 836\\ 940\\ 045\\ 149\\ 252\\ \end{array}$	426 532 637 742 846 951 055 159 263	437 542 647 752 857 961 065 169 273	447 553 658 763 867 972 076 180 283	458 563 668 773 878 982 086 190 294	468 574 679 784 888 993 097 200 304	479 584 689 794 899 *003 107 211 314	$\begin{array}{c} 10\\ \cdot1 \\ \cdot2\\ 2\\ 2\\ 2\\ 1\\ 2\\ 7\\ 7 \end{array}$
420		825	335	345	356	<b>36</b> 6	376	387	397	407	418	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$
421 422 423 424 425 426 427 428 429	63	428 531 634 736 839 941 043 144 245	$\begin{array}{r} 43\overline{8} \\ 54\overline{1} \\ 644 \\ 747 \\ 849 \\ 951 \\ 053 \\ 154 \\ 256 \end{array}$	449 552 654 757 859 961 063 164 266	459 562 66 <u>5</u> 76 <u>7</u> 86 <u>9</u> 97 <u>1</u> 07 <u>3</u> 175 276	469 572 675 777 879 981 983 185 286	480 582 685 788 890 992 093 195 296	490 593 695 798 900 *002 104 205 306	500 603 706 808 910 *012 114 215 316	510 613 716 8180 920 8120 *022 124 526	521 624 726 828 931 828 931 235 8 336	$\begin{array}{c} .8 \\ .9 \\ 9 \\ 9 \\ .4 \\ 10 \\ .1 \\ 1.0 \\ .2 \\ 2.0 \\ \end{array}$
430		347	357	367	377	387	397	407	417	427	437	$\begin{array}{c c} .3 & 3.0 \\ .4 & 4.0 \\ .5 & 5.0 \end{array}$
431 432 433 434 435 436 437 438 439	64	447 548 649 749 849 948 048 147 246	458 558 659 759 859 958 058 157 256	468 568 669 769 869 968 068 167 266	478 578 679 779 87 <u>9</u> 978 078 177 276	488 588 689 789 889 988 088 187 286	498 598 699 799 89 <u>9</u> 998 098 197 296	508 608 709 809 909 *008 107 207 306	518 618 719 819 919 *018 117 217 315	528 628 729 928 928 127 226 325	538 639 739 839 938 *038 137 236 335	.6   6.0 .7   7.0 .8   8.0 .9   9.0
440		345	355	365	375	384	394	404	414	424	434	$\cdot 2   1 \cdot 9   2   2   3   3   3   3   3   3   3   3$
441 442 443 444 445 446 447 448 449 450	65	444 542 640 738 836 933 031 128 224 821	453 552 650 748 846 943 040 137 234 331	463 562 660 758 855 953 050 147 244 340	473 571 670 767 865 962 060 157 253 350	875 972 069 166 263	982 079 176 273	18 <u>6</u> 282	512 611 709 806 904 *001 195 292 389	522 621 718 816 914 *011 205 302 302 398	923 *021 118 215 311	.3   3.8 .5   4.7 .6   5.7 .7   6.6 .8   7.6 .9   8.5
	- -						-			-		
N.		0	1	2	3	4	5	6	7	8	9	P. P.

#### TABLE V.-LOGARITHMS OF NUMBERS.

N.		0	1	2	3	4	5	6	7	8	9	P. P.
450	65	<u>32</u> 1	331	340	350	360	369	379	389	398	408	
451 452 453 454 455 456 457 458 459	66	417 514 610 705 801 896 991 086 181	427 523 619 715 810 906 *001 096 190	437 533 629 724 820 915 *010 105 200	44 <u>6</u> 542 638 734 830 925 *020 115 209	456 552 648 74 <u>4</u> 839 934 *029 124 219	466 562 657 753 849 944 *039 134 228	475 571 667 763 858 953 *048 143 238	485 581 677 772 868 963 *058 153 247	877 972 *067	504 600 696 791 887 982 *077 172 266	$\begin{array}{c c c} .1 & 1.0 \\ .2 & 2.0 \\ .3 & 3.0 \\ .4 & 4.0 \\ .5 & 5.0 \\ .6 & 6.0 \end{array}$
460		276	285	294	304	313	323	332	342	351	360	
$\begin{array}{r} 461 \\ 462 \\ 463 \\ 464 \\ 465 \\ 466 \\ 467 \\ 468 \\ 469 \end{array}$	67	370 464 558 652 745 835 931 024 117	$37\overline{9}$ $47\overline{3}$ $56\overline{7}$ 661 $75\overline{4}$ 848 941 034 $12\overline{6}$	389 483 577 670 764 857 950 043 136	398 492 586 680 773 860 959 052 145	408 502 595 689 782 876 969 061 154	417 511 60 <u>5</u> 698 792 885 978 071 163	42 <u>6</u> 520 614 708 801 894 987 080 173	436 530 62 <u>3</u> 717 810 904 996 089 182	539 633 726 820	45 <u>5</u> 548 642 736 829 922 *015 108 200	$ \begin{array}{c c}  & \overline{9} \\  & \cdot 1 & 0 \cdot \overline{9} \\  & \cdot 2 & 1 \cdot 9 \\  & \cdot 3 & 2 \cdot 8 \\  & \cdot 4 & 3 \cdot 8 \end{array} $
470		210	219	228	237	246	256	265	274	283	293	.5   4.7 .6   5.7 .7   6.6
471 472 473 474 475 476 477 478 479	, 68	302 394 486 578 669 760 852 943 033	311 403 495 587 678 770 861 952 042	320 412 504 596 687 779 870 961 051	329 422 513 605 697 788 879 970 060	339 431 52 <u>3</u> 614 706 797 888 979 070	348 440 532 623 715 806 897 988 079	357 449 541 633 724 815 906 997 088	36 <u>6</u> 458 550 642 73 <u>3</u> 824 91 <u>5</u> 91 <u>5</u> 006 097	376 467 559 651 742 833 924 833 924 5 106	385 477 568 660 751 842 933 933 *024 115	$ \begin{array}{c} .8 & 7.6 \\ .9 & 8.5 \\ \end{array} $
480		124	133	142	151	160	169	178	187	196	205	$ \begin{array}{c c} \cdot 2 & 1 \cdot 8 \\ \cdot 3 & 2 \cdot 7 \end{array} $
481 482 483 484 485 486 487 488 489		$\begin{array}{r} 21\overline{4}\\ 30\overline{4}\\ 39\overline{4}\\ 48\overline{4}\\ 574\\ 66\overline{3}\\ 753\\ 842\\ 931 \end{array}$	223 313 403 493 583 672 762 851 940	232 322 412 502 592 681 770 860 948	24 <u>1</u> 331 42 <u>1</u> 511 601 690 779 868 957	250 340 520 610 699 788 877 966	259 349 529 619 708 797 886 975	268 358 448 538 628 717 806 895 984	277 367 457 547 637 726 815 904 993	286 376 556 646 735 824 913 *C02	295 385 475 654 744 833 922 *010	.4 3.6 .5 4.5 .6 5.4 .7 6.3 .8 7.2 .9 8.1
490	69	019	028	037	046	055	064	073	081	09Ō	099	$1 \mid 0.\overline{8}$
491 492 493 494 495 496 497 498 499 <b>500</b>		$     \begin{array}{r}       108 \\       196 \\       284 \\       372 \\       460 \\       548 \\       635 \\       723 \\       810 \\       897 \\     \end{array} $	117 205 293 381 469 557 644 731 819 905	126 214 302 390 478 565 653 740 827 914	134 223 311 399 487 574 662 749 836 923	143 232 320 408 495 583 670 758 845 931	152 240 328 416 504 592 679 766 353 766 353 940	161 249 337 425 513 600 688 775 862 949	170 258 346 434 522 609 697 784 871 958	179 267 355 443 530 618 705 792 879 966	187 276 364 451 539 627 714 801 888 975	$\begin{array}{c} .1 \\ 2 \\ 1 \\ .7 \\ .3 \\ .4 \\ .5 \\ .4 \\ .5 \\ .4 \\ .5 \\ .4 \\ .5 \\ .4 \\ .5 \\ .5$
N.		0	1	2	3	4	5	6	7	8	9	Р. Р.

TABLE V.—LOGARITHMS	$\mathbf{OF}$	NUMBERS.
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-	INDER V. HOGMITTIMS OF NOMBERS.											
N.		0	1	2	3	4	5	6	7	8	9	Р. Р.
500	69	897	905	914	923	931	<b>94</b> ō	949	958	<b>96</b> 6	975	
501 502 503 504 505 506 507 508 509	70	984 070 157 243 329 415 501 586 672	999 079 165 125 17 332 955 5955 680	*001 087 17 <u>4</u> 260 346 432 518 603 689	*010 096 182 269 355 441 526 612 697	*018 105 191 277 363 449 535 620 706	*027 113 200 286 372 458 543 629 714	*036 122 208 294 380 466 552 637 723	*044 131 217 303 389 475 560 646 731	*05 <u>3</u> 139 226 312 398 48 <u>3</u> 569 654 740	*061 148 234 320 406 492 578 663 748	$\begin{array}{c} 9\\ \cdot 1 0 \\ 0 \\ \cdot 2 \\ 1 \\ \cdot 8\\ \cdot 3 \\ 2 \\ \cdot 7\\ \cdot 4 \\ \cdot 3 \\ \cdot 6\\ \cdot 5 \\ \cdot 4\\ \cdot 5\\ \cdot 6 \\ \cdot 5 \\ \cdot 4\\ \cdot 7 \\ \cdot 6 \\ \cdot 3\\ \cdot 8 \\ \cdot 7 \\ \cdot 6 \\ \cdot 3\\ \cdot 8 \\ \cdot 7 \\ \cdot 6 \\ \cdot 3\\ \cdot 8 \\ \cdot 7 \\ \cdot 6 \\ \cdot 3\\ \cdot 8 \\ \cdot 7 \\ \cdot 6 \\ \cdot 3\\ \cdot 8 \\ \cdot 1 \end{array}$
510		757	765	774	782	791	799	808	<b>8</b> 1ē	825	<b>83</b> 3	98.1
511 512 513 514 515 516 517 518 519	71	842 927 011 096 180 265 349 433 516	850 935 020 105 189 273 357 441 525	$\begin{array}{r} 859\\ 944\\ 028\\ 113\\ 197\\ 282\\ 366\\ 449\\ 533\end{array}$	$\begin{array}{r} 86\overline{7} \\ 95\overline{2} \\ 037 \\ 12\overline{1} \\ 206 \\ 290 \\ 374 \\ 458 \\ 542 \end{array}$	876 961 045 130 214 298 382 466 550	884 969 054 138 223 307 391 475 558	893 978 062 147 231 315 399 483 567	901 986 071 1559 324 408 491 575	910 995 079 164 332 416 500 583	918 003 088 172 256 340 424 502 592	$ \begin{array}{c}                                     $
520		<b>6</b> 00	608	617	625	633	642	650	659	667	675	.54.2 .65.1 .75.9 .86.8
521 522 523 524 525 526 527 528 529	72	684 767 850 933 016 098 181 263 345	692 775 858 941 024 107 189 271 354	700 783 867 949 032 115 197 280 362	709 792 875 958 040 123 206 288 370	717 800 883 966 949 131 214 296 378	7258 8091 974 977 140 222 304 386	734 817 900 983 065 148 230 312 395	742 825 908 991 074 156 238 321 403	750 833 916 999 082 164 247 329 411	758 842 925 *007 090 173 255 337 419	-917-6
530		427	436	444	452	<b>46</b> 0	468	476	485	493	501	·21.6 ·32.4
531 532 533 534 535 536 537 538 539	73	509 591 672 754 835 916 997 078 159	517 599 681 762 843 924 924 8005 086 167	526 607 689 770 851 932 932 932 932 932 932 932 932 932 932	534 615 697 778 859 941 102 183	542 624 705 786 868 949 *030 110 191	550 632 713 795 876 957 *038 118 199	558 640 721 803 884 965 *046 126 207	566 648 729 811 892 973 *054 134 215	575 656 738 819 900 981 *062 143 223	58 <u>3</u> 664 74 <u>6</u> 827 90 <u>8</u> 989 *070 151 231	.101.6 .32.4 .43.2 .54.0 .64.8 .75.6 .86.4 .97.2
540		239	247	255	263	271	279	287	295	303	311	.110.7
541 542 543 544 545 546 547 548 549		319 400 480 560 639 719 798 878 957	328 408 488 568 647 727 806 886 965	336 416 576 655 735 814 894 973	344 424 504 584 663 743 822 902 981	352 432 512 592 671 751 830 909 989	360 440 520 600 679 759 838 917 997	368 448 528 608 687 767 846 925 *004	376 456 536 536 536 536 535 695 855 853 9012 * 0012	384 464 544 6233 703 783 862 941 862 941 020 *020	392 472 552 631 711 791 870 9428 *028	.10.7 .21.5 .312.5 .413.0 .513.5 .614.5 .75.2 .816.0 .916.7
550	74	036	044	052	060	068	075	08 <u>3</u>	091	099	107	
N.		0	1	2	3	4	5	6	7	8	9	Р. Р,

TABLE V.-LOGARITHMS OF NUMBERS.

N.		0	1	2	3	4	5	6	7	8	9	Р. Р.
550	74	<b>03</b> ē	044	052	060	068	075	083	091	099	107	
551 552 553 554 555 556 557 558 559		$\begin{array}{r} 115\\ 194\\ 272\\ 351\\ 429\\ 507\\ 585\\ 663\\ 741 \end{array}$	123 202 280 359 437 515 593 671 749	131 209 288 366 445 523 601 679 756	139 217 296 374 453 531 609 687 764	$14\overline{6} \\ 22\overline{5} \\ 304 \\ 382 \\ 46\overline{0} \\ 53\overline{8} \\ 61\overline{6} \\ 694 \\ 772 \\$	$15\overline{4} \\ 233 \\ 312 \\ 390 \\ 468 \\ 546 \\ 624 \\ 702 \\ 780 \\ 7$	162 241 319 398 476 554 632 710 788	170 249 327 406 484 562 640 718 795	$   \begin{array}{r} 178 \\     257 \\     335 \\     413 \\     492 \\     570 \\     648 \\     725 \\     803 \\   \end{array} $	186 264 343 421 499 577 655 733 811	$ \begin{array}{c ccccc} 8 \\ \cdot 1 & 0.8 \\ \cdot 2 & 1.6 \\ \cdot 3 & 2.4 \end{array} $
560		819	826	834	842	<b>85</b> 0	857	865	873	881	888	$ \begin{array}{c c} \cdot 4 & 3 \cdot 2 \\ \cdot 5 & 4 \cdot 0 \end{array} $
561 562 563 564 565 566 567 568 569	75	89 <u>6</u> 973 051 128 205 28 <u>1</u> 358 435 511	904 981 058 135 212 289 366 442 519	912 989 066 143 220 297 373 450 526	919 997 074 151 228 304 381 458 534	927 004 158 235 312 389 465 541	935 *012 089 166 243 320 396 473 549	942 *020 097 174 251 327 404 480 557	950 *027 105 182 258 335 412 488 564	958 *035 112 189 266 343 419 496 572	966 *043 120 197 274 350 427 503 580	-6 4.8 -7 5.6 -8 6-4 -9 7.2
570		587	595	602	61Ō	618	625	633	641	648	656	
571 572 573 574 575 576 576 577 578 579	76	$\begin{array}{r} 66\overline{3} \\ 73\overline{9} \\ 815 \\ 891 \\ 967 \\ 042 \\ 117 \\ 193 \\ 268 \end{array}$	671 747 823 899 974 050 125 200 275	679 755 830 906 982 057 132 208 283	68 762 838 914 989 065 140 215 290	694 770 846 921 997 072 147 223 298	701 777 853 929 929 *004 080 155 230 305	709 785 861 936 *012 087 162 238 313	717 792 868 944 *019 095 170 245 320	724 800 876 951 *027 102 178 253 328	732 8083 9594 110 1850 335	7         1         0.7         .2         1.5         .3         .4         .5         .6         4.55         .7         5.62         .7         .8         .9         6.7
580		343	35Ō	358	365	372	380	387	395	402	410	
581 582 583 584 585 586 587 588 588 589	77	417 492 567 641 715 790 864 937 011	425 500 574 648 723 797 871 945 019	432 507 582 656 730 804 878 952 026	440 514 589 663 738 812 886 960 033	447 522 596 671 596 819 893 967 041	455 529 604 678 752 827 901 974 974 048	462 537 611 686 760 834 908 908 982 055	470 544 693 767 841 915 989 063	477 552 626 700 775 849 923 997 070	485 559 634 708 782 856 930 *004 078	$\begin{array}{c} & 7\\ .1 & 0.7\\ .2 & 1.4\\ .3 & 2.1 \end{array}$
590		085	092	100	107	114	122	129	136	144	151	·4 2·8 ·5 3·5
591 592 593 594 595 596 597 598 599		158 232 305 378 451 524 597 670 742	$     \begin{array}{r}       166\\       239\\       313\\       386\\       459\\       532\\       604\\       677\\       750     \end{array} $	$17\overline{3} \\ 247 \\ 320 \\ 39\overline{3} \\ 466 \\ 539 \\ 612 \\ 684 \\ 757 \\ 0.757 \\ $	$     \begin{array}{r}       181 \\       254 \\       327 \\       400 \\       473 \\       546 \\       619 \\       692 \\       764 \\       \hline       764 \\       \hline       $	188 261 335 408 481 554 626 699 771	195 269 342 415 488 561 634 706 779	203 276 349 422 495 568 641 713 786	210 283 356 430 503 575 648 721 793	217 291 364 437 510 583 655 728 800	225 298 371 444 517 590 663 735 808	.6   4.2 .7   4.9 .8   5.6 .9   6.3
600 		815	822	829	837	844	851	858	866	873	880	
Ν.		0	1	2	3	4	5	6	7	8	9	P. P.

TABLE V.-LOGARITHMS OF NUMBERS.

N.		0	1	2	3	4	5	6	7	8	9	Р. Р.
600	77	815	822	829	837	844	851	858	866	873	880	
601 602 603 604 605 606 607 608 609	78	887 959 031 103 175 247 319 390 461	894 967 039 111 182 254 326 397 469	902 974 046 118 190 261 333 404 476	909 981 053 125 197 269 340 412 483	91 <u>6</u> 988 060 132 204 27 <u>6</u> 347 419 490	923 995 067 139 211 283 354 426 497	931 *003 075 147 218 290 362 433 504	938 *010 .082 154 226 297 369 440 511	945 *017 089 161 233 304 376 447 518	952 *024 0968 240 311 383 454 526	·1 0 123 ·3 ·5 ·5 ·7
610		533	540	547	554	561	568	575	583	590	597	•4 3•0 •5 3•7
611 612 613 614 615 616 617 618 619	79	604 675 746 817 887 958 028 099 169	611 682 753 824 894 965 035 106 176	618 689 760 831 901 972 042 113 183	$\begin{array}{r} 62\overline{5} \\ 69\overline{6} \\ 76\overline{7} \\ 838 \\ 908 \\ 979 \\ 049 \\ 120 \\ 190 \end{array}$	632 703 774 845 915 986 056 127 197	$\begin{array}{r} 63\overline{9} \\ 71\overline{0} \\ 78\overline{1} \\ 852 \\ 923 \\ 993 \\ 06\overline{3} \\ 134 \\ 204 \end{array}$	64 <u>6</u> 717 788 859 930 *000 070 141 211	654 725 795 866 937 *007 078 148 218	661 732 802 873 944 *014 085 155 225	668 739 810 880 951 *021 092 162 232	.6 4.5 .7 5.2 .8 6.7 .9 6.7
620		239	246	253	260	267	274	281	288	295	<b>3</b> 02	
621 622 623 624 625 626 627 628 629		309 379 449 518 588 657 727 796 865	316 386 456 525 595 664 733 803 872	323 39 <u>3</u> 46 <u>2</u> 53 <u>2</u> 60 <u>2</u> 67 <u>1</u> 740 810 879	330 400 469 539 609 678 747 816 886	337 407 476 546 616 685 754 823 892	344 414 483 553 622 692 761 830 899	351 421 490 560 629 699 768 837 906	358 428 497 567 636 706 775 844 913	365 435 504 574 643 713 782 851 920	372 442 511 581 650 720 789 858 927	1     0.7       .2     1.4       .3     2.1       .4     2.8       .5     4.2       .6     4.2       .7     4.9       .8     5.6       .9     6.3
630		934	941	948	954	96Ī	968	975	98 <u>7</u>	989	996	
631 632 633 634 635 636 637 638 639	80	$\begin{array}{r} 003\\ 071\\ 140\\ 209\\ 277\\ 345\\ 414\\ 482\\ 550\\ \end{array}$	010 078 147 216 284 352 421 489 557	$\begin{array}{r} 01\overline{6} \\ 085 \\ 154 \\ 222 \\ 291 \\ 359 \\ 427 \\ 495 \\ 563 \end{array}$	023 092 161 229 298 366 434 502 570	030 099 168 236 304 373 441 509 577	$\begin{array}{r} 03\overline{7} \\ 106 \\ 174 \\ 243 \\ 311 \\ 380 \\ 448 \\ 516 \\ 584 \end{array}$	044 113 181 250 318 386 455 523 591	051 120 188 257 325 393 461 529 597	$\begin{array}{r} 058 \\ 126 \\ 195 \\ 263 \\ 332 \\ 400 \\ 468 \\ 536 \\ 604 \end{array}$	$\begin{array}{r} 065\\ 133\\ 202\\ 270\\ 339\\ 407\\ 475\\ 543\\ 611 \end{array}$	$ \begin{array}{c c} \overline{6} \\ \cdot 1 & \overline{6} \\ \cdot 2 & 1 \cdot 3 \\ \cdot 3 & 1 \cdot 9 \end{array} $
640		618	625	631	638	645	652	658	665	672	679	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$
641 642 643 644 645 646 647 648 649 650	81	686 753 821 888 956 023 090 157 224 	692 760 828 895 962 030 097 164 231 298	699 767 834 902 969 036 104 171 238 304	706 774 841 909 976 04 <u>3</u> 110 177 244 311	713 780 848 915 983 050 117 184 251 318	719 787 855 922 989 057 124 191 258 324	726 794 861 929 996 063 130 197 264 331	733 801 868 936 *003 070 137 204 271 338	740 807 942 *010 077 144 211 278 345	74 <u>6</u> 814 882 949 *01 <u>6</u> 083 151 218 284 351	.6   3.9 .7   4.5 .8   5.2 .9   5.8
N.		0	1	2	3	4	5	6	7	8	9	P. P.

### TABLE V.-LOGARITHMS OF NUMBERS.

	TABLE VLOGARITHMS OF NUMBERS.													
N.		0	1	2	3	4	5	6	7	8	9	P. P.		
650	81	291	298	304	311	318	324	331	338	345	351			
$\begin{array}{r} 651 \\ 652 \\ 653 \\ 654 \\ 655 \\ 656 \\ 657 \\ 658 \\ 659 \end{array}$		358 425 491 558 624 690 756 822 888	365 431 498 564 631 697 763 829 895	371 438 504 571 637 703 703 770 836 901	378 444 511 577 644 710 776 842 908	385 451 518 584 650 717 783 849 915	391 458 524 591 657 723 789 855 855 921	39 <u>8</u> 464 531 597 664 730 796 862 928	405 471 538 604 670 736 803 803 869 934	411 478 544 611 677 743 809 875 941	418 484 551 617 684 750 816 882 948	$\begin{array}{c c} & 7 \\ .1 & 0.7 \\ .2 & 1.4 \\ .3 & 2.1 \end{array}$		
660		954	961	967	974	9 <b>8</b> 0	987	994	*00ō	*007	*013	·4 2·8 ·5 3·5		
661 662 663 664 665 666 667 668 669	82	020 086 151 217 282 347 412 477 542	026 092 158 223 288 354 419 484 549	033 099 164 230 295 360 425 555	040 105 171 236 302 367 432 497 562	$\begin{array}{r} 04\overline{6} \\ 112 \\ 177 \\ 243 \\ 308 \\ 373 \\ 438 \\ 503 \\ 568 \end{array}$	053 118 184 249 315 380 445 510 575	059 125 190 256 321 386 451 516 581	06 <u>6</u> 131 197 262 328 393 458 523 588	$\begin{array}{r} 07\bar{2} \\ 138 \\ 203 \\ 269 \\ 33\bar{4} \\ 39\bar{9} \\ 46\bar{4} \\ 52\bar{9} \\ 59\bar{4} \end{array}$	$\begin{array}{r} 079 \\ 145 \\ 210 \\ 275 \\ 341 \\ 406 \\ 471 \\ 536 \\ 601 \end{array}$	.6   4.2 .7   4.9 .8   5.6 .9   6.3		
670		607	614	620	627	633	640	646	653	659	666			
671 672 673 674 675 676 677 678 679	83	672 737 801 866 930 994 059 123 187	678 743 808 872 937 *001 065 129 193	685 750 814 879 943 *007 071 136 200	691 756 821 885 949 *014 078 142 206	698 763 827 956 956 020 084 148 212	704 769 834 962 *027 091 155 219	711 775 840 904 969 *033 097 161 225	717 782 846 911 975 *039 103 168 231	724 788 853 917 982 *046 110 174 238	730 795 859 924 988 *052 116 180 244	$\begin{array}{c} 6 \\ .1 \\ .2 \\ .2 \\ .3 \\ .5 \\ $		
680		251	257	263	270	276	283	289	295	<b>3</b> 02	308			
681 682 683 684 685 686 687 688 688 689		314 378 442 505 569 632 695 759 822	321 385 448 512 575 638 702 765 828	327 391 455 518 581 645 708 771 834	33 <u>4</u> 397 46 <u>1</u> 524 588 65 <u>1</u> 714 778 841	340 404 531 594 657 721 784 847	34 <u>6</u> 410 474 537 600 664 727 790 853	353 416 480 543 607 670 733 670 735 859	359 423 486 550 613 676 740 803 866	36 <u>5</u> 429 493 55 <u>6</u> 619 683 74 <u>6</u> 80 <u>9</u> 872	372 435 562 626 689 752 815 878	$\begin{array}{c} 6 \\ \cdot 1 &   \ 0 \cdot 6 \\ \cdot 2 &   \ 1 \cdot 2 \\ \cdot 3 &   \ 1 \cdot 8 \end{array}$		
690		885	891	897	904	910	91 <del></del>	922	929	935	941	$ \begin{array}{c c} \cdot 4 & 2 \cdot 4 \\ \cdot 5 & 3 \cdot 0 \end{array} $		
691 692 693 694 695 696 697 698 699	84	948 010 073 136 198 261 323 385 447	954 017 079 142 204 267 329 392 454	960 023 086 148 211 273 335 398 460	966 029 092 154 217 279 342 404 466 528	97 <u>3</u> 03 <u>5</u> 098 161 223 286 348 410 472 534	979 042 104 167 229 292 354 416 479	985 048 111 173 236 298 360 423 485	992 054 117 179 242 304 367 429 491	998 061 123 186 248 311 373 435 497	*004 067 129 192 254 317 379 441 503	.6 3.6 .7 4.2 .8 4.8 .9 5.4		
700		510	516	522			541	547	553	559	565 			
N.		0	1	2	3	4	5	6	7	8	9	P. P.		

#### TABLE V.-LOGARITHMS OF NUMBERS.

	TABLE V.—LOGARITHMS OF NUMBERS.           N.         0         1         2         3         4         5         6         7         8         9         P. P.													
N.		0	1	2	3	4	5	6	7	8	9	Р, Р.		
700	84	510	516	522	528	534	541	547	553	559	565			
701 702 703 704 705 706 707 708 709	85	572 633 557 757 819 942 942 003 064	578 640 701 763 825 886 948 009 070	584 646 708 769 831 893 954 015 077	590 652 714 776 837 899 960 021 083	59 <u>6</u> 658 720 782 843 905 966 028 089	60 <u>3</u> 66 <u>4</u> 726 78 <u>8</u> 911 972 034 095	609 671 732 794 856 917 979 040 101	615 677 739 800 862 923 985 046 107	621 683 745 806 868 929 991 052 113	627 689 751 813 874 936 997 058 119	$.1   0.\overline{6}$		
710		126	132	138	144	150	156	162	168	174	181	·4 2·6 ·5 3·2		
711 712 718 714 715 716 717 718 719		187 248 309 370 430 491 552 612 673	193 254 315 376 436 497 558 618 679	$199 \\ 260 \\ 321 \\ 382 \\ 443 \\ 503 \\ 564 \\ 624 \\ 685 \\$	20 <u>5</u> 266 327 388 449 509 570 630 691	211 272 333 394 515 576 636 697	217 278 339 400 461 521 582 642 703	223 284 345 406 467 527 588 648 709	229 290 351 412 53 <u>3</u> 594 655 715	236 297 357 418 479 540 600 661 721	242 303 363 424 485 546 606 667 727	$ \begin{array}{c c c c c c c c c c c c c c c c c c c $		
720		733	739	745	75ī	757	763	769	775	781	787			
721 722 723 724 725 726 727 728 729	86	79 <u>3</u> 853 914 974 09 <u>3</u> 153 213 273	799 859 920 980 040 099 159 219 278	805 926 986 046 105 165 225 284	811 872 932 992 052 111 171 231 290	817 878 938 998 058 117 177 237 296	823 884 944 *004 123 183 243 302	829 890 950 *010 129 189 249 308	835 896 956 *016 075 135 195 255 314	841 902 962 *022 081 141 201 261 320	847 908 968 *028 087 147 207 267 326	$\begin{array}{c c c} & & & & & & & & & & & & & & & & & & &$		
730		<b>3</b> 32	338	344	350	356	362	368	374	380	386			
731 732 733 734 735 736 736 737 738 739		391 510 569 628 688 746 805 864	397 457 516 575 634 693 752 811 870	403 463 522 581 640 699 758 817 876	409 469 528 587 646 705 764 823 882	415 475 59 <u>3</u> 652 711 770 829 888	421 481 540 599 658 717 776 835 894	427 486 546 605 664 723 782 841 899	433 492 552 611 670 729 788 847 905	439 498 558 617 676 735 794 852 911	445 504 563 623 682 741 800 858 917	$egin{array}{c c} .1 & \overline{5} \\ .2 & 1 \cdot 1 \\ .3 & 1 \cdot 6 \end{array}$		
740		923	929	935	941	946	952	958	964	970	976	$ \begin{array}{c cc} \cdot 4 & 2 \cdot 2 \\ \cdot 5 & 2 \cdot 7 \end{array} $		
741 742 743 744 745 746 747 748 749 <b>750</b>	87	982 040 099 157 215 274 332 390 448 506	987 046 104 163 221 279 338 396 454 512	993 052 110 169 227 285 343 402 460 517	999 058 116 175 233 291 349 407 465 523	*005 064 122 180 239 297 355 413 471 529	*011 069 128 245 303 361 419 477 535	*017 075 134 192 250 309 367 425 483 541	*023 081 140 198 256 314 372 431 489 546	*028 087 145 204 262 320 378 436 494 552	*034 093 151 210 268 326 384 500 558	.5 .5 .6 3.3 .7 .8 4.4 .9 4.9		
N.		0	1	2	3	4	5	6	7	8	9	P. P.		
-	1			1						1				

TABLE V.-LOGARITHMS OF NUMBERS.

N.         0         1         2         3         4         5         6         7         8         9         P. I												
N.		0	1	2	3	4	5	6	7	8	9	P. P.
750	87	506	512	517	523	529	535	541	546	552	558	
751 752 753 754 755 756 757 758 759	88	564 622 679 737 794 852 909 967 024	570 627 685 743 800 858 915 972 030	57 <u>5</u> 633 691 748 80 <u>6</u> 863 921 978 035	581 639 697 754 812 869 927 984 041	587 645 702 760 817 875 932 932 990 047	766 823	598 656 714 771 829 886 944 *001 058	662 720 777 835 892 949 *007	668 725 783 840 898 955 *012	67 <u>3</u> 731 789 846 904 961 *018	6 ·1   0.6 ·2   1.2 ·3   1.8
760		081	087	093	098	104	110	115	121	127	133	$ \begin{array}{c c} \cdot 4 & 2 \cdot 4 \\ \cdot 5 & 3 \cdot 0 \end{array} $
761 762 763 764 765 766 767 768 769		$13\overline{8} \\ 19\overline{5} \\ 25\overline{2} \\ 30\overline{9} \\ 366 \\ 423 \\ 47\overline{9} \\ 536 \\ 59\overline{2} \\ 59\overline{2}$	$144 \\ 201 \\ 258 \\ 315 \\ 372 \\ 428 \\ 485 \\ 542 \\ 598 \\ \\ 598 \\ \\ \\ 598 \\ \\ \\ \\ 598 \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\$	$150 \\ 207 \\ 264 \\ 320 \\ 377 \\ 434 \\ 491 \\ 547 \\ 604$	$   \begin{array}{r} 15\overline{5} \\ 212 \\ 26\overline{9} \\ 326 \\ 383 \\ 440 \\ 496 \\ 553 \\ 609 \end{array} $	$16\overline{1} \\ 21\overline{8} \\ 275 \\ 332 \\ 389 \\ 445 \\ 502 \\ 55\overline{8} \\ 615 \\ \end{array}$	$167 \\ 224 \\ 281 \\ 337 \\ 394 \\ 451 \\ 508 \\ 564 \\ 621$	172 229 286 343 400 457 513 570 626	$   \begin{array}{r} 17\overline{8} \\ 23\overline{5} \\ 29\overline{2} \\ 349 \\ 406 \\ 46\overline{2} \\ 519 \\ 57\overline{5} \\ 632 \end{array} $	$     \begin{array}{r}       184 \\       241 \\       298 \\       355 \\       411 \\       468 \\       525 \\       581 \\       638 \\     \end{array} $	$247 \\ 303 \\ 360 \\ 417$	.6   3.6 .7   4.2 .8   4.2 .9   5.4
770		649	654	66Ō	666	67ī	677	683	688	694	700	_
771 772 773 774 775 776 777 778 779	89	705 761 818 874 930 986 042 098 153	711 767 823 879 936 992 047 103 159	716 773 829 885 941 997 053 109 165	722 778 835 891 947 *003 059 114 170	728 7840 8902 9528 9528 0684 120 176	733 790 846 902 958 *014 070 126 181	739 795 851 907 964 *019 075 131 187	745 801 913 969 *025 081 137 193	750 806 863 919 975 *031 087 142 198	756 812 868 924 980 *036 092 148 204	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$
780		209	215	22 <b>0</b>	226	231	237	243	248	254	259	
781 782 783 784 785 786 787 788 788 789		265 320 376 431 487 542 597 652 707	270 326 381 437 492 548 603 658 713	276 332 387 442 498 553 608 663 718	282 337 393 448 503 559 614 669 724	287 343 398 454 509 564 674 674 729	29 <u>3</u> 348 404 514 570 625 680 735	298 354 409 465 520 575 630 685 685 740	304 359 415 470 525 581 636 691 746	309 365 420 476 531 586 641 696 751	315 370 426 481 536 592 647 702 757	$\begin{array}{c} .1 & 5 \\ .2 & 0.5 \\ .2 & 1.0 \\ .3 & 1.5 \end{array}$
790		762	768	773	779	784	790	795	801	<b>8</b> 0ē	<b>8</b> 12	·4 2·0 ·5 2·5
791 792 793 794 795 796 797 798 799	90	817 872 927 982 036 091 146 200 254	823 878 933 987 042 097 151 205 260	828 883 938 993 047 102 156 211 265	834 889 943 998 053 107 162 216 271	839 949 949 *004 058 113 167 222 276	845 900 954 *009 064 118 173 227 282	850 905 960 *015 069 124 178 233 287	856 911 965 *020 075 129 184 238 292	86 <u>1</u> 916 971 *02 <u>6</u> 080 135 189 244 298	867 922 976 *031 086 140 195 249 303	.6   3.0 .7   3.5 .8   4.0 .9   4.5
800	_	809	814	320	325	<u>330</u>	336	341	347	352	358	
N.		0	1	2	3	4	5	6	7	8	9	Р. Р.

TABLE V.-LOGARITHMS OF NUMBERS.

				UMD	LILS:							
N.		0	1	2	3	. 4	5	6	7	8	9	Р. Р.
800	90	309	314	320	325	330	336	341	347	352	358	
801 802 803 804 805 806 807 808 808		36 <u>3</u> 417 52 <u>5</u> 57 <u>9</u> 63 <u>3</u> 687 741 795	368 423 477 531 585 639 692 746 800	374 428 536 590 644 698 752 805	379 433 488 542 596 649 703 757 811	385 439 547 601 655 709 762 816	390 444 552 606 660 714 768 821	396 450 504 558 612 66 <u>6</u> 71 <u>9</u> 773 827	401 455 509 563 617 671 725 778 832	40 <u>6</u> 460 515 569 622 67 <u>6</u> 730 784 838	412 466 520 574 628 682 736 789 843	
810		848	854	859	864	870	875	<b>88</b> 0	886	891	<b>89</b> 6	_
811 812 813 814 815 816 817 818 819	91	902 955 009 062 116 169 222 275 328	907 961 014 068 121 174 227 280 333	913 966 019 073 126 179 233 286 339	918 971 025 078 131 185 238 291 344	923 977 030 084 137 190 243 296 349	929 982 036 089 142 195 249 302 355	934 987 041 094 147 201 254 307 360	939 993 046 100 153 206 259 312 365	94 <u>5</u> 998 052 10 <u>5</u> 21 <u>1</u> 26 <u>4</u> 318 371	950 *003 057 110 163 217 270 323 376	$\begin{array}{c} & 5 \\ \cdot 1 & 0 \cdot \overline{5} \\ \cdot 2 & 1 \cdot 1 \\ \cdot 3 & 1 \cdot \overline{6} \\ \cdot 4 & 2 \cdot 2 \\ \cdot 5 & 2 \cdot \overline{7} \\ \cdot 6 & 3 \cdot 3 \\ \cdot 7 & 3 \cdot 8 \\ \cdot 8 & 4 \cdot 4 \\ \cdot 9 & 4 \cdot 9 \end{array}$
820		381	386	392	397	402	408	413	418	423	429	
821 822 823 824 825 826 826 827 828 829		434 487 540 592 645 698 750 803 855	439 492 545 598 650 703 756 808 860	445 497 550 603 656 708 761 813 866	450 503 556 608 661 714 766 819 871	455 508 561 614 666 719 771 824 876	461 513 566 671 724 777 829 881	466 519 571 624 677 729 782 834 887	471 524 577 629 682 735 787 839 892	47 <u>6</u> 529 582 635 687 740 792 845 897	482 534 587 640 692 745 798 850 902	
830		908	913	918	92 <del>3</del>	928	934	939	944	949	955	
831 832 833 834 835 836 837 838 837 838 839	92	960 012 064 116 220 272 324 376	965 017 069 122 174 226 277 329 381	970 023 075 127 179 231 283 335 386	976 028 080 132 184 236 288 34C 391	981 0335 137 189 241 293 345 397	986 038 090 142 194 246 298 350 402	$991 \\ 043 \\ 096 \\ 148 \\ 200 \\ 252 \\ 303 \\ 355 \\ 407 \\$	996 049 101 153 205 257 309 360 412	*002 054 106 158 210 262 314 366 417	*007 059 111 215 267 319 371 423	$\begin{array}{c} & 5 \\ .1 & 0.5 \\ .2 & 1.0 \\ .3 & 1.5 \\ .4 & 2.0 \\ .5 & 2.5 \\ .6 & 3.0 \\ .7 & 3.5 \\ .8 & 4.0 \\ .9 & 4.5 \end{array}$
840		428	433	438	<b>44</b> 3	448	454	459	464	469	474	
841 842 843 844 845 846 847 848 849 850		479 531 583 634 685 737 788 839 891 942	485 536 588 639 691 742 793 844 896 947	490 541 593 644 696 747 798 850 901 952	495 546 598 649 701 752 803 855 906 957	500 552 603 655 706 757 809 860 911 962	505 557 608 660 711 762 814 865 916 967	510 562 613 665 716 768 819 921 921 972	515 567 619 670 721 773 824 926 926 977	521 572 624 675 727 728 829 931 982	526 577 629 680 732 783 834 885 937 988	
<u>.</u>	-	0	1	2	3	4	5	6		8	9	Р. Р.
-	1											

#### TABLE V.-LOGARITHMS OF NUMBERS.

	TABLE V.—LOGARITHMS OF NUMBERS.       N.     0     1     2     3     4     5     6     7     8     9     P. P.													
N.		0	1	2	3	4	5	6	7	8	9	Р. Р.		
850	92	942	947	952	957	962	967	972	977	982	988			
851 852 853 854 855 856 857 858 859	93	993 044 095 146 196 247 298 348 399	$\begin{array}{r} 998\\ 049\\ 100\\ 151\\ 201\\ 252\\ 303\\ 354\\ 404\\ \end{array}$	*003 054 105 207 257 308 359 409	*008 059 110 161 212 262 313 364 414	*01 <u>3</u> 064 115 166 217 267 318 369 419	*018 069 120 171 222 272 323 374 424	*023 074 125 176 227 278 328 379 429	*028 079 130 181 232 283 333 384 434	084 135 186	*039 090 140 191 242 293 343 394 445	$\begin{array}{c} & \overline{5} \\ \cdot 1 &   & 0.5 \\ \cdot 2 & 1.1 \\ \cdot 3 &   & 1.6 \end{array}$		
860		<b>4</b> 50	455	460	465	470	475	480	485	490	495	$ \begin{array}{c c} \cdot 4 & 2 \cdot 2 \\ \cdot 5 & 2 \cdot 7 \end{array} $		
861 862 863 864 865 866 867 868 869		500 550 601 651 701 752 802 852 902	505 556 606 706 757 807 857 907	510 561 661 711 762 812 862 912	515 566 61 <u>6</u> 66 <u>6</u> 716 767 817 867 917	520 571 621 721 722 822 872 922	525 576 626 726 726 777 827 827 827 927	530 581 631 681 731 782 832 882 932	535 586 636 736 736 787 837 887 937	540 591 641 691 742 792 842 892 942	545 596 646 747 797 847 897 947	.4 .5 .5 .6 .7 .7 .8 .4 .4 .2 .7 .6 .3 .8 .8 .8 .8 .4 .4 .9		
870		952	957	962	967	<b>97</b> 2	977	982	987	992	997			
871 872 873 874 875 876 877 878 877 878 879	94	002 05 <u>1</u> 101 151 20 <u>1</u> 250 300 349 399	$\begin{array}{r} 007\\ 056\\ 106\\ 206\\ 255\\ 305\\ 354\\ 404 \end{array}$	$\begin{array}{c} 012\\ 061\\ 111\\ 161\\ 210\\ 260\\ 310\\ 359\\ 409 \end{array}$	017 066 116 215 265 315 364 413	022 071 121 220 270 320 369 418	02 <u>6</u> 07 <u>6</u> 126 17 <u>6</u> 225 27 <u>5</u> 324 37 <u>4</u> 37 <u>4</u>	$\begin{array}{c} 03\overline{1} \\ 08\overline{1} \\ 13\overline{1} \\ 181 \\ 230 \\ 280 \\ 329 \\ 329 \\ 379 \\ 428 \end{array}$	036 086 136 235 285 334 384 433	$\begin{array}{c} 04\overline{1} \\ 091 \\ 141 \\ 191 \\ 240 \\ 290 \\ 339 \\ 389 \\ 438 \end{array}$	04 <u>6</u> 096 146 245 295 344 394 443	$\begin{array}{c} 5\\ \cdot 1 & 0.5\\ \cdot 2 & 1.0\\ \cdot 3 & 1.5\\ \cdot 4 & 2.0\\ \cdot 5 & 2.5\\ \cdot 6 & 3.0\\ \cdot 7 & 3.5\\ \cdot 8 & 4.0\\ \cdot 9 & 4.5\end{array}$		
880		448	453	458	463	468	473	478	483	487	492			
881 882 883 884 885 886 887 888 888 889		497 547 596 645 694 743 792 841 890	502 552 601 650 699 748 797 846 895	507 556 606 655 704 753 802 851 900	$51\overline{2} \\ 56\overline{1} \\ 611 \\ 660 \\ 709 \\ 758 \\ 807 \\ 856 \\ 905 \\ $	517 566 615 665 714 763 812 861 909	522 571 620 670 719 768 817 865 914	527 576 625 674 724 773 821 870 910	532 581 630 728 728 777 826 875 825 924	537 586 635 684 733 782 831 880 929	542 591 649 738 737 836 885 934	$ \begin{array}{c c}  & 4 \\  & 0.4 \\  & 2 \\  & 0.9 \\  & 3 \\  & 1.3 \\ \end{array} $		
890		939	944	949	953	95 <del>8</del>	963	968	973	978	983	$.4   1.8 \\ .5   2.2$		
891 892 893 894 895 896 897 898 898 899	95	988 036 085 134 182 231 279 327 376	99 <u>2</u> 041 090 138 187 235 284 332 381	997 046 095 143 192 240 289 337 385	*002 051 099 148 197 245 294 342 390	*007 056 104 153 201 250 298 347 395	*012 061 109 158 206 255 303 352 400	*017 065 114 163 211 260 308 356 405	*022 070 119 167 216 264 313 361 410	*026 075 124 172 221 269 318 366 414	03 <u>1</u> 080 129 177 226 274 323 371 419	.6 2.7 .7 3.1 .8 3.6 .9 4.0		
900		424	429	434	438	443	448	453	458	463	467			
N.	•	D	1	2	3	4	5	6	7	8	9	P. P.		

TABLE V.-LOGARITHMS OF NUMBERS.

-	TABLE VLOGARITIMS OF NUMBERS.													
N.		0	1	2	3	4	5	6	7	8	9	Р. Р.		
900	95	424	429	434	438	443	448	453	458	463	467			
901 902 903 904 905 906 907 908 909	æ	472 520 569 617 665 713 760 808 856	477 525 573 621 669 717 765 813 861	482 530 578 626 674 722 770 818 866	487 535 583 631 679 727 725 823 870	492 540 588 636 684 732 780 827 875	49 <u>6</u> 544 593 641 689 737 784 832 880	501 549 597 645 693 741 789 837 885	50 <u>6</u> 55 <u>4</u> 60 <u>2</u> 65 <u>0</u> 69 <u>8</u> 74 <u>6</u> 794 842 890	511 559 607 655 703 751 799 847 894	516 564 612 660 708 756 804 851 899			
910		904	909	913	918	923	928	933	937	942	947			
911 912 913 914 915 916 917 918 919	96	952 999 047 094 142 189 237 284 331	956 *004 052 099 147 194 241 289 336	961 *009 056 104 151 199 246 293 341	966 *014 061 109 156 204 251 298 345	971 *018 066 113 161 208 256 303 350	97 <u>5</u> * 023 071 118 166 213 260 308 355	980 *028 075 123 170 218 265 312 360	*03 <u>3</u> 080 128 175 222	990 *037 085 132 180 227 275 322 369	994 *042 090 137 185 232 279 327 327	$\begin{array}{c ccccc} & & & & & 5 \\ & & & 1 & 0 & \cdot 5 \\ & & & 2 & 1 & \cdot 0 \\ & & & 3 & 1 & \cdot 5 \\ & & & .4 & 2 & \cdot 0 \\ & & & .5 & 2 & \cdot 5 \\ & & .6 & 3 & \cdot 0 \\ & & & .7 & 3 & \cdot 5 \\ & & .8 & 4 & \cdot 0 \\ & & .9 & 4 & \cdot 5 \end{array}$		
920		379	<b>38</b> 3	388	393	397	402	407	412	41ē	421			
921 922 923 924 925 926 927 928 929		426 473 520 567 614 661 708 755 801	430 478 525 572 619 666 712 759 806	435 482 529 576 623 670 717 764 811	440 487 534 581 628 675 722 769 815	445 492 539 586 633 680 726 773 820	449 543 590 637 684 731 778 825	454 501 548 595 642 689 736 783 829	459 506 553 600 647 694 741 787 834	$\begin{array}{r} 46\overline{3} \\ 511 \\ 558 \\ 605 \\ 69\overline{8} \\ 745 \\ 792 \\ 839 \end{array}$	468 515 562 609 656 703 750 797 843			
930		848	853	857	862	867	871	<b>87</b> 6	881	885	89 <u>0</u>			
931 932 933 934 935 936 937 938 939	97	895 941 988 034 127 174 220 266	89 <u>9</u> 946 993 039 086 132 178 225 271	$90\overline{4} \\ 951 \\ 997 \\ 044 \\ 090 \\ 137 \\ 183 \\ 229 \\ 276 \\$	909 955 002 048 095 141 188 234 280	$91\overline{3} \\ 960 \\ *007 \\ 05\overline{3} \\ 099 \\ 146 \\ 192 \\ 239 \\ 285 \\ \end{array}$	918 965 011 058 104 151 197 243 289	92 <u>3</u> 969 *01 <u>6</u> 062 109 155 202 248 294	927 974 *020 067 113 160 206 252 299	932 979 *025 072 118 164 211 257 303	937 983 *030 076 123 169 215 262 308	-1       0.4         .2       0.9         .3       1.3         .4       1.8         .5       2.7         .6       2.7         .7       3.6         .9       4.0		
940		813	317	322	<b>3</b> 2ē	331	336	340	345	349	354			
941 942 943 944 945 946 947 948 949 949 950		359 405 451 543 589 635 681 726 772	86 <u>3</u> 409 456 502 548 59 <u>3</u> 68 <u>5</u> 68 <u>5</u> 731 777	368 414 506 552 598 644 690 736 781	373 419 465 511 557 603 649 694 740 786	377 423 515 561 607 653 699 745 790	382 428 474 520 566 612 658 703 749 795	38 <u>6</u> 432 479 525 570 61 <u>6</u> 662 708 754 800	391 437 483 529 575 621 667 713 758 804	396 442 488 534 580 626 671 717 763 809	400 446 492 538 584 630 676 722 768 813			
N.		0	1	2	3	4	5	6	7	8	9	P. P.		

TABLE V.-LOGAL THMS OF NUMBERS.

N.         0         1         2         3         4         5         6         7         8         9         P.P.           950         97         777         777         781         786         795         800         803         809         813           951         863         864         844         845         850         853         859           952         956         866         864         864         854         859         964         955         956         964         965         977         927         928         986         941         945         996         941         945         966         941         945         966         947         948         946         948         946         948         953         358         358         358         358         358         358         358         358											MDE.	1
911         818         822         827         831         836         841         845         850         654         859           953         956         956         956         956         957         952         956         956         956         956         956         957         952         957         952         956         957         956         956         956         957         956         957         957         956         957         956         957         956         957         957         956         957	Ν.	0	1	2	3	4	5	6	7	8	9	P. P.
953 963 964 965 965 966 965 966 966 966 966 966 966	950	97 772	777	781	786	790	795	800	804	809	813	
961         277         277         281         286         290         295         304         305         313        6         3.0           962         317         322         326         331         335         344         349         353         358        6         3.0           963         362         367         371         376         360         385         384         394         398         403           965         452         457         461         466         470         475         475         484         488         493           967         542         547         551         556         566         574         578         583           968         632         637         641         646         650         655         663         668         677         762           970         677         641         646         650         653         704         708         713         717           971         7765         780         780         780         780         720         765         762         77         31         1.3         1.3         1.3 <th< th=""><th>952 953 954 955 956 957 958</th><td>863 909 955 98 000 046 091 136</td><td>868 914 959 005 050 095 141</td><td>873 918 964 009 055 100 145</td><td>923 968 01<u>4</u> 059 105 150</td><td>882 927 973 018 064 109 154</td><td>886 932 977 023 068 114 159</td><td>891 936 982 027 073 118 163</td><td>895 941 986 032 077 123 168</td><td>900 945 991 036 082 127 173</td><td>904 950 996 041 086 132 177</td><td><math display="block">\begin{array}{c c} .1 &amp; 0.5 \\ .2 &amp; 1.0 \\ .3 &amp; 1.5 \end{array}</math></td></th<>	952 953 954 955 956 957 958	863 909 955 98 000 046 091 136	868 914 959 005 050 095 141	873 918 964 009 055 100 145	923 968 01 <u>4</u> 059 105 150	882 927 973 018 064 109 154	886 932 977 023 068 114 159	891 936 982 027 073 118 163	895 941 986 032 077 123 168	900 945 991 036 082 127 173	904 950 996 041 086 132 177	$\begin{array}{c c} .1 & 0.5 \\ .2 & 1.0 \\ .3 & 1.5 \end{array}$
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	960	227	231	236	240	245	249	254	259	263	268	•4 2.0 •5 2.5
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	962 963 964 965 966 967 968	317 362 407 452 497 542 587	322 367 412 457 502 547 592	326 371 416 506 551 596	331 376 421 466 511 556 601	335 380 425 470 515 560 605	340 385 430 475 520 565 610	344 389 434 524 569 614	349 394 439 484 529 574 619	353 398 448 533 578 578 623	358 403 448 493 538 583 628	$ \begin{array}{c c} .7 & 3.5 \\ .8 & 4.0 \end{array} $
979       078       032       032       031       100       100       103       113       1	970	677	681	686	69Ō	695	699	704	708	713	717	
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	972 973 974 975 976 977 978	766 811 856 900 945 989 99 034	771 815 860 905 949 99 <u>4</u> 038	775 820 865 909 954 998 043	780 824 869 914 958 *003 047	784 829 873 918 963 *007 051	789 833 878 922 967 *011 056	793 838 882 927 971 *016 060	798 842 887 931 976 *020 065	802 847 891 936 980 *025 069	807 851 896 940 985 *029 074	<b>4</b> -1 0.9 -2 0.9 -3 1.8 -4 1.8 -5 2.7 -6 2.7 -7 3.6 -7 3.6 -9 4.0
983       255       260       264       268       273       277       282       286       290       295         984       293       304       308       312       317       321       326       330       335       339         985       343       348       352       357       361       365       370       374       379       383         986       387       332       396       401       405       409       414       418       423       427         987       431       436       440       445       449       453       458       462       467       471       1       0.4         988       519       524       528       533       537       541       546       550       554       559       .2       0.8         989       519       524       528       533       537       541       546       550       554       559       .2       0.8       1.2       0.8       1.2       0.8       1.2       0.8       1.2       0.8       1.2       0.8       1.2       0.8       1.2       0.8       3.2       0.8       1.2       0.8 </th <th>980</th> <td><math>12\overline{2}</math></td> <td>127</td> <td>131</td> <td>136</td> <td><math>14\overline{0}</math></td> <td>145</td> <td>149</td> <td>153</td> <td>158</td> <td>162</td> <td></td>	980	$12\overline{2}$	127	131	136	$14\overline{0}$	145	149	153	158	162	
990         563         568         572         576         581         585         590         594         598         603         -4         1.6           991         607         611         616         620         625         625         633         638         642         647         -5         2.0           992         651         655         660         664         663         677         682         686         690         -7         2.8           993         695         695         703         708         712         717         721         725         730         734         -8         3.2           994         738         743         747         751         756         760         765         769         773         778         -8         3.2           995         782         786         791         795         800         804         808         813         817         821           996         826         830         834         839         843         847         859         904         905           997         869         874         878         828         877 </th <th>982 983 984 985 986 986 987 988</th> <th>211 255 295 343 387 431 475</th> <th>215 260 304 348 392 436 480</th> <th>220 264 308 352 396 440 484</th> <th>224 268 312 357 401 445 489</th> <th><math display="block">\begin{array}{r} 229\\ 273\\ 31\underline{7}\\ 36\underline{1}\\ 40\underline{5}\\ 44\underline{9}\\ 493 \end{array}</math></th> <th>233 277 321 365 409 453 497</th> <th>282 326 370 414 458 502</th> <th>242 286 330 374 418 462 506</th> <th>24<u>6</u> 290 335 379 423 467 511</th> <th>251 295 339 383 427 471 515</th> <th>.1 0.4</th>	982 983 984 985 986 986 987 988	211 255 295 343 387 431 475	215 260 304 348 392 436 480	220 264 308 352 396 440 484	224 268 312 357 401 445 489	$\begin{array}{r} 229\\ 273\\ 31\underline{7}\\ 36\underline{1}\\ 40\underline{5}\\ 44\underline{9}\\ 493 \end{array}$	233 277 321 365 409 453 497	282 326 370 414 458 502	242 286 330 374 418 462 506	24 <u>6</u> 290 335 379 423 467 511	251 295 339 383 427 471 515	.1 0.4
991         607         611         616         620         625         629         633         638         642         647         .6         2.4           992         651         655         660         664         668         673         677         682         686         690         .73         2.8           993         695         699         703         708         712         717         721         725         730         734         .8         3.2           994         738         743         747         751         756         766         769         773         778         98         3.2           995         782         786         791         795         800         804         808         813         817         821           996         826         830         834         839         843         847         852         856         861         865         99         3.6           997         869         874         878         882         887         891         895         900         903         905         995         995         995         996         961         96	990	563	568	572	576	581	585	590	594	598	603	.4   1.6
	992 993 994 995 996 997 998 999	651 695 738 826 869 913 956	74 <u>3</u> 78 <u>6</u> 830 87 <u>4</u> 917 961	660 703 747 791 834 878 922 965	664 708 751 795 839 882 926 969	66 <u>8</u> 712 756 800 843 887 930 974	673 717 760 804 847 891 935 978	721 765 808 852 895 939 982	682 725 769 813 856 900 943 987	686 730 773 817 861 904 948 991	690 734 778 821 865 908 952 995	.6 .7 .8 .8 .9 3.6
N. 0 1 2 3 4 5 6 7 8 9 P.P.	1000	00 000	004	800	013	017	021	026	030	034	039	
	N.	0	1	2	3	4	5	6	7	8 )	9	P. P.

### TABLE V.-LOGARITHMS OF NUMBERS.

			T2	ABLE	S V	-100	JARI	THM	S OF	NU	MBE.	RS.
N.		0	1	2	3	4	5	6	7	8	9	P. P.
1000	000	000	043	087	130	173	217	260	304	347	39Ō	
01 02 03 04 05 06 07 08 09	001 002 003	434 867 301 733 166 598 029 460 891	477 911 344 777 209 641 072 503 934	521 954 387 820 252 684 115 546 977	564 997 431 863 295 727 159 590 *020	607 *041 474 906 339 770 202 633 *063	651 *084 517 950 382 814 245 676 *106	69 <u>4</u> *127 560 993 425 857 288 719 *149	737 *171 604 *036 468 900 331 762 *192	781 *214 647 *079 511 943 374 805 *235	824 *257 690 *123 555 986 417 848 *278	$\begin{array}{cccc} 4\overline{3} & 43 \\ \cdot 1 & 4 \cdot 3 & 4 \cdot 3 \\ \cdot 2 & 8 \cdot 7 & 8 \cdot 6 \\ \cdot 3 & 13 \cdot 0 & 12 \cdot 9 \end{array}$
1010	004	<b>3</b> 2ī	364	407	450	493	5 <b>3</b> ē	579	622	665	708	.417.417.2 .521.721.5
11 12 13 14 15 16 17 18 19	005 006 007 008	751 180 609 038 466 893 321 748 174	794 223 652 081 509 936 363 790 217	837 266 695 123 551 979 400 833 259	880 309 738 594 *022 449 875 302	923 352 781 209 637 *064 491 918 344	966 395 824 252 680 *107 534 961 387	*009 438 866 295 722 *150 577 *003 430	*051 481 909 337 765 *193 620 *046 472	*094 523 950 808 808 808 515 *089 515	*137 566 995 423 851 *278 705 131 557	.6 26.125.8 .730.430.1 .834.834.4 .939.138.7
1020		600	642	685	728	770	813	855	898	94 <b>0</b>	983	
21 22 23 24 25 26 27 28 29	009 010 011 012	025 451 875 300 724 147 570 993 415	068 493 918 342 766 189 612 612 *035 457	111 536 960 385 808 232 655 *077 500	15 <u>3</u> 578 *003 427 851 27 <u>4</u> 697 *120 542	196 621 *0459 893 316 739 *162 584	238 663 *088 512 935 359 782 782 626	281 706 554 978 401 824 824 668	323 748 *172 *020 443 866 *288 710	36 <u>6</u> 790 *215 63 <u>9</u> *062 48 <u>6</u> 908 *331 753	408 833 *257 681 *105 528 951 *373 795	$\begin{array}{c} 4\overline{2} & 42\\ \cdot 1 & 4 \cdot 2 & 4 \cdot 2\\ \cdot 2 & 8 \cdot 5 & 8 \cdot 4\\ \cdot 3 & 12 \cdot 7 & 12 \cdot 6\\ \cdot 4 & 17 \cdot 0 & 16 \cdot 8\\ \cdot 5 & 21 \cdot 2 & 21 \cdot 0\\ \cdot 6 & 25 \cdot 5 & 25 \cdot 2\\ \cdot 7 & 29 \cdot 7 & 29 \cdot 4\\ \cdot 8 & 34 \cdot 0 & 33 \cdot 6\\ \cdot 9 & 38 \cdot 2 & 37 \cdot 8\end{array}$
1030		837	879	92ī	963	*006	*048	*090	*132	174	216	
31 32 34 35 36 37 38 39	013 014 015 016	$\begin{array}{c} 25\overline{8} \\ 679 \\ 100 \\ 520 \\ 940 \\ 360 \\ 779 \\ 197 \\ 615 \end{array}$	301 722 142 562 982 401 820 239 657	343 764 184 6024 443 862 281 699	385 806 226 646 *066 485 904 323 741	427 848 268 688 *108 527 946 364 782	469 890 310 730 *150 569 988 406 824	511 932 352 772 *192 *030 448 866	553 97 <u>4</u> 39 <u>4</u> 814 *234 653 *072 490 908	595 *016 436 856 *276 695 *113 582 950	637 *058 478 898 *318 737 155 573 991	$\begin{array}{cccc} 4\overline{1} & 41 \\ .1 & 4.\overline{1} & 4.1 \\ .2 & 8.3 & 8.2 \\ .3 & 12.4 & 12.3 \\ .4 & 16.6 & 16.4 \end{array}$
1040	017	033	075	117	158	200	242	284	325	367	409	.5 20.7 20.5
41 42 43 44 45 46 47 48 49 <b>10</b> 50	018 019 020 021	$\begin{array}{r} 45\overline{0} \\ 86\overline{7} \\ 28\overline{4} \\ 70\overline{0} \\ 53\overline{1} \\ 94\overline{6} \\ 77\overline{5} \\ \hline 18\overline{9} \end{array}$	492 909 326 742 158 573 988 402 817 230	534 951 367 783 199 614 *029 444 858 272	576 992 409 825 241 656 *071 485 899 313	617 *034 451 867 282 697 *112 527 941 354	659 *076 492 908 324 739 *154 568 982 396	701 *117 534 950 365 780 *195 610 *024 437	742 *159 575 991 407 822 *237 651 *065 478	784 *201 617 *033 448 863 *278 692 *106 520	826 *242 659 *074 490 905 *320 734 *148 561	.6 24.9 24.6 .729.0 28.7 .833.2 32.8 .9 37.3 36.9
N.		0	1	2	3	4	5	6	7	8	9	P. P.
								<u> </u>				

6.0

### TABLE V.-LOGARITHMS OF NUMBERS.

			<b>T</b> 2	ABLI	L V	-LO	JARI	111.	15 01		MBE	ns.
N.	0		1	2	3	4	5	6	7	8	9	P. P.
1050	021	189	230	272	313	354	396	437	478	520	561	41
51 52 53 55 56 57 58 59	022 023 024	602 015 428 252 664 075 485 896	644 057 469 882 293 705 116 526 937	68 <u>5</u> 098 511 923 335 746 157 568 978	72 <u>6</u> 139 552 964 37 <u>6</u> 787 198 609 *019	768 181 593 *005 417 828 239 650 *060	809 222 634 *046 458 869 280 691 *101	85 <u>0</u> 263 676 *088 499 910 321 732 *142	892 304 717 *129 540 951 362 773 *183	933 346 758 *170 581 993 403 814 *224	974 387 799 *211 623 *034 444 855 *265	$\begin{array}{c ccccc} & 1 & 4 & 1 \\ & 2 & 8 & 3 \\ & 3 & 12 & 4 \\ & 4 & 16 & 6 \\ & 5 & 20 & 7 \\ & 6 & 24 & 9 \\ & 7 & 29 & 0 \\ & 8 & 33 & 2 \\ & 9 & 37 & 3 \end{array}$
1060	025	306	347	388	429	469	510	551	592	633	674	41
61 62 63 64 65 66 67 68 89	026 027 028	$71\overline{5} \\ 124 \\ 53\overline{3} \\ 94\overline{1} \\ 34\overline{9} \\ 757 \\ 16\overline{4} \\ 57\overline{1} \\ 97\overline{7}$	756 165 574 982 390 798 205 612 *018	797 206 615 *023 431 838 246 652 *059	838 247 656 *064 472 879 286 693 *099	879 288 696 *105 512 920 327 734 *140	920 329 737 553 961 368 774 *181	961 370 778 *186 594 *001 408 815 *22]	410 819 *227 635	*04 <u>2</u> 451 860 *268 675 *083 490 896 *302	*08 <u>3</u> 901 *309 71 <u>6</u> *12 <u>3</u> 530 937 *343	1       4.1         .2       8.2         .3       12.3         .4       16.4         .5       20.5         .6       24.6         .7       28.7         .8       32.8         .9       36.9
1070	029	384	424	465	505	546	5 <b>8</b> ē	627	668	708	749	40
71 72 73 74 75 76 77 78 79	030 031 032 033	789 195 599 004 408 812 215 619 021	830 235 640 044 449 852 256 659 061	870 276 680 085 489 893 296 699 102	911 316 721 529 933 336 739 142	951 357 761 166 570 973 377 780 182	992 397 802 206 610 *014 417 820 222	*032 438 842 247 651 *054 457 860 263	478 883 287 691	*114 519 923 327 731 *135 538 941 343	*154 559 964 368 772 *175 578 981 383	$\begin{array}{c ccccc} & 1 & 4 & 0 \\ \hline & 2 & 8 & 1 \\ & 3 & 12 & 1 \\ & 4 & 16 & 2 \\ & 5 & 20 & 2 \\ & 6 & 24 & 3 \\ & 7 & 23 & 3 \\ & 8 & 32 & 4 \\ & 9 & 36 & 4 \end{array}$
1080		424	464	504	544	584	625	665	705	745	785	10
81 82 83 84 85 86 87 88 89	034 035 036 037	825 227 628 029 429 830 229 629 028	866 267 668 069 470 870 269 669 068	90 <u>6</u> 307 708 109 510 910 309 708 107	94 <u>6</u> 347 748 149 550 950 349 748 147	986 388 789 189 590 990 389 788 187	*026 428 829 229 630 *029 429 828 227	*066 468 869 269 670 *069 469 868 267	*107 508 909 309 710 *109 509 908 307	147 548 949 349 750 *149 549 948 347	187 588 989 389 790 *189 589 988 386	40       .1     4.0       .2     8.0       .3     12.0       .4     16.0       .5     20.0       .6     24.0       .7     28.0       .8     32.0       .9     36.0
1090		<u>42</u> 6	466	506	546	586	625	665	705	745	785	. 39
91 92 93 94 95 96 97 98 99 <b>1100</b>	038 039 040 041	825 222 620 017 414 810 602 997 392	864 262 660 057 454 850 246 642 *037 432	904 302 699 096 493 890 286 681 *076 471	944 342 739 136 533 929 325 721 *116 511	984 381 779 176 572 969 365 760 *155	*008 404 800 *195	44 <u>4</u> 839 *234	501 898 295 691 *088 483 879 *274	335 731 *127 523 918 *313	771 *167 563 958 *353	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
N.		)	1	2	3	4	5	6	7	8	9	P. P.
				1	1	1		1	1	1	1	•

TABLI	E VI.—I	LOGARITHM	IIC SIN	IES AND TA	NGENTS OF	SMAL	LANGLES.
Log sin Log tar	$\begin{array}{l} \mathbf{h} \ \phi = \mathbf{h} \\ \mathbf{h} \ \phi = \mathbf{h} \end{array}$	$ \sup_{\substack{\phi \\ \phi \\ \phi \\ \phi \\ \phi'' + T. } } \phi'' + S. $	-	<b>0</b> °	$\log \phi' \log \phi'$	$i' = \log i$ $i' = \log i$	$ \frac{\sin \phi + S'}{\tan \phi + T'} $
"	•	S	т	Log. Sin.	S'	T'	Log. Tan.
0 60 120 180 240	0 1 2 3 4	4.685 57 57 57 57 57 57 57 57	57 57 57 57 57 57	$\begin{array}{c} -\infty \\ 6.46\ 37\overline{2} \\ .76\ 475 \\ .94\ 084 \\ 7.06\ 578 \end{array}$	5.314 42 42 42 42 42 42 42 42	42 42 42 42 42 42	$ \begin{array}{r}\infty \\ 6.4637\overline{2} \\ .76475 \\ .94084 \\ 7.06578 \\ \end{array} $
300 360 420 480 540	5 6 7 8 9	4.685 57 57 57 57 57	57 57 57 57 57 57	$7.16\ 269 \\ .24\ 187 \\ .30\ 882 \\ .36\ 681 \\ .41\ 797$	$5.3144\overline{2}$ $4\overline{2}$ $4\overline{2}$ $4\overline{2}$ $4\overline{2}$ $4\overline{2}$ $4\overline{2}$	42 42 42 42 42 42	$7.16\ 269 \\ .24\ 188 \\ .30\ 882 \\ .36\ 681 \\ .41\ 797$
600 660 720 780 840	$10 \\ 11 \\ 12 \\ 13 \\ 14$	4.685 57 57 57 57 57 57	57 57 57 57 57 57	$7.46\ 37\overline{2} \\ .50\ 512 \\ .54\ 290 \\ .57\ 767 \\ .60\ 98\overline{5}$	5.314 42 42 42 42 42 42	42 42 42 42 42 42 42	7 · 46 372 · 50 512 · 54 291 · 57 767 · 60 985
900 960 1020 1080 1140	15 16 17 18 19	4 · 685 57 57 57 57 57 57 57	58 58 58 58 58 58	$7.63 981 \\ .66 784 \\ .69 417 \\ .71 899 \\ .74 248$	5, 314 42 42 42 42 42 42 42	42 42 42 42 42 42	7.63 982 .66 785 .69 418 .71 900 .74 248
1200 1260 1320 1380 1440	20 21 22 23 24	4.685 57 57 57 57 57 57	58 58 58 58 58 58	$\begin{array}{r} 7\cdot 76 \ 475 \\ \cdot 78 \ 594 \\ \cdot 80 \ 614 \\ \cdot 82 \ 545 \\ \cdot 84 \ 393 \end{array}$	$5.31443 \\ 43 \\ 43 \\ 43 \\ 43 \\ 43 \\ 43 \\ 43$	42 42 42 42 42 42	7 · 76 476 · 78 595 · 80 615 · 82 546 · 84 394
1500 1560 1620 1680 1740	25 26 27 28 29	4.685 57 57 57 57 57 57	58 58 58 58 58 58	7.86 166 .87 869 .89 508 .91 088 .92 612	5.314 43 43 43 43 43 43	41 41 41 41 41	7.86 167 .87 871 .89 510 .91 089 .92 613
1800 1860 1920 1980 2040	30 31 32 33 34	4.685 57 57 57 57 57 57	58 58 59 59	7.94 084 .95 508 .96 887 .98 223 .99 520	5.31443 43 43 43 43 43 43	4 <u>1</u> 4 <u>1</u> 41 41 41	7.94 086 .95 510 .96 889 .98 225 .99 522
2100 2160 2220 2280 2340	35 36 37 38 39	4.685 5 <u>6</u> 5 <u>6</u> 5 <u>6</u> 5 <u>6</u>	59 59 59 59 59	8.00 778 .02 002 .03 192 .04 350 .05 478	$5.3144\overline{3}$ 43 43 43 43 43 43	41 41 40 40	$ \begin{array}{r} 8.00781\\ .02004\\ .03194\\ .04352\\ .05481\\ \end{array} $
2400 2460 2520 2580 2640	40 41 42 43 44	4.685 5 <u>6</u> 5 <u>6</u> 5 <u>6</u> 5 <u>6</u> 56	5 <u>9</u> 5 <u>9</u> 60 60	8.06 577 .07 650 .08 696 .09 718 .10 716	$5.314 \ \underline{43} \\ 43 \\ 43 \\ 43 \\ 43 \\ 43 \\ 43 \\ 43 \\$	40 40 40 40	8.06 580 .07 653 .08 699 .09 721 .10 720
2700 2760 2820 2880 2940	45 46 47 48 49	4.68556 5656 5656 5656	60 60 60 60 60 60	$\begin{array}{r} 8\cdot 11 \ 69\overline{2} \\ \cdot 12 \ 647 \\ \cdot 13 \ 581 \\ \cdot 14 \ 49\overline{5} \\ \cdot 15 \ 390 \end{array}$	5.314 44 $44$ $44$ $44$ $44$ $44$	40 40 39 39	$\begin{array}{r} 8 \cdot 11 \ 696 \\ \cdot 12 \ 651 \\ \cdot 13 \ 585 \\ \cdot 14 \ 499 \\ \cdot 15 \ 395 \end{array}$
3000 3060 3120 3180 3240	$50 \\ 51 \\ 52 \\ 53 \\ 54$	4.685 56 56 56 5 <u>6</u> 5 <u>5</u>	$egin{array}{c} 6\overline{0} \\ 6\overline{0} \\ 61 \\ 61 \\ 61 \\ 61 \end{array}$	8.16268 .17128 .17971 .18798 .19610	5.31444 44 44 44 44 44 44	3 <u>9</u> 39 39 39 39	$ \begin{array}{r} 8.16272\\ .17133\\ .17976\\ .18803\\ .19615 \end{array} $
3300 3360 3420 3480 3540	55 56 57 58 59	4.685 55 55 55 55 55 55 55	6 <u>1</u> 6 <u>1</u> 6 <u>1</u> 61 62	$\begin{array}{r} 8 \cdot 20 \ 407 \\ \cdot 21 \ 189 \\ \cdot 21 \ 958 \\ \cdot 22 \ 713 \\ \cdot 23 \ 455 \end{array}$	$5.314\ 4\bar{4} \\ 4\bar{4}$	3 <u>9</u> 3 <u>8</u> 38 38 38 38	$\begin{array}{r} 8 \cdot 20 \ 41\overline{2} \\ \cdot 21 \ 195 \\ \cdot 21 \ 964 \\ \cdot 22 \ 719 \\ \cdot 23 \ 462 \end{array}$

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Log si Log ta	$\begin{array}{c}n \phi = 1\\ a \phi = 1\end{array}$	$\begin{array}{l} \operatorname{og} \phi'' + S. \\ \operatorname{og} \phi'' + T. \end{array}$		1°	$\log \phi'' \log \phi''$	$l = \log log = log$	$ \frac{\sin \phi + S'}{\tan \phi + T'} $
"		S	т	Log. Sin.	S'	T'	Log. Tan.
3600 3660 3720 3780 3840	0 1 2 3 4	4.685 55 55 55 55 55 55 55	62 62 62 62 62	$\begin{array}{r} 8 \cdot 24 \ 18\overline{5} \\ \cdot 24 \ 90\overline{3} \\ \cdot 25 \ 60\overline{9} \\ \cdot 26 \ 304 \\ \cdot 26 \ 988 \end{array}$	$     5 \cdot 314 \ 4\overline{4} \\     45 \\     4$	38 38 3 <u>8</u> 37 37	$\begin{array}{r} 8 \cdot 24 \ 192 \\ \cdot 24 \ 910 \\ \cdot 25 \ 616 \\ \cdot 26 \ 311 \\ \cdot 26 \ 995 \end{array}$
3900 3960 4020 4080 4140	5 6 7 8 9	4.685555 55 54 54 54 54 54	62 63 63 63 63 63	$\begin{array}{r} 8 \cdot 27 \ 66\overline{1} \\ \cdot 28 \ 32\overline{4} \\ \cdot 28 \ 97\overline{7} \\ \cdot 29 \ 62\overline{0} \\ \cdot 30 \ 25\overline{4} \end{array}$	5.314 45 45 45 45 45	37 37 37 37 37 36	8 · 27 669 · 28 332 · 28 985 · 29 629 · 30 263
4200 4260 4320 4380 4440	$     \begin{array}{r}       10 \\       11 \\       12 \\       13 \\       14     \end{array} $	4.685 5 <u>4</u> 5 <u>4</u> 54 54 54 54	6 <u>3</u> 63 64 64 64	8 · 30 879 · 31 495 · 32 102 · 32 701 · 33 292	5.31445 45 45 46 46 46	36 36 36 36 36	$\begin{array}{r} 8 \cdot 30 \ 88 \overline{8} \\ \cdot 31 \ 50 \overline{4} \\ \cdot 32 \ 11 2 \\ \cdot 32 \ 71 \overline{1} \\ \cdot 33 \ 30 \overline{2} \end{array}$
4500 4560 4620 4680 4740	15 16 17 18 19	4.685 54 54 54 54 54 5 <u>4</u> 5 <u>3</u>	64 64 65 65 65	8 33 875 34 450 35 018 35 578 36 131	5.31446 4646 4646 4646	35 35 35 35 35 35	$\begin{array}{r} 8.33\ 885\\ .34\ 461\\ .35\ 029\\ .35\ 589\\ .36\ 143\end{array}$
4800 4860 4920 4980 5040	20 21 22 23 24	4.685 5 <u>3</u> 5 <u>3</u> 5 <u>3</u> 5 <u>3</u> 5 <u>3</u> 53	655 655 66 66	8.36 677 .37 217 .37 750 .38 276 .38 796	5·314 4 <u>6</u> 4 <u>6</u> 4 <u>6</u> 46 47	34 34 34 34 34	8.36 689 .37 229 .37 762 .38 289 .38 809
5100 5160 5220 5280 5340	25 26 27 28 29	4.68553 53 53 52 52 52	6 <u>6</u> 66 67 67 67	8.39 310 .39 818 .40 320 .40 816 41 307	$5.314 \begin{array}{c} 47 \\ 47 \\ 47 \\ 47 \\ 47 \\ 47 \\ 47 \\ 47 $	3 <u>3</u> 33 33 33 33 33	$ \begin{array}{r} 8.39\ 32\overline{3}\\.39\ 83\overline{1}\\.40\ 334\\.40\ 83\overline{0}\\.41\ 32\overline{1}\end{array} $
5400 5460 5520 5580 5640	30 31 32 33 34	4.685 5 <u>2</u> 5 <u>2</u> 52 52 52 52	67 67 68 68 68	$\begin{array}{r} 8\cdot 41 \ 792 \\ \cdot 42 \ 271 \\ \cdot 42 \ 746 \\ \cdot 43 \ 215 \\ \cdot 43 \ 680 \end{array}$	5.31447 47 47 47 48 48 48	32 32 32 32 32 31	$\begin{array}{r} 8 \cdot 41 \ 807 \\ \cdot 42 \ 287 \\ \cdot 42 \ 762 \\ \cdot 43 \ 231 \\ \cdot 43 \ 696 \end{array}$
5700 5760 5820 5880 5940	35 36 37 38 39	4.685 52 5 <u>1</u> 5 <u>1</u> 5 <u>1</u> 5 <u>1</u>	68 69 69 69 69	$\begin{array}{r} 8.44 \ 13\bar{9} \\ .44 \ 594 \\ .45 \ 044 \\ .45 \ 48\bar{9} \\ .45 \ 930 \end{array}$	$5.314 \ 48 \\ 48 \\ 48 \\ 48 \\ 48 \\ 48 \\ 48 \\ 4$	31 31 3 <u>0</u> 30	$\begin{array}{r} 8.44 \\ .44 \\ .45 $
6000 6060 6120 6180 6240	40 41 42 43 44	4.68551 51 51 51 51 51 51 51 51 51 51 51 51	69 70 70 70 70 70	8 · 46 365 · 46 798 · 47 226 · 47 650 · 48 069	$5.314\ 48\ 49\ 49\ 49\ 49\ 49\ 49\ 49\ 49\ 49\ 49$	30 30 3 <u>0</u> 2 <u>9</u> 29	$\begin{array}{r} 8 \cdot 46 \ 385 \\ \cdot 46 \ 817 \\ \cdot 47 \ 245 \\ \cdot 47 \ 669 \\ \cdot 48 \ 089 \end{array}$
6300 6360 6420 6480 6540	45 46 47 48 49	4.685 50 50 50 50 50 50	7 <u>1</u> 7 <u>1</u> 7 <u>1</u> 7 <u>2</u> 72	8 · 48 485 · 48 896 · 49 304 · 49 708 · 50 108	$5.314 \ 49 \\ 49 \\ 49 \\ 49 \\ 50 $	29 28 28 28 28 28	8.48 505 .48 917 .49 325 .49 729 .50 130
6600 6660 6720 6780 6840	50 51 52 53 54	4.68550 50 50 49 49 49	7 <u>2</u> 72 73 73 73 73	$\begin{array}{r} 8.50 50\overline{4} \\ .50 89\overline{7} \\ .51 28\overline{6} \\ .51 67\overline{2} \\ .52 055 \end{array}$	5.31450 50 50 50 50 50 50	27 27 27 27 27 26	8 - 50 526 - 50 920 - 51 310 - 51 696 - 52 079
6900 6960 7020 7080 7140	55 56 57 58 59	$\begin{array}{r} 4.685\ 4\overline{9} \\ 49 \\ 49 \\ 49 \\ 49 \\ 49 \\ 49 \\ 49 \\ $	73 74 74 74 75	$\begin{array}{r} 8.52\ 43\overline{4}\\ .52\ 810\\ .53\ 183\\ .53\ 55\overline{2}\\ .53\ 918\end{array}$	5.31450 51 51 51 51 51 51	26 26 25 25 25	8 · 52 458 · 52 835 · 53 208 · 53 578 · 53 944

TABLE VI.-LOGARITHMIC SINES AND TANGENTS OF SMALL ANGLES.

TABLI	£ VI.—	LOGARITH	AIC SIL	NES AND TA	NGENTS OF		
Log sir Log tar	$\phi = \log \phi$ $\phi = \log \phi$	$ \sup_{\substack{\phi \\ \phi \\ \phi \\ \phi \\ \phi'' + T. } } \frac{\phi'' + S.}{T.} $		<b>2</b> °	$\log \phi'' \log \phi''$	$= \log = \log \log$	$ \sin \phi + S'_{\cdot} $ $ \tan \phi + T'_{\cdot} $
"	,	s	T	Log. Sin.	S'	T'	Log. Tan.
7200 7260 7320 7380 7440	0 1 2 3 4	4.685 48 48 48 48 48 48 48	75 75 76 76	8.54 282 .54 642 .54 999 .55 354 .55 705	$   \begin{array}{r}     5 \cdot 314 & 5\overline{1} \\     5\overline{1} \\     5\overline{1} \\     52 \\     52 \\     52   \end{array} $	25 24 24 24 23	8 · 54 308 · 54 669 · 55 027 · 55 381 · 55 733
7500 7560 7620 7680 7740	5 6 7 8 9	4.685 48 48 47 47 47 47	76 7 <u>7</u> 77 77 77 78	8 · 56 054 · 56 400 · 56 743 · 57 083 · 57 421	5.314 52 52 52 52 52 52	23 23 22 22 22 22	8.56083 .56429 .56772 .57113 .57452
7800 7860 7920 7980 8040	10 11 12 13 14	4.68547 47 47 46 46 46	78 78 79 79 79	8.57 756 .58 089 .58 419 .58 747 .59 072	5.314 53 53 53 53 53 53	22 21 21 21 21 20	8.57 787 .58 121 .58 45 <u>1</u> .58 779 .59 105
8100 8160 8220 8280 8340	15 16 17 18 19	<b>4 ⋅ 685</b> 46 46 46 46 45	80 80 80 81 81	8.59 395 .59 715 .60 033 .60 349 .60 662	$5.3145\overline{3}$ 54 54 54 54 54 54 54 54	20 2 <u>0</u> 19 19 19	8.59 428 .59 749 .60 067 .60 384 .60 698
8400 8460 8520 8580 8640	20 21 22 23 24	4.685 4 <u>5</u> 45 45 45 45 45	81 82 82 82 83	$\begin{array}{r} 8\cdot 60 \ 97\overline{3} \\ \cdot 61 \ 28\overline{2} \\ \cdot 61 \ 589 \\ \cdot 61 \ 89\overline{3} \\ \cdot 62 \ 196 \end{array}$	$5.31454 5 \frac{5}{5} $	18 18 18 17 17	$\begin{array}{r} 8.61\ 009\\ .61\ 319\\ .61\ 626\\ .61\ 931\\ .62\ 234\end{array}$
8700 8760 8820 8880 8940	25 26 27 28 29	4.685 4 <u>4</u> 4 <u>4</u> 44 44 44 44	8 <u>3</u> 83 84 84 84 84	8.62 496 .62 795 .63 091 .63 385 .63 677	5.314 5 <u>5</u> 5 <u>5</u> 55 56 56 56	1 <u>6</u> 16 1 <u>6</u> 1 <u>5</u> 15	8.62535 .62834 .63131 .63425 .63718
9000 9060 9120 9180 9240	30 31 32 33 34	4.685 4 <u>3</u> 4 <u>3</u> 43 43 43 43 43	85 85 86 86 86	8.63 968 .64 256 .64 543 .64 827 .65 110	5.314 5 <u>6</u> 5 <u>6</u> , 56 , 57 57 57	$15 \\ 14 \\ 14 \\ 14 \\ 14 \\ 13 \\ 13$	$\begin{array}{r} 8.64\ 00\overline{9}\\ .64\ 298\\ .64\ 58\overline{5}\\ .64\ 870\\ .65\ 153\end{array}$
9300 9360 9420 9480 9540	35 36 37 38 39	4.685 4 <u>3</u> 42 42 42 42 42 42	8 <u>7</u> 8 <u>7</u> 8 <u>7</u> 8 <u>8</u> 88	8.65 391 .65 670 .65 947 .66 223 .66 497	5.314 57 57 57 58 58 58	$13 \\ 12 \\ 12 \\ 12 \\ 12 \\ 12 \\ 11 \\ 11 \\ $	$\begin{array}{r} 8.65 \ 435 \\ .65 \ 715 \\ .65 \ 993 \\ .66 \ 269 \\ .66 \ 543 \end{array}$
9600 9660 9720 9780 9840	40 41 42 43 44	$\begin{array}{r} 4\cdot 685\ 42\ 41\ 41\ 41\ 41\ 41\ 41\ \end{array}$	89 89 90 90	8.66769 .67039 .67308 .67575 .67840	5.314 5 <u>8</u> 58 58 59 59	11 10 10 10 09	8.66816 .67087 .67356 .67624 .67890
9900 9960 10020 10080 10140	45 46 47 48 49	$\begin{array}{r} 4 \cdot 685 \ 41 \\ 40 \\ 40 \\ 40 \\ 40 \\ 40 \\ 40 \end{array}$	91 91 91 92 92	$ \begin{array}{r} 8.68 & 10\overline{4} \\ .68 & 36\overline{6} \\ .68 & 627 \\ .68 & 89\overline{6} \\ .69 & 144 \end{array} $	5.814 5 <u>9</u> 59 59 60 60	0 <u>9</u> 0 <u>8</u> 0 <u>8</u> 07	$\begin{array}{r} 8.68 \ 15\overline{4} \\ .68 \ 417 \\ .68 \ 678 \\ .68 \ 938 \\ .69 \ 19\overline{6} \end{array}$
$10200 \\ 10260 \\ 10320 \\ 10380 \\ 10440$	50 51 52 53 54	$4.685  \frac{40}{39} \\ 39 \\ 39 \\ 39 \\ 39 \\ 39 \\ 39 \\ 39 \\$	9 <u>3</u> 9 <u>3</u> 9 <u>3</u> 9 <u>4</u> 9 <u>4</u>	8.69 400 .69 654 .69 907 .70 159 .70 409	$5.31460 \\ 60 \\ 60 \\ 61 \\ 61 \\$	07 06 06 05	8.69453 .69708 .69961 .70214 .70464
$10500 \\ 10560 \\ 10620 \\ 10680 \\ 10740$	55 56 57 58 59	4.685 38 38 38 38 38 38	9 <u>5</u> 9 <u>5</u> 9 <u>6</u> 97	8.70 657 .70 905 .71 150 .71 395 .71 638	$5.31461 \\ 61 \\ 61 \\ 62 \\ 62 \\ 62 \\ 62 \\ 62 \\ $	05 04 03 03	8.70 714 .70 962 .71 208 .71 453 .71 697

#### TABLE VI.-LOGARITHMIC SINES AND TANGENTS OF SMALL ANGLES

### TABLE VII.—LOGARITHMIC SINES, COSINES, TANGENTS, AND COTANGENTS.

v							
'	Log. Sin.	D	Log. Tan.	Com. D.	Log. Cot.	Log. Cos.	
0 1 2 3 4	$\begin{array}{r} -\infty \\ 6.4637\overline{2} \\ 6.7647\overline{5} \\ 6.9408\overline{4} \\ 7.0657\overline{8} \end{array}$	30103 17609 12494 9691	$\begin{array}{r}\infty \\ 6\cdot 46\ 37\overline{2} \\ 6\cdot 76\ 47\overline{5} \\ 6\cdot 94\ 084 \\ 7\cdot 06\ 57\overline{8} \end{array}$	30103 17609 12494 9691	$ \begin{array}{r} + \infty \\ 3 \cdot 53 \ 627 \\ 3 \cdot 23 \ 524 \\ 3 \cdot 05 \ 915 \\ 2 \cdot 93 \ 421 \\ \end{array} $	$\begin{array}{c} 0 & 00 & 000 \\ 0 & 00 & 000 \\ 0 & 00 & 000 \\ 0 & 00 & 000 \\ 0 & 00 & 000 \\ 0 & 00 & 000 \end{array}$	60 59 58 57 56
5 6 7 8 9	$\begin{array}{c} 7\cdot 16 \ 26\bar{9} \\ 7\cdot 24 \ 18\bar{7} \\ 7\cdot 30 \ 88\bar{2} \\ 7\cdot 36 \ 68\bar{1} \\ 7\cdot 41 \ 797 \end{array}$	9091 7918 6695 5799 5115 4575	$\begin{array}{c} 7\cdot 16 \ 269 \\ 7\cdot 24 \ 188 \\ 7\cdot 30 \ 882 \\ 7\cdot 36 \ 681 \\ 7\cdot 41 \ 797 \end{array}$	57918 6694 5799 5115 4575	$\begin{array}{c} 2 \cdot 83 \ 73\bar{0} \\ 2 \cdot 75 \ 812 \cdot \\ 2 \cdot 69 \ 11\bar{7} \\ 2 \cdot 63 \ 31\bar{8} \\ 2 \cdot 58 \ 203 \end{array}$	$\begin{array}{c} 0 \cdot 00 \ 000 \\ 0 \cdot 00 \ 000 \end{array}$	55 54 53 52 51
10 11 12 13 14	7 · 46 372 7 · 50 512 7 · 54 290 7 · 57 767 7 · 60 985	4139 3778 3476 3218	7.46 372 7.50 512 7.54 291 7.57 767 7.60 985	4139 3779 3476 3218	$\begin{array}{r} 2.53 \ 62\overline{7} \\ 2.49 \ 488 \\ 2.45 \ 709 \\ 2.42 \ 233 \\ 2.39 \ 014 \end{array}$	$\begin{array}{c} 0.00 & 000 \\ 0.00 & 000 \\ 9.99 & 999 \\ 9.99 & 999 \\ 9.99 & 999 \\ 9.99 & 999 \\ 9.99 & 999 \end{array}$	$50 \\ 49 \\ 48 \\ 47 \\ 46$
15 16 17 18 19	7.63 98 <u>1</u> 7.66 78 <u>4</u> 7.69 417 7.71 899 7.74 248	2996 2803 2633 2482 2348	$\begin{array}{c} 7.63 & 982 \\ 7.66 & 785 \\ 7.69 & 418 \\ 7.71 & 900 \\ 7.74 & 248 \end{array}$	2996 2803 263 <u>3</u> 2482 2348	$\begin{array}{c} 2 \cdot 36 \ 018 \\ 2 \cdot 33 \ 215 \\ 2 \cdot 30 \ 582 \\ 2 \cdot 28 \ 099 \\ 2 \cdot 25 \ 751 \end{array}$	9.99999 <u>9</u> 9.99999 <u>9</u> 9.99999 <u>9</u> 9.99999 <u>9</u> 9.99999 <u>9</u> 9.99999	45 44 43 42 41
20 21 22 23 24	$\begin{array}{c} 7 \cdot 76 \ 475 \\ 7 \cdot 78 \ 594 \\ 7 \cdot 80 \ 614 \\ 7 \cdot 82 \ 545 \\ 7 \cdot 84 \ 393 \end{array}$	2227 2119 2020 1930 1848	$\begin{array}{r} 7.76 \ 476 \\ 7.78 \ 595 \\ 7.80 \ 615 \\ 7.82 \ 546 \\ 7.84 \ 394 \end{array}$	2227 2119 2020 1930 1848	$\begin{array}{c} 2 \cdot 23 \ 524 \\ 2 \cdot 21 \ 405 \\ 2 \cdot 19 \ 384 \\ 2 \cdot 17 \ 454 \\ 2 \cdot 15 \ 605 \end{array}$	9.999999 9.99999 9.99999 9.99999 9.99999 9.99999	40 39 38 37 36
25 26 27 28 29	7.86 166 7.87 869 7.89 508 7.91 088 7.92 612	$     \begin{array}{r}       1772 \\       1703 \\       1639 \\       1579 \\       1524 \\     \end{array} $	7 · 86 167 7 · 87 871 7 · 89 510 7 · 91 089 7 · 92 613	$     \begin{array}{r}       1773 \\       1703 \\       1639 \\       1579 \\       1524 \\       \hline       7524 \\       \hline       7524 \\       \hline       7524 \\        7524 \\       7$	$\begin{array}{c} 2.13 \ 83\overline{2} \\ 2.12 \ 129 \\ 2.10 \ 490 \\ 2.08 \ 91\overline{0} \\ 2.07 \ 38\overline{6} \end{array}$	9.999999 9.999999 9.99998 9.99998 9.99998 9.99998	35 34 33 32 31
30 31 32 33 34	7.94 084 7.95 508 7.96 887 7.98 223 7.99 520	1472 1424 1379 1336 1296	7.94086 7.95510 7.96889 7.98225 7.99522	1472 1424 1379 1336 1296	$\begin{array}{r} 2.05\ 914\\ 2.04\ 490\\ 2.03\ 111\\ 2.01\ 774\\ 2.00\ 478\end{array}$	9.99 998 9.99 998 9.99 998 9.99 998 9.99 998 9.99 998	30 29 28 27 26
35 36 37 38 39	$\begin{array}{r} 8.00\ 77\overline{8}\\ 8.02\ 002\\ 8.03\ 192\\ 8.04\ 350\\ 8.05\ 478\end{array}$	125 <u>8</u> 1223 1190 1158 1128	$\begin{array}{r} 8.00\ 781\\ 8.02\ 004\\ 8.03\ 194\\ 8.04\ 352\\ 8.05\ 481\end{array}$	125 <u>9</u> 1223 1190 <sup>7</sup> 115 <u>8</u> 1128	$ \begin{array}{r} 1.99 219 \\ 1.97 995 \\ 1.96 805 \\ 1.95 647 \\ 1.94 519 \end{array} $	9.99 997 9.99 997 9.99 997 9.99 997 9.99 997 9.99 997	25 24 23 22 21
40 41 42 43 44	8.06 577 8.07 650 8.08 696 8.09 718 8.10 716	109 <u>9</u> 107 <u>2</u> 1046 1022 998	$\begin{array}{r} 8.06\ 58\overline{0}\\ 8.07\ 653\\ 8.08\ 699\\ 8.09\ 72\overline{1}\\ 8.10\ 72\overline{0}\end{array}$	$     \begin{array}{r} 1099 \\     1072 \\     1046 \\     1022 \\     999 \\     \end{array} $	$ \begin{array}{r} 1.93 41\overline{9} \\ 1.92 347 \\ 1.91 300 \\ 1.90 27\overline{8} \\ 1.89 27\overline{9} \end{array} $	$\begin{array}{c} 9.99 & 997 \\ 9.99 & 997 \\ 9.99 & 997 \\ 9.99 & 997 \\ 9.99 & 996 \\ 9.99 & 996 \\ 9.99 & 996 \end{array}$	20 19 18 17 16
45 46 47 48 49	$\begin{array}{r} 8\cdot11\ 69\overline{2}\\ 8\cdot12\ 647\\ 8\cdot13\ 58\underline{1}\\ 8\cdot14\ 49\overline{5}\\ 8\cdot15\ 39\overline{0}\end{array}$	97 <u>6</u> 954 934 914 895	$\begin{array}{r} 8 \cdot 11 \ 69\overline{6} \\ 8 \cdot 12 \ 651 \\ 8 \cdot 13 \ 585 \\ 8 \cdot 14 \ 499 \\ 8 \cdot 15 \ 395 \end{array}$	97 <u>6</u> 954 934 914 895	$ \begin{array}{r} 1 \cdot 88 \ 30\overline{3} \\ 1 \cdot 87 \ 349 \\ 1 \cdot 86 \ 415 \\ 1 \cdot 85 \ 50\overline{0} \\ 1 \cdot 84 \ 605 \end{array} $	9.99996 9.99996 9.99996 9.99996 9.99996 9.99995	$15 \\ 14 \\ 13 \\ 12 \\ 11$
50 51 52 53 54	8 · 16 268 8 · 17 128 8 · 17 971 8 · 18 798 8 · 19 610	877 860 843 827 811	$\begin{array}{r} 8\cdot 16 \ 27\overline{2} \\ 8\cdot 17 \ 133 \\ 8\cdot 17 \ 97\overline{6} \\ 8\cdot 18 \ 80\overline{3} \\ 8\cdot 19 \ 61\overline{5} \end{array}$	87 <u>7</u> 86 <u>0</u> 843 827 812	$ \begin{array}{r} 1 \cdot 83 \ 72\overline{7} \\ 1 \cdot 82 \ 867 \\ 1 \cdot 82 \ 02\overline{3} \\ 1 \cdot 81 \ 19\overline{6} \\ 1 \cdot 80 \ 38\overline{4} \end{array} $	$\begin{array}{c} 9.99 & 995\\ 9.99 & 995\\ 9.99 & 995\\ 9.99 & 995\\ 9.99 & 995\\ 9.99 & 995\\ 9.99 & 994\end{array}$	10 9 8 7 6
55 56 57 58 59	$\begin{array}{r} 8 \cdot 20 \ 407 \\ 8 \cdot 21 \ 189 \\ 8 \cdot 21 \ 958 \\ 8 \cdot 22 \ 713 \\ 8 \cdot 23 \ 455 \end{array}$	79 <u>7</u> 78 <u>2</u> 76 <u>8</u> 755 742	$\begin{array}{r} 8\cdot 20 \ 41\overline{2} \\ 8\cdot 21 \ 195 \\ 8\cdot 21 \ 964 \\ 8\cdot 22 \ 719 \\ 8\cdot 23 \ 462 \end{array}$	797 78 <u>3</u> 76 <u>8</u> 75 <u>5</u> 742	$ \begin{array}{r} 1.79 58\overline{7} \\ 1.78 80\overline{4} \\ 1.78 036 \\ 1.77 280 \\ 1.76 538 \end{array} $	$\begin{array}{r} 9.99 \ 994 \\ 9.99 \ 994 \\ 9.99 \ 994 \\ 9.99 \ 994 \\ 9.99 \ 994 \\ 9.99 \ 994 \\ 9.99 \ 993 \end{array}$	5 4 3 2 1
<u>60</u>	8.24 185 Log. Cos.	730 D	8 · 24 192 Log. Cot.	730 Com. D.	1.75 808 Log. Tan.	9.99 993 Log. Sin.	

90°

0°

605

1°

### TABLE VII.—L'OGARITHMIC SINES, COSINES, TANGENTS, AND COTANGENTS.

1			AND COTA	tion in			110
1	Log. Sin.	D	Log. Tan.	Com. D.	Log. Cot.	Log. Cos.	
0 1 2 3 4	$\begin{array}{r} 8.24 \ 18\overline{5} \\ 8.24 \ 90\overline{3} \\ 8.25 \ 60\overline{9} \\ 8.26 \ 304 \\ 8.26 \ 988 \end{array}$	718 706 694 684	$\begin{array}{r} 8 \cdot 24 \ 192 \\ 8 \cdot 24 \ 910 \\ 8 \cdot 25 \ 616 \\ 8 \cdot 26 \ 311 \\ 8 \cdot 26 \ 995 \end{array}$	718 706 695 684	$ \begin{array}{r} 1.75\ 808\\ 1.75\ 090\\ 1.74\ 383\\ 1.73\ 688\\ 1.73\ 004 \end{array} $	9.99993 9.99993 9.99993 9.9999 <u>3</u> 9.9999 <u>2</u> 9.9999 <u>2</u>	60 59 58 57 56
5 6 7 8 9	$\begin{array}{c} 8 \cdot 27 \ 66 \overline{1} \\ 8 \cdot 28 \ 32 \overline{4} \\ 8 \cdot 28 \ 97 \overline{7} \\ 8 \cdot 29 \ 62 \overline{0} \\ 8 \cdot 30 \ 25 \overline{4} \end{array}$	673 663 • 653 643 634	8 • 27 66 <u>9</u> 8 • 28 33 <u>2</u> 8 • 28 985 8 • 29 62 <u>9</u> 8 • 30 263	67 <u>3</u> 663 65 <u>3</u> 64 <u>3</u> 634	$\begin{array}{c} 1 \cdot 72 \ 331 \\ 1 \cdot 71 \ 667 \\ 1 \cdot 71 \ 014 \\ 1 \cdot 70 \ 371 \\ 1 \cdot 69 \ 736 \end{array}$	9.99992 9.99992 9.99992 9.99991 9.99991 9.99991	55 54 53 52 51
10 11 12 13 14	$\begin{array}{c} 8\cdot 30 \ 87\overline{9} \\ 8\cdot 31 \ 49\overline{5} \\ 8\cdot 32 \ 10\overline{2} \\ 8\cdot 32 \ 70\overline{1} \\ 8\cdot 33 \ 29\overline{2} \end{array}$	625 616 607 599 591	$\begin{array}{c} 8\cdot 30 \ 88\bar{8} \\ 8\cdot 31 \ 504 \\ 8\cdot 32 \ 112 \\ 8\cdot 32 \ 71\bar{1} \\ 8\cdot 33 \ 30\bar{2} \end{array}$	625 61 <u>6</u> 607 599 591	$ \begin{array}{c} 1.69 \\ 1.68 \\ 495 \\ 1.67 \\ 888 \\ 1.67 \\ 288 \\ 1.66 \\ 697 \\ \end{array} $	9.99 99 <u>1</u> 9.99 99 <u>0</u> 9.99 990 9.99 990 9.99 990 9.99 990	50 49 48 47 46
15 16 17 18 19	$\begin{array}{r} 8\cdot 33 & 87\overline{5} \\ 8\cdot 34 & 450 \\ 8\cdot 35 & 018 \\ 8\cdot 35 & 57\overline{8} \\ 8\cdot 36 & 13\overline{1} \end{array}$	583 575 567 560 553	$\begin{array}{r} 8\cdot 33 & 88\overline{5} \\ 8\cdot 34 & 461 \\ 8\cdot 35 & 029 \\ 8\cdot 35 & 58\overline{9} \\ 8\cdot 36 & 143 \end{array}$	583 575 568 560 553	$ \begin{array}{r} 1.66 \\ 1.65 \\ 539 \\ 1.64 \\ 971 \\ 1.64 \\ 410 \\ 1.63 \\ 857 \\ \end{array} $	9.9998 <u>9</u> 9.99989 9.99989 9.99989 9.99989 9.99988	45 44 43 42 41
20 21 22 23 24	8 · 36 677 8 · 37 217 8 · 37 750 8 · 38 276 8 · 38 796	54 <u>6</u> 539 533 526 520	8 · 36 689 8 · 37 229 8 · 37 762 8 · 38 289 8 · 38 809	54 <u>6</u> 539 533 527 520	$ \begin{array}{r} 1.63 31\overline{0} \\ 1.62 771 \\ 1.62 238 \\ 1.61 711 \\ 1.61 191 \end{array} $	9.99988 9.99988 9.99987 9.99987 9.99987 9.99987	40 39 38 37 36
25 26 27 28 29	$8 \cdot 39 310$ $8 \cdot 39 818$ $8 \cdot 40 320$ $8 \cdot 40 816$ $8 \cdot 41 307$	514 508 502 496 491	$\begin{array}{r} 8.39\ 32\bar{3}\\ 8.39\ 83\bar{1}\\ 8.40\ 33\underline{4}\\ 8.40\ 83\bar{0}\\ 8.41\ 32\bar{1} \end{array}$	514 508 502 496 491	$ \begin{array}{r} 1.60\ 67\overline{6} \\ 1.60\ 168 \\ 1.59\ 666 \\ 1.59\ 16\overline{9} \\ 1.58\ 678 \end{array} $	9.99 98 <u>6</u> 9.99 986 9.99 986 9.99 986 9.99 986 9.99 985	35 34 33 32 31
30 31 32 33 34	$\begin{array}{r} 8 \cdot 41 \ 792 \\ 8 \cdot 42 \ 271 \\ 8 \cdot 42 \ 746 \\ 8 \cdot 43 \ 215 \\ 8 \cdot 43 \ 680 \end{array}$	485 479 474 469 464	$\begin{array}{r} 8.41 \\ 8.42 \\ 287 \\ 8.42 \\ 762 \\ 8.43 \\ 231 \\ 8.43 \\ 696 \end{array}$	$\begin{array}{r} 485\\ 480\\ 475\\ 469\\ 464\\ \end{array}$	1.58 1931.57 7131.57 2381.56 7681.56 304	9.99985 9.99985 9.99984 9.99984 9.99984 9.99984	30 29 28 27 26
35 36 37 38 39	$\begin{array}{r} 8.44.139\\ 8.44.594\\ 8.45.044\\ 8.45.489\\ 8.45.489\\ 8.45.930\end{array}$	$ \begin{array}{r} 45\overline{9} \\ 454 \\ 450 \\ 44\overline{5} \\ 440 $	$\begin{array}{r} 8.44 \\ 8.44 \\ 611 \\ 8.45 \\ 061 \\ 8.45 \\ 507 \\ 8.45 \\ 948 \end{array}$	$ \begin{array}{r} 460 \\ 455 \\ 450 \\ 445 \\ 441 \\ 441 \\ 407 $	1.55 8441.55 3891.54 9381.54 4931.54 4931.54 052	$\begin{array}{r} 9.99 \ 983 \\ 9.99 \ 983 \\ 9.99 \ 982 \\ 9.99 \ 982 \\ 9.99 \ 982 \\ 9.99 \ 982 \\ 9.99 \ 982 \end{array}$	25 24 23 22 21
40 41 42 43 44	$\begin{array}{r} 8 \cdot 46 \ 36\overline{6} \\ 8 \cdot 46 \ 798 \\ 8 \cdot 47 \ 22\overline{6} \\ 8 \cdot 47 \ 650 \\ 8 \cdot 48 \ 06\overline{9} \end{array}$	436 432 428 423 419	$\begin{array}{r} 8 \cdot 46 \ 385 \\ 8 \cdot 46 \ 817 \\ 8 \cdot 47 \ 245 \\ 8 \cdot 47 \ 669 \\ 8 \cdot 48 \ 089 \end{array}$	437 432 428 424 419	$\begin{array}{r} 1\cdot 53 \ 615 \\ 1\cdot 53 \ 183 \\ 1\cdot 52 \ 754 \\ 1\cdot 52 \ 330 \\ 1\cdot 51 \ 911 \end{array}$	9.99 98 <u>1</u> 9.99 98 <u>1</u> 9.99 98 <u>1</u> 9.99 98 <u>1</u> 9.99 98 <u>0</u> 9.99 980	20 19 18 17 16
45 46 47 48 49	$\begin{array}{r} 8.48 \ 485 \\ 8.48 \ 896 \\ 8.49 \ 304 \\ 8.49 \ 708 \\ 8.50 \ 108 \end{array}$	415 411 407 404 400 200	$\begin{array}{r} 8 \cdot 48 \ 505 \\ 8 \cdot 48 \ 917 \\ 8 \cdot 49 \ 325 \\ 8 \cdot 49 \ 729 \\ 8 \cdot 50 \ 130 \end{array}$	416 412 408 404 400 396	1.51 4951.51 0831.50 6751.50 2701.49 870	9.99979 9.99979 9.99979 9.99979 9.99978 9.99978	15 14 13 12 11
50 51 52 53 54	$\begin{array}{r} 8.50 50\overline{4} \\ 8.50 89\overline{7} \\ 8.51 28\overline{6} \\ 8.51 67\overline{2} \\ 8.52 055 \end{array}$	396 393 389 38 <u>6</u> 38 <u>2</u> 38 <u>2</u>	$\begin{array}{r} 8.50 \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \$	393 390 386 383	$1.49 47\overline{3} \\ 1.49 080 \\ 1.48 690 \\ 1.48 304 \\ 1.47 921$	9.99978 9.99977 9.99977 9.99977 9.99976 9.99976	10 9 8 7 6
55 56 57 58 59	$\begin{array}{r} 8\cdot 52 \ 43\overline{4} \\ 8\cdot 52 \ 810 \\ 8\cdot 53 \ 183 \\ 8\cdot 53 \ 55\overline{2} \\ 8\cdot 53 \ 91\overline{8} \end{array}$	37 <u>9</u> 375 373 369 366	$\begin{array}{r} 8.52 & 45\overline{8} \\ 8.52 & 835 \\ 8.53 & 208 \\ 8.53 & 578 \\ 8.53 & 94\overline{4} \end{array}$	379 376 373 370 366 864	$\begin{array}{r} 1\cdot47 \ 54\overline{1} \\ 1\cdot47 \ 165 \\ 1\cdot46 \ 792 \\ 1\cdot46 \ 422 \\ 1\cdot46 \ 055 \end{array}$	$\begin{array}{r} 9.99 \ 975\\ 9.99 \ 975\\ 9.99 \ 975\\ 9.99 \ 975\\ 9.99 \ 974\\ 9.99 \ 974\end{array}$	5 4 3 2 1
<u>60</u>	8.54 282 Log. Cos.	363 D	8 · 54 308 Log. Cot.	364 Com. D.	<u>1.45 691</u> Log. Tan.	9.99 973 Log. Sin.	-o
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### TABLE VII.—LOGARITHMIC SINES, COSINES, TANGENTS, AND COTANGENTS.

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'	Log. Sin.	D	Log. Tan.	Com. D.	Log. Cot.	Log. Cos.	_
0 1 2 3 4	$\begin{array}{r} 8.54 & 282 \\ 8.54 & 642 \\ 8.54 & 999 \\ 8.55 & 354 \\ 8.55 & 705 \end{array}$	360 357 354 351 348	$\begin{array}{r} 8.54 & 30\overline{8} \\ 8.54 & 669 \\ 8.55 & 027 \\ 8.55 & 381 \\ 8.55 & 73\overline{3} \end{array}$	$36\bar{0} \\ 358 \\ 354 \\ 352 \\ 349 \\ 340 \\ 3$	$\begin{array}{c} 1\cdot 45 \ 69\overline{1} \\ 1\cdot 45 \ 331 \\ 1\cdot 44 \ 973 \\ 1\cdot 44 \ 618 \\ 1\cdot 44 \ 265 \end{array}$	$\begin{array}{c} 9\cdot 99 \ 97\overline{3} \\ 9\cdot 99 \ 97\overline{3} \\ 9\cdot 99 \ 97\overline{2} \\ 9\cdot 99 \ 97\overline{1} \end{array}$	60 59 58 57 56
5 6 7 8 9	8.56 054 8.56 400 8.56 74 <u>3</u> 8.57 08 <u>3</u> 8.57 421	$340 \\ 346 \\ 343 \\ 340 \\ 338 \\ 335$	8.56 083 8.56 429 8.56 772 8.57 113 8.57 452	$346 \\ 343 \\ 341 \\ 338 \\ 338 \\ 338 \\ 338 \\ 338 \\ 338 \\ 338 \\ 338 \\ 338 \\ 338 \\ 338 \\ 338 \\ 338 \\ 348 $	$ \begin{array}{r} 1 \cdot 43 \ 917 \\ 1 \cdot 43 \ 571 \\ 1 \cdot 43 \ 227 \\ 1 \cdot 42 \ 886 \\ 1 \cdot 42 \ 548 \end{array} $	9.99971 9.99971 9.99970 9.99970 9.99970 9.99969	55 54 53 52 51
10 11 12 13 14	8.57 756 8.58 039 8.58 419 8.58 747 8.59 072	33 <u>2</u> 33 <u>0</u> 327 325 323	8.57 787 8.58 12 <u>1</u> 8.58 45 <u>1</u> 8.58 779 8.59 105	33 <u>5</u> 333 328 328 325 323	$\begin{array}{r}1\cdot42\ 21\bar{2}\\1\cdot41\ 879\\1\cdot41\ 54\bar{8}\\1\cdot41\ 22\bar{0}\\1\cdot40\ 895\end{array}$	9.9996 <u>9</u> 9.99968 9.99968 9.99967 9.99967	$50 \\ 49 \\ 48 \\ 47 \\ 46$
15 16 17 18 19	8.59 395 8.59 715 8.60 033 8.60 349 8.60 662	320 318 316 313 311	8.59 428 8.59 749 8.60 067 8.60 384 8.60 698	323     320     318     316     314     311     311	$\begin{array}{c} 1\cdot 40 \ 57\overline{1} \\ 1\cdot 40 \ 251 \\ 1\cdot 39 \ 93\overline{2} \\ 1\cdot 39 \ 616 \\ 1\cdot 39 \ 302 \end{array}$	$\begin{array}{c} 9.99 \ 966\\ 9.99 \ 966\\ 9.99 \ 965\\ 9.99 \ 965\\ 9.99 \ 965\\ 9.99 \ 965\\ 9.99 \ 964\end{array}$	$45 \\ 44 \\ 43 \\ 42 \\ 41$
20 21 22 23 24	8.60 973 8.61 282 8.61 589 8.61 893 8.62 196	309 306 304 302 300	$\begin{array}{c} 8 \cdot 61 & 00\overline{9} \\ 8 \cdot 61 & 319 \\ 8 \cdot 61 & 626 \\ 8 \cdot 61 & 931 \\ 8 \cdot 62 & 234 \end{array}$	309 307 305 303	$\begin{array}{c} 1\cdot 38 \ 990\\ 1\cdot 38 \ 681\\ 1\cdot 38 \ 374\\ 1\cdot 38 \ 068\\ 1\cdot 37 \ 765\end{array}$	9.9996 <u>4</u> 9.9996 <u>3</u> 9.9996 <u>3</u> 9.9996 <u>3</u> 9.99962 9.99962	40 39 38 37 36
25 26 · 27 28 29	8.62 496 8.62 795 8.63 091 8.63 385 8.63 677	298 29 <u>6</u> 294 292	$\begin{array}{r} 8\cdot 62 \ 535 \\ 8\cdot 62 \ 834 \\ 8\cdot 63 \ 131 \\ 8\cdot 63 \ 425 \\ 8\cdot 63 \ 718 \end{array}$	300 299 297 294 293	$\begin{array}{c} 1\cdot 37 \ 465 \\ 1\cdot 37 \ 166 \\ 1\cdot 36 \ 869 \\ 1\cdot 36 \ 574 \\ 1\cdot 36 \ 281 \end{array}$	9.99961 9.9996 <u>1</u> 9.9996 <u>0</u> 9.99959 9.99959	35 34 33 32 31
30 31 32 33 34	8.63 968 8.64 256 8.64 543 8.64 827 8.65 110	290 288 286 284 282	$\begin{array}{r} 8.64 & 00\overline{9} \\ 8.64 & 298 \\ 8.64 & 58\overline{5} \\ 8.64 & 87\overline{0} \\ 8.65 & 15\overline{3} \end{array}$	29 <u>1</u> 28 <u>8</u> 287 285 283	$ \begin{array}{r} 1.35 990 \\ 1.35 702 \\ 1.35 414 \\ 1.35 129 \\ 1.34 846 \end{array} $	9.99 958 9.99 958 9.99 957 9.99 957 9.99 957 9.99 956	30 29 28 27 26
35 36 37 38 39	8.65 391 8.65 670 8.65 947 8.66 223 8.66 497	281 27 <u>9</u> 27 <u>7</u> 275 274	$\begin{array}{r} 8.65 & 435 \\ 8.65 & 715 \\ 8.65 & 993 \\ 8.66 & 269 \\ 8.66 & 543 \end{array}$	281 280 278 27 <u>6</u> 27 <u>4</u>	$ \begin{array}{r} 1.34565\\1.34285\\1.34007\\1.38731\\1.33456\end{array} $	$\begin{array}{r} 9.99 \ 956 \\ 9.99 \ 955 \\ 9.99 \ 954 \\ 9.99 \ 954 \\ 9.99 \ 954 \\ 9.99 \ 953 \end{array}$	25 24 23 22 21
40 41 42 43 44	8.66769 8.67039 8.67308 8.67575 8.67840	272 270 268 267 265	$\begin{array}{r} 8.66 816 \\ 8.67 087 \\ 8.67 356 \\ 8.67 624 \\ 8.67 890 \end{array}$	272 271 26 <u>9</u> 267 266	$\begin{array}{r} 1.33 \ 184 \\ 1.32 \ 913 \\ 1.32 \ 643 \\ 1.32 \ 376 \\ 1.32 \ 110 \end{array}$	9.99953 9.99952 9.99952 9.99952 9.99951 9.99950	20 19 18 17 16
45 46 47 48 49	8.68 104 8.68 366 8.68 627 8.68 886 8.69 144	264 262 260 259 257	$\begin{array}{r} 8\cdot 68 \ 15\overline{4} \\ 8\cdot 68 \ 417 \\ 8\cdot 68 \ 67\overline{8} \\ 8\cdot 68 \ 938 \\ 8\cdot 69 \ 19\overline{6} \end{array}$	264 262 261 259 258	$\begin{array}{r} 1\cdot 31 \ 84\overline{5} \\ 1\cdot 31 \ 583 \\ 1\cdot 31 \ 321 \\ 1\cdot 31 \ 321 \\ 1\cdot 31 \ 062 \\ 1\cdot 30 \ 80\overline{3} \end{array}$	$\begin{array}{r}9.99&950\\9.99&949\\9.99&948\\9.99&948\\9.99&948\\9.99&948\\9.99&948\end{array}$	15 14 13 12 11
50 51 52 53 54	8.69 400 8.69 654 8.69 907 8.70 159 8.70 409	25 <u>6</u> 25 <u>4</u> 25 <u>3</u> 251 250	8.69 453 8.69 708 8.69 961 8.70 214 8.70 464	256 255 253 252 250	$ \begin{array}{r} 1 \cdot 30 547 \\ 1 \cdot 30 292 \\ 1 \cdot 30 038 \\ 1 \cdot 29 786 \\ 1 \cdot 29 535 \end{array} $	$\begin{array}{r} 9.99\ 947\\ 9.99\ 946\\ 9.99\ 945\\ 9.99\ 945\\ 9.99\ 945\\ 9.99\ 945\\ 9.99\ 944\end{array}$	10 9 8 7 6
55 56 57 58 59	8.70 657 8.70 905 8.71 150 8.71 395 8.71 638	248 247 245 244 243	$\begin{array}{r} 8.70\ 714\\ 8.70\ 962\\ 8.71\ 208\\ 8.71\ 453\\ 8.71\ 697\end{array}$	249 248 246 245 243	$ \begin{array}{r} 1 \cdot 29 \ 286 \\ 1 \cdot 29 \ 038 \\ 1 \cdot 28 \ 791 \\ 1 \cdot 28 \ 546 \\ 1 \cdot 28 \ 303 \end{array} $	$\begin{array}{r} 9.99 94\overline{3} \\ 9.99 943 \\ 9.99 943 \\ 9.99 942 \\ 9.99 942 \\ 9.99 942 \\ 9.99 941 \end{array}$	5 4 3 2 1
60	8.71 880 Log. Cos.	241 D	8.71 939	242 Com. D.	1.28 060	9.99 940	<u> </u>
-	Lug. 003.		Log. Cot.		Log. Tan.	Log. Sin.	1

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TABLE VII.-LOGARITHMIC SINES, COSINES, TANGENTS, AND COTANGENTS.

3°	ТАВ		v 11	-170	GA.	AND		TAN			JSINES, TANGENTS, 176
	Log. Sin.	d.	Log.	Tan.	c.d.	Log.	Cot.	Log.	Cos.		P. P.
0	8 · 71 880 8 · 72 120	$24\overline{0}$	$8.71 \\ 8.72$	$93\overline{9}$ $18\overline{0}$	241	$1.28 \\ 1.27$	060 819	9.99 9.99	$94\bar{0} \\ 940$	60 59	<b>330 320 310 300</b> 6  33.0  32.0  31.0  30.0
23	$8 \cdot 72 \ 120 \ 8 \cdot 72 \ 359 \ 8 \cdot 72 \ 597 \ 8 \cdot 72 \ 833$	$\frac{239}{23\overline{7}}$	8 · 72 8 · 72 8 · 72 8 · 72 8 · 72	420 659	$\begin{array}{c} 240 \\ 238 \end{array}$	1.20 1.27 1.27 1.27 1.27 1.27	579 341 104	9.99 9.99	93 <u>9</u> 938	58 57	$\begin{array}{c} 6 \\ 7 \\ 38 \cdot 5 \\ 8 \\ 44 \cdot 0 \\ 42 \cdot 6 \\ 41 \cdot 3 \\ 40 \cdot 6 \\ 41 \cdot 3 \\ 40 \cdot 0 \\ 42 \cdot 6 \\ 41 \cdot 3 \\ 40 \cdot 0 \\ 40$
4	8.72 833	236 235	8.72	896	237 235	1.27	104		938	56	9 49.5 48.0 46.5 45.0
5 6	8 · 73 069 8 · 73 302 8 · 73 535	233	8 · 73 8 · 73 8 · 73	$\begin{array}{c}13\overline{1}\\36\overline{6}\\59\overline{9}\end{array}$	235 233	$1.26 \\ 1.26$	86 <u>8</u> 63 <u>3</u>	9.99 9.99		55 54	201110.01106.61103.31100.0
6 7 8	8 · 73 535 8 · 73 766	$     \begin{array}{r}       233 \\       231 \\       230     \end{array}   $	8.73	831	232 231	1.26 1.26 1.26 1.26 1.25	$\begin{array}{r} 400 \\ 168 \end{array}$	9.99 9.99	935 93 <u>5</u>	53 52	30 165 · 0 160 · 0 155 · 0 150 · 0 40 220 · 0 213 · 3 206 · 6 200 · 0 50 275 · 0 266 · 6 258 · 3 250 · 0
$\frac{9}{10}$	8.73 997 8.74 226		$\frac{8\cdot74}{8\cdot74}$	062 292	229	1.25	937 708	9.99 9.99		$\frac{51}{50}$	
11	8.74 453	229 227 226 225	8.74 8.74 8.74 8.74	520 748	228	$1.25 \\ $	479 252		933 932	49 48	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
$12 \\ 13 \\ 14$	8 · 74 680 8 · 74 905	$\frac{225}{224}$	8.74	974 974	226 225	$1.25 \\ 1.25$	026	9.99	93Ī	47	8 38.6 37.3 36.0 34.6
$\frac{14}{15}$	8.75 129 8.75 35 <u>3</u>	22 <u>3</u>	8.75 8.75	199 422 645	$22\bar{3}$	$\frac{1\cdot 24}{1\cdot 24}$	801 577	$9.99 \\ 9.99$	931 930	$\frac{46}{45}$	9 43.5 42.0 40.5 39.0
$\frac{16}{17}$	8 · 75 574 8 · 75 795	221 221	8.75	645 867	$223 \\ 221 \\ 221$	1.24	$35\overline{4}$ 133	9.99 9.99	92 <u>9</u> 928	44 43	$\begin{array}{cccccccccccccccccccccccccccccccccccc$
$\overline{18}$ 19	8 · 76 015 8 · 76 233	1220	8.76 8.76	087 306	$\begin{array}{c} 220\\ 219 \end{array}$	$1.24 \\ 1.23 \\ 1.23 \\ 1.23$	913 693	9.99	928 927	42 41	$\begin{array}{c} 30 \\ 40 \\ 193 \\ .3 \\ .3 \\ .3 \\ .3 \\ .3 \\ .3 \\ .3 \\ $
20	8.76 451	$217 \\ 216 \\ 215 \\ 214 \\ 214 \\ 014 $	8.76	$52\overline{4}$	$\frac{218}{217}$	1.23	475	9.99	926	40	
21 22	8.76 667 8.76 883	$\tilde{2}\tilde{1}\tilde{5}$	8.76 8.76 8.76 8.77	741 958	$217 \\ 216 \\ 214 \\ 214$	$1.23 \\ 1.23$	$\frac{258}{042}$	9.99 9.99	925 925	39 38	6 25.0 24.0 23.0 22.0
23 24	8.77 097 8.77 310	213	8.77	172 386	214	$1 \cdot 23 \\ 1 \cdot 23 \\ 1 \cdot 22 \\ 1 \cdot 22 \\ 1 \cdot 22 \\$	$\frac{827}{613}$	9.99 9.99	$924 \\ 923$	37 36	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
25 26	8 · 77 522 8 · 77 733 8 · 77 943 8 · 78 152	$21\overline{2}$ 211	8 · 77 8 · 77 8 · 78	599 811	$213 \\ 212 \\ 210$	1.22	$40\overline{0}$	9.99 9.99	922 922	$\frac{35}{34}$	10 41.6 40.0 38.3 36.6
27 28	8.77733 8.77943 8.78152		8 · 78 8 · 78	022 232	210	$1 \cdot 22 \\ 1 \cdot 21 \\ 1 \cdot 21 \\ 1 \cdot 21$	$18\overline{8} \\ 978 \\ 768 \\ \end{array}$	9.99 9.99	921	33 32	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
<u>29</u>	8.78 360	208 207	8.78	441	209 207	1.21	559	9.99	<u>919</u>	31	$\begin{array}{c} 30 \\ 125 \\ 0 \\ 125 \\ 0 \\ 166 \\ 0 \\ 166 \\ 0 \\ 160 \\ 0 \\ 153 \\ 0 \\ 0 \\ 191 \\ 0 \\ 183 \\ 0 \\ 0 \\ 191 \\ 0 \\ 183 \\ 0 \\ 0 \\ 191 \\ 0 \\ 183 \\ 0 \\ 0 \\ 191 \\ 0 \\ 183 \\ 0 \\ 0 \\ 191 \\ 0 \\ 183 \\ 0 \\ 0 \\ 183 \\ 0 \\ 0 \\ 183 \\ 0 \\ 0 \\ 191 \\ 0 \\ 183 \\ 0 \\ 0 \\ 191 \\ 0 \\ 100 \\ 0 \\ 100 \\ 0 \\ 100 \\ 0 \\ 100 \\ 0 \\ $
$\frac{30}{31}$	8 · 78 567 8 · 78 773	206	8 · 78 8 · 78	$64\overline{8} \\ 85\overline{5}$	207	${}^{1\cdot 21}_{1\cdot 21}$	$35\overline{1}$ $14\overline{4}$	9.99 9.99	918	30 29	210 200 190 180
32 33	8 · 78 978 8 · 79 183	$20\overline{4}$	8.79 8.79	$\begin{array}{c} 06\overline{1}\\ 266 \end{array}$	$\begin{array}{c} 206 \\ 204 \\ \end{array}$	$1.20 \\ 1.20$	938 734	9.99 9.99	$917 \\ 916$	28 27	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
$\frac{34}{35}$	<u>8.79386</u>	203 202	8.79	470 673	204 203	1.20	530 327	9.99	916 915	26 25	8 28.0 26.6 25.3 24.0 9 31.5 30.0 28.5 27.0
36	8.79 789	$\begin{array}{c} 20\overline{1} \\ 200 \end{array}$	8 · 79 8 · 79	875	$\begin{array}{c} 202\\ 201 \end{array}$	1.20	125	9.99 9.99	914	24	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
37 38	8 · 79 989 8 · 80 189	$19\overline{9}$ $19\overline{8}$	8.80 8.80	$27\bar{6}$	$200 \\ 199$	1.19	723	$9.99 \\ 9.99$		23 22	$\begin{array}{c} 20 & 70.0 \\ 30 & 105.0 & 100.0 \\ 40 & 140.0 & 133.3 \\ 50 & 175.0 & 166.6 \\ 158.3 & 150.0 \\ \end{array}$
$\frac{39}{40}$	8.80387 8.80585	197	8.80 8.80	476 674	198	$\frac{1.19}{1.19}$	524 326	<u>9.99</u> 9.99	912 911	$\frac{21}{20}$	50 175.0 166.6 158.3 150.0
41 42	8.80 782 8.80 977 8.81 172 8.81 366	$197 \\ 195 $	8.80	871	$\frac{197}{197}$	$1.19 \\ 1.18 \\ 1.18 \\ 1.18$	$128 \\ 931$	9.99 9.99		19 18	<b>9 9 8 7 6 5</b>
43 44	$     8 81 17\overline{2}     8 81 36\overline{6} $	$\begin{array}{c} 195 \\ 194 \end{array}$	8.81 8.81 8.81	264 459	195 195	$1.18 \\ 1.18 \\ 1.18$	736	9.99 9.99	<u>908</u>	$\tilde{17}$ 16	$\begin{array}{c} 6 \\ 0 \cdot \overline{9} \\ 0 \cdot 9 \\ $
45	8.81 560	102	8.81	653	194	$\frac{1\cdot 10}{1\cdot 18}$	347	9.99	907	15	$\begin{array}{c} 7   1 \cdot 1   1 \cdot \overline{0}   0 \cdot \overline{9}   0 \cdot 8   0 \cdot 7   0 \cdot 6 \\ 8   1 \cdot \overline{2}   1 \cdot 2   1 \cdot \overline{0}   0 \cdot \overline{9}   0 \cdot 8   0 \cdot \overline{6} \\ 9   1 \cdot \overline{4}   1 \cdot \overline{3}   1 \cdot 2   1 \cdot \overline{0}   0 \cdot 9   0 \cdot \overline{7} \\ 1 0   1 \cdot 6   1 \cdot 5   1 \cdot \overline{3}   1 \cdot 1   1 \cdot 0   0 \cdot \overline{8} \end{array}$
46 47	8.81 752 8.81 94 <u>3</u>	191 191	8.81 8.82	84 <u>6</u> 038	19 <u>3</u> 19 <u>2</u> 19 <u>1</u>	1.18 1.18 1.17 1.17	$154 \\ 961$	9.99 9.99	90 <u>6</u> 90 <u>5</u>	14 13	$\begin{array}{c} 9 & 1 \cdot \overline{4} & 1 \cdot \overline{3} & 1 \cdot 2 & 1 \cdot \overline{0} & 0 \cdot 9 & 0 \cdot \overline{7} \\ 10 & 1 \cdot \underline{6} & 1 \cdot 5 & 1 \cdot \overline{3} & 1 \cdot 1 & 1 \cdot 0 & 0 \cdot \overline{8} \\ 20 & 3 \cdot \overline{1} & 3 \cdot 0 & 2 \cdot \overline{6} & 2 \cdot \overline{3} & 2 \cdot 0 & 1 \cdot \overline{6} \end{array}$
48 49	8 · 82 134 8 · 82 324	189	8 · 82 8 · 82	230	190	$1.17 \\ 1.17$	$\frac{770}{579}$	9.99 9.99	90 <u>4</u> 903	$\frac{12}{11}$	$\begin{array}{c} 0 & 1 & . \\ 1 &$
$\overline{50}$ $51$	8 · 82 513 8 · 82 701	189	8 82	610	$\begin{array}{c}190\\18\overline{8}\end{array}$	$1.17 \\ $		9.99	902	10 9	50 7.9 7.5 6.6 5.8 5.0 4.1
52	8.82 888	$18\overline{7}$ $18\overline{6}$	8.82	987	$18\frac{1}{2}$ $18\frac{7}{2}$	1.17	201 012	9.99 9.99	901	8	$\begin{array}{c} \mathbf{\ddot{4}} & 4 & 3 & 2 & 1 & \mathbf{\bar{0}} \\ 6 0.\mathbf{\bar{4}} 0.4 0.3 0.2 0.1 0.\mathbf{\bar{0}} \end{array}$
53 54	8 · 83 075 8 · 83 260	185 185	8 · 82 8 · 82 8 · 83 8 · 83 8 · 83	361	186	1.16 1.16	638	9.99 9.99	<u>89</u> 9	6	70.50.40.30.20.10.0
55 56	8 · 83 44 <u>5</u> 8 · 83 629	184	0 00	517	1100	1.16 1.16 1.16 1.15 1.15 1.15	453 268	9.99 9.99		5 4	$\begin{array}{c} 9 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\$
57	8 · 83 813 8 · 83 995 8 · 84 177	$18\overline{3}$ $18\overline{2}$	8 · 83 8 · 83 8 · 84 8 · 84	916 100	$     \begin{array}{r}       185 \\       184 \\       183 \\       182 \\       182     \end{array} $	1.16	083	9.99 9.99	896	3	$\begin{array}{c} 10 & 0.7 & 0.0 & 0.5 & 0.5 & 0.1 \\ 20 & 1.5 & 1.3 & 1.0 & 0.6 & 0.3 & 0.1 \\ 30 & 2.2 & 2.0 & 1.5 & 1.0 & 0.5 & 0.2 \end{array}$
58 59 60			8.84	282	1100	1.15	717	9.99	895	1	$403.02.\overline{6}2.01.\overline{3}0.\overline{6}0.3$
<u>00</u>	8.84 358 Log. Cos		<u>8.84</u> Log.			1.10	_	9.99 Log.	<u>894</u> Sin	A DESCRIPTION OF	<u>50 3.7 3.3 2.5 1.6 0.8 0.4</u> P. P.
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#### TABLE VII.—LOGARITHMIC SINES, COSINES, TANGENTS, AND COTANGENTS.

-4°		AND CO	JTANGENTS	· 175°
	Log. Sin. d.	Log. Tan. c.d. Log. Cot	Log. Cos.	P. P.
01234	8 · 84 358 8 · 84 538 8 · 84 718 8 · 84 897 8 · 84 897 8 · 85 075	$     \begin{bmatrix}       8 & 84 & 640 \\       8 & 84 & 826 \\       8 & 85 & 005 \\       8 & 85 & 184 \\       8 & 85 & 184 \\       179 \\       1 & 14 & 99     \end{bmatrix} $	19.99 892 58 19.99 891 57	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
5 6 7 8 9	$\begin{array}{c} 3.85 & 257 \\ 8.85 & 257 \\ 8.85 & 429 \\ 8.85 & 605 \\ 8.85 & 605 \\ 175 \\ 8.85 & 780 \\ 8.85 & 954 \\ 8.85 & 954 \\ 174 \\ 8.85 & 954 \\ 174 \\ \end{array}$	$\begin{array}{c} 8.85 & 717 \\ 8.85 & 893 \\ 8.85 & 893 \\ 8.86 & 068 \\ 175 \\ 1.13 & 93 \\ 1.13 & 93 \\ \end{array}$	9 9 9 9 888 54 3 9 9 9 888 53 7 9 9 887 52 1 9 9 886 51	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$
10 11 12 13 14 15	$\begin{array}{c} 8.86 & 120 \\ 8.86 & 301 \\ 172 \\ 8.86 & 474 \\ 171 \\ 8.86 & 645 \\ 171 \\ 8.86 & 816 \\ 171 \\ 8.86 & 816 \\ 171 \\ 170 \\ 170 \end{array}$	$\begin{array}{c} 8 \cdot 86 & 243 \\ 8 \cdot 86 & 417 \\ 173 \\ 173 \\ 1 \cdot 13 \\ 8 \cdot 86 \\ 590 \\ 172 \\ 1 \cdot 13 \\ 400 \\ 8 \cdot 86 \\ 763 \\ 172 \\ 1 \cdot 13 \\ 23 \\ 8 \\ 8 \\ 8 \\ 8 \\ 8 \\ 8 \\ 935 \\ 172 \\ 1 \\ 1 \\ 3 \\ 20 \\ 1 \\ 1 \\ 3 \\ 20 \\ 1 \\ 1 \\ 3 \\ 20 \\ 1 \\ 1 \\ 3 \\ 20 \\ 1 \\ 1 \\ 3 \\ 20 \\ 1 \\ 1 \\ 3 \\ 20 \\ 1 \\ 1 \\ 3 \\ 20 \\ 1 \\ 1 \\ 3 \\ 20 \\ 1 \\ 1 \\ 1 \\ 3 \\ 20 \\ 1 \\ 1 \\ 1 \\ 3 \\ 20 \\ 1 \\ 1 \\ 1 \\ 1 \\ 1 \\ 1 \\ 20 \\ 1 \\ 1 \\ 1 \\ 1 \\ 1 \\ 1 \\ 1 \\ 1 \\ 1 \\ $	$\begin{array}{c} \overline{2} 9.99884 & 49 \\ \overline{9} 9.99883 & 48 \\ 7 9.99882 & 47 \\ 5 9.99881 & 46 \end{array}$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
15 16 17 18 19 20	$     \begin{array}{r}       8 \cdot 87 \ 15\overline{6} \ 169 \\       8 \cdot 87 \ 32\overline{5} \ 169 \\       8 \cdot 87 \ 494 \ 16\overline{7} \\       8 \cdot 87 \ 66\overline{1} \ 167 \\       \hline       1 \ 67 \\  $	$\begin{array}{c} 8 \cdot 87 \ 277 \ 170 \ 1 \cdot 12 \ 723 \\ 8 \cdot 87 \ 447 \ 169 \ 1 \cdot 12 \ 553 \\ 8 \cdot 87 \ 616 \ 169 \ 1 \cdot 12 \ 384 \\ 8 \cdot 87 \ 785 \ 169 \ 1 \cdot 12 \ 215 \\ 8 \cdot 87 \ 785 \ 169 \ 1 \cdot 12 \ 215 \\ \hline \end{array}$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$
21 22 23 24 25			$9.9987\overline{4}39$ 9.9987438 79.9987337 9.9987236	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
26 27 28 29 30	$\begin{array}{c} 8 & 88 & 654 \\ 8 & 88 & 817 \\ 8 & 88 & 980 \\ 8 & 89 & 142 \\ 8 & 89 & 303 \\ 8 & 89 & 464 \\ 161 \\ 8 & 89 & 464 \\ 161 \\ \end{array}$	$\begin{array}{c} 8 \cdot 88 \ 947 \ 163 \ 1 \cdot 11 \ 052 \ 8 \cdot 89 \ 111 \ 163 \ 1 \cdot 10 \ 889 \ 8 \cdot 89 \ 274 \ 163 \ 1 \cdot 10 \ 726 \ 8 \cdot 89 \ 274 \ 162 \ 1 \cdot 10 \ 726 \ 8 \cdot 89 \ 436 \ 162 \ 1 \cdot 10 \ 563 \ 1 \cdot 10 \ 10 \ 1 \ 10 \ 10 \ 10 \ 10 \$	9.99 870 34 9.99 869 33 9.99 868 32 9.99 867 31	$\begin{array}{c c c c c c c c c c c c c c c c c c c $
31 32 33 34	$\begin{array}{c} 8 \cdot 89 & 62\overline{4} & 159 \\ 8 \cdot 89 & 784 & 159 \\ 8 \cdot 89 & 943 & 158 \\ 8 \cdot 90 & 101 & 158 \\ \hline \end{array}$	$\begin{array}{c} 8.89 & 759 \\ 8.89 & 759 \\ 161 \\ 1.10 & 240 \\ 8.89 & 920 \\ 160 \\ 1.10 & 976 \\ 8.90 & 080 \\ 159 \\ 1.09 & 169 \\ 1.09 & 760 \\ \hline \end{array}$	9.99 865 29 9.99 864 28 9.99 863 27 9.99 862 26	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
38 <u>39</u>	$     \begin{array}{r}       8 \cdot 90 \ 259 \ 157 \\       8 \cdot 90 \ 417 \ 156 \\       8 \cdot 90 \ 573 \ 156 \\       8 \cdot 90 \ 729 \ 156 \\       8 \cdot 90 \ 885 \ 156 \\       8 \cdot 90 \ 885 \ 156 \\     \end{array} $	$\begin{array}{c} 8.90 & 398 \\ 8.90 & 557 \\ 157 \\ 157 \\ 157 \\ 1.09 & 443 \\ 8.90 & 714 \\ 157 \\ 1.09 & 285 \\ 8.90 & 872 \\ 156 \\ 1.08 & 971 \\ 1.09 & 128 \\ 8.91 & 028 \\ 156 \\ 1.08 & 971 \\ 1$	9.99 860 24 9.99 859 23 9.99 858 22 9.99 857 21	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
41 42 43 44	$\begin{array}{c} 8.91 \ 040 \ 154 \\ 8.91 \ 195 \ 154 \\ 8.91 \ 349 \ 153 \\ 8.91 \ 502 \ 153 \\ 8.91 \ 655 \ 157 \end{array}$	$ \begin{array}{c}       8.91 \\       8.91 \\       340 \\       155 \\       1.08 \\       660 \\       8.91 \\       495 \\       154 \\       1.08 \\       55 \\       1.08 \\       1.08 \\       55 \\       1.08 \\       55 \\       1.08 \\       1.08 \\       55 \\       1.08 \\       1.08 \\       55 \\       1.08 \\       1.08 \\       55 \\       1.08 \\       1.08 \\       55 \\       1.08 \\       1.08 \\       1.08 \\       55 \\       1.08 \\   $	$\begin{array}{r} 9.99 \ 855 \ 19 \\ 9.99 \ 853 \ 18 \\ 9.99 \ 852 \ 17 \\ 9.99 \ 851 \ 16 \end{array}$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$
47 48 49	$\begin{array}{c} 8 \cdot 91 & 807 & 151 \\ 8 \cdot 91 & 959 & 151 \\ 8 \cdot 92 & 110 & 150 \\ 8 \cdot 92 & 261 & 150 \\ 8 \cdot 92 & 411 & 150 \\ 8 \cdot 92 & 411 & 150 \end{array}$	$\begin{array}{c c c c c c c c c c c c c c c c c c c $	$\begin{array}{r} 9.99\ 84\bar{9}\ 14\\ 9.99\ 84\bar{8}\ 13\\ 9.99\ 84\bar{7}\ 12\\ 9.99\ 84\bar{6}\ 11 \end{array}$	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$
51 52 53 54	$\begin{array}{c} 8.92 561 149 \\ 8.92 710 148 \\ 8.92 858 148 \\ 8.93 007 147 \\ 8.93 154 147 \\ 147 \\ 147 \\ 147 \\ 147 \end{array}$	$\begin{array}{c} 3.92 & 715 & 150 & 1.07 & 284 \\ 8.92 & 866 & 149 & 1.07 & 134 \\ 8.93 & 015 & 149 & 1.06 & 984 \\ 8.93 & 164 & 149 & 1.06 & 835 \\ 8.93 & 313 & 149 & 1.06 & 686 \end{array}$	$\begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	
56 57 58 59	$\begin{array}{c} 8.93 & 301 \\ 8.93 & 448 \\ 146 \\ 8.93 & 594 \\ 8.93 & 740 \\ 8.93 & 885 \\ 8.93 & 885 \\ 147 \end{array}$	$\begin{array}{c} 8 \cdot 93 \ 461 \\ 8 \cdot 93 \ 609 \\ 147 \\ 1 \cdot 06 \ 390 \\ 8 \cdot 93 \ 609 \\ 147 \\ 1 \cdot 06 \ 390 \\ 146 \\ 1 \cdot 06 \ 97 \\ 8 \cdot 93 \ 903 \\ 146 \\ 1 \cdot 06 \ 97 \\ 8 \cdot 94 \ 049 \\ 146 \\ 1 \cdot 05 \ 950 \end{array}$	$\begin{array}{c ccccc} 9.99&839&4\\ 9.99&837&3\\ 9.99&836&2\\ 9.99&835&1\\ \hline \end{array}$	$ \begin{array}{c} 0 & 14 \cdot 0 & 14 \cdot 3 & 0 \cdot 1 & 0 \cdot 1 & 0 \cdot 0 \\ 7 & 17 \cdot 0 & 16 \cdot 9 & 0 \cdot 2 & 0 \cdot 1 & 0 \cdot 0 \\ 8 & 19 \cdot 4 & 19 \cdot 3 & 0 \cdot 2 & 0 \cdot 1 & 0 \cdot 0 \\ 9 & 21 \cdot 9 & 21 \cdot 7 & 0 \cdot 2 & 0 \cdot 1 & 0 \cdot 1 \\ 10 & 24 \cdot 3 & 24 \cdot 1 & 0 \cdot 2 & 0 \cdot 1 & 0 \cdot 1 \\ 20 & 48 \cdot 6 & 48 \cdot 3 & 0 \cdot 5 & 0 \cdot 3 & 0 \cdot 1 \\ 30 & 73 \cdot 0 & 72 \cdot 5 & 0 \cdot 7 & 0 \cdot 5 & 0 \cdot 2 \\ 40 & 97 \cdot 3 & 96 \cdot 6 & 1 \cdot 0 & 0 \cdot 6 & 0 \cdot 3 \\ 50 & 121 \cdot 6 & 120 \cdot 8 & 1 \cdot 2 & 0 \cdot 8 & 0 \cdot 4 \\ \end{array} $
<u>60</u>	$\frac{8.94\ 029}{\text{Log. Cos.}} \frac{144}{\text{d.}}$	$\frac{8.94\ 195}{\text{Log. Cot.}} \frac{145}{\text{c.d.}} \frac{1.05\ 805}{\text{Log. Tan}}$	Transferrer Statement and Statement	P. P.
~				0.59

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# TABLE VII.—LOGARITHMIC SINES, COSINES, TANGENTS, AND COTANGENTS.

<b>5</b> °			515	A TT	L	001	AN	D C	OTA			S. 174°
7	Log. S	Sin.	d.	Log.	Tan.	lc.d.	Log	Cot.	Log.	Cos.	1	P. P.
0	8.94 0	00ā		8.94	195	1003000000	A CONTRACTOR	805		834	60	145 144 143 142 141
$\frac{1}{2}$	8.941 8.943	74 i	40 I	8.94 8.94	34Ō	$145 \\ 144 $	1.05		9.99	833	59	6 14.5 14.4 14.3 14.2 14.1
3 4	8.94 4 8.94 6	160 +	풍앙	8.94 8.94	629	$\frac{14\overline{4}}{144}$	1.05	37 <u>0</u>	9.99	831	57	8 19.3 19.2 19.0 18.9 18.8
5	8.94 7	745 1	42	8.94	917	$\frac{14\bar{3}}{14\bar{2}}$	1.05	083	9.99	829	55	$10 \ 24 \cdot 1 \ 24 \cdot 0 \ 23 \cdot 8 \ 23 \cdot 6 \ 23 \cdot 5$
67	8.94 8 8.95 0		4.7.1	8.95 8.95	059 202	142	$1.04 \\ 1.04$				54 53	20 48.3 48.0 47.6 47.3 47.0 30 72.5 72.0 71.5 71.0 70.5
8 9	8.95 1 8.95 3	169 †	41 40	8.95 8.95 8.95	344 485	$\begin{array}{c}142\\141\end{array}$	1.04	656	9.99 9.99	825	52 51	30 72.5 72.0 71.5 71.0 70.5 40 96.6 96.0 95.3 94.6 94.0 50 120.8 120.0 119.1 118.3 117.5
10	8.95 4	150 1	쐶	8.95	626	$\begin{array}{c}141\\141\end{array}$	1.04	373	9.99	823	50	140 139 138 137 136
$     11 \\     12   $	8.95 5 8.95 7	728 1	38	8.95 8.95	907	$140 \\ 140$	$1.04 \\ 1.04$	$09\overline{2}$	9.99 9.99	821	49 48	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
$13 \\ 14$	8.95 8 8.96 0	$\frac{507}{005}$	38	8.96 8.96		139	1.03 1.03	952 813	9.99 9.99		47 46	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
$15 \\ 16$	8.96 1 8.96 2	1301	0/1	8.96 8.96	ARA	190	$1.03 \\ 1.03$		$9.99 \\ 9.99$		$\frac{45}{44}$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$
$\overline{17}$ 18	8.96 4 8.96 5	171	38	8-96 8-96	602	137	$1.03 \\ 1.03$	398	$9.99 \\ 9.99$	815	$\frac{43}{42}$	30 70.0 69.5 69.0 68.5 68.0
<u>19</u>	8.96 6	389	2	8.96	876	137 137	1.03	123	9.99	813	41	40 93.3 92.6 92.0 91.3 90.6 50 116.6 115.8 115.0 114.1 113.3
$\frac{20}{21}$	8.96 8 8.96 9			8.97 8.97	$149 \\ 149$	138	$1.02 \\ 1.02$	85 <b>0</b>		811 810	40 39	135 134 133 132 6  13.5  13.4  13.3  13.2
22 23	8-97 0 8-97 2	$\frac{194}{229}$	34 34	8.97 8.97 8.97	285 421	195	$1.02 \\ 1.02$	579	9.99 9.99	808	38 37	7 15.7 15.6 15.5 15.4
2 <u>4</u> 25	8.973 8.974	863	33	<u>8.97</u> 8.97	5561		$\frac{1.02}{1.02}$	and the second s	9.99 9.99	807 805	<u>36</u> 35	9 20.2 20.1 19.9 19.8
26 27	8.97 6		32 32	8.97 8.97	825	700	1.02 1.02	175	9.99 9.99	804	34 33	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
28 29	8.97 8 8.98 0	94 t	32	8.98 8.98	092	$133 \\ 133$	1.01	908	9.99 9.99	802	32 31	30 67.5 67.0 66.5 66.0 40 90.0 89.3 88.6 88.0 50 112.5 111.6 110.8 110.0
30	8.98 1	57 1	31	8.98	357		1.01	$64\overline{2}$	9.99	799	30	
31 32	8.98 2 8.98 4		30	8.98 8.98	490 621		1.01 1.01	3781	9.99 9.99	798 797	29 28	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
33 34	8.98 5 8.98 6	79 1	30	8.98 8.98	884	T31	1.01 1.01	$\begin{array}{c} 247 \\ 116 \end{array}$	9.99 9.99	$796 \\ 794$	27 26	$\begin{array}{cccccccccccccccccccccccccccccccccccc$
	8.98 8 8.98 9		29	8.99 8.99	145	130	$1.00 \\ 1.00$		9.99 9.99	793	25 24	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
	8.99 0 8.99 1		$28 \\ 28$	8.99 8.99	275	129	1.00 1.00 1.00	725	9.99	791 789	23 22	20 43.6 43.3 43.0 42.6
39	8.99 3	322	27	8.99	533	129	1.00	466	9.99	788	21	30 65.5 65.0 64.5 64.0 40 87.3 86.6 86.0 85.3 50 109.1 108.3 107.5 106.6
<b>40</b> 41	8.994 8.995	577	27	8.99 8.99	791		$1.00 \\ 1.00$	209	9.99		20 19	127 126 125 124 123
42 43	8.997 8.998	30 1	00	8.99 9.00	919	1081	1.00 0.99	081 953	9.99 9.99	784 783	18 17	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
4 <u>4</u> 45	8.99 9 9.00 0		25	9.00 9.00	1/4	126	0.99 0.99	Statistics.		782 781	$\frac{16}{15}$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
46 47	9.00 2 9.00 3		25 25	9.00 9.00	427	120	0.99	57 <u>3</u>	9.99	779	14	$\begin{array}{cccccccccccccccccccccccccccccccccccc$
48	9.00 4 9.00 5	156 1	24	9.00	679	12일	0.99	321	9.99	777		$\begin{array}{cccccccccccccccccccccccccccccccccccc$
$\frac{49}{50}$	9.00 7	704 1	24	9.00	930	125	0.99	070	<u>9.99</u> 9.99	776 774	$\frac{11}{10}$	50 105.8 105.0 104.1 103.3 102.5
51 52	9.00 8 9.00 9		23	9.01 9.01	179		0.98 0.98	821	9.99 9.99	773 772	9 8	122 121 120 T 1 0
53 54	9.01 0 9.01 1	1981	$22 \\ 22$	9.01 9.01	303	$124 \\ 124$	0.98 0.98	697		770 769	7 6	$ \begin{bmatrix} 12.2 \\ 2 \\ 12.2 \\ 14.2 \\ 14.1 \\ 14.0 \\ 0.2 \\ 0.1 \\ 0.2 \\ 0.1 \\ 0.0 \\ 0.2 \\ 0.1 \\ 0.0 $
55 56	9.01 3 9.01 4	318 1	$\frac{22}{22}$	9.01 9.01	550	$\frac{123}{123}$	0.98	450	9.99	76 <u>8</u>	54	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$
57	9.01 5	561 +	31	9.01	796	102	0.98	204		76 <u>6</u> 765	3	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$
58 59	9.01 8 9.01 8	803 1	20 20	9.01 9.02	040	122		959	$9.99 \\ 9.99$	764 763	$\frac{2}{1}$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$
<u>60</u>	<u>9.01</u> Log. (	540	d.	$\frac{9.02}{100}$	162 Cot.	12Ī	0.97 Log.	838 Tan.			<u> </u>	50 101.6 100.8 100.0 1.2 0.8 0.4 P. P.
-	1-°5' (		"'	- 5	000	1	1-08	1 ani	1-05	0		I

### TABLE VII.—LOGARITHMIC SINES, COSINES, TANGENTS, AND COTANGENTS.

0						-						
-	Log.	Sin.					Log.	Cot.	Log.	Cos.		P. P.
101234 56789	9.01 9.02 9.02 9.02 9.02 9.02 9.02 9.02 9.02	043 163 282 401 520 638 756	119 119 118 118 118	9.02 9.02 9.02 9.02 9.02 9.02 9.02 9.02	645 765 885 004 123	$12\overline{0}$ 120 $11\overline{9}$ $11\overline{9}$ $11\overline{9}$ $11\overline{9}$	0.97 0.97 0.97 0.97 0.97 0.97 0.97 0.96 0.96	716 595 475 354 234 115 995 876	19.99	753 752 750	60 59 58 57 56 55 55 54 53 52	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
90123456789	9.02 9.03 9.03 9.03 9.03 9.03 9.03 9.03 9.03	992 109 225 342 458 574 689 805 919 034	114 114 114 114	9.03 9.03 9.03 9.03 9.03 9.03 9.03 9.04 9.04 9.04 9.04	242 361 479 597 714 831 948	110 110 110 110 115	0.96 0.96 0.96 0.96 0.96 0.96 0.95 0.95 0.95	757 639 521 403 285 168 935 935 818	9.99 9.99 9.99 9.99 9.99 9.99 9.99 9.9	748 745 745 742 742 742 742 742 742 742 742 742 739 739 739 739	49 48 47 46 45 44 43 42	$\begin{array}{c} 117 \ 117 \ 116 \ 115 \\ 6 \ 11.7 \ 11.7 \ 11.6 \ 11.5 \\ 7 \ 13.7 \ 13.6 \ 13.5 \ 13.4 \\ 8 \ 15.6 \ 15.6 \ 15.4 \ 15.3 \\ 9 \ 17.6 \ 17.5 \ 17.4 \ 17.2 \\ 10 \ 19.6 \ 19.5 \ 19.3 \ 19.1 \end{array}$
20 22 22 23 24 256 27 89	9.04 9.04 9.04 9.04 9.04 9.04 9.05 9.05 9.05	262 376 489 602 715 828 940 052 163 275	$ \begin{array}{c} 114\\ 113\\ 113\\ 113\\ 113\\ 112\\ 112\\ 112\\ 112$	9.04 9.04 9.04 9.04 9.05 9.05 9.05 9.05	528 643 758 872 987 101 214 327 440 553		0.95 0.95 0.95 0.95 0.95 0.95 0.94 0.94	47 5 35 5 24 5 12 5 01 1 89 1 89 1 78 1 67 1 55 1 44	9.99 9.99 9.99 9.99 9.99 9.99 9.99 9.9	9 734 9 732 9 731 9 730 9 725 9 725 9 725 9 725 9 725 9 725 9 721	40 39 38 37 36 37 35 34 33 32 31	$\begin{array}{c} \textbf{114} \textbf{114} \textbf{113} \textbf{112} \textbf{111} \\ \textbf{6}   1.4 \\ \textbf{11.4}   1.1.4 \\ \textbf{11.3}   1.2 \\ \textbf{11.5}   1.2 \\ \textbf{11.5}   1.2 \\ \textbf{11.5}   1.5 \\ 1$
30 31 32 83 84 35 36 37 38 39	9.06	496 607 717 827 936 046 155 264 373	110 110 110 109 109 109 109 109 109 109	9.06 9.06 9.06 9.06 9.06 9.06	778 890 113 224 335 445 555 665		0.94	4 222 4 110 3 999 3 88 3 779 3 66 3 55 3 66 3 55 3 44 3 33	7 9.99 5 9.99 5 9.99 4 9.99 4 9.99	9718 9717 9717 9714 9714 9714 9714 9714 9714	29 28 27 26 27 26 25 25 25 24 23 22 23 22 21	$\begin{array}{c} \textbf{110} \ \textbf{110} \ \textbf{109} \ \textbf{108} \\ \textbf{6} \\ \textbf{[1.0]} \ \textbf{11.0} \ \textbf{10.9} \ \textbf{10.8} \\ \textbf{7} \\ \textbf{12.9} \ \textbf{12.8} \ \textbf{12.7} \ \textbf{12.6} \\ \textbf{8} \ \textbf{14.7} \ \textbf{14.6} \ \textbf{14.5} \ \textbf{14.4} \\ \textbf{9} \ \textbf{16.6} \ \textbf{16.5} \ \textbf{16.3} \ \textbf{16.2} \\ \textbf{10} \ \textbf{18.4} \ \textbf{18.3} \ \textbf{18.1} \ \textbf{18.0} \\ \textbf{20} \ \textbf{36.6} \ \textbf{36.6} \ \textbf{36.6} \ \textbf{36.3} \ \textbf{36.0} \\ \textbf{30} \ \textbf{55.2} \ \textbf{55.0} \ \textbf{55.5} \ \textbf{54.0} \\ \textbf{40} \ \textbf{73.6} \ \textbf{73.3} \ \textbf{72.6} \ \textbf{72.0} \\ \textbf{50} \ \textbf{90.0} \end{array}$
40 41 42 43 44 45 46 47 48 49 50	9.06 9.06 9.06 9.07 9.07 9.07	588 696 803 910 124 230 336 442	108 107 107 107 107 106 106 106 106	9.00 9.00 9.00 9.07 9.07 9.07 9.07 9.07	884 994 102 21] 319 428 535 643 750		0.92	3 11 3 00 2 89 2 78 2 680 2 57 2 57 2 57 2 57 2 57 2 57 2 57 2 57	9.99	9 704 9 702 9 701 9 693 9 695 9 695 9 695	19 18 17 16 15 14 13 12 11	$\begin{array}{c} 107 \\ 107 \\ 107 \\ 10.7 \\ 10.7 \\ 10.7 \\ 10.7 \\ 10.7 \\ 10.7 \\ 10.7 \\ 10.5 \\ 12.5 \\ 12.5 \\ 12.5 \\ 12.3 \\ 12.2 $
51 52 53 54 55 56 57 58 59 <b>60</b>	9.07 9.07 9.07 9.08 9.08 9.08 9.08 9.08 9.08 9.08 9.08	653 758 863 967 072 176 279 383 486	$   \begin{array}{r}     10\overline{4} \\     10\underline{3} \\   \end{array} $	9.07 9.08 9.08 9.08 9.08 9.08 9.08 9.08 9.08	964 071 177 283 389 494 600 705 810 914		0.92 0.91 0.91 0.91 0.91 0.91 0.91 0.91 0.91	035 929 822 716 611 505 400 295 190 085	9.99 9.99 9.99 9.99 9.99 9.99 9.99 9.9	689 687 686 684 683 683 679 678 676 675	9	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
-		5051	<u> </u>	-vg		1.1.1		· ani	5.	5		

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 TABLE VII.—LOGARITHMIC SINES, COSINES, TANGENTS,

 AND COTANGENTS.

-	,		ind (	JOINIGEN IS	172
	Log. Sin.	d. Log. Tan	c.d. Log. C	ot. Log. Cos.	P. P.
01234 56789	$\begin{array}{c} 9.08 58\bar{9}\\ 9.08 692\\ 9.08 794\\ 9.08 897\\ 9.08 999\\ 9.09 101\\ 9.09 20\bar{2}\\ 9.09 30\bar{3}\\ 9.09 404\\ 9.09 50\bar{5} \end{array}$	$\begin{array}{c c c c c c c c c c c c c c c c c c c $	$\begin{array}{c} 104 \\ 0.90 \\ 9 \\ 103 \\ 0.90 \\ 7 \\ 103 \\ 0.90 \\ 103 \\ 0.90 \\ 103 \\ 0.90 \\ 103 \\ 0.90 \\ 103 \\ 102 \\ 0.90 \\ 0.90 \\ 102 \\ 0.90 $	639.9966554 609.9966453 589.9966252	$\begin{array}{c} 104 \ 103 \ 102 \ 101 \\ 6 10.4 10.3 10.2 10.1 \\ 7 12.1 12.0 11.9 11.8 \\ 8 13.8 13.7 13.6 13.4 \\ 9 15.6 15.4 15.8 15.1 \\ 10 17.3 17.1 17.0 16.8 \\ 20 34.6 34.3 34.0 33.6 \\ 30 52.0 51.5 51.0 50.5 \\ 40 69.3 68.6 68.0 67.5 \end{array}$
$\frac{19}{20}$	$\begin{array}{c} 9.09 & 606\\ 9.09 & 706\\ 9.09 & 806\\ 9.09 & 906\\ 9.10 & 106\\ 9.10 & 105\\ 9.10 & 205\\ 9.10 & 303\\ 9.10 & 303\\ 9.10 & 402\\ 9.10 & 501\\ 9.10 & 599\\ 9.10 & 697\\ 9.10 & 697\\ \end{array}$	$\begin{array}{c} 100\\ 9 \\ 99\\ 99\\ 99\\ 90\\ 99\\ 90\\ 90\\ 90\\ $	$ \begin{array}{c} 101 \\ 102 \\ 103 \\ 101 \\ 0.89 \\ 101 \\ 0.89 \\ 74 \\ 101 \\ 0.89 \\ 64 \\ 101 \\ 0.89 \\ 64 \\ 101 \\ 0.89 \\ 64 \\ 101 \\ 0.89 \\ 64 \\ 100 \\ 0.89 \\ 14 \\ 100 \\ 0.89 \\ 14 \\ 100 \\ 0.89 \\ 14 \\ 100 \\ 0.89 \\ 0.$	$\begin{array}{c} 48 & 9 \cdot 99 & 654 & 47 \\ 47 & 9 \cdot 99 & 653 & 46 \\ 46 & 9 \cdot 99 & 651 & 45 \\ 45 & 9 \cdot 99 & 650 & 44 \\ 44 & 9 \cdot 99 & 648 & 43 \\ 44 & 9 \cdot 99 & 646 & 42 \\ 44 & 9 \cdot 99 & 645 & 41 \\ \end{array}$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
22 23 24 25 26 27 28 29 31 32 33 32 33 4	$\begin{array}{c} 9 & 10 & 795\\ 9 & 10 & 892\\ \hline 9 & 10 & 892\\ 9 & 10 & 87\\ 9 & 11 & 184\\ 9 & 11 & 281\\ 9 & 11 & 281\\ 9 & 11 & 377\\ \hline 9 & 11 & 473\\ 9 & 11 & 570\\ 9 & 11 & 655\\ 9 & 11 & 761\\ 9 & 11 & 856\\ 9 & 11 & 952\\ \end{array}$	$\begin{array}{c} 9.11 \\ 9.11 \\ 9.7 \\ 9.11 \\ 254 \\ 9.7 \\ 9.11 \\ 254 \\ 9.7 \\ 9.11 \\ 455 \\ 0.11 \\ 550 \\ 9.7 \\ 9.11 \\ 550 \\ 9.11 \\ 747 \\ 9.5 \\ 9.11 \\ 9.11 \\ 9.5 \\ 9.11 \\ 9.11 \\ 9.5 \\ 9.11 \\ 9.12 \\ 1.00 \\ 1$	$\begin{array}{c} \begin{array}{c} 0.88 & 84\\ 99 & 0.88 & 74\\ 99 & 0.88 & 64\\ 98 & 0.88 & 54\\ 98 & 0.88 & 54\\ 98 & 0.88 & 54\\ 98 & 0.88 & 25\\ 98 & 0.88 & 25\\ 98 & 0.88 & 25\\ 98 & 0.88 & 25\\ 98 & 0.88 & 25\\ 97 & 0.87 & 86\\ 97 & 0.87 & 66\\ 96 & 0.87 & 0.88 & 0\\ 96 & 0.88 & 0\\ 98 & 0.8$	$\begin{array}{c} \underline{15} 9 \cdot 99 \cdot 640 \\ \underline{15} 9 \cdot 99 \cdot 638 \\ \underline{15} 9 \cdot 99 \cdot 638 \\ \underline{15} 9 \cdot 99 \cdot 635 \\ \underline{15} 9 \cdot 99 \cdot 635 \\ \underline{15} 9 \cdot 99 \cdot 633 \\ \underline{15} 9 \cdot 99 \cdot 633 \\ \underline{15} 9 \cdot 99 \cdot 632 \\ \underline{15} 9 \cdot 99 \cdot 630 \\ \underline{15} 9 \cdot 99 \cdot 628 \\ \underline{29} 9 \cdot 99 \cdot 622 \\ \underline{26} 9 \cdot 99 \cdot 622 \\ \underline{26} 9 \cdot 99 \cdot 622 \\ \underline{26} \end{array}$	$\begin{array}{c} 30 & 67 \cdot 0 & 66 \cdot \overline{6} & 66 \cdot 0 & 65 \cdot \overline{3} \\ 50 & 83 \cdot 7 & 83 \cdot 8 & 82 \cdot 5 & 81 \cdot 6 \\ \hline 97 & 97 & 96 & 95 \\ 6 & 9 \cdot 7 & 9 \cdot 7 & 9 \cdot 6 & 9 \cdot 5 \\ 7 & 11 \cdot 4 & 11 \cdot 2 & 11 \cdot 1 \\ 8 & 13 \cdot 0 & 12 \cdot 9 & 12 \cdot 8 & 12 \cdot 6 \\ 9 & 14 \cdot 6 & 14 \cdot 5 & 14 \cdot 4 & 14 \cdot 2 \\ 10 & 16 \cdot 2 & 16 \cdot 1 & 16 \cdot 0 & 15 \cdot 8 \\ 20 & 32 \cdot 5 & 32 \cdot 3 & 32 \cdot 0 & 31 \cdot 6 \\ 30 & 48 \cdot 7 & 48 \cdot 5 & 48 \cdot 0 & 47 \cdot 5 \\ 40 & 66 \cdot 2 & 16 \cdot 6 & 4 \cdot 0 & 63 \cdot 3 \\ 50 & 81 \cdot 2 & 80 \cdot 80 & 0 & 079 \cdot 1 \\ \end{array}$
86 37 38 39 40 41 42 43 44 45 46 47	$\begin{array}{c} 9.12\ 047\\ 9.12\ 141\\ 9.12\ 236\\ 9.12\ 330\\ 9.12\ 330\\ 9.12\ 425\\ 9.12\ 518\\ 9.12\ 612\\ 9.12\ 706\\ 9.12\ 706\\ 9.12\ 706\\ 9.12\ 892\\ 9.12\ 892\\ 9.12\ 892\\ 9.12\ 85\\ 9.13\ 078\\ 9.13\ 170\\ 9.13\ 263\\ \end{array}$	9.12 4225 9.4499.12 6217 9.94499.12 6217 9.94499.12 6217 9.12 813 9.12 813 9.913 0.994 9.933 9.12 806 9.933 9.13 0.994 9.933 9.13 1946 9.933 9.13 384 9.933 9.13 384 9.13 384 9.14 394 9.14 394	$\begin{array}{c} 96 \\ 0.87 \\ 96 \\ 0.87 \\ 47 \\ 96 \\ 0.87 \\ 47 \\ 96 \\ 0.87 \\ 47 \\ 96 \\ 0.87 \\ 47 \\ 18 \\ 95 \\ 0.86 \\ 99 \\ 95 \\ 0.86 \\ 99 \\ 95 \\ 0.86 \\ 90 \\ 95 \\ 0.86 \\ 91 \\ 0.86 \\ 10 \\ 94 \\ 0.86 \\ 52 \\ 94 \\ 0.86 \\ 87 \\ 94 \\ 0.86 \\ 87 \\ 94 \\ 0.86 \\ 87 \\ 94 \\ 0.86 \\ 87 \\ 94 \\ 0.86 \\ 87 \\ 94 \\ 0.86 \\ 87 \\ 94 \\ 0.86 \\ 87 \\ 94 \\ 0.86 \\ 87 \\ 94 \\ 0.86 \\ 87 \\ 87 \\ 87 \\ 87 \\ 87 \\ 87 \\ 87 \\ $	$\begin{array}{c} 759 \cdot 99 \cdot 617 & 24\\ 79 \cdot 9 \cdot 99 \cdot 615 & 23\\ 33 \cdot 99 \cdot 613 & 22\\ 37 \cdot 9 \cdot 99 \cdot 611 & 21\\ 91 \cdot 9 \cdot 99 \cdot 610 & 20\\ 96 \cdot 9 \cdot 99 \cdot 606 & 18\\ 95 \cdot 9 \cdot 99 \cdot 606 & 18\\ 95 \cdot 9 \cdot 99 \cdot 605 & 17\\ 10 \cdot 9 \cdot 99 \cdot 605 & 16\\ 10 \cdot 9 \cdot 99 \cdot 601 & 15\\ 31 \cdot 9 \cdot 99 \cdot 600 & 14\\ 10 \cdot 9 \cdot 90 \cdot 600 & 14\\ 10 \cdot 9 \cdot 90 \cdot 90 \cdot 90 \cdot 90 & 14\\ 10 \cdot 9 \cdot 90 \cdot 90 \cdot 90 \cdot 90 & 14\\ 10 \cdot 9 \cdot 90 \cdot 90 \cdot 90 \cdot 90 & 14\\ 10 \cdot 9 \cdot 90 \cdot 90 \cdot 90 \cdot 90 & 14\\ 10 \cdot 9 \cdot 90 \cdot 90 \cdot 90 \cdot 90 & 14\\ 10 \cdot 9 \cdot 90 \cdot 90 \cdot 90 \cdot 90 & 14\\ 10 \cdot 9 \cdot 90 \cdot 90 \cdot 90 \cdot 90 & 14\\ 10 \cdot 9 \cdot 90 \cdot 90 \cdot 90 \cdot 90 & 14\\ 10 \cdot 9 \cdot 90 \cdot 90 \cdot 90 & 14\\ 10 \cdot 9 \cdot 90 \cdot 90 \cdot 90 \cdot 90 & 14\\ 10 \cdot 9 \cdot 90 \cdot 90 \cdot 90 \cdot 90 + 14\\ 10 \cdot 9 \cdot 90 \cdot 90 \cdot 90 + 14\\ 10 \cdot 9 \cdot 90 \cdot 90 \cdot 90 + 14\\ 10 \cdot 9 \cdot 90 \cdot 90 \cdot 90 + 14\\ 10 \cdot 9 \cdot 90 \cdot 90 \cdot 90 + 14\\ 10 \cdot 9 \cdot 90 \cdot 90 \cdot 90 + 14\\ 10 \cdot 9 \cdot 90 $	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
<b>49</b> <b>50</b> <b>51</b> <b>523</b> <b>54</b> <b>56</b> <b>57</b> <b>58</b> <b>59</b> <b>60</b>		$\begin{array}{c} 92 \\ 9 \\ 9 \\ 9 \\ 9 \\ 9 \\ 1 \\ 9 \\ 1 \\ 9 \\ 1 \\ 9 \\ 1 \\ 9 \\ 1 \\ 9 \\ 1 \\ 9 \\ 1 \\ 9 \\ 1 \\ 9 \\ 1 \\ 9 \\ 1 \\ 1$	$\begin{array}{c} 0.86 \\ 29\\ 993\\ 0.86 \\ 14\\ 93\\ 0.85 \\ 93\\ 0.85 \\ 93\\ 0.85 \\ 93\\ 0.85 \\ 93\\ 0.85 \\ 93\\ 0.85 \\ 93\\ 0.85 \\ 93\\ 0.85 \\ 43\\ 92\\ 0.85 \\ 43\\ 0.85 \\ 10\\ 0.85 \\ 1$	$\begin{array}{c} \underline{39} 9 \cdot 99 \cdot 594 \\ \underline{11} \\ \underline{16} 9 \cdot 99 \cdot 593 \\ \underline{52} 9 \cdot 99 \cdot 593 \\ \underline{52} 9 \cdot 99 \cdot 591 \\ \underline{92} 9 \cdot 99 \cdot 585 \\ \underline{56} 9 \cdot 99 \cdot 586 \\ \underline{56} 9 \cdot 99 \cdot 576 \\ \underline{56} 9 \cdot 99 \cdot 575 \\ \underline{56} 9 \cdot $	9 <b>T</b> 91 90 2 <b>T</b> $6 9\cdot1 9\cdot1 9\cdot0 0\cdot2 0\cdot1 $ $7 10\cdot7 10\cdot6 10\cdot5 0\cdot2 0\cdot2 0\cdot2 $ $8 12\cdot2 12\cdot1 12\cdot0 0\cdot2 0\cdot2 0\cdot2 $ $9 13\cdot7 13\cdot6 13\cdot5 0\cdot3 0\cdot2 0\cdot2 $ $10 15\cdot2 15\cdot1 15\cdot0 0\cdot3 0\cdot2 $ $20 30\cdot5 30\cdot3 30\cdot0 0\cdot6 0\cdot5 $ $30 45\cdot7 45\cdot5 45\cdot0 1\cdot0 0\cdot7 $ $40 6 1\cdot0 60\cdot6 60\cdot0 1\cdot3 1\cdot0 $ $50 76\cdot2 75\cdot8 75\cdot0 1\cdot6 1\cdot2 $ P. P.
	Log. Cos.	d. Log. Cot.	c.d. Log. Ta	in. Log. Sin.	

## TABLE VII.—LOGARITHMIC SINES, COSINES, TANGENTS, AND COTANGENTS.

72 5	TAB	LE	VII.—LU	GAI			TAN(	IES. IFN		SINES, TANGEN1S, 171°
P				, 1	AND				1.0.	
+	Log. Sin.	d.	Log. Tan.	c.d.	Log.	Cot.	Log.	Cos.		P. P.
	9.14355	90	9.14 780	9Ī	0.85	219	9.99	575	60	
	9.14445 9.14535	<b>8</b> 9	$9.14872 \\ 9.14963$	91	$0.85 \\ 0.85$	$128 \\ 037$	9.99 9.99	573 571	59 58	9 <u>1</u> 91 90 89
3	$9.1462\bar{4}$	89 89	$9.1505\overline{4}$	91 91	0.84	945	9.99	570	57	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
4	9.14 713	89	9.15145	91			9.99		56	
5	$9.1480\overline{2}$ $9.1489\overline{1}$	89	$9.15\ 23\overline{6}\ 9.15\ 327$	9 <u>0</u>	0 · 84 0 · 84	673	9.99 9.99		55 54	$\begin{array}{c}9 \\ 13 \cdot 7 \\ 10 \\ 15 \cdot 2 \\ 15 \cdot 1 \\ 15 \cdot 0 \\ 14 \cdot 8 \\ \end{array}$
17	9.14 980	8 <u>8</u> 8 <u>8</u>	9.15 417	90 90	0.84	$58\bar{2}$	9.99	563	53	20 30 . 5 30 . 3 30 . 0 29 . 6
89	$9.1506\overline{8}$ 9.15157	88	9.15507 9.15598	9Ō	0.84 0.84		9.99 9.99	561 559	52 51	30 45 · 7 45 · 5 45 · 0 44 · 5 40 61 · 0 60 · 6 60 · 0 59 · 3 50 76 · 2 75 · 8 75 · 0 74 · <b>1</b>
1.0		88 88	$9.15 \ 68\overline{7}$	89 90	0.84 0.84	312	9.99		50	50 76.2 75.8 75.0 74. <b>1</b>
	9.15333 9.15421	88	9.15777 9.15867 9.15956		0.84	222	9.99 9.99	555 553	49 48	
1.3	9.15 508	87 87	$9.15\ 95\overline{6}$	89 89	$0.84 \\ 0.84$	043	9.99	552	47	00 00 0 <b>0</b> 00
.5	9.15595	87	9.16045	89	0.83		9.99		46	88 88 87 86 6  8 8  8 8  8 7  8 6 7 10 3 10 2 10 1 10 0
.5	9.15 683 9.15 770	87	$9.16\ 134{9}.16\ 223{1}$	89	0 · 83 0 · 83	865 776	9.99 9.99		45 44	7 10.3 10.2 10.1 10.0
.6	9.15 857	87 86	9.16 312	89 88	0.83	687	9.99	54 <u>4</u>	43	$\begin{array}{c} 8 & 11 \cdot 8 & 11 \cdot \overline{7} & 11 \cdot 6 & 11 \cdot \overline{4} \\ 9 & 13 \cdot 3 & 13 \cdot 2 & 13 \cdot \overline{0} & 12 \cdot 9 \end{array}$
.8 19	$9.1594\bar{3}9.16030$	86	9.16 401 9.16 489	88	0 · 83 0 · 83	511	9.99 9.99	542 541	42 41	$10   14 \cdot \overline{7}   14 \cdot \overline{6}   14 \cdot 5   14 \cdot \overline{3}$
20	$9.1611\overline{6}$	86 86	9.16577	88 88	0.83	422	9.99		40	$\begin{array}{c} 20 \\ 29 \\ \cdot 5 \\ 30 \\ 44 \\ \cdot 2 \\ 44 \\ \cdot 0 \\ 43 \\ \cdot 5 \\ 43 \\ \cdot 0 \\ \end{array} \begin{array}{c} 29 \\ \cdot 0 \\ 28 \\ \cdot \overline{6} \\ 30 \\ \cdot 43 \\ \cdot 0 $
21	$9.16\ 20\overline{2}$ $9.16\ 28\overline{8}$	86	9.16 665 9.16 753	87	0 · 83 0 · 83	334	9.99 9.99	537	39 38	40 59 · 0 58 · 6 58 · 0 57 · 3
22 23	9.16 374	8 <u>6</u> 85	9.16841	88 87	0.83	159	9.99	<u>533</u>	37	50 73.7 73.3 72.5 71.6
24	9.16460	85	$9.1692\overline{8}$	87	0.83		<u>9.99</u>		36	
25 26 27	9.16545 9.16630	85	9.17 015 9.17 103	87	0 · 82 0 · 82		9.99 9.99		35 34	$\begin{bmatrix} 8\overline{5} & 85 & 84 & 83 \\ 6 & 8 \cdot 5 & 8 \cdot 5 & 8 \cdot 4 & 8 \cdot 3 \end{bmatrix}$
27	9.16 716	85 85	9.17190	87 86	0.82	810	9.99	526	33	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
28 29	9.16 801 9.16 885	84	$9.17\ 27\overline{6}\ 9.17\ 36\overline{3}$	87	0 · 82 0 · 82		9.99 9.99			$\begin{array}{c c c c c c c c c c c c c c c c c c c $
30		84 84	9.17 450	86	0.82	550	9.99	52 <b>0</b>	30	$\begin{array}{c} 7 & 10.0 & 9.5 & 0.1 & 0.1 \\ 7 & 10.0 & 9.9 & 9.8 & 9.7 \\ 8 & 11.4 & 11.3 & 11.2 & 11.0 \\ 9 & 12.8 & 12.7 & 12.6 & 12.4 \\ 10 & 14.2 & 14.1 & 14.0 & 13.8 \\ 20 & 28.5 & 28.3 & 28.0 & 27.6 \\ 30 & 42.7 & 42.5 & 42.0 & 41.5 \\ 30 & 42.7 & 65.6 & 5 \end{array}$
30 31 32	$9.1705\overline{4}$ 9.17139	84	9.17 53 <u>6</u> 9.17 622	86 86	0.82	464	9.99 9.99	518	29 28	20 28 . 5 28 . 3 28 . 0 27 . 6
33	9.17 223	84 84	9.17 708	86 85	0.82 0.82	291	9.99	$51\overline{4}$	27	$30 42\cdot7 42\cdot5 42\cdot0 41\cdot5 40 57,0 56,6 56,0 55,3 $
34	9.17307	84	9.17794	86	0.82					20 28 5 28 3 28 0 27 6 30 42 7 42 5 42 0 41 5 40 57 0 56 6 56 0 55 3 50 71 2 70 8 70 0 69 1
35	$9.17391 \\ 9.17474$	83	9.17800 9.17965	85	0 · 82 0 · 82			509	$\frac{25}{24}$	
37	9.17 558	83 83	9.18 051 9.18 136	85 85	Ì0∙81	949	9.99		23	
38 39	$9.17641 \\ 9.17724$	83	9.18136 9.18221	85	0.81 0.81					$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
40	9.17 807	83 83	9.18 30 <u>6</u>	85	0.81	694	9.99		20	7 9.6 9.5 9.4 9.3
41 42	9.17 890 9.17 972	82	9.18 390 9.18 475	84 84 84	0.81	. 609 525	9.99 9.99	499	19 18	$\begin{array}{c} 8 \\ 11 \\ 0 \\ 12 \\ \cdot 4 \\ 12 \\ \cdot 3 \\ 12 \\ \cdot 1 \\ 12 \\ \cdot 4 \\ 12 \\ \cdot 3 \\ 12 \\ \cdot 1 \\ 12 \\ \cdot 1 \\ 12 \\ \cdot 0 \\ \end{array}$
43	9.18055	8 <u>2</u> 82	9.18 559	84 84	0.81	. 44Ō	9.99	495	17	$\begin{array}{c} 9 \\ 12 \\ 10 \\ 13 \\ 7 \\ 13 \\ 6 \\ 13 \\ 7 \\ 13 \\ 6 \\ 13 \\ 5 \\ 13 \\ 5 \\ 13 \\ 5 \\ 13 \\ 5 \\ 13 \\ 5 \\ 13 \\ 5 \\ 13 \\ 3 \\ 20 \\ 27 \\ 5 \\ 27 \\ 3 \\ 27 \\ 0 \\ 26 \\ 6 \\ 6 \end{array}$
44 45	9.18137 9.18219	82	<u>9.18 644</u> 9.18 728	84	0.81		<u>9.99</u> 9.99	-	$\frac{16}{15}$	$30 41\cdot2 41\cdot0 40\cdot5 40\cdot0$
46	$9.1830\overline{1}$	82	9.18 812	84	0.81	. 188	9.99	489	14	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
47 48	$9.1838\overline{3}$ 9.18465	82 81	9.18 89 <u>6</u> 9.18 979	84 83 83	0.81					30100.1100.3107.3100.0
49	9.18546	81	9.19063	83	0.80					
50	9.18 628	81 81	9.19146	8 <u>3</u> 83	0.80	854	9.99			79 2 1
51 52	9.18 709 9.18 790	81	9.19 22 <u>9</u> 9.19 312	83	0 · 80 0 · 80	) 687	9.99 9.99			$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
53	9.18 871	80 81	9.19 395	8 <u>3</u> 82	10 - 80	604 (	9.99	476	7	$8 10 \cdot 6 0 \cdot \overline{2} 0 \cdot 2$
54 55	_	8 <u>0</u>	<u>9.19478</u> 9.19560	82	0.80	_				$\begin{array}{c} 8 & 10 \cdot 90 \cdot 2 \\ 9 & 11 \cdot 90 \cdot 3 & 0 \cdot 2 \\ 10 & 13 \cdot 2 & 0 \cdot 3 & 0 \cdot 2 \\ 20 & 26 \cdot 5 & 0 \cdot 6 & 0 \cdot 5 \\ 30 & 39 \cdot 7 & 1 \cdot 0 & 0 \cdot 7 \\ 40 & 53 \cdot 0 & 1 \cdot 3 & 1 \cdot 0 \\ 50 & 66 \cdot 2 & 1 \cdot 6 & 1 \cdot 2 \end{array}$
56	9.19 113	80 80	9.19 643	82 82	0.80	357	9.99	470	4	20 26 . 50 . 60 . 5
57 58	$9.1919\overline{3}$ 9.19273	80	9.19 725 9.19 807	82	0.80		9.99 9.99			$\begin{array}{c} 30 \\ 30 \\ 40 \\ 53 \\ 0 \\ 1 \\ 1 \\ 1 \\ 1 \\ 1 \\ 1 \\ 1 \\ 1 \\ 1$
59		80 79	<u>9.19 889</u>	82 82	0.80	110	9.99	464	1	50 66 2 1 6 1 2
<u>6</u>			<u>9.19.97</u>	_	0.80	_	<u>9.99</u>	-	$\frac{0}{2}$	D D
_	Log. Cos.	d.	Log. Cot.	c.d.	Log.	ian.	Log.	Sin.		P. P.
-	-0									0

## TABLE VII.—LOGARITHMIC SINES, COSINES, TANGENTS, AND COTANGENTS.

9°       AND COTANGENTS.       17         '       Log. Sin. d. 9 · 19 433       Log. Tan. c. d. 9 · 19 592       Log. Tan. c. d. 9 · 19 592       Log. Cot. 9 · 19 · 10 · 10 · 10 · 10 · 10 · 10 · 1	<pre>' Log. Sin. 0 9.19 433 1 9.19 513 2 9.19 592 3 9.19 672 4 9.19 751</pre>
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	$\begin{array}{c}1 & 9 \cdot 19 & 513 \\2 & 9 \cdot 19 & 592 \\3 & 9 \cdot 19 & 672 \\4 & 9 \cdot 19 & 751\end{array}$
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{array}{c} 6 & 9 \cdot 19 \ 909 \\ 7 & 9 \cdot 19 \ 988 \\ 8 & 9 \cdot 20 \ 066 \\ \hline 9 & 9 \cdot 20 \ 145 \\ 10 \ 9 \cdot 20 \ 223 \\ 11 \ 9 \cdot 20 \ 301 \\ 12 \ 9 \cdot 20 \ 301 \\ 13 \ 9 \cdot 20 \ 375 \\ 15 \ 9 \cdot 20 \ 613 \\ 16 \ 613 \ 613 \\ 16 \ 613 \ 613 \\ 16 \ 613 $
	$\begin{array}{r} 28 & 9 \cdot 21 & 605 \\ 29 & 9 \cdot 21 & 685 \\ 30 & 9 \cdot 21 & 685 \\ 31 & 9 \cdot 21 & 836 \\ 32 & 9 \cdot 21 & 916 \\ 31 & 9 \cdot 21 & 836 \\ 32 & 9 \cdot 21 & 916 \\ 33 & 9 \cdot 21 & 916 \\ 34 & 9 \cdot 22 & 062 \\ 35 & 9 \cdot 22 & 1987 \\ 36 & 9 \cdot 22 & 216 \\ 36 & 9 \cdot 22 & 216 \\ 37 & 9 \cdot 22 & 236 \\ 39 & 9 \cdot 22 & 435 \\ 41 & 9 \cdot 22 & 509 \\ 51 & 9 \cdot 23 & 807 $

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TABLE VII.-LOGARITHMIC SINES, COSINES, TANGENTS, AND COTANGENTS.

-	TABL	ΞE	VII.—LO		AND CO	SINES		SINES, TANGENTS,
10					AND CO			169°
1	Log. Sin.	d.	Log. Tan.	c. d.	Log. Cot.	Log. Cos		P. P.
01234 56789	$\begin{array}{r} 9 \cdot 23 \ 967 \\ 9 \cdot 24 \ 038 \\ 9 \cdot 24 \ 110 \\ 9 \cdot 24 \ 181 \\ 9 \cdot 24 \ 252 \\ 9 \cdot 24 \ 323 \\ 9 \cdot 24 \ 323 \\ 9 \cdot 24 \ 323 \\ 9 \cdot 24 \ 394 \\ 9 \cdot 24 \ 536 \\ 9 \cdot 24 \ 607 \end{array}$	71 71 71 71 71 71 71 71 71	$\begin{array}{c} 9 \cdot 24 & 632 \\ 9 \cdot 24 & 705 \\ 9 \cdot 24 & 779 \\ 9 \cdot 24 & 853 \\ 9 \cdot 24 & 926 \\ 9 \cdot 25 & 000 \\ 9 \cdot 25 & 073 \\ 9 \cdot 25 & 146 \\ 9 \cdot 25 & 146 \\ 9 \cdot 25 & 292 \\ 9 \cdot 25 & 292 \end{array}$	73 74 73 73 73 73 73 73 73 73 73 73	$\begin{array}{c} 0.75 & 368 \\ 0.75 & 294 \\ 0.75 & 220 \\ 0.75 & 147 \\ 0.75 & 073 \\ 0.75 & 000 \\ 0.74 & 927 \\ 0.74 & 854 \\ 0.74 & 781 \\ 0.74 & 708 \\ \end{array}$	9.99333 9.99333 9.99333 9.99322 9.99322 9.99322 9.9932 9.9932 9.9931 9.9931 9.9931	59 58 57 56 55 55 53 52	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
10 11 12 13 14 15 16 17 18 19		70 70 70 70 70 70 70 70 70 70 70 70 70 7	$\begin{array}{c} 9.25 & 365\\ 9.25 & 437\\ 9.25 & 510\\ 9.25 & 582\\ 9.25 & 654\\ 9.25 & 727\\ 9.25 & 729\\ 9.25 & 799\\ 9.25 & 871\\ 9.25 & 871\\ 9.25 & 943\\ 9.26 & 014\\ \end{array}$	73 72 72 72 72 72 72 72 72 72 72 72 72 72	$\begin{array}{c} 0.74 \ 635\\ 0.74 \ 562\\ 0.74 \ 562\\ 0.74 \ 490\\ 0.74 \ 417\\ 0.74 \ 345\\ 0.74 \ 273\\ 0.74 \ 273\\ 0.74 \ 201\\ 0.74 \ 129\\ 0.74 \ 129\\ 0.74 \ 985\\ \end{array}$	9.9931 9.9931 9.9930 9.9930 9.9930 9.9930 9.9929 9.9929 9.9929 9.9929 9.9929 9.99292	49 48 47 46 45 44 43 42	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
20 21 22 23 24 25 26 27 28 29	$\begin{array}{r} 9 \cdot 25 & 376 \\ 9 \cdot 25 & 445 \\ 9 \cdot 25 & 514 \\ 9 \cdot 25 & 583 \\ 9 \cdot 25 & 652 \\ 9 \cdot 25 & 652 \\ 9 \cdot 25 & 721 \\ 9 \cdot 25 & 790 \\ 9 \cdot 25 & 858 \\ 9 \cdot 25 & 927 \\ 9 \cdot 25 & 995 \\ \end{array}$	69 69 69 69 69 60 60 60 60 60 60 60 60 60 60 60 60 60	$\begin{array}{c} 9 \cdot 26 & 086\\ 9 \cdot 26 & 158\\ 9 \cdot 26 & 229\\ 9 \cdot 26 & 300\\ 9 \cdot 26 & 371\\ 9 \cdot 26 & 371\\ 9 \cdot 26 & 514\\ 9 \cdot 26 & 5184\\ 9 \cdot 26 & 5585\\ 9 \cdot 26 & 555\\ 9 \cdot 26 & 726\\ 9 \cdot 26 & 726\\ \end{array}$	$\begin{array}{c} 72\\71\\71\\71\\71\\71\\70\\70\\70\\70\\70\\70\\70\\70\\70\\70\\70\\70\\70\\$	$\begin{array}{c} 0.73 & 91\overline{3} \\ 0.73 & 842 \\ 0.73 & 771 \\ 0.73 & 69\overline{9} \\ 0.73 & 62\overline{8} \\ 0.73 & 557 \\ 0.73 & 48\overline{6} \\ 0.73 & 41\overline{5} \\ 0.73 & 34\overline{4} \\ 0.73 & 274 \end{array}$	9.99 290 9.99 285 9.99 285 9.99 285 9.99 285 9.99 285 9.99 275 9.99 275 9.99 275 9.99 275 9.99 275 9.99 269	40 39 38 37 36 35 34	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
$     \begin{array}{r}       30 \\       31 \\       32 \\       33 \\       34 \\       35 \\       36 \\       37 \\       38 \\       39 \\       40 \\       40     \end{array} $	$9 \cdot 26 \ 131$ $9 \cdot 26 \ 199$ $9 \cdot 26 \ 267$ $9 \cdot 26 \ 335$ $9 \cdot 26 \ 402$ $9 \cdot 26 \ 470$ $9 \cdot 26 \ 537$ $9 \cdot 26 \ 672$ $9 \cdot 26 \ 72$	68 68 67 67 67 67 67 67 67 67	$\begin{array}{c} 9 \cdot 26 & 79\overline{6} \\ 9 \cdot 26 & 867 \\ 9 \cdot 26 & 937 \\ 9 \cdot 27 & 007 \\ 9 \cdot 27 & 078 \\ 9 \cdot 27 & 148 \\ 9 \cdot 27 & 218 \\ 9 \cdot 27 & 218 \\ 9 \cdot 27 & 357 \\ 9 \cdot 27 & 357 \\ 9 \cdot 27 & 49\overline{6} \\ \hline 9 \cdot 27 & 49\overline{6} \end{array}$	7070707070707070970970970970970970970970	$\begin{array}{c} 0.73 & 06\overline{2} \\ 0.72 & 99\overline{2} \\ 0.72 & 922 \\ 0.72 & 852 \\ 0.72 & 782 \\ 0.72 & 782 \\ 0.72 & 782 \\ 0.72 & 71\overline{2} \\ 0.72 & 64\overline{2} \\ 0.72 & 573 \\ 0.72 & 50\overline{3} \end{array}$	9.99 26 9.99 26 9.99 26 9.99 25 9.99 25 9.99 25 9.99 25 9.99 25 9.99 24 9.99 24 9.99 24 9.99 24 9.99 24		$\begin{array}{cccccccccccccccccccccccccccccccccccc$
$\begin{array}{r} 41 \\ 42 \\ 43 \\ 44 \\ 45 \\ 46 \\ 47 \\ 48 \\ 49 \\ 50 \end{array}$	$\begin{array}{c} 9 \cdot 26 \ 80 \overline{6} \\ 9 \cdot 26 \ 87 \overline{3} \\ 9 \cdot 26 \ 940 \\ 9 \cdot 27 \ 007 \\ 9 \cdot 27 \ 07 \overline{3} \\ 9 \cdot 27 \ 140 \\ 9 \cdot 27 \ 20 \overline{6} \\ 9 \cdot 27 \ 27 \overline{2} \\ 9 \cdot 27 \ 339 \\ 9 \cdot 27 \ 405 \end{array}$	67 67 66 66 66 66 66 66 66 66 66 66	$9 \cdot 27 566$ $9 \cdot 27 635$ $9 \cdot 27 703$ $9 \cdot 27 773$ $9 \cdot 27 842$ $9 \cdot 27 911$ $9 \cdot 27 980$ $9 \cdot 28 049$ $9 \cdot 28 117$ $9 \cdot 28 186$	69 69 69 69 69 69 69 60 89 60 80 80 80 80 80 80 80 80 80 80 80 80 80	0.72 434 0.72 365 0.72 295 0.72 226 0.72 157 0.72 028 0.72 020 0.71 951 0.71 882 0.71 814	$\begin{array}{c} 9.99 \ 240\\ 9.99 \ 238\\ 9.99 \ 236\\ 9.99 \ 238\\ 9.99 \ 238\\ 9.99 \ 238\\ 9.99 \ 228\\ 9.99 \ 228\\ 9.99 \ 228\\ 9.99 \ 224\\ 9.99 \ 221\\ 9.99 \ 219\\ 9.99 \ 219\end{array}$	19 18 17 16 15 14	$\begin{array}{cccccccccccccccccccccccccccccccccccc$
51 52 53 54 55 56 57 58 59 <b>60</b>	$\begin{array}{r} 9 \cdot 27 \ 471 \\ 9 \cdot 27 \ 586 \\ 9 \cdot 27 \ 602 \\ 9 \cdot 27 \ 668 \\ 9 \cdot 27 \ 733 \\ 9 \cdot 27 \ 739 \\ 9 \cdot 27 \ 799 \\ 9 \cdot 27 \ 864 \\ 9 \cdot 27 \ 929 \\ 9 \cdot 27 \ 995 \\ 9 \cdot 27 \ 995 \\ 9 \cdot 28 \ 060 \end{array}$	0 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	$\begin{array}{c} 9 \cdot 28 & 254 \\ 9 \cdot 28 & 322 \\ 9 \cdot 28 & 390 \\ 9 \cdot 28 & 459 \\ 9 \cdot 28 & 527 \\ 9 \cdot 28 & 527 \\ 9 \cdot 28 & 569 \\ 2 & 369 \\ 9 \cdot 28 & 569 \\ 9 \cdot 28 & 730 \\ 9 \cdot 28 & 730 \\ 9 \cdot 28 & 797 \\ 9 \cdot 28 & 865 \\ \end{array}$	68 68 68 68 68 67 67 67 67 67	$\begin{array}{c} 0.71 \ 746\\ 0.71 \ 677\\ 0.71 \ 609\\ 0.71 \ 541\\ 0.71 \ 473\\ 0.71 \ 405\\ 0.71 \ 337\\ 0.71 \ 337\\ 0.71 \ 270\\ 0.71 \ 202\\ 0.71 \ 135\\ \end{array}$	9.99 216 9.99 214 9.99 212 9.99 209 9.99 207 9.99 207 9.99 204 9.99 195 9.99 197 9.99 197	9 8 7 6 5 4 3 2 1	$\begin{array}{c} \overline{2} & 2 \\ 6 0 \cdot \overline{2} 0 \cdot 2 \\ 7 0 \cdot \underline{3} 0 \cdot 2 \\ 8 0 \cdot \overline{3} 0 \cdot 2 \\ 9 0 \cdot 4 0 \cdot \underline{3} \\ 10 0 \cdot \underline{4} 0 \cdot \underline{8} \\ 20 0 \cdot \underline{8} 0 \cdot 6 \\ 30 1 \cdot \underline{2} 1 \cdot 0 \\ 40 1 \cdot \underline{6} 1 \cdot \underline{3} \\ 50 2 \cdot 1 1 \cdot 6 \\ \end{array}$
_	Log. Cos.	d.	Log. Cot.	c. d.	Log. Tan.	Log. Sin	1	P. P.

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### TABLE VII.-LOGARITHMIC SINES, COSINES, TANGENTS,

11°

AND COTANGENTS.

11°	AND COTANG	GEN 15. 168
' Log. Sin. d.	Log. Tan. c. d. Log. Cot. Log.	Cos. P. P.
$\begin{array}{c} 0 & 9 \cdot 28 & 060 \\ 1 & 9 \cdot 28 & 125 \\ 2 & 9 \cdot 28 & 189 \\ 3 & 9 \cdot 28 & 254 \\ 4 & 9 \cdot 28 & 319 \\ 5 & 9 \cdot 28 & 383 \\ 5 & 9 \cdot 28 & 383 \\ \end{array}$	$\begin{array}{c} 9 \cdot 29 \ 067 \\ 9 \cdot 29 \ 134 \\ 9 \cdot 29 \ 134 \\ 9 \cdot 29 \ 201 \\ \hline 9 \cdot 29 \ 201 \\ \hline 9 \cdot 29 \ 201 \\ \hline 67 \\ 0 \cdot 70 \ 70 \ 798 \\ \hline 9 \cdot 99 \\ \hline 0 \cdot 70 \ 798 \\ \hline 9 \cdot 99 \\ \hline 9 \cdot 99 \\ \hline \end{array}$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$
$\begin{array}{c} 5 & 9 \cdot 28 & 383 \\ 6 & 9 \cdot 28 & 448 \\ 7 & 9 \cdot 28 & 512 \\ 8 & 9 \cdot 28 & 576 \\ 9 & 28 & 576 \\ \hline 9 & 9 \cdot 28 & 641 \\ \hline 1 & 9 & 28 & 641 \\ \hline 1 & 9 & 28 & 641 \\ \hline \end{array}$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
$\begin{array}{c} 1 \\ 1 \\ 1 \\ 1 \\ 5 \\ 9 \\ 2 \\ 1 \\ 1 \\ 1 \\ 1 \\ 1 \\ 1 \\ 1 \\ 1 \\ 1$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$
$\begin{array}{c} 20 & 9 \cdot 29 & 340 \\ 21 & 9 \cdot 29 & 403 \\ 22 & 9 \cdot 29 & 466 & 62 \\ 23 & 9 \cdot 29 & 528 & 63 \\ 24 & 9 \cdot 29 & 591 \\ 25 & 9 \cdot 29 & 591 \\ 25 & 9 \cdot 29 & 654 \\ 62 & 9 \cdot 29 & 716 \\ 62 & 62 \end{array}$	$9 \cdot 30 \ 260 \ 65 \ 0 \cdot 69 \ 739 \ 9 \cdot 99 \ 9 \cdot 30 \ 326 \ 65 \ 0 \cdot 69 \ 674 \ 9 \cdot 99$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{c} 3.30 & 532 \\ 9.30 & 587 & 65 \\ 9.30 & 552 & 65 \\ 9.30 & 552 & 65 \\ 9.30 & 717 & 65 \\ 9.30 & 717 & 65 \\ 9.30 & 781 & 64 \\ 9.69 & 218 \\ 9.99 \\ 9.30 & 846 \\ 9.5 \\ \hline 0.69 & 218 \\ 9.99 \\ 9.9 \\ 9.30 \\ 846 \\ 9.5 \\ \hline 0.69 & 218 \\ 9.99 \\ 9.9 $	$\begin{array}{cccccccccccccccccccccccccccccccccccc$
<b>30</b> 9 · 29 965 62 31 9 · 30 027 62 32 9 · 30 089 62 33 9 · 30 151 61 <u>34</u> 9 · 30 213 61	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{array}{c c c c c c c c c c c c c c c c c c c $
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
$\begin{array}{c} 55\\ 55\\ 56\\ 9\cdot 31\\ 549\\ 57\\ 9\cdot 31\\ 669\\ 57\\ 9\cdot 31\\ 669\\ 59\\ 58\\ 9\cdot 31\\ 728\\ 59\\ 59\\ 59\\ 59\\ 59\\ 59\\ 59\\ 59\\ 59\\ 59$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$
60 9 31 788 Log. Cos. d.	9 32 747 0.67 232 9.99	

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### TABLE VII.—LOGARITHMIC SINES, COSINES, TANGENTS, AND COTANGENTS.

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'	Log. Sin.	d.	Log. Tan.	c.d.	Log.	Cot.	Log.	Cos.		P, P,
0	9.31788	59	$9.3274\overline{7}$	62	0.67		9.99		60	
$\frac{1}{2}$	9.31 847 9.31 906	59	9.32 809 9.32 871	62	$0.67 \\ 0.67$	$19\overline{0}$ $12\overline{8}$	9.99 9.99		59 58	
3	9.31 966	59 59	9.32 933	62 62	0.67	066	9.99	03 <u>2</u>	57	$62  6\overline{1}  61$
<u>4</u> 5	9.32025 9.32084	59	9.32 995 9.33 057	61	0.67		<u>9.99</u> 9.99		<u>56</u> 55	$egin{array}{c c} 6 & 6 \cdot 2 & 6 \cdot \overline{1} & 6 \cdot 1 \ 7 & 7 \cdot \overline{2} & 7 \cdot 2 & 7 \cdot 1 \end{array}$
6	9.32143	59 59	$9.3311\overline{8}$	$6\overline{1}$ 62	0.66	881	9.99	$02\overline{4}$	54	8 8 2 8 2 8 1
78	9 · 32 202 9 · 32 260	58	9 · 33 180 9 · 33 242	61	0.66	819	9.99 9.99	$021 \\ 019$	53 52	$\begin{array}{cccccccccccccccccccccccccccccccccccc$
9	$9.32\overline{319}$	59 50	9.33 303	61	0.66	696	9.99	016	51	$20 20 \cdot \overline{6} 20 \cdot \overline{5} 20 \overline{3}$
10 11	9.32378	58 58	$9.3336\bar{4}$	6 <u>1</u> 61	0.66		9.99 9.99		$\frac{50}{49}$	$\begin{array}{c} 20 \\ 20 \\ 30 \\ 31 \\ 41 \\ 30 \\ 50 \\ 51 \\ 6 \\ 51 \\ 51 \\ 6 \\ 51 \\ 51 \\ 51 \\$
12	9-32436 9-32495	58 58	9.33 426 9.33 487	61 61	0 · 66 0 · 66		9.99	008	49 48	50 51 6 51 2 50 8
13 14	9 · 32 553 9 · 32 611	58	9.33 548 9.33 609	61	0.66		9.99 9.99		47 46	
15	9.32 670	58	9.33 670	60	0.66				45	$6\overline{0}$ $60$ $5\overline{9}$ $59$
16	9.32 728	58 58	9.33 731	61 61			9.98		44	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
17 18	9.32786 9.32844	58	9.33 792 9.33 852	60	0.66	147	9.98 9.98	994 991	43 42	8 8.0 8.0 7.9 7.8
19	<u>9.32 902</u>	58 58	<u>9.33 913</u>	61 60	0.66		The second s		41	10 10 1 10 0 9 9 9 8
20 21	9.32 960 9.33 017	57	9.33 974 9.34 034	6 <u>0</u>	0.66		9.98 9.98		40 39	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
22	9.33 075	58 57	9.34 095	60 60	0.65	905	9.98	<u>ម80</u>	38	$40 40 \cdot \overline{3} 40 \cdot 0 39 \cdot \overline{6} 39 \cdot \overline{3}$
23 24	9.33133 9.33190	57 57	9.34155 9.34215	6Ō	0.65 0.65				37	$50 50\cdot 4 50\cdot 0 49\cdot 6 49\cdot 1$
25	9.33 248	57 57	9.34 275	60 60	0.65	724	9.98	972	35	
26 27	9.33 305 9.33 362	57	9.34336 9.34396	60	0.65				34	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
28	9.33419	57 57	9.34 456		0.65	544	9.98	963	32	7 6.8 6.7 6.7 6.6
29 30	9.33476 9.33533	57	$9.3451\overline{5}$ $9.3457\overline{5}$	60	0.65				$\frac{31}{20}$	9 8.8 8.7 8.6 8.5
31	9.33 590	57 57	9.34 635	60 59	0.65	i 364	9.98	955	30 29	1 10 9.7 9.6 9.6 9.5
82 83	9.33 647 9.33 704	57	9.34695 9.34754	59	0.65		9.98 9.98	952 040	28 27	30 29 . 2 29 . 0 28 . 7 28 . 5
34	9.33 761	56	9.34814	59	0.65				26	$\begin{array}{c} 40 & 39 \cdot \underline{0} \\ 50 & 48 \cdot \overline{7} \\ 48 \cdot \overline{3} & 47 \cdot 9 \\ 47 \cdot 5 \end{array}$
35 36	9.33817 9.33874	56	9.34873						25	
.37	9.33 930	56 56	9.34 933 9.34 992			5 008	9.98	93 <u>8</u>	24 23	$5\overline{6}$ 56 $5\overline{5}$ 55
38 39	9.33 987 9.34 043	56	9.35 05 9.35 110	50		948 889			22 21	6 5.6 5.6 5.5 5.5
40	Concession of the local division of the loca	56	9.35 169	59	the second value of the se	830	the second se		$\frac{4}{20}$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$
41	9.34 156	56	9.35 228	50	0.64	L 77]	9.98	927	19	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$
42 43	9.34212 9.34268	56 56	9.35 287 9.35 346	59 59	0.64	1712 653	9.98	921	18 17	20 18 8 18 6 18 5 18 3
44	9.34 324	55	9.35 405	58		594			16	$\begin{array}{c} 30 & 28 \cdot 2 \\ 40 & 37 \cdot 6 \\ 37 \cdot 6 & 37 \cdot 3 \\ 37 \cdot 0 \\ 37 \cdot 6 \end{array} \begin{array}{c} 27 \cdot 7 \\ 37 \cdot 27 \cdot 5 \\ 37 \cdot 3 \\ 37 \cdot 0 \\ 36 \cdot 6 \\ \end{array}$
45 46	9.34 379 9.34 435	56	9.35 464 9.35 522	58	0.64 0.64	536 477	9.98 9.98		15 14	$\begin{array}{c} 40 \\ 50 \\ 47 \cdot 1 \\ 46 \cdot 6 \\ 46 \cdot 2 \\ 45 \cdot 8 \\ \end{array}$
47	9.34 491	55	9.35 581	1 29	0.64	418	9.98	910	13	
48 49	9.34 547 9.34 602	55	9.35 640 9.35 698	58		8360 302			$12 \\ 11$	$\begin{array}{cccc} \mathbf{5\overline{4}} & 3 & \mathbf{\overline{2}} \\ 6 & 5 \cdot \mathbf{\overline{4}}   0 \cdot 3   0 \cdot \mathbf{\overline{2}} \end{array}$
50	9.34 658	55	9.35 756	58	0.64	243	9.98	901	10	7 6.3 0.3 0.3
51 52	$9.3471\overline{3}$ $9.3476\overline{8}$	55	9.35 815 9.35 873	58		185 127			9	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
53	9.34 824	55	9.35 931	58 58	0.64	068	9.98	892	7	$10 9 \cdot 1 0 \cdot 5 0 4$
<u>54</u> 55	9.34879 $9.3493\overline{4}$	55	9.35 989 9.36 047	58	$0.64 \\ 0.63$	010 952			<u>6</u> 5	$\begin{array}{cccccccccccccccccccccccccccccccccccc$
56	9.34 989	55 55	9.36 105	58 57	0,63	894	9.98	884	4	$40\ 36\ \overline{3}\ 2\cdot 0\ 1\cdot \overline{6}$
57 58	$9.3504\overline{4}$ 9.35099	54	9.36 163 9.36 221	58	0 · 63 0 · 63	837	9.98	881 878	32	50 45 . 4 2 . 5 2 . 1
<u>5</u> 9	9.35 154	55	9.36 278	57	0.63	721	<u>9.98</u>	875	ĩ	
<u>60</u>		55	9.36 336	58	0.63		<u>9.98</u>	_	$\frac{0}{2}$	0.0
	Log. Cos.	d.	Log. Cot.	c. d.	Log.	l an	Log.	Sin.		· P. P.

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# TABLE VII.—LOGARITHMIC SINES, COSINES, TANGENTS, AND COTANGENTS.

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13	AND COTA	INGENIS.	166
' Log. Sin.	d. Log. Tan. c. d. Log. Cot. Log	g. Cos.	P. P.
$\begin{array}{c} 0 \\ 9 \cdot 35 \\ 2 \\ 9 \cdot 35 \\ 2 \\ 9 \cdot 35 \\ 35 \\ 3 \\ 9 \cdot 35 \\ 372 \\ 4 \\ 9 \cdot 35 \\ 472 \end{array}$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	98 866 58 98 863 57 98 860 56 57	7_ 57 58 56
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	98     858     55     6     5       98     855     54     7     6       98     855     54     8     7       98     852     53     9     8	$\begin{array}{cccccccccccccccccccccccccccccccccccc$
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	18         831         46           18         828         45         5	5 55 54 54
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
$\begin{array}{c} 23 \\ 9 \cdot 36 \\ 448 \\ 24 \\ 9 \cdot 36 \\ 501 \\ 25 \\ 9 \cdot 36 \\ 557 \\ 26 \\ 9 \cdot 36 \\ 607 \\ 27 \\ 9 \cdot 36 \\ 660 \\ 28 \\ 9 \cdot 36 \\ 713 \end{array}$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	3 53 52 52
$\begin{array}{c} 29 \\ \hline 9 \cdot 36 & 766 \\ 30 \\ 9 \cdot 36 & 818 \\ 31 \\ 9 \cdot 36 & 871 \\ 32 \\ 9 \cdot 36 & 923 \\ 33 \\ 9 \cdot 36 & 976 \\ 34 \\ 9 \cdot 37 & 028 \\ \end{array}$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	8 783 30 9 8 8 780 29 10 8 2017	0 7.9 7.9 7.8
$\begin{array}{c} 35 & 9 \cdot 37 \ 081 \\ 36 & 9 \cdot 37 \ 133 \\ 37 & 9 \cdot 37 \ 185 \\ 38 & 9 \cdot 37 \ 237 \\ 39 & 9 \cdot 37 \ 289 \\ \hline 40 & 9 \cdot 37 \ 341 \\ \end{array}$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	8 765 24 8 765 24 8 762 23 8 759 22 6 8 755 21 7	$\begin{array}{cccccccccccccccccccccccccccccccccccc$
$\begin{array}{r} 41 & 9 \cdot 37 & 39\overline{3} \\ 42 & 9 \cdot 37 & 445 \\ 43 & 9 \cdot 37 & 497 \\ 44 & 9 \cdot 37 & 548 \end{array}$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	8     749     19     9       8     746     18     10       8     743     17     20       8     740     16     30       8     737     15     40	$\begin{array}{c} 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 7 & 7 & 7 & 7 & 6 & 7 & 6 \\ 8 & 6 & 8 & 5 & 8 & 4 & 4 \\ 7 & 1 & 17 & 0 & 16 & 8 & 5 \\ 5 & 7 & 25 & 5 & 25 & 2 & 2 & 2 \\ 4 & 3 & 34 & 0 & 33 & 6 & 2 \\ 2 & 9 & 42 & 5 & 42 & 1 \end{array}$
$\frac{49}{509.37857}$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	8 731 13 8 728 12	3 3 2 0.310.810.2
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{c} \frac{1}{2} & 9 \cdot 39 & 244 \\ 9 \cdot 39 & 299 & 54 \\ 1 & 9 \cdot 39 & 299 & 54 \\ 9 \cdot 39 & 353 & 54 \\ 1 & 9 \cdot 39 & 353 & 54 \\ 1 & 9 \cdot 39 & 407 & 54 \\ 1 & 9 \cdot 39 & 407 & 54 \\ 1 & 9 \cdot 39 & 407 & 54 \\ 1 & 9 \cdot 39 & 461 & 54 \\ 1 & 0 \cdot 60 & 597 & 9 \cdot 98 \\ 1 & 9 \cdot 39 & 461 & 54 \\ 1 & 0 \cdot 60 & 538 & 9 \cdot 98 \\ 1 & 0 \cdot 60 & 538 & 9 \\ 1 & 0 \cdot 60 & 538 & 9 \\ 1 & 0 \cdot 60 & 538 & 9 \\ 1 & 0 \cdot 60 & 538 & 9 \\ 1 & 0 \cdot 60 & 538 & 9 \\ 1 & 0 \cdot 60 & 538 & 9 \\ 1 & 0 \cdot 60 & 538 & 9 \\ 1 & 0 \cdot 60 & 538 & 9 \\ 1 & 0 \cdot 60 & 538 & 9 \\ 1 & 0 \cdot 60 & 538 & 9 \\ 1 & 0 \cdot 60 & 538 & 9 \\ 1 & 0 \cdot 60 & $	3 715     8     9       3 712     7     10       3 709     6     20       3 706     5     30       3 703     4     40	$1 \cdot \frac{1}{7}   1 \cdot 5   0 \cdot \frac{4}{8}   1 \cdot \frac{1}{7}   1 \cdot 5   1 \cdot \frac{2}{8}   2 \cdot 3   2 \cdot 0   1 \cdot 6$
$\begin{array}{c} 57 & 9.38 & 215 \\ 58 & 9.38 & 266 \\ 59 & 9.38 & 317 \\ \hline 60 & 9.38 & 367 \end{array}$	10         9         39         515         54         0         60         484         9         95           1         9         39         569         54         0         60         483         9         95           1         9         39         623         54         0         60         483         9         95           9         39         623         54         0         60         376         9         98           0         60         876         9         9         0         60         376         9         98         98         98         98         98         98         98         98         98         98         98         98         98	69 <u>6</u> 2 693 1	P. P.
	<b>, , , , , , , , , ,</b>	1 1	

TABLE VII.-LOGARITHMIC SINES, COSINES, TANGENTS, AND COTANGENTS.

140	TABI	16	VII.—LO		AND COTANGEN		SINI	
	1	d	ling Tap					
49 50 51 52 53 54		$\begin{array}{c} d \\ 5555 $	Log. Tan. 0.396777 9.39784 9.39784 9.39784 9.39784 9.39784 9.39784 9.39784 9.399784 9.399784 9.399784 9.399784 9.39982 9.39992 9.40106 9.402125 9.41205 9.412126 9.412126 9.412247 9.412247 9.412247 9.412247 9.422348 9.42348 9.42348 9.42348 9.42348 9.42348 9.42348 9.42348 9.42348 9.42348 9.42348 9.42348 9.42348 9.42348 9.42348 9.4234	A . 434343333300033333300333330033330003330003300030000	AND COTANGEN	TS. d. 300 30 30 30 30 30 30 30 30 30 30 30 30	$ \begin{bmatrix} 0 \\ 59 \\ 58 \\ 57 \\ 6 \\ 55 \\ 55 \\ 55 \\ 55 \\ 55 \\ 55 $	$\begin{array}{c} 54 & 5\overline{3} & 53 \\ \hline & & & & & & & \\ \hline & & & & & & \\ \hline & & & &$

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# TABLE VII.—LOGARITHMIC SINES, COSINES, TANGENTS, AND COTANGENTS.

15	o TAB	LE	VII.—LOGA			SINES.		SIN	ES, TANGENTS, 164°
,	Log. Sin.	d.	Log. Tan. c. d	Log.	Cot.L	og. Cos.	[ d.		P. P.
0 1 2 3 4	$\begin{array}{r} 9.41\ 29\overline{9}\\ 9.41\ 34\overline{6}\\ 9.41\ 394\\ 9.41\ 441\\ 9.41\ 488\end{array}$	47 47 47 47	$\begin{array}{r} 9.42\ 805\\ 9.42\ 856\ 50\\ 9.42\ 906\ 50\\ 9.42\ 956\ 50\\ 9.43\ 007\ 50\end{array}$	$0.57 \\ $	195 9 144 9 094 9 043 9	·98 494 ·98 491 ·98 487 ·98 487 ·98 484 ·98 481		60 59 58 57 56	50 50 6  5.0  5.0
5 6 7 8 9	$\begin{array}{r} 9.41 53\overline{4} \\ 9.41 581 \\ 9.41 628 \\ 9.41 628 \\ 9.41 675 \\ 9.41 721 \end{array}$	46 47 4 <u>7</u> 46 46 47	$\begin{array}{c} 500 \\ \hline 9.43 & 057 \\ \hline 9.43 & 107 \\ \hline 9.43 & 157 \\ \hline 9.43 & 208 \\ \hline 9.43 & 258 \\ \hline 9.43 & 258 \\ \hline 50 \\ \hline 50$	$0.56 \\ 0.56$	8929 8429 7929 7429	·98 477 ·98 474 ·98 470 ·98 467 ·98 467	<b>SI CO COICOICOI</b>	55 54 53 52 51	7 5.9 5.8 8 6.7 6.6 9 7.6 7 5
$10 \\ 11 \\ 12 \\ 13 \\ 14 \\ 15 \\ 15 \\ 10 \\ 10 \\ 10 \\ 10 \\ 10 \\ 10$	9.41768 9.41815 9.41861 9.41908 9.41954 9.41954	4 <u>6</u> 6 4 <u>6</u> 6 46	$\begin{array}{c} 9.43 \ 308 \\ 9.43 \ 358 \\ 50 \\ 9.43 \ 408 \\ 50 \\ 9.43 \ 458 \\ 9.43 \ 508 \\ 9.43 \ 508 \\ 458 \\ 50 \\ 9.43 \ 508 \\ 458 \\ 50 \\ 9.43 \ 508 \\ 458 \\ 50 \\ 9.43 \ 508 \\ 458 \\ 50 \\ 9.43 \ 508 \\ 458 \\ 50 \\ 9.43 \ 508 \\ 458 \\ 50 \\ 9.43 \ 508 \\ 458 \\ 50 \\ 9.43 \ 508 \\ 458 \\ 50 \\ 9.43 \ 508 \\ 458 \\ 50 \\ 9.43 \ 508 \\ 50 \\ 50 \\ 50 \\ 50 \\ 50 \\ 50 \\ 50 $	0.56	642 9 592 9 542 9 492 9	·98 460 ·98 457 ·98 453 ·98 450 ·98 446	ରା ଭାରାଭାରାର	50 49 48 47 46	$\begin{array}{c} 10 & 8.4 \\ 10 & 8.4 \\ 20 & 16.8 \\ 16.6 \\ 30 & 25.2 \\ 25.0 \\ 40 & 33.6 \\ 33.3 \\ 50 & 42.1 \\ 41.6 \\ 4\overline{9} & 49 & 4\overline{8} & 48 \end{array}$
15 16 17 18 19	$9.42\ 000$ $9.42\ 047$ $9.42\ 093$ $9.42\ 139$ $9.42\ 185$	46 46 46 46 46	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$0.56 \\ $	$     \begin{array}{r}       39\overline{2} \\       343 \\       29\overline{3} \\       24\overline{3} \\       9     \end{array} $	.98 443 .98 439 .98 436 .98 433 .98 429 .98 429	လ၊ လ၊လ၊လ လ၊လ၊	45 44 43 42 41	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
20 21 22 23 24 25	9.42232 9.42278 9.42324 9.42369 9.42415 9.42461	46 45 45 46 46	$\begin{array}{r} 9.43 & 806 & 49 \\ 9.43 & 855 & 49 \\ 9.43 & 905 & 49 \\ 9.43 & 954 & 49 \\ 9.44 & 003 & 49 \\ 9.44 & 053 & 49 \\ 9.44 & 053 & 49 \end{array}$	$0.56 \\ 0.56 \\ 0.56 \\ 0.55 \\ 0.55$	$   \begin{array}{r}     14\overline{4} & 9 \\     095 & 9 \\     045 & 9 \\     996 & 9   \end{array} $	98 426 98 422 98 419 98 415 98 412 98 412	ାରାରାରାରାର ଭା	40 39 38 37 36 35	$ \begin{array}{c} 0 & 0 \cdot 0 & 0 \cdot 1 & 0 \cdot 1 & 0 \cdot 1 \\ 9 & 7 \cdot 3 & 7 \cdot 3 & 7 \cdot 2 \\ 10 & 8 \cdot 2 & 8 \cdot 1 & 8 \cdot 1 & 8 \cdot 0 \\ 20 & 16 \cdot 5 & 16 \cdot 3 & 16 \cdot 1 & 16 \cdot 0 \\ 30 & 24 \cdot 7 & 24 \cdot 5 & 24 \cdot 2 & 24 \cdot 0 \\ 40 & 33 & 0 & 32 \cdot 6 & 32 \cdot 3 & 32 \cdot 0 \\ 50 & 41 \cdot 2 & 40 \cdot 8 & 40 \cdot 4 & 40 \cdot 0 \end{array} $
26 27 28 29 30	$9.42 \ 401$ $9.42 \ 507$ $9.42 \ 553$ $9.42 \ 598$ $9.42 \ 644$ $9.42 \ 690$	46 45 45 46 45	$\begin{array}{c}9.44\ 102\ 49\\9.44\ 151\ 49\\9.44\ 200\ 49\\9.44\ 249\ 49\\9.44\ 249\ 49\\0\ 44\ 290\ 49\end{array}$	$0.55 \\ $	89 <u>8</u> 9 84 <u>8</u> 9 79 <u>9</u> 9 7509		ରା ପାରାରାରା	$     \begin{array}{r}       33 \\       32 \\       31 \\       30     \end{array}   $	$\begin{array}{cccccccccccccccccccccccccccccccccccc$
31 32 33 34 35	9.42 830 9.42 735 9.42 781 9.42 826 9.42 871 9.42 917	4 <u>5</u> 4 <u>5</u> 4 <u>5</u> 4 <u>5</u> 4 <u>5</u>	$\begin{array}{c} 9 \cdot 44 \ 348 \ 49 \ 9 \cdot 44 \ 397 \ 49 \ 9 \cdot 44 \ 397 \ 49 \ 9 \cdot 44 \ 446 \ 9 \cdot 44 \ 494 \ 48 \ 9 \cdot 44 \ 494 \ 48 \ 9 \cdot 44 \ 54^{\frac{1}{2}} \ 49 \ 49 \ 49 \ 49 \ 49 \ 49 \ 49 \ $	$0.55 \\ $	652 9 603 9 554 9 505 9	·98 387 ·98 384 ·98 384 ·98 380 ·98 377 ·98 373	ରା ପାରାପାରା	29 28 27 26 25	$\begin{array}{c} 9 & 7 \cdot 1 & 7 \cdot 0 & 7 \cdot 0 \\ 10 & 7 \cdot 9 & 7 \cdot 8 & 7 \cdot 7 & 7 \cdot 6 \\ 20 & 15 \cdot 8 & 15 \cdot 6 & 15 \cdot 5 & 15 \cdot 3 \\ 30 & 23 \cdot 7 & 23 \cdot 5 & 23 \cdot 2 & 23 \cdot 0 \\ 40 & 31 \cdot 6 & 31 \cdot 3 & 31 \cdot 0 & 30 \cdot 6 \\ 50 & 39 \cdot 6 & 39 \cdot 1 & 38 \cdot 7 & 38 \cdot 3 \end{array}$
36	9.42962 9.43007 9.43052 9.43098 9.43143	45 45 45 45 45	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$0.55 \\ $	4079 3599 3109 2619	98 370 98 366 98 363 98 359	ଭାର୍ଡା ଭାରାରାରା	24 23 22 21 20	$\begin{array}{cccccccccccccccccccccccccccccccccccc$
41 42	$\begin{array}{r} 9.43 & 143 \\ 9.43 & 233 \\ 9.43 & 278 \\ 9.43 & 322 \\ 9.43 & 367 \end{array}$	45 45 4 <u>5</u> 44 45	$\begin{array}{r} 9.44 83\overline{5} \\ 48 \\ 9.44 884 \\ 9.44 93\overline{2} \\ 9.44 981 \\ 9.44 981 \\ 48 \\ 48 \\ 48 \\ 48 \\ 48 \\ 48 \\ 48 \\ $	$0.55 \\ $	$16\overline{4}9$ 1169 0679 0199	98 352 98 348 98 345 98 341 98 341	4133133		$\begin{array}{c} 9 & 6.8 & 6.7 & 6.7 & 6.6 \\ 10 & 7.6 & 7.5 & 7.4 & 7.3 \\ 20 & 15 \cdot 1 & 15 \cdot 0 & 14 \cdot \overline{8} & 14 \cdot \overline{6} \\ \end{array}$
46 47 48 49	$\begin{array}{r} 9.43 \ 412 \\ 9.43 \ 457 \\ 9.43 \ 501 \\ 9.43 \ 546 \\ \theta.43 \ 591 \end{array}$	44 45	$\begin{array}{r} 9.45 \ 077 \\ 9.45 \ 126 \\ 48 \\ 9.45 \ 174 \\ 9.45 \ 222 \\ 0.45 \ 222 \\ 48 \\ 0.45 \ 275 \\ 48 \end{array}$	$0.54 \\ 0.54 \\ 0.54$	9229 8749 8259 7779	98 334 98 331 98 327 98 324 98 324	ାରାରାରାଭାର 4ା	$     \begin{array}{r}       13 \\       12 \\       11 \\       10     \end{array}   $	$50 37 \cdot 9 37 \cdot 5 37 \cdot 1 36 \cdot \overline{6}$ $4  \overline{3}  3$ $6 0 \cdot \frac{4}{5} 0 \cdot \overline{3} 0 \cdot \overline{3}$
51 52 53	$\begin{array}{r} 9.43 & 635 \\ 9.43 & 635 \\ 9.43 & 680 \\ 9.43 & 724 \\ 9.43 & 768 \\ 9.43 & 813 \end{array}$	44 44 44 44	$\begin{array}{r}9\cdot 45 \ 31\overline{8} \\9\cdot 45 \ 367 \\9\cdot 45 \ 45 \ 48 \\9\cdot 45 \ 415 \\9\cdot 45 \ 463 \\9\cdot 45 \ 463 \\4\overline{7} \end{array}$	$0.54 \\ 0.54 \\ 0.54 \\ 0.54 \\ 0.54$	6819 6339 5859 5379	98 316 98 313 98 309 98 306 98 302	୍ୟାରାରାରାର ସା	9 8 7 6 5	$\begin{array}{c} 30 \\ 30 \\ 30 \\ 31 \\ 32 \\ 4 \\ 30 \\ 31 \\ 30 \\ 31 \\ 30 \\ 31 \\ 30 \\ 31 \\ 31$
56 57 58 59	9.43857 9.43901 9.43945 9.43989 9.43989 9.43089	44	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	0.54	44 <u>1</u> 9 3939 3469 2989	98 298 98 295 98 291 98 291 98 288 98 284	୍ୟାର୍ଚ୍ଚାର୍ଚ୍ଚାର ସ	4 3 2 1 0	$\begin{array}{c} 100.600.600.5\\ 201.31.11.0\\ 302.01.71.5\\ 402.62.32.0\\ 5013.312.912.5\end{array}$
	Log. Cos.	d.	Log. Cot. c. d.	Log. 1	COLUMN STREET,	og. Sin.	d.	- <u>'</u>	_ P. P.

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### TABLE VII.—LOGARITHMIC SINES, COSINES, TANGENTS, AND COTANGENTS.

° <b>16</b>					IND		ANGEN	10.		163-
'	Log. Sin.	d.	Log. Tan.	c. d.	Log.	Cot.	Log. Cos.	d,		P. P.
0 1 2 3 4	$\begin{array}{r} 9.44 & 034 \\ 9.44 & 078 \\ 9.44 & 122 \\ 9.44 & 166 \\ 9.44 & 209 \end{array}$	44 44 43 43	9.45749 9.45797 9.45845 9.45892 9.45940	48 47 47 47 47 47	0.54	202 155 107 060	9.98 284 9.98 280 9.98 277 9.98 273 9.98 273 9.98 269	ାର୍ଚାରାର 4 ାର	60 59 58 57 56	$\begin{array}{cccccccccccccccccccccccccccccccccccc$
5 6 7 8 9	9.44 428	44 43 43 44	9.45 987 9.46 035 9.46 082 9.46 129 9.46 177	47 47 47 47 47	0 · 53 0 · 53 0 · 53 0 · 53 0 · 53	965 917 870 823	9.98 26 <u>6</u> 9.98 26 <u>2</u> 9.98 25 <u>8</u> 9.98 25 <u>5</u> 9.98 25 <u>5</u> 9.98 25 <u>1</u>	ାର୍ଚ୍ଚାର ମ୍ବାର୍ଚ୍ଚାର	55 54 53 52 51	$\begin{array}{cccccccccccccccccccccccccccccccccccc$
10 11 12 13 14	9.44472 9.44515 9.44559 9.44602 9.44602 9.44646	43 43 43 43 43	9.46 22 <u>4</u> 9.46 27 <u>1</u> 9.46 318 9.46 366 9.46 413	47 47 47 47 47 47	0.53 0.53	$72\overline{8} \\ 681 \\ 634$	$9 \cdot 98 24\overline{7}$ $9 \cdot 98 244$ $9 \cdot 98 244$ $9 \cdot 98 24\overline{0}$ $9 \cdot 98 23\overline{6}$ $9 \cdot 98 233$	4ାର୍ଚ୍ଚାର 4ାର୍ଚ୍ଚା	50 49 48 47 46	$\begin{array}{c} 20 & 16 \cdot 0 & 15 \cdot 8 & 15 \cdot 6 \\ 30 & 24 \cdot 0 & 23 \cdot 7 & 23 \cdot 5 \\ 40 & 32 \cdot 0 & 31 \cdot 6 & 31 \cdot 3 \\ 50 & 40 \cdot 0 & 39 \cdot 6 & 39 \cdot 1 \end{array}$
15 16 17 18 19	3144 002	43 43 43 43 43	9.46460 9.46507 9.46554 9.46601 9.46647	47 47 47 47 46 47	0 · 53 0 · 53	493 446 39 <u>9</u> 352	$\begin{array}{r} 9.98 \ 22\overline{9} \\ 9.98 \ 225 \\ 9.98 \ 222 \\ 9.98 \ 218 \\ 9.98 \ 214 \\ 9.98 \ 214 \end{array}$	13 41313 4 13	45 44 43 42 41	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
20 21 22 23 24	9.44940 9.44991 9.45034 9.45077	43 43 43 43	$9.4669\overline{4}$ $9.4674\overline{1}$ $9.4678\underline{8}$ $9.4683\overline{4}$ $9.4683\overline{4}$	47 46 46 47 46		$212 \\ 165 \\ 118 $	9.98211 9.98207 9.98203 9.98200 9.98200 9.98196	3 4 1 3 1 3 4 1 3	40 39 38 37 36	$\begin{array}{c} 20 & 15 \cdot 5 & 15 \cdot 3 & 15 \cdot 1 & 15 \cdot 0 \\ 30 & 23 \cdot 2 & 23 \cdot 0 & 22 \cdot 7 & 22 \cdot 5 \\ 40 & 31 \cdot 0 & 30 \cdot 6 & 30 \cdot 3 & 30 \cdot 0 \\ 50 & 38 \cdot 7 & 38 \cdot 3 & 37 \cdot 9 & 37 \cdot 5 \end{array}$
25 26 27 28 729	0.40 201	42 43 43 42 42 42	9.46928 9.46974 9.47021 9.47067 9.47114	$4\overline{6} \\ 4\overline{6} \\ 46$	$0.53 \\ 0.52 \\ $	979 932 886	$9.9819\overline{2}$ $9.9818\overline{8}$ 9.98185 9.98181 9.98181 $9.9817\overline{7}$	413 413	35 34 33 32 31	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
30 31 32 33 34	$9.4550\overline{4}$	4 <u>3</u> 4 <u>2</u> 4 <u>2</u> 4 <u>2</u>	$9.47 16\overline{0}$ 9.47 207 9.47 253 $9.47 29\overline{9}$ 9.47 345	$4\overline{6} \\ 46 \\ 46 \\ 46 \\ 46 \\ 46 \\ 4\overline{6} \\ 4\overline{6}$	$0.52 \\ $	793 74 <u>7</u> 70 <u>0</u> 654	9.98173 9.98170 9.98166 9.98162 9.98158 9.98158	434343	30 29 28 27 26	$\begin{array}{c c c c c c c c c c c c c c c c c c c $
35 36 37 38 89	9.45547 9.45589 9.45631 9.45674 9.45716	42 42 42 42 42	9.47392 9.47438 947484 947530 947576	46 46 46 46 46	$0.52 \\ $	$562 \\ 516 \\ 469 \\ 423 \\ 423 \\ $	9.98155 9.98151 9.98147 9.98143 9.98143 9.98140	43434	25 24 23 22 21	$\begin{array}{cccccccccccccccccccccccccccccccccccc$
40 41 42 43 44	$9.4575\overline{8}$ 9.45800 9.45842 9.45885 9.45927	42 42 42 42	$9.47 62\overline{2}$ 9.47 668 9.47 714 9.47 760 9.47 806	46 45 46 46 46 45	$0.52 \\ $	$33\overline{1} \\ 286 \\ 240 \\ 194$	9.98136 9.98132 9.98128 9.98128 9.98124 9.98121	3443	20 19 18 17 16	$ \begin{array}{c} 1 \\ 8 \\ 5 \\ 6 \\ 7 \\ 7 \\ 8 \\ 9 \\ 6 \\ 4 \\ 6 \\ 7 \\ 1 \\ 1 \\ 1 \\ 1 \\ 1 \\ 1 \\ 1 \\ 1 \\ 1$
45 46 47 48 49	9.45969 9.46011 9.46052 9.46094 9.46136	42 41 42 42	9.47851 9.47897 9.47943 9.47989 9.47989 9.48034	46 45 46 45	$0.52 \\ 0.52 \\ 0.52 \\ 0.52 \\ 0.51 \\ $	$10\overline{2} \\ 057 \\ 011 \\ 965$	$\begin{array}{r}9.98\ 117\\9.98\ 113\\9.98\ 109\\9.98\ 109\\9.98\ 105\\9.98\ 102\\9.98\ 102\end{array}$	413 4 413 4	,15 14 13 12 11	50 35.4 35.0 34.6 34.I 4 3 6]0.4 0.3
50 51 52 53 54	9.46178 9.46220 9.46261 9.46303 9.46345	$\begin{array}{c} 42 \\ 41 \\ 41 \\ 42 \end{array}$	9.48080 9.48125 9.48171 9.48216 9.48262	45555 4455 455	$0.51 \\ $	829 783 738	9.980989.980949.980949.98090000000000000	4134413	10 9 8 7 6	$\begin{array}{c} 70.40.4\\ 80.50.4\\ 90.60.5\\ 100.60.6\\ 201.31.1\end{array}$
55 56 57 58 59	$9.4638\overline{6}$ 9.46428 9.46469 9.46511 9.46552	$\begin{array}{c} 4\overline{1} \\ 4\overline{1} \\ 4\overline{1} \\ 4\overline{1} \\ 4\overline{1} \\ 41 \\ 4\overline{1} \\ 4\overline{1} \end{array}$	9.48307 9.48353 9.48398 9.48443 9.48443 9.48488	45 45 45 45 45 45	$0.51 \\ $	647 602 556 511	9.98079 9.98075 9.98071 9.98067 9.98067 9.98063	344 <u>3</u> 44	5 4 3 2 1	3022.011.77 4022.62.3 503.32.9
<u>60</u>	9.46 593 Log. Cos.	d.	<u>9.48 534</u> Log. Cot.	1	0.51 Log.	_	<u>9.98059</u> Log. Sin.	<u> </u>	<u> </u>	P. P.
1				1	<u> </u>			1	1	

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# FABLE VII.—LOGARITHMIC SINES, COSINES, TANGENTS, AND COTANGENTS.

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_	Log. Sin.	d.	Log. Tan.	c.d.	Log.	Cot.	Log. Cos.	d.		P. P.
01234 56789	$\begin{array}{c} 9.46 & 59\overline{3} \\ 9.46 & 635 \\ 9.46 & 676\overline{7} \\ 9.46 & 717\overline{8} \\ 9.46 & 758\overline{9} \\ 9.46 & 758\overline{9} \\ 9.46 & 881\overline{1} \\ 9.46 & 881\overline{1} \\ 9.46 & 922\overline{3} \\ 9.46 & 96\overline{3} \end{array}$	$ \begin{array}{c} 41\\ 41\\ 41\\ 41\\ 41\\ 41\\ 41\\ 41\\ 41\\ 41\\$	9.48534 9.48579 9.48624 9.48669 9.48714 9.48714 9.48714 9.48714 9.48704 9.48704 9.48804 9.48849 9.48894 9.48939	45 45 45 45 45 45 45 45 45 45 45 45	$\begin{array}{c} 0.51 \\ 0.51 \\ 0.51 \\ 0.51 \\ 0.51 \\ 0.51 \\ 0.51 \\ 0.51 \\ 0.51 \\ 0.51 \end{array}$	421 376 330 285 240 195 151 106 061	$\begin{array}{c} 9 \cdot 98 & 056 \\ 9 \cdot 98 & 052 \\ 9 \cdot 98 & 048 \\ 9 \cdot 98 & 044 \\ 9 \cdot 98 & 040 \\ 9 \cdot 98 & 036 \\ 9 \cdot 98 & 036 \\ 9 \cdot 98 & 032 \\ 9 \cdot 98 & 028 \\ 9 \cdot 98 & 028 \\ 9 \cdot 98 & 024 \end{array}$	3444334444	60 59 58 57 56 55 55 54 53 52 51	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
10 11 12 13 14 15 16 17 18 19	$\begin{array}{c} 9 \cdot 47 & 00\overline{4} \\ 9 \cdot 47 & 04\overline{5} \\ 9 \cdot 47 & 086 \\ 9 \cdot 47 & 127 \\ 9 \cdot 47 & 168 \\ 9 \cdot 47 & 20\overline{8} \\ 9 \cdot 47 & 249 \\ 9 \cdot 47 & 249 \\ 9 \cdot 47 & 33\overline{0} \\ 9 \cdot 47 & 33\overline{1} \end{array}$	$\begin{array}{c} 41 \\ 41 \\ 40 \\ 41 \\ 40 \\ 40 \\ 40 \\ 40 \\$	$\begin{array}{c} 9.48 & 984\\ 9.49 & 028\\ 9.49 & 073\\ 9.49 & 118\\ 9.49 & 162\\ 9.49 & 162\\ 9.49 & 252\\ 9.49 & 252\\ 9.49 & 256\\ 9.49 & 296\\ 9.49 & 341\\ 9.49 & 385\\ \end{array}$	4544544 4444 44444 4444 4444 4444	$\begin{array}{c} 0.50 \\ 0.50 \\ 0.50 \\ 0.50 \\ 0.50 \\ 0.50 \\ 0.50 \\ 0.50 \end{array}$	971 926 882 837 792 748 703 659 614	9.98021 9.98017 9.98013 9.98009 9.98005 9.98001 9.98001 9.97997 9.97993 9.97985 9.97985 9.97985	344444	$50 \\ 49 \\ 48 \\ 47 \\ 46 \\ 45 \\ 44 \\ 43 \\ 42 \\ 41$	$\begin{array}{c} 20 \ 15 \cdot \overline{1} \ 15 \cdot 0 \ 14 \cdot \overline{3} \ 14 \cdot \overline{6} \\ 30 \ 22 \cdot \overline{7} \ 22 \cdot 5 \ 22 \cdot 22 \ 22 \cdot 2 \\ 40 \ 30 \cdot 3 \ 30 \ 0 \ 29 \cdot \overline{6} \ 29 \cdot \overline{3} \\ 50 \ 37 \cdot 9 \ 37 \cdot 5 \ 37 \cdot 1 \ 36 \cdot \overline{6} \\ \hline \begin{array}{c} 4\overline{3} & 4\overline{3} \\ 6 \ 4 \cdot \overline{3} & 4 \cdot 3 \\ 7 \ 5 \cdot 1 \ 5 \cdot 0 \\ 8 \ 5 \cdot 8 \ 5 \cdot \overline{7} \\ 9 \ 6 \cdot \overline{5} \ 6 \cdot \overline{4} \\ 10 \ 7 \cdot 2 \ 7 \cdot \overline{1} \end{array}$
20 21 22 23 24 25 26 27 28	$9.4741\overline{1}$ 9.47452 9.47452 9.47532 9.47532 9.47573 9.47613 9.47613 9.47653 9.47653 9.47694 9.47734	$\begin{array}{c} 40\\ 40\\ 40\\ 40\\ 40\\ 40\\ 40\\ 40\\ 40\\ 40\\$	9.49430 9.49474 9.49518 9.49563 9.49607 9.49607 9.49651 9.49651 9.49695 9.49740 9.49740 9.497840	44444444444444444444444444444444444444	$\begin{array}{c} 0.50 \\ 0.50 \\ 0.50 \\ 0.50 \\ 0.50 \\ 0.50 \\ 0.50 \\ 0.50 \\ 0.50 \end{array}$	481 437 392 348 304 260 216	9.97973 9.97969 9.97966 9.97966 9.97962 9.97958 9.97954 9.97950	44433444444	40 39 38 37 36 35 34 33 32	$\begin{array}{c} 20 14.5 14.\overline{3}\\ 30 21.7 21.5\\ 40 29.0 28.6\\ 50 36.2 35.8\\ \hline \\ 4\overline{1}  41  4\overline{0}  40\\ 6   4.\overline{1}   4.1   4.0   4.0\\ 7   4.8   4.8   4.7   4.6\\ \end{array}$
31 32 33 34 35 36 37	$9 \cdot 47 774 \\9 \cdot 47 814 \\9 \cdot 47 854 \\9 \cdot 47 894 \\9 \cdot 47 934 \\9 \cdot 47 974 \\9 \cdot 48 014 \\9 \cdot 48 054 \\9 \cdot 48 053 \\9 \cdot 48 133$	$\begin{array}{c} 40 \\ 40 \\ 40 \\ 40 \\ 40 \\ 40 \\ 40 \\ 39 \\ 40 \end{array}$	$\begin{array}{c} 9 \cdot 49 & 828 \\ 9 \cdot 49 & 872 \\ 9 \cdot 49 & 916 \\ 9 \cdot 49 & 960 \\ 9 \cdot 50 & 004 \\ 9 \cdot 50 & 048 \\ 9 \cdot 50 & 092 \\ 9 \cdot 50 & 136 \\ 9 \cdot 50 & 179 \\ 9 \cdot 50 & 223 \end{array}$	44 44 43 44 44 44 44 44 44 44 44 44 44	$0.49 \\ 0.49$	128 083 039 996 952 908 864 820	$9 \cdot 97 946  9 \cdot 97 942  9 \cdot 97 938  9 \cdot 97 938  9 \cdot 97 930  9 \cdot 97 926  9 \cdot 97 922  9 \cdot 97 918  9 \cdot 97 914  9 \cdot 97 910  9 \cdot 97 910 \\ 9 \cdot$	44444444444	$     \begin{array}{r}       31 \\       30 \\       29 \\       28 \\       27 \\       26 \\       25 \\       24 \\       23 \\       20     \end{array} $	$\begin{array}{cccccccccccccccccccccccccccccccccccc$
$     \begin{array}{r}       39 \\       40 \\       41 \\       42 \\       43 \\       44 \\       45 \\       46     \end{array} $	$\begin{array}{r} 9.48 & 173 \\ 9.48 & 213 \\ 9.48 & 252 \\ 9.48 & 292 \\ 9.48 & 331 \\ 9.48 & 371 \\ 9.48 & 371 \\ 9.48 & 410 \\ 9.48 & 450 \\ 9.48 & 489 \\ \end{array}$	39 40 99 99 99 99 99 99 99 99 99 99 99 99 99	$\begin{array}{r} 9.50\ 267\\ 9.50\ 311\\ 9.50\ 354\\ 9.50\ 398\\ 9.50\ 442\\ 9.50\ 485\\ 9.50\ 529\\ 9.50\ 529\\ 9.50\ 572\\ 9.50\ 616\end{array}$	4333433433 443343 4433433 4433433 4433433	$   \begin{array}{r}     0.49 \\     0.49 \\     0.49 \\     0.49 \\     0.49 \\     0.49 \\     0.49 \\     0.49 \\     0.49 \\     0.49 \\     0.49 \\   \end{array} $	733 689 645 602 558 514 471 427	9.97 906 9.97 902 9.97 898 9.97 898 9.97 894 9.97 890 9.97 886 9.97 881 9.97 881 9.97 887 9.97 87 9.97 87	4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	$\begin{array}{c} 22\\ 21\\ 20\\ 19\\ 18\\ 17\\ 16\\ 15\\ 14\\ 13 \end{array}$	
48 49 50 51 52 53 54 55 56	9.485299.485689.486079.486469.486469.486869.487259.487649.488039.488039.48842	39 39 39 39 39 39 39 39 39 39 39 39 39	$\begin{array}{c} 9.50 & 659\\ 9.50 & 702\\ 9.50 & 746\\ 9.50 & 789\\ 9.50 & 832\\ 9.50 & 832\\ 9.50 & 876\\ 9.50 & 919\\ 9.50 & 962\\ 9.50 & 962\\ 9.51 & 005\\ \end{array}$	43 43 43 43 43 43 43 43 43 43 43 43 43 4	$\begin{array}{c} 0.49 \\ 0.49 \\ 0.49 \\ 0.49 \\ 0.49 \\ 0.49 \\ 0.49 \\ 0.49 \\ 0.49 \\ 0.49 \\ 0.49 \\ 0.48 \end{array}$	340 297 254 210 167 124 081 038 994	$\begin{array}{c} 9.97 & 869 \\ 9.97 & 865 \\ 9.97 & 865 \\ 9.97 & 857 \\ 9.97 & 857 \\ 9.97 & 853 \\ 9.97 & 849 \\ 9.97 & 845 \\ 9.97 & 841 \\ 9.97 & 837 \\ \end{array}$	44 44444 4444 4444	$     \begin{array}{c}       12 \\       11 \\       10 \\       9 \\       8 \\       7 \\       6 \\       5 \\       4     \end{array} $	$\begin{array}{cccccccccccccccccccccccccccccccccccc$
58 59	9.48 88 <u>1</u> 9.48 92 <u>0</u> 9.48 95 <u>9</u> 9.48 959 9.48 998 Log. Cos.	39	9.51 048 9.51 09 $\frac{1}{9}$ 9.51 13 $\frac{1}{4}$ 9.51 17 $\frac{7}{1}$ Log. Cot.	43 43 43	0.48 0.48 0.48 0.48 0.48 Log.	90 <u>8</u> 865 822	9 · 97 833 9 · 97 829 9 · 97 824 9 · 97 820 Log. Sin.	4 4 4 d.	3 2 1 0 /	50 3.7 3.32.9 P. P.

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TABLE VII.-LOGARITHMIC SINES, COSINES, TANGENTS, AND COTANCENTS

18°		AND COTANGENTS.	161°
' Log. Sin.	d. Log. Tan. c.	l. Log. Cot. Log. Cos. d.	P, P,
$\begin{array}{c} 0 & 9.48 & 998 \\ 1 & 9.49 & 037 \\ 2 & 9.49 & 076 \\ 3 & 9.49 & 114 \\ 4 & 9.49 & 153 \\ 5 & 9.49 & 192 \\ 6 & 9.49 & 231 \\ 7 & 9.49 & 268 \\ 8 & 9.49 & 308 \\ 9 & 9.49 & 346 \\ \end{array}$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
$\begin{array}{c} 5 & 0.40 & 315 \\ 10 & 9.49 & 385 \\ 11 & 9.49 & 423 \\ 12 & 9.49 & 462 \\ 13 & 9.49 & 500 \\ 14 & 9.49 & 539 \\ 15 & 9.49 & 577 \end{array}$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{array}{c} 30 21 \cdot 5 21 \cdot 2 21 \cdot 0\\ 40 28 \cdot 6 28 \cdot 3 28 \cdot 0\\ 50 35 \cdot 8 35 \cdot 4 35 \cdot 0\\ \hline \end{array}$
$\begin{array}{c} 16 & 9 \cdot 49 & 615 \\ 17 & 9 \cdot 49 & 653 \\ 18 & 9 \cdot 49 & 692 \\ 19 & 9 \cdot 49 & 730 \\ 20 & 9 \cdot 49 & 768 \\ 21 & 9 \cdot 49 & 806 \end{array}$	$\begin{array}{c} 38 \\ 38 \\ 9 \\ 51 \\ 9 \\ $	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
$\begin{array}{c} 22 & 9 \cdot 49 & 844 \\ 23 & 9 \cdot 49 & 882 \\ 24 & 9 \cdot 49 & 920 \\ 25 & 9 \cdot 49 & 958 \\ 26 & 9 \cdot 49 & 996 \\ 27 & 9 \cdot 50 & 034 \\ 28 & 9 \cdot 50 & 072 \end{array}$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{c} 10 & 13 \cdot 8 & 13 \cdot 6 \\ 20 & 13 \cdot 8 & 13 \cdot 6 \\ 30 & 20 \cdot 7 & 120 \cdot 5 \\ 40 & 27 \cdot 6 & 27 \cdot 3 \\ 50 & 34 \cdot 6 & 34 \cdot 1 \\ \hline \\ 39 & 38 & 38 \\ 6 & 3 \cdot 9 & 3 \cdot 8 \\ 6 & 3 \cdot 9 & 3 \cdot 8 \\ 7 & 4 \cdot 5 & 4 \cdot 5 & 4 \cdot 4 \\ \end{array}$
$\begin{array}{c} 29 & 9.50 & 110 \\ 30 & 9.50 & 147 \\ 31 & 9.50 & 185 \\ 32 & 9.50 & 223 \\ 33 & 9.50 & 260 \\ 34 & 9.50 & 298 \\ 35 & 9.50 & 336 \end{array}$	$\begin{array}{c} 337 \\ 9 \cdot 52 \ 410 \\ 37 \\ 9 \cdot 52 \ 452 \\ 37 \\ 9 \cdot 52 \ 494 \\ 42 \\ 37 \\ 9 \cdot 52 \ 536 \\ 42 \\ 37 \\ 9 \cdot 52 \ 536 \\ 42 \\ 38 \\ 9 \cdot 52 \ 578 \\ 41 \\ 9 \cdot 52 \ 578 \\ 41 \\ 38 \\ 9 \cdot 52 \ 518 \\ 41 \\ 41 \\ 41 \\ 41 \\ 41 \\ 41 \\ 41 \\ $	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
$\begin{array}{c} 36 & 9 \cdot 50 & 373 \\ 37 & 9 \cdot 50 & 411 \\ 38 & 9 \cdot 50 & 448 \\ 39 & 9 \cdot 50 & 486 \\ 40 & 9 \cdot 50 & 523 \\ 41 & 9 \cdot 50 & 561 \\ 42 & 9 \cdot 50 & 561 \\ 43 & 9 \cdot 50 & 635 \end{array}$	$\begin{array}{c} 37\\ 9,52\\ 70\\ 37\\ 9,52\\ 745\\ 37\\ 9,52\\ 787\\ 9,52\\ 787\\ 41\\ 37\\ 9,52\\ 870\\ 41\\ 37\\ 9,52\\ 870\\ 41\\ 41\\ 37\\ 9,52\\ 9,52\\ 9,52\\ 9,52\\ 9,52\\ 9,52\\ 9,52\\ 9,52\\ 41\\ 42\\ 37\\ 9,52\\ 9,52\\ 41\\ 42\\ 37\\ 9,52\\ 9,52\\ 41\\ 42\\ 42\\ 37\\ 9,52\\ 9,52\\ 41\\ 42\\ 42\\ 42\\ 42\\ 42\\ 42\\ 42\\ 42\\ 42\\ 42$	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{c} 3\overline{7} & 37 & 3\overline{6} \\ 6 & 3 \cdot 7 & 3 \cdot 7 & 3 \cdot 6 \\ 7 & 4 \cdot 4 & 4 \cdot 3 & 4 \cdot 2 \\ 8 & 5 \cdot 0 & 4 \cdot 9 & 4 \cdot 8 \\ 9 & 5 \cdot 6 & 5 \cdot 5 & 5 \cdot 5 \\ 10 & 6 \cdot 2 & 6 \cdot 1 & 6 \cdot 1 \\ 20 & 12 \cdot 5 & 12 \cdot 3 & 12 \cdot 1 \\ \end{array}$
$\begin{array}{c} \underline{44} \\ \underline{9.50} \\ 672 \\ 45 \\ 9.50 \\ 710 \\ 46 \\ 9.50 \\ 747 \\ 47 \\ 9.50 \\ 784 \\ 48 \\ 9.50 \\ 821 \\ \underline{49} \\ 9.50 \\ 858 \\ 85$	$\begin{array}{c} 37\\ 3\overline{7}\\ 9.53\\ 0.53\\ $	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	$ \begin{array}{c} 30 18.7 18.5 18.2\\ 40 25.0 24.\overline{6} 24.3\\ 50 31.2 30.8 30.4\\ \hline \underline{4}\\ 6 0.\overline{4} 0.4\\ \hline \end{array} $
$\begin{array}{c} 50 & 9 \cdot 50 & 89 \overline{5} \\ 51 & 9 \cdot 50 & 93 \overline{2} \\ 52 & 9 \cdot 50 & 96 \overline{9} \\ 53 & 9 \cdot 51 & 00 \overline{6} \\ 54 & 9 \cdot 51 & 04 \overline{3} \\ 55 & 9 \cdot 51 & 08 \overline{0} \\ 56 & 9 \cdot 51 & 117 \end{array}$	$\begin{array}{c} 37 & 9 \cdot 53 & 285 \\ 37 & 9 \cdot 53 & 326 \\ 37 & 9 \cdot 53 & 368 & 41 \\ 37 & 9 \cdot 53 & 409 & 41 \\ 37 & 9 \cdot 53 & 450 \\ 37 & 9 \cdot 53 & 450 \\ 36 & 9 \cdot 53 & 491 & 41 \\ 36 & 9 \cdot 53 & 491 & 41 \\ \end{array}$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{array}{c} 7 \ 0 \cdot 5 \ 0 \cdot \frac{4}{8} \\ 8 \ 0 \cdot 6 \ 0 \cdot 5 \\ 9 \ 0 \cdot 7 \ 0 \cdot 6 \\ 10 \ 0 \cdot 7 \ 0 \cdot 6 \\ 20 \ 1 \cdot 5 \ 1 \cdot 3 \\ 3 \ 0 \ 2 \cdot 2 \ 2 \cdot 2 \\ 40 \ 3 \cdot 0 \ 2 \cdot 6 \\ 50 \ 3 \cdot 7 \ 3 \cdot 3 \end{array}$
57 9.51 154 58 9.51 190 59 9.51 227 60 9.51 264 Log. Cos.	$\begin{array}{c} 37 \\ 36 \\ 37 \\ 36 \\ 9.53 \\ 574 \\ 41 \\ 37 \\ 9.53 \\ 656 \\ 9.53 \\ 656 \\ 41 \\ 9.53 \\ 697 \\ 41 \\ 41 \\ 41 \\ 41 \\ 9.53 \\ 697 \\ 41 \\ 41 \\ 41 \\ 61 \\ 100$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	5013.7]3.3 P. P.

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#### TABLE VII.—LOGARITHMIC SINES, COSINES, TANGENTS, AND COTANGENTS.

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1	og. Sin.	d.	Log. Tan.	c. d. Lo	g. Cot	Log. Cos.	d.	[	P. P.
$     \begin{array}{c}       1 & 9 \\       2 & 9 \\       3 & 9     \end{array} $	$\begin{array}{r} \cdot 51 \ 264 \\ \cdot 51 \ 301 \\ \cdot 51 \ 337 \\ \cdot 51 \ 374 \\ \cdot 51 \ 410 \end{array}$	37 36 36 36	9.53 697 9.53 738 9.53 779 9.53 820 9.53 861	$\begin{array}{c} 41 \\ 41 \\ 0 \\ 41 \\ 0 \\ 41 \\ 0 \\ 0 \\ \end{array}$	46 303 46 262 46 221 46 180 46 139	29.97562 19.97558	4444	60 59 58 57 56	$\begin{array}{c} 41 & 4\overline{0} & 40 \\ 6  & 4 \cdot 1  & 4 \cdot \overline{0}  & 4 \cdot \underline{0} \end{array}$
69 79 89 99	51 447 51 483 51 520 51 556 51 593 51 629	366 366 366 366 36 36	$\begin{array}{r} 9.53 & 902 \\ 9.53 & 943 \\ 9.53 & 983 \\ 9.54 & 024 \\ 9.54 & 065 \\ 9.54 & 106 \\ 9.54 & 106 \end{array}$	$\begin{array}{c} 41 \\ 40 \\ 41 \\ 0 \\ 41 \\ 40 \\ 40 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\$	46 098 46 05 46 01 45 97 45 93 45 93	79.97541 59.97536 59.97532 49.97527	4141414	55 54 53 52 51 50	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
11 9 12 9 13 9 14 9	·51 665 ·51 702 ·51 738 ·51 774	3 <u>6</u> 3 <u>6</u> 3 <u>6</u> 3 <u>6</u> 3 <u>6</u>	9.541479.541879.542289.54269	$\begin{array}{c} 41 \\ 40 \\ 40 \\ 0 \\ 41 \\ 0 \\ 41 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ $	45 85 45 81 45 77 45 73	3 9 · 97 519 2 9 · 97 514 2 9 · 97 510 1 9 · 97 505	414141414 4	49 48 47 46	30 20 5 20 2 20 0 40 27 3 27 0 26 6 50 34 1 33 7 33 3 39 39
16 9 17 9 18 9 19 9	.51 810 .51 847 .51 883 .51 919 .51 955 .51 991	36 36 36 36 36 36	9.54309 9.54350 9.54390 9.54431 9.54471 9.54512	4000.400.400.400.4000.4000.4000.4000.000000	$\begin{array}{r} 45 & 69 \\ 45 & 65 \\ 45 & 60 \\ 45 & 56 \\ 45 & 52 \\ 45 & 52 \\ 45 & 48 \\ \end{array}$	0 9 · 97 497 9 9 · 97 492 9 9 · 97 488 9 9 · 97 488 8 9 · 97 483	<b>4</b>	45 44 43 42 41 40	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$
21 9 22 9 23 9 24 9	·52 027 ·52 063 ·52 099 ·52 135 ·52 170	36 36 36 36 35	9.545129.545529.545939.546339.546739.54714		$\begin{array}{r} 45 & 40 \\ 45 & 40 \\ 45 & 36 \\ 45 & 32 \\ 45 & 32 \\ 45 & 28 \end{array}$	79.97475 79.97470 79.97466 9.97461 9.97461	쉐쉐쉐쉐   쉐	39 38 37 36 35	20 13 1 13 0 30 19 7 19 5 40 28 3 26 0 50 32 9 32 5
26 9 27 9 28 9 29 9	·52 206 ·52 242 ·52 278 ·52 314 ·52 349	36 35 35 35 35 35	9.54754 9.54794 9.54834 9.54874	$\begin{array}{c} 40 \\ 40 \\ 40 \\ 0 \\ 40 \\ 40 \\ 0 \\ 4\overline{0} \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\$	45 24 45 20 45 16 45 12	$     \begin{array}{r}       6 9 \cdot 97 \ 45\overline{2} \\       5 9 \cdot 97 \ 448 \\       5 9 \cdot 97 \ 443 \\       5 9 \cdot 97 \ 439 \\       5 9 \cdot 97 \ 439 \\     \end{array} $	14114141414 141	$     \begin{array}{r}       34 \\       33 \\       32 \\       31 \\       30     \end{array} $	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
31 9 32 9 33 9 34 9	·52 385 ·52 421 ·52 456 ·52 492 ·52 492	36 35 35 35 35	9.54955 9.54995 9.55035 9.55075	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	45 04 45 00 44 96 44 92 44 92	59.97430 59.97425 9.97421 9.97416 9.97416	14114141414	29 28 27 26 25	$ \begin{array}{c} 6 & 3 \cdot 7 & 3 \cdot 5 & 0 & 3 \cdot 6 \\ 7 & 4 \cdot 3 & 4 \cdot 2 & 4 \cdot 2 \\ 8 & 4 \cdot 9 & 4 \cdot 8 & 4 \cdot 8 \\ 9 & 5 \cdot 5 & 5 \cdot 5 & 5 \cdot 4 \\ 10 & 6 \cdot 1 & 6 \cdot 1 & 6 \cdot 1 & 6 \cdot 0 \\ 20 & 12 \cdot 3 & 12 \cdot 1 & 12 \cdot 0 \\ 30 & 18 \cdot 5 & 18 \cdot 2 & 18 \cdot 0 \\ 40 & 24 \cdot 6 & 24 \cdot 3 & 24 \cdot 0 \\ 50 & 30 \cdot 8 & 30 \cdot 4 & 30 \cdot 0 \\ \end{array} $
36 9 · 37 9 · 38 9 · 39 9 ·	· 52 563 · 52 598 · 52 634 · 52 669	35555 335 35 35 35 35 35	9.55155 9.55195 9.55235 9.55275 9.55275	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	14 848 44 808 44 768 14 725 14 685	9.97407 9.9740 <u>3</u> 9.97398 9.97394	1414141414 141	24 23 22 21 20	$\begin{array}{cccccccccccccccccccccccccccccccccccc$
$\begin{array}{c} 42 & 9 \\ 43 & 9 \\ \underline{44} & 9 \\ \end{array}$	·52 704 ·52 740 ·52 775 ·52 810 ·52 848 ·52 881	355 355 35 35 35 35	9.55355 9.55394 9.55434 9.55474	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{array}{r} 14 & 645 \\ 14 & 605 \\ 14 & 565 \\ 14 & 526 \\ 14 & 486 \end{array}$	9.97 38 <u>5</u> 9.97 380 9.97 37 <u>6</u> 9.97 37 <u>1</u>	1414141414 141	$     \begin{array}{r}       19 \\       18 \\       17 \\       16 \\       15     \end{array} $	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
46 9 · 47 9 · 48 9 · 49 9 ·	.52 916 .52 951 .52 986 .53 021	35 35 35 35 35 35	9.55553 9.55593 9.55633 9.55633 9.55672	$\begin{array}{c} 3 \\ 4 \\ 0 \\ 3 \\ \overline{9} \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ $	$\begin{array}{c} 14 & 44 \overline{6} \\ 14 & 40 \overline{6} \\ 14 & 36 \overline{7} \\ 14 & 32 \overline{7} \end{array}$	9.97 362 9.97 358 9.97 353 9.97 353 9.97 349	1414141414 14	14 13 12 11	$5\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ $
51 9. 52 9. 53 9. 54 9.	- 53 056 - 53 091 - 53 126 - 53 161 - 53 196	35 35 35	9.55712 9.55751 9.55791 9.55831 9.55870	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{r} 14 & 288 \\ 14 & 248 \\ 14 & 208 \\ 14 & 208 \\ 14 & 169 \\ 14 & 129 \\ 14 & 129 \\ 14 & 000 \\ 14 &$	9 · 97 340 9 · 97 335 9 · 97 330 9 · 97 326	4445444	10 9 8 7 6	70.60.50.4 80.60.60.5 90.70.70.6 100.80.70.6
56 9 · 57 9 · 58 9 · 59 9 ·	53 231 53 266 53 301 53 335 53 370		$\begin{array}{r} 9.55 909 \\ 9.55 949 \\ 9.55 988 \\ 9.56 028 \\ 9.56 067 \end{array}$	39 39 39 0.4 39 0.4 39 0.4	4 090 4 051 4 011 3 972 3 932	9.97 317 9.97 312 9.97 308 9.97 303	14141414 5 14	54321	201.61.51.51.3 302.52.222 403.33.02.6 504.13.73.3
	53 405 og. Cos.	d.	9.56 106 Log. Cot. c		<u>13 893</u> 5 Tan.	9.97 298 Log. Sin.	d.	<u> </u>	P. P.

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TABLE VII.-LOGARITHMIC SINES, COSINES, TANGENTS, AND COTANGENTS.

20	• TAB	LE	VII.—LO				) SINES, FANGEN		SINI	ES, TANGENTS, 159°
	Log. Sin.	d.	Log. Tan.	c.d.	Log.	Cot.	Log. Cos.	d.		P. P.
0	9.53 405	—	$9.5610\overline{6}$	39	0.43	893	9.97 298	4	60	
$\frac{1}{2}$	$9.53440 \\ 9.53474$	35 34 34	$9.56\ 146 \\ 9.56\ 185 \\ 9.56\ 224$	3 <u>9</u> 39	$0.43 \\ 0.43$	815	9.97 29 <u>4</u> 9.97 289	444	59 58	
34	9.53 509 9.53 544	35	$9.56\ 22\overline{4}$ $9.56\ 26\overline{3}$	39	$0.43 \\ 0.43$	77 <u>5</u> 736	9 · 97 285 9 · 97 280	5	57 56	$\begin{array}{ccc} \mathbf{3\overline{9}} & 39 \\ 6 & 3 \cdot 9 & 3 \cdot 9 \end{array}$
5 6	9.53 578 9.53 61 <u>3</u>	3 <u>4</u> 3 <u>4</u>	9 · 56 303 9 · 56 342	39 39	$0.43 \\ 0.43$	697 658	9 · 97 275 9 · 97 27 <u>1</u>	444	55 54	$\begin{array}{cccccccccccccccccccccccccccccccccccc$
78	9.53647	34 34 34 34 34	9.56 381 9.56 420	39 3 <u>9</u>	0.43	619	9.97 26 <u>6</u>	4 5 4	53 52	9 5.9 5.8
9	9.53682 9.53716	34	9.56 459	39 39	0.43	540	<u>9.9725</u> 7	444	51	2013.113.0
10 11	9.53750 9.53785	$3\bar{4} \\ 3\bar{4}$	9 · 56 498 9 · 56 537 9 · 56 576	39 39	$0.43 \\ 0.43 \\ 0.43$	¦ 46⊇	9.97252 9.97248	4 5	50 49	30 19 · 7 19 · 5 40 26 · 3 26 · 0 50 32 · 9 32 · 5
12 13	9.53819 9.53854	$3\overline{4}$ 34	9.56 615	3 <u>9</u> 38	$0.43 \\ $		9.97243 9.97238	5 4 4	48 47	00102-0102-0
$\frac{14}{15}$	9.53 888 9.53 922	$3\overline{4}$ $3\overline{4}$	9.56654 9.56693	39 39	0.43	346 307	9.97 229		$\frac{46}{45}$	$3\overline{8}$ $38$ $3\overline{7}$ 6 3 $\overline{8}$ 3 $\overline{8}$ 3 $\overline{7}$
$16 \\ 17$	9.53 95 <u>6</u> 9.53 990	34 34	9.56732 9.56771 9.56810 9.56848	39 39	0.43 0.43	268 229	9 · 97 224 9 · 97 220	51414 514	44 43	$\begin{array}{cccccccccccccccccccccccccccccccccccc$
18 19	9.54 025 9.54 059	34	9.56 81 <u>0</u> 9.56 848	38	$0.43 \\ $	$190 \\ 151$	9.97 220 9.97 215 9.97 210	4 4	42 41	9 5.8 5.7 5.6
$\overline{\begin{array}{c} 20 \\ 21 \end{array}}$	9.54093 9.54127	34 34 34	9.56 887 9.56 926	3 <u>9</u> 38	$0.43 \\ 0.43$	$11\overline{2}$ 1074	9.97 206		40 39	
22 23	9.54127 9.54161 9.54195	34	9.56 96 <u>5</u> 9.57 003	3 <u>9</u> 3 <u>8</u>	$0.43 \\ 0.42$	035	9.97201 9.97196 9.97191	4 5 4	38 37	$\begin{array}{c} 30 \ 19 \cdot \overline{2} \ 19 \cdot 0 \ 18 \cdot \overline{7} \\ 40 \ 25 \cdot \overline{6} \ 25 \cdot \overline{3} \ 25 \cdot 0 \\ 50 \ 32 \cdot 1 \ 31 \cdot \overline{6} \ 31 \cdot \overline{2} \end{array}$
$\frac{\overline{24}}{25}$	$\frac{9.54229}{9.54263}$	34 33	$\frac{9.57042}{9.57081}$	38 39	0.42	<u>958</u>	9.97 187	1 4	<u>36</u> 35	00102.1101.0101.2
25 26 27	9.54 203 9.54 297 9.54 331	34 34	$9.57\ 119$ $9.57\ 158$ $9.57\ 196$ $9.57\ 196$	38 38			9.97177 9.97177 9.97173	54	34 33	$\begin{array}{cccccccccccccccccccccccccccccccccccc$
27 28 29	9.54351 9.54365 9.54398	34 33	9.57156 9.57196 9.57235	38 38		2 803	9.97173 9.97168 9.97163	2	32 31	$\begin{array}{cccccccccccccccccccccccccccccccccccc$
30	$9.5443\overline{2}$	34 34	9.57 274	3 <u>9</u> 38	0.42	2 726		45	30	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
31 32	$\begin{array}{r}9.54 & 46\overline{6} \\ 9.54 & 500\end{array}$	34 33 34	9.57 350	3 <u>8</u> 38	0.42 0.42	3 649	19.97 149	1 #	29 28	$2011.\overline{6}11.511.\overline{3}$ $3017.517.\overline{2}17.0$
33 34	9.54 534 9.54 567	34 33	9.57 38 <u>9</u> 9.57 427	38	$\begin{array}{c} 0.42\\ 0.42\end{array}$	$2611 \\ 3572$		Ĭ	27 26	
35 36	9.54601 9.54634	3 <u>3</u> 33	9.5746 <u>6</u> 9.57504	38		2534 2495			$\frac{25}{24}$	001201120112010
37 38	9.5468 9.54702	34 3 <u>3</u> 33	9.57 50 <u>4</u> 9.57 542 9.57 581	38 38 38	$0.42 \\ 0.42$	$2\ 457$ $2\ 419$	9.97 125	14	23 22	3 <u>3</u> 33 6 3.3 3. <u>3</u>
$\frac{39}{40}$	9.54 735 9.54 769	33	<u>9.57619</u> 9.57657	38	$\frac{0.42}{0.42}$	2 <u>38</u> 0 2 342		5 4	$\frac{21}{20}$	7 3.9 3.8 8 4.4 4. <u>4</u>
40 41 42	9.54802 9.54836	3333 333 333 333 333 333 333 333 333 3	9.57 696 9.57 734	38 38	$0.42 \\ 0.42$	2 3 0 4	9.97 106	2	19 18	
43 44	9.54869 9.54902	33	9.57 772 9.57 810	38	0.4	$2 22\overline{2}$	9 . 97 097	5	17 16	2011.111.0 3016.716.5
45	9.54 936	3 <u>3</u> 33	9.57 848	38	0.42	2 15]		45	15	$\begin{array}{c} 9 & 5 \cdot 0 & 4 \cdot 9 \\ 10 & 5 \cdot 6 & 5 \cdot 5 \\ 20 & 11 \cdot 1 & 11 \cdot 0 \\ 30 & 16 \cdot 7 & 16 \cdot 5 \\ 40 & 22 \cdot 3 & 22 \cdot 0 \\ 50 & 27 \cdot 9 & 27 \cdot 5 \end{array}$
46 47	$9.5496\overline{9}$ $9.5500\overline{2}$	3 <u>3</u> 33	9 · 57 886 9 · 57 925	38 38 38		2 075	9.97 078	1 2	14 13	
48 49	9.55 036 9.55 069	33	9.57963 9.58001	38	$0.42 \\ 0.42$	2 037 L 999	9.97 073 9.97 068		$\frac{12}{11}$	5 4 610.510.4
$50 \\ 51$	9.55 135	33	9.58 039 9.58 077	38	0·4 0·4	L 923	89.97 058	5	10 9	$\begin{array}{c} & \mathbf{b} & 4^{4} \\ & 6^{0} \cdot 5^{0} \cdot 4 \\ & 7^{0} \cdot 6^{0} \cdot 5 \\ & 8^{0} \cdot 6^{0} \cdot 6 \\ & 9^{0} \cdot 7^{0} \cdot 7 \\ & 10^{0} \cdot 8^{0} \cdot 7 \\ & 20^{1} \cdot 6^{1} \cdot 5 \\ & 8^{0} 2 \cdot 5^{2} \cdot 2^{2} \\ & 40^{3} \cdot 3^{3} 3 \cdot 0 \\ & 50^{1} 4 \cdot 1^{3} \cdot 7 \end{array}$
51 52 53	$9.5516\overline{8}$ 9.55202	33 3 <u>3</u> 33 33	9.58 115 9.58 153	38 38 37	0.4	l 885 l 84 <u>7</u>	9 · 97 054 9 · 97 049	2	8 7	90.70.7 100.80.7
<u>54</u> 55	9.55 235 9.55 268	33	9.58 190 9.58 229	38	$\frac{0.4}{0.4}$	1 809	9.97 044	4	<u>6</u> 5	201:61:5 302:52:2 403:33:0 504:13:7
56 57	9.55 301 9.55 334	33 33	$9.58\ 266$ $9.58\ 304$ $9.58\ 304$	38 38 37	0.4	1 733	9 · 97 034 9 · 97 029		4	$403.\overline{3}3.0$ 504.13.7
58 59	9.55 367 9.55 400	33 33	9.58 342 9.58 380	38	0.4 0.4	L 628	89.97 025	5		
<u>60</u>	9.55 433	33	9.58 417	37	0.4	L 582	9.97 015	5		
-	Log. Cos.	d.	Log. Cot.	c. d.	Log.	Tan	Log. Sin.	d.	<u> '</u>	P. P.

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 TABLE VII.—LOGARITHMIC SINES, COSINES, TANGENTS,

 AND COTANGENTS.

158<sup>e</sup>

21				ANI	0.00	JTANGEN	TS.		158
'	Log. Sin.	d.	Log. Tan.			t. Log. Cos.	⁻d,		P. P.
0 1 2 3 4	9.55 433 9.55 466 9.55 498 9.55 531 9.55 564	33 32 33 33 33 32	9.58 493 9.58 493 9.58 531 9.58 568	$     \begin{array}{c}       38 \\       37 \\       37 \\       0.4$	_	79.97005 99.97000 19.96995	4 5 5 5 4	60 59 58 57 56	38 37 37 6 3.8 3.7 37
5 6 7 8 9	9.555597 9.55630 9.55662 9.55695 9.55728	33 32 32 32 32 32 32	$9.58\ 606$ $9.58\ 644$ $9.58\ 681$ $9.58\ 719$ $9.58\ 756$	$\begin{array}{c c} 37 \\ 38 \\ 37 \\ 37 \\ 37 \\ 37 \\ 37 \\ 37 \\ 37 \\ 37$	356	9.96 986	455545	55 54 53 52 51	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
10 11 12 13 14	9.55760 9.55793 9.55826 9.55858 9.55891	32 33 32 32 32	9.58794 9.58831 9.58869 9.58906 9.58944	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	168 131 093 056		5 54 5	$50 \\ 49 \\ 48 \\ 47 \\ 46$	$\begin{array}{c} 3019 \cdot 018 \cdot 718 \cdot 5 \\ 4025 \cdot 325 \cdot 024 \cdot 6 \\ 5031 \cdot 631 \cdot 230 \cdot 8 \end{array}$
15 16 17 18 <u>19</u>	9.55923 9.55956 9.55988 9.56020 9.56053	3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3	$9.59\ 056 \\ 9.59\ 093 \\ 9.59\ 131$	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	981 944 906 869	9 · 96 937 9 · 96 932 9 · 96 92 <u>7</u> 9 · 96 92 <u>7</u> 9 · 96 922	55554 E	45 44 43 42 41	$\begin{array}{c} 36 & 36 \\ 6 & 3 \cdot 6 & 3 \cdot 6 \\ 7 & 4 \cdot 2 & 4 \cdot 2 \\ 8 & 4 \cdot 8 & 4 \cdot 2 \\ 8 & 5 \cdot 5 & 5 \cdot 4 \\ 9 & 5 \cdot 5 & 5 \cdot 4 \\ 10 & 6 \cdot 1 & 6 \cdot 0 \end{array}$
20 21 22 23 24	$9.56\ 085$ $9.56\ 118$ $9.56\ 150$ $9.56\ 182$ $9.56\ 214$	3 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	$\begin{array}{r} 9.59 & 188 \\ 9.59 & 205 \\ 9.59 & 242 \\ 9.59 & 280 \\ 9.59 & 317 \end{array}$	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	794 757 720 683	9.96 912 9.96 907 9.96 902 9.96 902 9.96 897	5 5 5 5 5 5 5	40 39 38 37 36	10 6.1 6.0 2012.1 12.0 3018.2 18.0 4024.3 24.0 5030.4 30.0
25 26 27 28 29	9.56247 9.56279 9.56311 9.56343 9.56375	32 32 32 32 32 32 32 32 32	$\begin{array}{c} 9.59 & 354 \\ 9.59 & 391 \\ 9.59 & 428 \\ 9.59 & 465 \\ 9.59 & 502 \end{array}$	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	$     \begin{array}{r}       60\overline{8} \\       57\overline{1} \\       53\overline{4} \\       49\overline{7}     \end{array} $	9 · 96 887 9 · 96 882 9 · 96 877 9 · 96 877 9 · 96 873	555545	35 34 33 32 31	$\begin{array}{cccccccccccccccccccccccccccccccccccc$
30 31 32 33 34	9.564079.564399.564719.565039.565359.56535	32 32 32 32 32 32 32	9.59540 9.59577 9.59614 9.59651 9.59688	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	423 386 349 312	9.96 863 9.96 858 9.96 853 9.96 853 9.96 848	555555	30 29 28 27 26	$\begin{array}{c} 10 & 5.5 & 5.4 & 5.3 \\ 20 & 11.0 & 10.8 & 10.6 \\ 30 & 16.5 & 16.2 & 16.0 \\ 40 & 22.0 & 21.6 & 21.3 \\ 50 & 27.5 & 27.1 & 26.6 \end{array}$
35 36 37 38 <u>39</u>	9.565679.565999.566319.566639.566639.56695	32 32 31 32 32 32	9.59724 9.59761 9.59798 9.59835 9.59872	$\begin{array}{c} 37 \\ 37 \\ 37 \\ 0.40 \\ 37 \\ 0.40 \\ 36 \\ 0.40 \\ 0.40 \\ 0.40 \end{array}$	$23\overline{8} \\ 20\overline{1} \\ 16\overline{4} \\ 128$	9 · 96 833 9 · 96 828 9 · 96 823	55555555	25 24 23 22 21	$\begin{array}{ccc} 3\overline{1} & 31 \\ 6  & 3 \cdot \overline{1} & 3 \cdot 1 \\ 7  & 3 \cdot 7 & 3 \cdot \underline{6} \end{array}$
40 41 42 43 44	$\begin{array}{r} 9.56 & 727 \\ 9.56 & 758 \\ 9.56 & 790 \\ 9.56 & 822 \\ 9.56 & 854 \end{array}$	31 32 31 32	$\begin{array}{c} 9.59 & 909 \\ 9.59 & 946 \\ 9.59 & 982 \\ 9.60 & 019 \\ 9.60 & 056 \end{array}$	$     \begin{array}{c}       37 \\       36 \\       37 \\       0.40 \\       37 \\       0.37 \\       0.39 \\       36 \\       0.39 \\      0.39 \\      0.39 \\      $	054 017 980 944	9 · 96 808 9 · 96 802 9 · 96 797	55555555	20 19 18 17 16	$\begin{array}{c} 8 & 4 \cdot 2 \\ 9 & 4 \cdot 7 \\ 10 & 5 \cdot 2 \\ 20 & 10 \cdot 5 \\ 10 \cdot 5 & 10 \cdot 3 \\ 30 & 15 \cdot 7 & 15 \cdot 5 \\ 40 & 21 \cdot 9 & 20 \cdot 6 \end{array}$
45 46 47 48 49	$9.5688\overline{5}$ 9.56917 9.56949 9.56949 9.56980 9.57012	3 3 3 3 1 3 1 3 1 3 1 3 1 3	$\begin{array}{c} 9 \cdot 60 & 129 \\ 9 \cdot 60 & 166 \\ 9 \cdot 60 & 203 \\ 9 \cdot 60 & 239 \end{array}$	$     \begin{array}{c}       36 \\       37 \\       36 \\       36 \\       36 \\       36 \\       0.39 \\       36 \\       3$	87 <u>0</u> 833 797 760	9 · 96 787 9 · 96 782 9 · 96 777 9 · 96 772	5 5 5 5 5 5 5 5	15 14 13 12 11	$50^{1}26 \cdot 2^{1}25 \cdot 8$ $\overline{5}$ $5$ $\overline{4}$ $6 0 \cdot \overline{5} 0 \cdot 5 0 \cdot 4$
50 51 52 53 54	$\begin{array}{r} 9.57 & 043 \\ 9.57 & 075 \\ 9.57 & 106 \\ 9.57 & 138 \\ 9.57 & 169 \\ 9.57 & 169 \end{array}$	3 3 1 3 1 3 1 3 1 3 1 3 1 3 1	9.60312 9.60349 9.60386 9.60422	$     \begin{array}{ccccccccccccccccccccccccccccccccc$	687 650 614 577	9.96762 9.96757 9.96752 9.96752 9.96747	55555555	10 9 8 7 6	$\begin{array}{c} 7 \\ 0 \cdot \overline{6} \\ 0 \cdot 7 \\ 0 \cdot \overline{6} \\ 0 \cdot 7 \\ 0 \cdot 9 \\ 0 \cdot 8 \\ 0 \cdot 7 \\ 0 \cdot 9 \\ 0 \cdot 8 \\ 0 \cdot 7 \\ 0 \\ 0 \cdot 9 \\ 0 \cdot 8 \\ 0 \cdot 7 \\ 0 \\ 0 \cdot 7 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\$
55 56 57 58 59	$\begin{array}{c} 9\cdot 57 \ 201 \\ 9\cdot 57 \ 232 \\ 9\cdot 57 \ 263 \\ 9\cdot 57 \ 295 \\ 9\cdot 57 \ 326 \\ 9\cdot 57 \ 326 \end{array}$	31 31 31 31 31 31	$\begin{array}{c} 9.60 & 439 \\ 9.60 & 495 \\ 9.60 & 531 \\ 9.60 & 568 \\ 9.60 & 604 \end{array}$	$     \begin{array}{ccccccccccccccccccccccccccccccccc$	$50\overline{4}$ 468 432 395	9.96732 9.9672 <u>7</u> 9.96721	5555555	5 4 3 2 1	201.81.61.5 302.72.52.2 403.63.33.0 504.64.13.7
<u>60</u>	9.57 357 Log. Cos.	d.	9.00 041	. d. Log,	-		d.	<u> </u>	P. P.

111°

21°

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## TABLE VII.—LOGARITHMIC SINES, COSINES, TANGENTS, AND COTANGENTS.

22°		AND	COTANGEN	ITS.	157°
' Log. Sin.	d. Log. Tan	. c. d. Log.	Cot. Log. Cos.	d,	P. P.
$\begin{array}{c} 0 & 9.57 & 357 \\ 1 & 9.57 & 387 \\ 2 & 9.57 & 420 \\ 3 & 9.57 & 451 \\ 4 & 9.57 & 482 \\ 5 & 9.57 & 513 \\ 6 & 9.57 & 513 \\ 6 & 9.57 & 544 \\ 7 & 9.57 & 544 \\ 7 & 9.57 & 567 \\ 9 & 9.57 & 669 \\ 11 & 9.57 & 700 \\ 12 & 9.57 & 731 \\ 13 & 9.57 & 762 \end{array}$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$		$\begin{array}{c} 9 & 559   9.96 & 716 \\ 9 & 322   9.96 & 716 \\ 9 & 322   9.96 & 701 \\ 9 & 250   9.96 & 701 \\ 9 & 250   9.96 & 701 \\ 9 & 213   9.96 & 696 \\ 9 & 177   9.96 & 686 \\ 9 & 105   9.96 & 686 \\ 9 & 105   9.96 & 675 \\ 8 & 960   9.96 & 675 \\ 8 & 996   9.96 & 675 \\ 8 & 996   9.96 & 655 \\ 8 & 924   9.96 & 655 \\ 8 & 888   9.96 & 655 \\ \end{array}$	55555555555555555555555555555555555555	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{array}{c} 30 & 9 \cdot 61 & 144 \\ 31 & 9 \cdot 61 & 184 \\ 31 & 9 \cdot 61 & 225 \\ 30 & 9 \cdot 61 & 225 \\ 31 & 9 \cdot 61 & 295 \\ 31 & 9 \cdot 61 & 295 \\ 30 & 9 \cdot 61 & 323 \\ 30 & 9 \cdot 61 & 364 \\ 31 & 9 \cdot 61 & 436 \\ 31 & 9 \cdot 61 & 57 \\ 30 & 9 & 57 \\ 30 & 9 & 57 \\ 30 & 9 & 57 \\ 30 & 9 & 57 \\ 30 & 9 & 57 \\ 30 & 9 & 57 \\ 30 & 9 & 57 \\ 30 & 9 & 57 \\ 30 & 9 & 57 \\ 30 & 9 & 57 \\ 30 & 9 & 57 \\ 30 & 9 & 57 \\ 30 & 9 & 57 \\ 30$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{array}{c} 8 & 852 \\ 9 & 96 & 644 \\ 8 & 816 \\ 9 & 96 & 634 \\ 8 & 780 \\ 9 & 96 & 629 \\ 8 & 708 \\ 9 & 96 & 629 \\ 8 & 708 \\ 9 & 96 & 629 \\ 8 & 708 \\ 9 & 96 & 629 \\ 8 & 708 \\ 9 & 96 & 619 \\ 8 & 636 \\ 9 & 96 & 613 \\ 8 & 600 \\ 9 & 96 & 608 \\ 3 & 528 \\ 9 & 96 & 598 \\ 8 & 492 \\ 9 & 96 & 598 \\ 8 & 492 \\ 9 & 96 & 598 \\ \end{array}$	5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{c} 31 \\ 30 \\ 30 \\ 30 \\ 9 \\ 61 \\ 65 \\ 80 \\ 9 \\ 9 \\ 61 \\ 65 \\ 80 \\ 9 \\ 61 \\ 65 \\ 80 \\ 9 \\ 61 \\ 65 \\ 80 \\ 9 \\ 61 \\ 72 \\ 80 \\ 9 \\ 61 \\ 72 \\ 80 \\ 9 \\ 61 \\ 72 \\ 80 \\ 9 \\ 61 \\ 72 \\ 80 \\ 9 \\ 61 \\ 72 \\ 80 \\ 9 \\ 61 \\ 72 \\ 80 \\ 9 \\ 61 \\ 72 \\ 80 \\ 9 \\ 61 \\ 72 \\ 80 \\ 9 \\ 61 \\ 72 \\ 80 \\ 9 \\ 61 \\ 80 \\ 9 \\ 80 \\ 9 \\ 61 \\ 80 \\ 9 \\ 80 \\ 80$	36         0         38           35         0         38           365         0         38           365         0         38           365         0         38           365         0         38           365         0         38           365         0         38           365         0         38           365         0         38           365         0         38           35         0         38	$\begin{array}{c} 3 \ 456 \ 9 \ .96 \ 587 \\ 3 \ 420 \ 9 \ .96 \ 587 \\ 3 \ 420 \ 9 \ .96 \ 572 \\ 3 \ 321 \ 9 \ .96 \ 572 \\ 3 \ 327 \ 9 \ .96 \ 572 \\ 3 \ 277 \ 9 \ .96 \ 576 \\ 3 \ 277 \ 9 \ .96 \ 576 \\ 3 \ 277 \ 9 \ .96 \ 576 \\ 3 \ 277 \ 9 \ .96 \ 576 \\ 3 \ 277 \ 9 \ .96 \ 576 \\ 3 \ 277 \ 9 \ .96 \ 576 \\ 3 \ 277 \ 9 \ .96 \ 576 \\ 5 \ 277 \ 9 \ .96 \ 576 \\ 5 \ 576 \ 576 \\ 5 \ 576 \ 576 \ 576 \\ 5 \ 576 \ 576 \ 576 \\ 5 \ 576 \ 576 \ 576 \ 576 \\ 5 \ 576 \ 5$	15 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
$\begin{array}{c} 37 & 9 \cdot 58 & 497 \\ 38 & 9 \cdot 58 & 527 \\ 39 & 9 \cdot 58 & 558 \\ 40 & 9 \cdot 58 & 588 \\ 42 & 9 \cdot 58 & 618 \\ 42 & 9 \cdot 58 & 618 \\ 42 & 9 \cdot 58 & 678 \\ 44 & 9 \cdot 58 & 708 \\ 44 & 9 \cdot 58 & 708 \\ 45 & 9 \cdot 58 & 738 \\ 46 & 9 \cdot 58 & 769 \\ \end{array}$	$\begin{array}{c} 30 \\ 9 \cdot 61 \\ 972 \\ 30 \\ 9 \cdot 62 \\ 001 \\ 30 \\ 9 \cdot 62 \\ 001 \\ 30 \\ 9 \cdot 62 \\ 001 \\ 9 \cdot 62 \\ 001 \\ 149 \\ 30 \\ 9 \cdot 62 \\ 220 \\ 30 \\ 9 \cdot 62 \\ 20 \\ 30 \\ 9 \\ 10 \\ 10 \\ 10 \\ 10 \\ 10 \\ 10 \\ 10$	0.387           3350         0.37           33550         0.37           35550         0.37           35550         0.37           35550         0.37           35550         0.37           35550         0.37           35500         0.37           35500         0.37           35500         0.37           35500         0.37           35500         0.37           35500         0.37           35500         0.37	$\begin{array}{c} 0.28 \\ 9.96 \\ 9.92 \\ 9.96 \\ 5.19 \\ 9.96 \\ 5.14 \\ 9.96 \\ 5.14 \\ 9.96 \\ 5.14 \\ 9.96 \\ 5.03 \\ 8.15 \\ 9.96 \\ 4.98 \\ 8.15 \\ 9.96 \\ 4.98 \\ 7.79 \\ 9.96 \\ 4.98 \\ 7.44 \\ 9.96 \\ 4.82 \\ 7.08 \\ 9.96 \\ 4.82 \\ 7.08 \\ 9.96 \\ 4.82 \\ 7.08 \\ 9.96 \\ 4.82 \\ 7.08 \\ 9.96 \\ 4.82 \\ 7.08 \\ 9.96 \\ 4.82 \\ 7.08 \\ 9.96 \\ 4.92 \\ 9.96 \\ 4.82 \\ 7.08 \\ 9.96 \\ 4.92 \\ 9.96 \\ 4.92 \\ 7.08 \\ 7.08 \\ 7.$	$\begin{array}{c} 23\\ 5\\ 5\\ 5\\ 5\\ 5\\ 5\\ 5\\ 5\\ 5\\ 5\\ 5\\ 5\\ 5\\$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
$\begin{array}{c} 47 & 9 & 58 & 799 \\ 48 & 9 & 58 & 829 \\ 49 & 9 & 58 & 859 \\ 50 & 9 & 58 & 859 \\ 51 & 9 & 58 & 819 \\ 52 & 9 & 58 & 919 \\ 52 & 9 & 58 & 949 \\ 53 & 9 & 58 & 979 \\ 54 & 9 & 59 & 038 \\ 55 & 9 & 59 & 038 \\ 57 & 9 & 59 & 038 \\$	$\begin{array}{c} 30 & 9 \cdot 62 & 322\\ 30 & 9 \cdot 62 & 397\\ 30 & 9 \cdot 62 & 438\\ 30 & 9 \cdot 62 & 438\\ 30 & 9 \cdot 62 & 468\\ 30 & 9 \cdot 62 & 503\\ 30 & 9 \cdot 62 & 503\\ 30 & 9 \cdot 62 & 574\\ 29 & 9 \cdot 62 & 679\\ 30 & 9 \cdot 62 & 644\\ 29 & 9 \cdot 62 & 644\\ 29 & 9 \cdot 62 & 715\\ 29 & 9 \cdot 62 & 715\\ \end{array}$	35 35 35 35 50 35 50 35 50 37 35 50 35 50 37 35 50 37 35 50 37 35 50 37 35 50 37 35 50 37 35 50 37 35 50 37 35 50 37 35 50 37 37 35 50 37 37 35 50 37 37 35 50 37 37 35 50 37 37 37 35 50 37 37 37 37 37 35 50 37 37 37 37 37 37 37 37 37 37 37 37 37	$\begin{array}{c} 53\overline{1} 9 \cdot 96 \ 45\overline{0} \\ 49\overline{6} 9 \cdot 96 \ 445 \\ 461 \ 9 \cdot 96 \ 445 \\ 426 \ 9 \cdot 96 \ 434 \\ 39\overline{0} 9 \cdot 96 \ 42\overline{9} \\ 35\overline{5} 9 \cdot 96 \ 42\overline{9} \\ 35\overline{5} 9 \cdot 96 \ 424 \\ 32\overline{0} 9 \cdot 96 \ 41\overline{3} \\ 285 \ 9 \cdot 96 \ 41\overline{3} \end{array}$	11 10 9 8 7 6 5 4 3 2	$\begin{array}{c} \overline{5} & 5 \\ 6[0.5]{0.6} \\ 7[0.6]{0.6} \\ 0.70.6 \\ 9[0.8]{0.7} \\ 10[0.9]{0.8} \\ 201.66 \\ 30[2.7]{2.5} \\ 40[3.6]{3.3} \\ 50[4.6]{4.1} \end{array}$
59 9.59 158 60 9.59 188	$\begin{array}{c} 30 \\ 30 \\ 30 \\ 9 \cdot 62 \\ 785 \\ \hline 0 \cdot 62 \\ 750 \\ \hline 0 \cdot 62 \\ 785 \\ \hline 0 \cdot 62 \\ \hline 0 \hline 0 \hline 0 \hline 0 \\ \hline 0 \hline 0 \hline 0 \hline 0 \\ \hline 0 \hline 0$	35 0.37 0.37	215 9.96 402	$\frac{5}{5} \frac{1}{0}$	P. P.

112°

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# TABLE VII.—LOGARITHMIC SINES, COSINES, TANGENTS, AND COTANGENTS.

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~0										100
'	Log. Sin.	d.	Log. Tan.	c. d.	Log.	Cot.	Log. Cos.	d.		P. P.
0 1 2 3 4	9.59 188 9.59 217 9.59 247 9.59 277 9.59 277 9.59 306	29 30 29 29	9 · 62 785 9 · 62 820 9 · 62 855 9 · 62 890 9 · 62 925	35 35 35 35 35	0 · 37 0 · 37 0 · 37 0 · 37 0 · 37	179 144 109	9.96 402 9.96 397 9.96 392 9.96 386 9.96 386 9.96 381	ା ପାପାପ ପା	60 59 58 57 56	
5 6 7 8 9	9.59 336 9.59 366 9.59 395 9.59 425 9.59 454	30999999 2099999	9.62 960 9.62 995 9.63 030 9.63 065 9.63 100	35 35 35 35 35	0 · 37 0 · 36 0 · 36		9 · 96 375 9 · 96 370 9 · 96 365 9 · 96 359 9 · 96 359 9 · 96 354	55555	55 54 53 52 51	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
10 11 12 13 14	9.59 48 <u>4</u> 9.59 513 9.59 54 <u>3</u> 9.59 572 9.59 602	1919191919 22291919 22291919	$\begin{array}{r} 9.63 \ 13\overline{5} \\ 9.63 \ 170 \\ 9.63 \ 20\overline{5} \\ 9.63 \ 240 \\ 9.63 \ 275 \end{array}$	35 35 3 <u>5</u> 34 35	0.36 0.36 0.36 0.36	864 829 8794	9.96 349 9.96 343 9.96 338 9.96 338 9.96 332	1 ଫାପାପାପାପ	$50 \\ 49 \\ 48 \\ 47 \\ 46$	30 17.7 17.5 40 23.6 23.3 50 29.6 29.1
15 16 17 18 19	9.59631 9.59661 9.59690 9.59719 9.59749	19 19 19 19 19 19 19 19 19 19 19 19 19 1	$\begin{array}{r} 9\cdot 63 \ 310\\ 9\cdot 63 \ 34\underline{4}\\ 9\cdot 63 \ 37\underline{9}\\ 9\cdot 63 \ 414\\ 9\cdot 63 \ 449 \end{array}$	35 34 35 35 34	0 · 36 0 · 36 0 · 36 0 · 36	690 655	9.96 321 9.96 316 9.96 311 9.96 311 9.96 305	1 0	45 44 43 42 41	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
20 21 22 23 24	9 · 59 778 9 · 59 807 9 · 59 837 9 · 59 866 9 · 59 895	29 29 29 29 29 29	9 · 63 484 9 · 63 518 9 · 63 553 9 · 63 588 9 · 63 622	354 34 35 35 35 35 37	0.36	3 48ī 3 447	9.96289 9.96283 9.96278	୩ ଫାଫାଫାଫା	40 39 38 37 36	20 11 · 5 11 · 3 30 17 · 2 17 · 0 40 23 · 0 22 · 6 50 28 · 7 28 · 3
25 26 27 28 29	$\begin{array}{c} 9.59 \ 92\overline{4} \\ 9.59 \ 95\overline{3} \\ 9.59 \ 98\overline{2} \\ 9.60 \ 012 \\ 9.60 \ 041 \end{array}$	29 29 29 29 29 29	9 · 63 657 9 · 63 692 9 · 63 726 9 · 63 761 9 · 63 795	34 35 34 34 34 34 34 34 34 34 34 34 34 34 34	0.36 0.36 0.36	$   \begin{array}{c}     343 \\     3 308 \\     3 273 \\     3 239 \\     3 204 \\   \end{array} $	9 · 96 261 9 · 96 256 9 · 96 251	ା ପାପ ପାପାପା	35 34 33 32 31	30 6] 3.0 7] 3.5 8] 4.0
30 31 32 33 34	9.60 070 9.60 099 9.60 128 9.60 157 9.60 186	29 29 29 29 29	9 · 63 830 9 · 63 864 9 · 63 899 9 · 63 933 9 · 63 968	34 34 34 34 34 34 34 34 34 34 34 34 34 3	0.36	$     \begin{array}{r}       3 170 \\       5 135 \\       5 101 \\       5 066 \\       5 032 \\     \end{array} $	9 · 96 234 9 · 96 229 9 · 96 223	ା ସାପାପାପା	30 29 28 27 26	$\begin{array}{c} 9 \\ 10 \\ 5.0 \\ 20 \\ 10.0 \\ 30 \\ 15.0 \\ 40 \\ 20.0 \\ 50 \\ 25.0 \end{array}$
35 36 37 38 39	$\begin{array}{r} 9.60\ 215\\ 9.60\ 244\\ 9.60\ 273\\ 9.60\ 301\\ 9.60\ 330\end{array}$	29 29 29 28 29	$\begin{array}{r} 9.64\ 00\overline{2}\\ 9.64\ 037\\ 9.64\ 071\\ 9.64\ 106\\ 9.64\ 140\end{array}$	34 34 34 34 34 34 34 34	0.35 0.35 0.35	5928	9.96 206 9.96 20 <u>1</u>	। ପାପାପାର ପା	25 24 23 22 21	$\begin{array}{cccccccccccccccccccccccccccccccccccc$
$     \begin{array}{r}             40 \\             41 \\             42 \\             43 \\             44 \\           $	$\begin{array}{r} 9.60\ 359\\ 9.60\ 388\\ 9.60\ 417\\ 9.60\ 445\\ 9.60\ 474\\ \end{array}$	29 28 29 28 29 28 29	$9.64 17\overline{4} \\9.64 209 \\9.64 243 \\9.64 243 \\9.64 277 \\9.64 312$	34 34 34 34 34 34	0.35	5 825 5 791 5 756 5 722 5 688	9.96 179 9.96 173 9.96 16 <u>8</u>	ଫାଫାଫାପା	20 19 18 17 16	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
45 46 47 48 49	9.60 503 9.60 532 9.60 560 9.60 589 9.60 618	28 29 28 28 28 29	$   \begin{array}{r}     9.6434\overline{6} \\     9.64380 \\     9.64415 \\     9.6449 \\     9.64483 \\     9.64483 \\   \end{array} $	34 34 34 34 34 34	0.35 0.35 0.35 0.35	5 65 <u>3</u> 5 619 5 585 5 551 5 517	9.96 157 9.96 151 9.96 146	151515615	15 14 13 12 11	50 24.6)24.1 23.7
50 51 52 53 54	9.60 646 9.60 675 9.60 703 9.60 732 9.60 760	288 288 288 288 288 288 288 288 288 288	9.645179.645519.645519.645859.646209.64654	04	0 · 35 0 · 35 0 · 35 0 · 35	5 482	9.96 129 9.96 123 9.96 118 9.96 118 9.96 112	6 5101015	10 9 8 7 6	$\begin{array}{c}6 \\ 0 \\ -6 \\ 0 \\ -5 \\ -7 \\ 0 \\ -7 \\ 0 \\ -7 \\ 0 \\ -7 \\ 0 \\ -7 \\ 0 \\ -7 \\ 0 \\ -7 \\ 0 \\ -7 \\ 0 \\ -7 \\ -7$
55 56 57 58 59	9.60 789 9.60 817 9.60 846 9.60 874 9.60 903	288888888	$\begin{array}{r} 9.64 & 634 \\ 9.64 & 688 \\ 9.64 & 722 \\ 9.64 & 756 \\ 9.64 & 790 \\ 9.64 & 824 \end{array}$	34 34 34 34	0.35 0.35 0.35 0.35	5 312 5 278 5 244	9.96 101 9.96 095 9.96 090 9.96 084	5151516	5 4 3 2 1	$\begin{array}{c} 10 & 1 & 0 & 0 & 0 & 0 & 0 \\ 10 & 1 & 0 & 0 & 0 & 0 & 0 \\ 20 & 2 & 0 & 1 & 3 & 1 & 6 \\ 30 & 3 & 0 & 2 & 7 & 2 & 5 \\ 40 & 4 & 0 & 3 & 6 & 3 & 3 \\ 50 & 5 & 0 & 4 & 6 & 4 & 1 \end{array}$
<u>60</u>		28	9.64 858	34 c.d.	0.35 Log.	i 141	9.96 073 Log. Sin.	5 d.	$\frac{1}{0}$	P. P.
		<u> </u>	1 .0	1	1					

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TABLE VII.—LOGARITHMIC SINES, COSINES, TANGENTS, AND COTANGENTS.

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'	Log. Sin.	d.	Log. Tan.	c. d.	Log. Cot.	Log. Cos.	d,		P. P.
0 1 2 3 4	$\begin{array}{r} 9.60 \ 93\overline{1} \\ 9.60 \ 95\overline{9} \\ 9.60 \ 988 \\ 9.61 \ 01\overline{6} \\ 9.61 \ 04\overline{4} \end{array}$	28 28 28 28 28 28 28 28	$9 \cdot 64 858 9 \cdot 64 892 9 \cdot 64 926 9 \cdot 64 960 9 \cdot 64 994 904 904 904 904 904 904 904 904 90$	34 3 <u>4</u> 33 34 34	$\begin{array}{c} 0.35 \ 10\overline{7} \\ 0.35 \ 07\overline{3} \\ 0.35 \ 040 \\ 0.35 \ 006 \end{array}$	<u>9.96 050</u>	ପା ପାଡ ପାପ୍ରା	60 59 58 57 56	04 00 00
56789 10	9.61073 9.61101 9.61129 9.61157 9.61186 9.61214	28 28 28 28 28 28	9.65028 9.65062 9.65096 9.65129 9.65163 9.65197	34 34 33 34 34	$\begin{array}{c} 0.34 \ 972 \\ 0.34 \ 938 \\ 0.34 \ 904 \\ 0.34 \ 870 \\ 0.34 \ 836 \\ 0.34 \ 802 \end{array}$	9.96 03 <u>9</u> 9.96 033 9.96 028 9.96 022 9.96 016	ପାପା ଡ ପାପାଡ	55 54 53 52 51 50	$\begin{array}{c} 34 & 33 & 33 \\ 6 & \mathbf{3 \cdot 4} & \mathbf{3 \cdot 3} & \mathbf{3 \cdot 3} \\ 7 & \mathbf{3 \cdot 9} & \mathbf{3 \cdot 9} & \mathbf{3 \cdot 8} \\ 7 & \mathbf{3 \cdot 9} & \mathbf{3 \cdot 9} & \mathbf{3 \cdot 8} \\ 8 & \mathbf{4 \cdot 5} & \mathbf{4 \cdot 4} & \mathbf{4 \cdot 4} \\ 9 & \mathbf{5 \cdot 1} & \mathbf{5 \cdot 0} & \mathbf{4 \cdot 9} \\ 10 & \mathbf{5 \cdot 6} & \mathbf{5 \cdot 6} & \mathbf{5 \cdot 5} \\ 20 & \mathbf{11 \cdot 3} & \mathbf{11 \cdot 4} & \mathbf{11 \cdot 0} \end{array}$
$   \begin{array}{c}     11 \\     12 \\     13 \\     14 \\     15 \\     16   \end{array} $	9.61242 9.61270 9.61298 9.61326 9.61326 9.61354 9.61382	28 28 28	9.65231 9.65265 9.65299 9.65332 9.65366 9.65400	34 33 34 33 34 33	$\overline{0.34633}$	$9.96\ 011$ $9.96\ 005$ $9.95\ 999$ $9.95\ 994$ $9.95\ 988$ $9.95\ 982$	ପାପାଡ ପାପାଡ	49 48 47 46 45 44	$\begin{array}{c} 20   1 \cdot 3   1 \cdot 1   1   1 \cdot 5 \\ 30   1 \cdot 0   1 6 \cdot 7   1 6 \cdot 5 \\ 40   22 \cdot 6   22 \cdot 3   22 \cdot 0 \\ 50   28 \cdot 3   27 \cdot 9   27 \cdot 5 \end{array}$
$     \begin{array}{r}       17 \\       18 \\       19 \\       20 \\       21     \end{array} $	9.61 410 9.61 438 9.61 466 9.61 494 9.61 522	28 28 28 28	9.65433 9.65467 9.65501 9.65535 9.65568	ର 4ାର 3 3 3 4ାରାରାରାର 3 3 3 3 3 3 3 3 3	$\begin{array}{r} 0.34 56\overline{6} \\ 0.34 532 \\ 0.34 499 \\ 0.34 465 \\ 0.34 431 \end{array}$	9.959779.959719.959659719.9595959595959595959595959595959595959	565656	$     \begin{array}{r}             43 \\             42 \\             41 \\             40 \\             39 \\             38 \\             38         \end{array}     $	28 28 6 2.8 2.8 7 3.3 3.2 8 3.8 3.7
22 23 24 25 26 27	9.61550 9.61578 9.61606 9.61634 9.61661 9.61689	28 28 28 27 28 27 28 27	9.65 602 9.65 635 9.65 669 9.65 703 9.65 736 9.65 770	ାରୀର <del>ସ୍</del> ୱାରାରାରାର ଉଚ୍ଚ ପର୍ଚ୍ଚର ଭର୍ଚ୍ଚ ଭ	$\begin{array}{r} 0.34 & 364 \\ 0.34 & 331 \\ 0.34 & 297 \\ 0.34 & 263 \\ 0.34 & 230 \end{array}$	$\begin{array}{r} 9.95 \ 94\bar{2} \\ 9.95 \ 937 \\ 9.95 \ 931 \\ 9.95 \ 92\bar{5} \\ 9.95 \ 91\bar{9} \end{array}$	55 65 65	37 36 35 34 33	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
28 29 30 31 32 33	9.61717 9.61745 9.61772 9.61800 9.61828 9.61856	28 27 28 27 28 27 28 27 28 27	9.65803 9.65837 9.65870 9.65904 9.65937 9.65937 9.65971	3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3	$\begin{array}{r} 0.34\ 163\\ 0.34\ 129\\ 0.34\ 096\\ 0.34\ 062\\ 0.34\ 029\\ \end{array}$	9.95914 9.95908 9.95902 9.95802 9.95896 9.95891 9.9585	6 15 6 5 6 6	32 31 30 29 28 27	27_ 27
34 35 36 37 38 39	9.61883 9.61911 9.61938 9.61966 9.61994 9.62021	27 27 27 27 28 27	$\begin{array}{r} 9.66\ 004\\ 9.66\ 03\overline{7}\\ 9.66\ 071\\ 9.66\ 10\overline{4}\\ 9.66\ 13\overline{7}\\ 9.66\ 13\overline{7}\\ 9.66\ 171\end{array}$	3333 333 333 333 333 333 333 333 333 3	0.33 962 0.33 929 0.33 895 0.33 862	9.95 879 9.95 873 9.95 867 9.95 867 9.95 862 9.95 856 9.95 856	5 6 5 6 5	26 25 24 23 22 21	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
40 41 42 43 44	$\begin{array}{r} 9\cdot 62 & 049 \\ 9\cdot 62 & 076 \\ 9\cdot 62 & 104 \\ 9\cdot 62 & 131 \\ 9\cdot 62 & 131 \\ 9\cdot 62 & 158 \end{array}$	27 27 27 27 27 27 27 27	9.662049.662379.662719.663049.66337	33 33 33 33 33 33 33 33 33 33 33 33 33	$\begin{array}{c} 0\cdot 33 & 79\overline{5} \\ 0\cdot 33 & 76\overline{2} \\ 0\cdot 33 & 729 \\ 0\cdot 33 & 69\underline{6} \\ 0\cdot 33 & 66\overline{2} \end{array}$	$9.9584\overline{4}$ 9.95838 9.95838 9.95833 9.95827 9.95821	6 6 5 6 5 6	20 19 18 17 16	30 13.77 13.5 40 18.3 18.0 50 22.9 22.5
$     \begin{array}{r}       45 \\       46 \\       47 \\       48 \\       49 \\       50     \end{array} $	$\begin{array}{r} 9.62 \ 186\\ 9.62 \ 213\\ 9.62 \ 241\\ 9.62 \ 268\\ 9.62 \ 295\\ 9.62 \ 295\\ 9.62 \ 323 \end{array}$	27 27 27 27 27 27 27 27	9.66370 9.66404 9.66437 9.66470 9.66503 9.66536	33 33 33 33 33 33 33	$\begin{array}{c} 0\cdot 33 & 52\overline{9} \\ 0\cdot 33 & 49\overline{6} \end{array}$	9.95815 9.95809 9.95804 9.95798 9.95798 9.95792 9.95786	6 <u>1</u> 5 6 6 5	$     \begin{array}{r}       15 \\       14 \\       13 \\       12 \\       11 \\       10     \end{array} $	65 6 0.6 0.5 7 0.7 0.6 8 0.8 0.7
51 52 53 54 55	9.623509.623779.624049.624329.624329.62459	27 27 27 27 27 27 27 27	9.66570 9.66603 9.66636 9.66669 9.66702	33 33 33 33 33 33 33	$\begin{array}{c} 0.33 \ 430 \\ 0.33 \ 397 \\ 0.33 \ 364 \\ 0.33 \ 331 \\ 0.33 \ 298 \end{array}$	9.95780 9.95774 9.95768 9.95768 9.95763 9.95763	6 6 5 6 6	9 8 7 6 5	90.90.8 101.00.9 202.01.8 303.02.7 404.03.6 505.04.6
56 57 58 59 <b>60</b>		27 27 27 27	$\begin{array}{r} 9.66735\\ 9.66768\\ 9.66801\\ 9.66834\\ 9.66834\\ 9.66867\\ \hline \end{array}$	3 <u>3</u> 33 33 33	$\begin{array}{c} 0.33 & 265 \\ 0.33 & 232 \\ 0.33 & 198 \\ 0.33 & 165 \\ \hline 0.33 & 13\overline{2} \end{array}$	9.95751 9.95745 9.95739 9.95733 9.95733 9.95727	6 5 6 6	4 3 2 1 0	
	Log. Cos.	d.	Log. Cot.	c.d.	Log. Tan.	Log. Sin.	d.		P. P.

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TABLE VII.—LOGARITHMIC SINES, COSINES, TANGENTS, AND COTANGENTS.

25°		AND COTANGEN	15.	154°
' Log. Sin. d.	Log. Tan. c. c	Log. Cot. Log. Cos.	d.	P. P.
$\begin{array}{c} 0 \\ 9 \cdot 62 595 \\ 1 \\ 9 \cdot 62 622 \\ 27 \\ 2 \\ 9 \cdot 62 649 \\ 27 \\ 3 \\ 9 \cdot 62 676 \\ 27 \\ 4 \\ 9 \cdot 62 703 \\ 27 \\ 4 \\ 9 \cdot 62 703 \\ 27 \\ 27 \\ 27 \\ 27 \\ 27 \\ 27 \\ 27 \\ 2$	$\begin{array}{c} 9.66867\\ 9.66900\\ 3.3\\ 9.66933\\ 9.66966\\ 3.3\\ 9.66966\\ 3.3\\ 9.66999\\ 3.3\\ 3.3\\ 9.66999\\ 3.3\\ 3.3\\ 3.3\\ 3.3\\ 3.3\\ 3.3\\ 3.3\\ $	$\begin{array}{c} 0.33 \ 13\overline{2} \ 9.95 \ 72\overline{7} \\ 0.33 \ 100 \ 9.95 \ 72\overline{1} \\ 0.33 \ 067 \ 9.95 \ 716 \\ 0.33 \ 034 \ 9.95 \ 710 \\ 0.33 \ 001 \ 9.95 \ 700 \\ 0.95 \ 700 \ 700 \\ 0.95 \ 700 \ 700 \\ 0.95 \ 700 $	$ \begin{array}{c} 6 \\ 5 \\ 5 \\ 6 \\ 5 \\ 5 \\ 5 \\ 5 \\ 5 \\ 6 \\ 5 \\ 6 \\ 5 \\ 6 \\ 5 \\ 5 \\ 5 \\ 5 \\ 5 \\ 5 \\ 5 \\ 5 \\ 5 \\ 5$	
$\begin{array}{c} 5 & 9 \cdot 62 & 757 \\ 6 & 9 \cdot 62 & 757 & 27 \\ 7 & 9 \cdot 62 & 784 & 27 \\ 8 & 9 \cdot 62 & 811 & 27 \\ 9 & 9 \cdot 62 & 838 & 27 \\ \hline 9 & 9 \cdot 62 & 838 & 267 \\ \hline \end{array}$	$\begin{array}{c cccccc} 9 \cdot 67 & 032 & 33 \\ 9 \cdot 67 & 065 & 33 \\ 9 \cdot 67 & 097 & 33 \\ 9 \cdot 67 & 130 & 33 \\ 9 \cdot 67 & 163 & 33 \\ 9 \cdot 67 & 196 & 33 \\ 9 \cdot 67 & 196 & 33 \\ 9 \cdot 67 & 196 & 32 \\ 9 \cdot 67 & 226 & 32 \end{array}$	$\begin{array}{c} 0.32 \ 968 \ 9.95 \ 698 \\ 0.32 \ 935 \ 9.95 \ 692 \\ 0.32 \ 935 \ 9.95 \ 686 \\ 0.32 \ 869 \ 9.95 \ 686 \\ 0.32 \ 869 \ 9.95 \ 686 \\ \hline 0.32 \ 836 \ 9.95 \ 674 \\ \hline 0.32 \ 803 \ 9.95 \ 668 \\ \hline \end{array}$	$\begin{array}{c} 6 & 55 \\ 6 & 54 \\ 5 & 53 \\ 6 & 51 \\ 6 & 51 \\ 6 & 50 \\ \end{array}$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
$\begin{array}{c ccccc} 11 & 9 \cdot 62 & 891 & 27 \\ 12 & 9 \cdot 62 & 918 & 27 \\ 13 & 9 \cdot 62 & 945 & 26 \\ 14 & 9 \cdot 62 & 972 & 26 \\ 15 & 9 \cdot 62 & 999 & 27 \\ \end{array}$	$\begin{array}{c} 9 \cdot 67 & 222 \\ 9 \cdot 67 & 294 \\ 9 \cdot 67 & 327 \\ 9 \cdot 67 & 327 \\ 9 \cdot 67 & 360 \\ 9 \cdot 67 & 360 \end{array}$	$\begin{array}{c} 0\cdot32 \ 771 \ 9\cdot95 \ 66\overline{2} \\ 0\cdot32 \ 738 \ 9\cdot95 \ 65\overline{6} \\ 0\cdot32 \ 70\overline{5} \ 9\cdot95 \ 65\overline{0} \\ 0\cdot32 \ 70\overline{5} \ 9\cdot95 \ 64\overline{4} \\ 0\cdot32 \ 67\overline{2} \ 9\cdot95 \ 63\overline{8} \end{array}$	$ \begin{array}{c ccc} 0 & 49 \\ 6 & 48 \\ 6 & 47 \\ 6 & 46 \\ 6 & 45 \\ \end{array} $	$\begin{array}{c} 20 \\ 11 \\ 0 \\ 10 \\ 0 \\ 16 \\ 0 \\ 16 \\ 0 \\ 22 \\ 0 \\ 21 \\ 0 \\ 16 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ $
$\begin{array}{c} 10 & 9.63 & 052 \\ 17 & 9.63 & 052 \\ 18 & 9.63 & 079 \\ 19 & 9.63 & 106 \\ 20 & 9.63 & 132 \\ 21 & 9.63 & 159 \\ 22 & 9.63 & 186 \\ 22 & 9.63 & 186 \\ 22 \end{array}$	$\begin{array}{c} 9.67 \\ 425 \\ 9.67 \\ 458 \\ 9.67 \\ 491 \\ 9.67 \\ 523 \\ 9.67 \\ 523 \\ 9.67 \\ 523 \\ 9.67 \\ 556 \\ 9.67 \\ 589 \\ 325 \\ 9.67 \\ 589 \\ 325 \\ 32$		$\begin{array}{c} 40 \\ 5 \\ 5 \\ 6 \\ 41 \\ 6 \\ 40 \\ 6 \\ 39 \\ 6 \\ 38 \\ 6 \\ 8 \\ 8 \\ 8 \\ 8 \\ 8 \\ 8 \\ 8 \\ 8 \\ $	27 6 2.7 7 3.1 8 3.6
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$9.6765\overline{4}33$	$\begin{array}{c} 0.32\ 37\overline{5}\ 9.95\ 591\\ \hline 0.32\ 34\overline{5}\ 9.95\ 585\\ \hline 0.32\ 313\ 9.95\ 579\\ \hline 0.32\ 280\ 9.95\ 573\\ \hline 0.32\ 248\ 9.95\ 573\\ \hline 0.32\ 248\ 9.95\ 576\\ \hline 0.32\ 215\ 9.95\ 561\\ \hline 0.32\ 183\ 9.95\ 555\\ \end{array}$	$\begin{array}{cccc} 0 & 37 \\ 6 & 36 \\ 6 & 35 \\ 6 & 34 \\ 6 & 33 \\ 6 & 32 \\ 6 & 31 \end{array}$	9 4.0 10 4.5 20 9.0 30 13.5 40 18.0 50 22.5
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{array}{c} 9.67 84\overline{9} \\ 9.67 882 \\ 9.67 91\overline{4} \\ 9.67 947 \\ 9.67 97\overline{9} \\ 327 \\ 9.67 97\overline{9} \\ 327 \\$	$\begin{array}{c} 0.32 \ 150 \\ 0.32 \ 150 \\ 0.32 \ 150 \\ 0.32 \ 118 \\ 0.95 \ 543 \\ 0.32 \ 053 \\ 0.95 \ 530 \\ 0.32 \ 020 \\ 9.95 \ 530 \\ 0.32 \ 020 \\ 9.95 \ 524 \\ 0.31 \ 988 \\ 9.95 \ 518 \end{array}$	$\begin{array}{c cccc} 6 & 30 \\ 6 & 29 \\ 6 & 28 \\ 6 & 27 \\ 6 & 26 \\ 6 & 25 \\ \end{array}$	26 26 25 6 2.6 2.6 2.5 7 3.1 3.0 3.0
$\begin{array}{c} 36 & 9 \cdot 63 & 557 & 26 \\ 37 & 9 \cdot 63 & 583 & 26 \\ 38 & 9 \cdot 63 & 609 & 26 \\ 39 & 9 \cdot 63 & 636 & 26 \\ 40 & 9 \cdot 63 & 662 & 26 \\ 40 & 9 \cdot 63 & 662 & 26 \\ 41 & 9 \cdot 63 & 662 & 26 \\ \end{array}$	$\begin{array}{c}9.68 & 0.4\overline{4} \\ 9.68 & 0.77 \\ 9.68 & 109 \\ \underline{9.68 \ 141} \\ 9.68 & 174 \\ 9.68 & 174 \\ 32 \\ 9.68 & 0.6\overline{4} \end{array}$	$ \begin{array}{c} 0.31 955 9.95 512 \\ 0.31 923 9.95 506 \\ 0.31 921 9.95 506 \\ 0.31 891 9.95 500 \\ 0.31 858 9.95 500 \\ 0.31 826 9.95 494 \\ 0.31 826 9.95 488 \\ 0.31 793 9.95 488 \\ \end{array} $	$     \begin{array}{c}       6 & 24 \\       6 & 23 \\       6 & 22 \\       6 & 21 \\       6 & 20 \\       6 & 10 \\       6 & 10 \\     \end{array} $	$\begin{array}{c} 8 & 3.5 \\ 9 & 4.0 \\ 10 & 4.2 \\ 20 \\ 8.8 \\ 3.9 \\$
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	9.68 238 9.68 271 9.68 303 9.68 335 9.68 368 9.68 368 9.68 368 9.68 368 9.68 368	$\begin{array}{c} 0.3 & 76 \\ \hline 9.95 & 476 \\ 0.31 & 729 \\ 9.95 & 476 \\ \hline 0.31 & 696 \\ \hline 9.95 & 464 \\ \hline 0.31 & 664 \\ 9.95 & 458 \\ \hline 0.31 & 632 \\ 9.95 & 458 \\ \hline 0.31 & 602 \\ 9.95 & 452 \\ \hline 0.31 & 600 \\ 9.95 & 445 \\ \hline \end{array}$	$ \begin{array}{c}             6 & 18 \\             6 & 17 \\             6 & 16 \\             6 & 15 \\             6 & 14 \\             6 & 13 \\         \end{array} $	665
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{array}{c} 9.68 \ 43\overline{2} \\ 9.68 \ 46\overline{4} \\ 9.68 \ 497 \\ 9.68 \ 529 \\ 9.68 \ 561 \\ 32 \\ 9.68 \ 561 \\ 32 \\ 32 \\ 32 \\ 32 \\ 32 \\ 32 \\ 32 \\ 3$	$ \begin{bmatrix} 0 & 3 & 1 & 567 \\ 0 & 31 & 567 \\ 0 & 31 & 535 \\ 0 & 31 & 535 \\ 0 & 31 & 503 \\ 0 & 31 & 503 \\ 0 & 31 & 471 \\ 0 & 91 & 427 \\ 0 & 31 & 471 \\ 0 & 91 & 425 \\ 0 & 31 & 439 \\ 0 & 95 & 415 \\ 0 & 31 & 406 \\ 0 & 95 & 409 \\ \end{bmatrix} $	$\begin{array}{c}     6 \\     6 \\     6 \\     11 \\     6 \\     10 \\     6 \\     9 \\     6 \\     8 \\     6 \\     7 \\   \end{array}$	$\begin{array}{c} 6 & 0 \cdot \overline{5} \\ 7 & 0 \cdot \overline{7} & 0 \cdot 7 & 0 \cdot \overline{5} \\ 8 & 0 \cdot \overline{8} & 0 \cdot 8 & 0 \cdot \overline{7} \\ 9 & 1 \cdot 0 & 0 \cdot 9 & 0 \cdot 8 \\ 1 & 1 \cdot 1 & 1 \cdot 0 & 0 \cdot 9 \\ 2 & 0 & 2 \cdot \overline{12} & 2 \cdot 0 & 1 \cdot 8 \\ 3 & 0 & 3 \cdot \overline{23} & 3 \cdot 0 & 2 \cdot \overline{7} \\ 4 & 0 & 4 \cdot 3 & 4 \cdot 0 & 3 \cdot 6 \end{array}$
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{array}{c} 0.31 & 374 \\ 0.31 & 374 \\ 0.31 & 342 \\ 0.31 & 342 \\ 0.31 & 310 \\ 0.31 & 310 \\ 0.95 & 397 \\ 0.31 & 278 \\ 0.31 & 278 \\ 0.31 & 246 \\ 0.95 & 378 \\ 0.31 & 214 \\ 0.95 & 378 \\ \end{array}$	6 6 6 6 6 8 6 3 2 1	30 5 2 3 0 2 7 40 4 3 4 0 3 6 50 5 4 5 0 4 6
60 9.64 184 Log. Cos. d.	9.68 818 Log. Cot. c. d	0.31 182 9.95 366	$\frac{6}{d}$ $\frac{-}{\prime}$	P. P.

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	TAB	ĹΕ	VIILO	GA1	RITHMI	C SINES,	CO	SIN	ES, TANG <b>ENTS</b> ,
2	6°			4	AND CO	TANGEN	TS.		153°
	Log. Sin.		Log. Tan.	<b>c.</b> d.	Log. Cot.	Log. Cos.	d.		P. P.
111111111111111111111111111111111111111	$\begin{array}{cccccccccccccccccccccccccccccccccccc$		$\begin{array}{c} 9.68 \\ 8.18 \\ 9.68 \\ 8.502 \\ 9.68 \\ 8.502 \\ 9.68 \\ 9.68 \\ 9.68 \\ 9.68 \\ 9.68 \\ 9.69 \\ 9.69 \\ 0.69 \\ $	33322 33333333333333333333333333333333	$\begin{array}{c} 0.81 02 \\ 0.30 98 \\ 0.30 95 \\ 0.30 95 \\ 0.30 926 \\ 0.30 894 \\ 0.30 862 \\ 0.30 80 \\ 0.30 766 \\ 0.30 766 \\ 0.30 762 \\ 0.30 762 \\ 0.30 607 \\ 0.30 630 \\ 0.30 607 \\ 0.30 607 \end{array}$	$\begin{array}{c} 9.95\ 34\overline{1}\\ 9.95\ 34\overline{1}\\ 9.95\ 329\\ 9.95\ 329\\ 9.95\ 329\\ 9.95\ 310\\ 9.95\ 310\\ 9.95\ 292\\ 9.95\ 292\\ 9.95\ 292\\ 9.95\ 273\\ 9.95\ 273\\ 9.95\ 267\\ 9.95\ 264\end{array}$	000000000000000000000000000000000000000	$\begin{array}{c} 60\\ 59\\ 57\\ 56\\ 55\\ 55\\ 55\\ 55\\ 55\\ 55\\ 55\\ 55\\ 55$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
2	9 9.64 673 0 9.64 698	25	$9.6945\overline{6}$	31 32	0.30575 0.30543	9.95 242	<u>6</u>	$\frac{41}{40}$	

	Log. Cos.			c.d.	Log. Tan.		d.	7	P. P.
55 56 57 58 59 <b>60</b>	$\begin{array}{r} 9.65 580 \\ 9.65 605 \\ 9.65 630 \\ 9.65 655 \\ 9.65 655 \\ 9.65 680 \\ 9.65 704 \end{array}$	23 24 25 25	9.70560 9.70591 9.70623 9.70654 9.70685 9.70716	31 31 31 31 31 31 31	$\begin{array}{r} 0.29 \ 43\underline{9} \\ 0.29 \ 408 \\ 0.29 \ 377 \\ 0.29 \ 34\underline{6} \\ 0.29 \ 31\underline{4} \\ 0.29 \ 28\overline{3} \end{array}$	$\begin{array}{r} 9.95\ 020\\ 9.95\ 014\\ 9.95\ 007\\ 9.95\ 001\\ 9.94\ 994\\ 9.94\ 988\\ 9.94\ 988\end{array}$	ରା ଡାଡାଡାଡ ଡା	54321 0	40 16.3 4.3 4.0 50 20.4 5.4 5.0
50 51 52 53 54	9.65456 9.65481 9.65506 9.65530 9.655530 9.65555	25 25 24 25	9.70403 9.70435 9.70466 9.70497 9.70529	31 31 31 31 31	$\begin{array}{c} 0.29 & 59\overline{6} \\ 0.29 & 565 \\ 0.29 & 53\overline{3} \\ 0.29 & 50\overline{2} \\ 0.29 & 471 \end{array}$	$\begin{array}{c} 9.95 \\ 0.95 \\ 0.95 \\ 0.95 \\ 0.95 \\ 0.39 \\ 0.95 \\ 0.33 \\ 0.95 \\ 0.26 \end{array}$	0101010	9 8 7 6	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
45 46 47 48 49	9.65331 9.65356 9.65381 9.65406 9.65431	25 25 25 25	9.70 246 9.70 278 9.70 309 9.70 341 9.70 372	31 31 31 31 31	$\begin{array}{c} 0.29 & 75\overline{3} \\ 0.29 & 722 \\ 0.29 & 69\overline{0} \\ 0.29 & 659 \\ 0.29 & 628 \\ 0.29 & 628 \end{array}$	9.95084 9.95078 9.95071 9.95065 9.95058	0101010	15 14 13 12 11	$\begin{array}{cccccccccccccccccccccccccccccccccccc$
40 41 42 43 44	9.65 205 9.65 230 9.65 255 9.65 280 9.65 305	25 25 25 25	9.70 089 9.70 121 9.70 152 9.70 183 9.70 215	3113131	0.29 87 <u>9</u> 0.29 847 0.29 816	9.95116 9.95109 9.95103 9.95097 9.95090	010 010	20 19 18 17 16	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
35 36 37 38 39	$\begin{array}{r} 9.65\ 079\\ 9.65\ 104\\ 9.65\ 129\\ 9.65\ 155\\ 9.65\ 180\end{array}$		9.69 931 9.69 963 9.69 994 9.70 026 9.70 058	3312211	0.30 037 0.30 005	9.95147 9.95141 9.95135 9.95128 9.95122	0 6 6 6 6	25 24 23 22 21	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
30 31 32 33 34 35	9.64 952 9.64 978 9.65 003 9.65 028 9.65 054	205 205 205 205 205	9.69 77 <u>3</u> 9.69 805 9.69 837 9.69 868 9.69 900	31 32 31 31 31	0.30 226 0.30 194	9.95179 9.95173 9.95166 9.95160 9.95154	9 01010	80 29 28 27 26	26 25 25 6  2. <u>6</u>   2.5  2.t
25 26 27 28 29	9.64826 9.64851 9.64876 9.64902 9.64927	25 25 25 25 25 25 25 25 25 25 25 25 25 2	$9.69 61\overline{5} \\ 9.69 647 \\ 9.69 67\overline{8} \\ 9.69 710 \\ 9.69 742 \\ 9.69 742 \\ 9.69 742 \\ 9.69 742 \\ 0.6$	32 31 32 31 32	0.30 32 <u>1</u> 0.30 289 0.30 258	$\begin{array}{c} 9.95 \ 21\bar{0} \\ 9.95 \ 20\bar{4} \\ 9.95 \ 198 \\ 9.95 \ 19\bar{1} \\ 9.95 \ 18\bar{5} \\ 9.95 \ 18\bar{5} \end{array}$	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	35 34 33 32 31	$\begin{array}{c} 20 & 10 \cdot \underline{5} & 10 \cdot \overline{3} \\ 30 & 15 \cdot \overline{7} & 15 \cdot \underline{5} \\ 40 & 21 \cdot 0 & 20 \cdot \overline{6} \\ 50 & 26 \cdot \overline{2} & 25 \cdot \overline{8} \end{array}$
20 21 22 23 24	$\begin{array}{r} 9.64 & 698 \\ 9.64 & 724 \\ 9.64 & 749 \\ 9.64 & 775 \\ 9.64 & 800 \end{array}$	2552	9.69 45 <u>6</u> 9.69 488 9.69 520 9.69 552 9.69 583	32 31 32 31	$\begin{array}{c} 0.30 54\bar{3} \\ 0.30 51\bar{1} \\ 0.30 480 \\ 0.30 448 \\ 0.30 41\bar{6} \end{array}$	$9.95242 \\ 9.95235 \\ 9.95229 \\ 9.95223 \\ 9.95223 \\ 9.95217 \\ \end{array}$	6 6 6	10 39 38 37 36	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
14 15 16 17 18 19	9.64570 9.64596 9.64622 9.64647 9.64673	25 25 26 25 25 25 25	9.692979.693299.693619.693939.693939.69425	32 3 <u>2</u> 31 32 32 32 31	0.30 702 0.30 670 0.30 639 0.30 607 0.30 575	$\begin{array}{c} 9.95\ 273\\ 9.95\ 267\\ 9.95\ 260\\ 9.95\ 254\\ 9.95\ 248\end{array}$	6 6 6 6 6	45 44 43 42 41	. 31. 31
14	9.64 545	22	9.69 265	31	0.30 734	9.95 279	0	46	50(27.1120.0

63°

 
 TABLE VII.—LOGARITHMIC SINES, COSINES, TANGENTS, AND COTANGENTS.

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## TABLE VII.—LOGARITHMIC SINES, COSINES, TANGENTS, AND COTANGENTS.

28	0	AND COTANGENTS.	151-
'	Log. Sin. d	Log. Tan. c. d. Log. Cot. Log. Cos. d.	P. P.
· 01234 56789 10112134 156789 10112134 15167189	$\begin{array}{c c c c c c c c c c c c c c c c c c c $	$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	$\begin{array}{c c c c c c c c c c c c c c c c c c c $
20 $21$ $223$ $24$ $25$ $27$ $29$ $31$ $323$ $34$ $35$ $37$ $39$ $39$	$\begin{array}{c} 9.67 \\ 9.67 \\ 656 \\ 2.7 \\ 9.67 \\ 773 \\ 2.7 \\ 9.67 \\ 773 \\ 2.7 \\ 2$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
<b>4</b> 414444444444444444444444444444444444	$\begin{array}{c} \hline 9.68\ 098\ 2\\ 2\\ 9.68\ 121\ 2\\ 2\\ 9.68\ 121\ 2\\ 2\\ 9.68\ 121\ 2\\ 2\\ 2\\ 9.68\ 121\ 2\\ 2\\ 2\\ 9.68\ 213\ 2\\ 2\\ 9\\ 9.68\ 255\ 2\\ 2\\ 9\\ 9.68\ 255\ 2\\ 2\\ 9\\ 9.68\ 351\ 2\\ 2\\ 9\\ 9.68\ 351\ 2\\ 2\\ 9\\ 9.68\ 420\ 2\\ 9\\ 9.68\ 443\ 2\\ 9\\ 9.68\ 443\ 2\\ 9\\ 9.68\ 443\ 2\\ 9\\ 9.68\ 451\ 2\\ 9\\ 9.68\ 451\ 2\\ 9\\ 9.68\ 511\ 2\\ 1\\ 9.68\ 511\ 2\\ 1\\ 9.68\ 511\ 2\\ 1\\ 9.68\ 511\ 2\\ 1\\ 1\\ 1\\ 1\ 1\\ 1\ 1\ 1\ 1\ 1\ 1\ 1\ 1\ 1\ 1\ 1\ 1\ 1\ $	$\begin{array}{c c c c c c c c c c c c c c c c c c c $	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
<u>60</u>	9.68 557 Log. Cos. d.	9.74375 29 $0.256259.94182$	P. P.

118°

280

61°

# TABLE VII.—LOGARITHMIC SINES, COSINES, TANGENTS, AND COTANGENTS.

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TABLE VII.-LOGARITHMIC SINES, COSINES, TANGENTS.

1	49	8

TABLE VII.-LOGARITHMIC SINES, COSINES, TANGENTS. AND COTANGENTS.

31 <sup>è</sup>	TABI		VII.—LO				FANG			01111	ES, TANGENTS. 148°
	Log. Sin.	d.	Log. Tan.	c.d.	Log.	Cot.	Log. C	os.	d.		P. P.
$\begin{bmatrix} 0 \\ 1 \\ 2 \\ 3 \\ 4 \end{bmatrix} 5 \\ 6 \\ 7 \\ 8 \\ 9 \end{bmatrix} \begin{bmatrix} 0 \\ 1 \\ 1 \\ 2 \\ 3 \\ 2 \\ 2 \\ 2 \\ 2 \\ 2 \\ 2 \\ 2 \\ 2$	$\begin{array}{c} 9.71 & 184\\ 9.71 & 206\\ 9.71 & 226\\ 9.71 & 226\\ 9.71 & 226\\ 9.71 & 226\\ 9.71 & 268\\ 9.71 & 268\\ 9.71 & 268\\ 9.71 & 268\\ 9.71 & 268\\ 9.71 & 351\\ 9.71 & 351\\ 9.71 & 351\\ 9.71 & 393\\ 9.71 & 310\\ 9.71 & 435\\ 9.71 & 435\\ 9.71 & 435\\ 9.71 & 456\\ 9.71 & 456\\ 9.71 & 456\\ 9.71 & 456\\ 9.71 & 456\\ 9.71 & 456\\ 9.71 & 539\\ 9.71 & 561\\ 9.71 & 622\\ 9.72 & 102\\ 9.72 & 102\\ 9.72 & 102\\ 9.72 & 216\\$		$egin{array}{ c c c c c c c c c c c c c c c c c c c$		$\begin{array}{c} 0 & 222\\ 0 & 2$	$\begin{array}{c} 122\\ 0.945\\ 0.037\\ 0.037\\ 0.08\\ 0.07\\ 0.08\\ 0.07\\ 0.08\\ 0.0$	$\begin{array}{c} 9.93 \\ 9.93 \\ 2.22 \\ 9.93 \\ 2.22 \\ 2.23 \\ 2.$	306 32991 3284 3276 32991 3284 3276 3261 32921 32255 32222 32225 32225 32225 32225 32225 32225 32225 32225 32225 32225 32225 32255 32555 32555 32555 3255 32555 32555 32555 32555 32555 32555 32555 35	° ° 21888 21888 218878 ° 718871 8871871 8871871 8718718 7187198 7187198 7187198 7187198 718719	$\begin{bmatrix} 0 9 \\ 5 \\ $	$\begin{array}{c} 29 & 28 & 28 \\ 6 & 2.9 & 2.8 \\ 7 & 3.4 & 3.38 & 3.7 \\ 8 & 3.8 & 3.8 & 3.7 \\ 9 & 4.33 & 4.3 & 4.7 \\ 10 & 4.33 & 4.7 & 4.63 \\ 20 & 9.5 & 14.0 \\ 4.33 & 4.7 & 4.6 \\ 20 & 9.5 & 14.0 \\ 4.33 & 4.7 & 4.6 \\ 30 & 14.5 & 14.7 & 4.6 \\ 30 & 14.5 & 14.2 & 14.0 \\ 40 & 19.3 & 19.0 & 18.6 \\ 50 & 24.1 & 23.7 & 23.3 \\ \hline \\ 8 & 2.4 & 2.7 & 2.0 \\ 7 & 2.4 & 2.7 & 2.0 \\ 10 & 3.5 & 3.4 & 3.6 \\ 8 & 3.1 & 3.1 & 3.0 \\ 10 & 3.5 & 3.4 & 3.6 \\ 8 & 3.1 & 3.1 & 3.0 \\ 10 & 3.5 & 3.4 & 3.6 \\ 30 & 10.5 & 10.2 & 10.0 \\ 40 & 14.0 & 13.6 & 13.3 \\ 50 & 17.5 & 17.1 & 16.6 \\ \hline \\ 8 & 7 \\ 7 & 0.9 & 0.9 \\ 8 & 1.0 & 1.0 \\ 9 & 1.2 & 1.1 \\ 10 & 1.33 & 1.2 \\ 20 & 2.0 \\ 50 & 6.6 & 6.2 \\ \hline \end{array}$
	Log. Cos.	d.	Log. Cot.	c. d.	Log.	Tan.	Log. S	Sin.	d.	1	P. P.

121°

636

### TABLE VII.-LOGARITHMIC SINES, COSINES, TANGENTS, COTANCENTE

32°			AND COT	<b>FANGEN</b>	TS.		147
· Log. Sin	. d.	Log. Tan. c. c	d. Log. Cot.	Log. Cos.	d.		P. P.
$\begin{array}{c c c c c c c c c c c c c c c c c c c $		$\begin{array}{c} 9.79\ 579\ 263\\ 9.79\ 607\ 263\\ 9.79\ 607\ 263\\ 9.79\ 607\ 263\\ 9.79\ 607\ 263\\ 9.79\ 607\ 263\\ 9.79\ 607\ 263\\ 9.79\ 607\ 263\\ 9.79\ 607\ 263\\ 9.79\ 707\ 203\\ 9.79\ 707\ 203\\ 9.79\ 707\ 203\\ 9.79\ 707\ 203\\ 9.79\ 803\ 203\\ 9.79\ 807\ 223\\ 9.79\ 943\ 203\\ 9.79\ 943\ 203\\ 9.79\ 943\ 203\\ 9.79\ 943\ 203\\ 9.79\ 943\ 203\\ 9.79\ 943\ 203\\ 9.79\ 943\ 203\\ 9.79\ 943\ 203\\ 9.79\ 943\ 203\\ 9.79\ 943\ 203\\ 9.79\ 943\ 203\\ 9.79\ 943\ 203\\ 9.79\ 943\ 203\\ 9.79\ 943\ 203\\ 9.80\ 025\ 203\ 203\ 203\ 203\ 203\ 203\ 203\ 203$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	Log. Cos. 9.92 842 9.92 842 9.92 813 9.92 810 9.92 810 9.92 786 9.92 771 9.92 7786 9.92 7786 9.92 7786 9.92 7786 9.92 7786 9.92 7789 9.92 7689 9.92 7699 9.92 7699 9.92 7699 9.92 7699 9.92 7699 9.92 7699 9.92 7699 9.92 6919 9.92 6691 9.92 6433 9.92 643 9.92 643 9	d.         6 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	09 387 6 5 432 5 10 9 48 44 432 41 039 837 6 5 4332 10 9 48 44 432 41 039 837 6 5 4332 10 9 48 44 432 10 9 837 6 5 4332 10 9 10 10 10 10 10 10 10 10 10 10	P. P. $2\overline{8}$ 28 27 6  2.8 2.8 27 7  3.3 3.2 2.3 2.2 8  3.8 3.7 3.6 9  4.3 4.2 4.1 10  4.7 4.6 4.6 20  9.5 9.3 9.1 30  14.2 14.0 13.7 40  19.0 18.6 18.3 50  23.7 23.3 22.9 10  3.4 2.3 8  2.7 2.6 2.6 9  3.1 3.0 2.9 10  3.4 3.3 3.2 20  6.8 6.6 8.5 30  10.9 7
$\begin{array}{r} 3\frac{4}{5} & 9.73 & 10\\ 85 & 9.73 & 12\\ 86 & 9.73 & 14\\ 87 & 9.73 & 16\\ 88 & 9.73 & 18\\ 89 & 9.73 & 19\\ 40 & 9.73 & 21\\ 41 & 9.73 & 23\\ 42 & 9.73 & 22\\ 43 & 9.73 & 27\\ 44 & 9.73 & 29\\ 45 & 9.73 & 32\\ 46 & 9.73 & 32\\ 46 & 9.73 & 32\\ 47 & 9.73 & 32\\ 48 & 9.73 & 32\\ 48 & 9.73 & 32\\ 50 & 9.73 & 41\\ 51 & 9.73 & 42\\ 53 & 9.73 & 42\\ 55 & 9.73 & 42\\ 55 & 9.73 & 42\\ 55 & 9.73 & 52\\ 56 & 9.73 & 52\\ 5$		8.00         5.58         2           9.80         558         2           9.80         558         2           9.80         641         2           9.80         641         2           9.80         641         2           9.80         641         2           9.80         641         2           9.80         641         2           9.80         642         2           9.80         752         2           9.80         752         2           9.80         752         2           9.80         808         2           9.80         808         2           9.80         808         2           9.80         8047         2           9.80         947         3           9.81         030         2           9.81         030         3           9.81         030         3           9.81         143         3           9.81         143         3           9.81         148         3           9.81         148         3	0.19 470	$\begin{array}{c} 9.92 570\\ 9.92 546\\ 9.92 546\\ 9.92 546\\ 9.92 546\\ 9.92 538\\ 9.92 556\\ 9.92 556\\ 9.92 556\\ 9.92 556\\ 9.92 556\\ 9.92 489\\$		$\begin{array}{c} \underline{26} \\ \underline{25} \\ \underline{222} \\ \underline{222} \\ \underline{20} \\ 19 \\ 18 \\ 17 \\ 16 \\ 15 \\ 14 \\ 13 \\ 12 \\ 1 \\ 10 \\ 9 \\ 8 \\ 7 \\ 6 \\ 5 \\ 4 \\ 3 \\ 2 \\ 1 \\ 0 \\ \end{array}$	$\begin{array}{c} 8 & 8 & 7 \\ 6 & 0 & 1 \\ 0 & 1 & 0 \\ 0 & 1 \\ 0 &$
Log. Co		And the Party of t	d. Log. Tan			<i>~</i>	P. P.

122°

637

57º

# TABLE VII.—LOGARITHMIC SINES, COSINES, TANGENTS, AND COTANGENTS.

123°

56°

146°

## TABLE VII.-LOGARITHMIC SINES, COSINES, TANGENTS, AND COTANGENTS.

124°

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55

# TABLE VII.—LOGARITHMIC SINES, COSINES, TANGENTS, AND COTANGENTS.

35°	4	AND COTANGENTS.	144°
· Log. Sin. d.	Log. Tan. c. d.	Log. Cot. Log. Cos. d.	P. P.
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	$\begin{array}{c} 9.84522\\ 9.84563\\ 9.84563\\ 9.84575\\ 9.84657\\ 9.84657\\ 9.84657\\ 9.84657\\ 9.84657\\ 9.84657\\ 9.84657\\ 9.84657\\ 9.84774\\ 9.85774\\ 9.85774\\ 9.855640\\ 9.85660\\ 9.855640\\ 9.855600\\ 9.856600\\ 9.856600\\ 9.856600\\ 9.856600\\ 9.856600\\ 9.856600\\ 9.85$	$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	$\begin{array}{c} 27 & 26 \\ 6 & 2.7 & 2.6 \\ 7 & 3.1 & 3.1 \\ 8 & 3.6 & 3.5 \\ 9 & 4.0 & 4.0 \\ 10 & 4.5 & 4.4 \\ 20 & 9.0 & 8.8 \\ 30 & 13.5 & 13.2 \\ 40 & 18.0 & 17.6 \\ 50 & 22.5 & 22.1 \\ \end{array}$
60 9 . 76 922 Log. Cos. d	9.86 126 20 Log. Cot. c d.	0.13 874 9.90 796 9 0 Log. Tan. Log. Sin. d. /	P. P.
leeb. coal a	Logi ouile ui	ijeogi ramjeogi Simj u j	1

125°

640

# TABLE VII.—LOGARITHMIC SINES, COSINES, TANGENTS, AND COTANGENTS.

36°	AND COTANGENTS.	143°
· Log. Sin. d.	Log. Tan. c. d. Log. Cot. Log. Cos. d.	P. P.
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	$\begin{array}{c c c c c c c c c c c c c c c c c c c $	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
Log. Cosil a	Irogi conternited tantradi and a	1 1 1 1 1 1 1

126°

00

53°

## TABLE VII.-LOGARITHMIC SINES, COSINES, TANGENTS,

37°

AND COTANGENTS.

1420

$ \begin{array}{c c c c c c c c c c c c c c c c c c c $
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
Log, Cos, d. Log, Cot, c. d. Log, Tan, Log, Sin, d. ' P. P.

642

38°

ĺ ł TABLE VII .-- LOGARITHMIC SINES, COSINES, TANGENTS, AND COTANGENTS.

$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	00									112
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	1	Log. Sin.	d.	Log. Tan.	c.d.	Log. Cot	Log. Cos.	d.		P. P.
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\left  \begin{array}{c} \cdot \\ 0 \\ 1 \\ 2 \\ 3 \\ 4 \\ 5 \\ 6 \\ 7 \\ 8 \\ 9 \\ 1 \\ 1 \\ 1 \\ 1 \\ 1 \\ 1 \\ 1 \\ 1 \\ 1$	$\begin{array}{c} \hline 9.78 & 934\\ 9.78 & 950\\ 9.78 & 950\\ 9.78 & 9839\\ 9.78 & 9839\\ 9.79 & 0151\\ 9.79 & 0151\\ 9.79 & 0451\\ 9.79 & 047\\ 9.79 & 047\\ 9.79 & 047\\ 9.79 & 112\\ 9.79 & 107\\ 9.79 & 507\\ 9.79 & 507\\ 9.79 & 508\\ 9.79$	$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	$\begin{array}{c} 9.89\ 281\\ 9.89\ 307\\ 9.89\ 359\\ 9.89\ 359\\ 9.89\ 359\\ 9.89\ 359\\ 9.89\ 359\\ 9.89\ 359\\ 9.89\ 411\\ 9.89\ 463\\ 9.89\ 451\\ 9.89\ 451\\ 9.89\ 567\\ 9.89\ 593\\ 9.89\ 593\\ 9.89\ 619\\ 9.89\ 593\\ 9.89\ 619\ 619\\ 9.89\ 619\ 619\ 619\ 619\ 619\ 619\ 619\ 61$	32232         22232         22232         22232         22232         22232         22232         22232         22232         22232         22232         22232         22232         22232         22232         22232         22322         2232         22322         2232         22322         2232         22322         22322         2232         22322         2232         22322         2232         22322         2232         2232         2232         2232         2232         2232         2232         2232         223         2232         223         223         2232         223         233         233         233         233         233         233         233         233         233 <td><math display="block">\begin{array}{c} \hline 0.10 &amp; 715\\ 0.10 &amp; 615\\ 0.10 &amp; 663\\ 0.10 &amp; 663\\ 0.10 &amp; 682\\ 0.10 &amp; 563\\ 0.10 &amp; 563\\ 0.10 &amp; 563\\ 0.10 &amp; 563\\ 0.10 &amp; 513\\ 0.10 &amp; 433\\ 0.10 &amp; 453\\ 0.10 &amp; 255\\ 0.10 &amp; 103\\ 0.10 &amp; 10</math></td> <td><math display="block">\begin{array}{c} 9 \cdot 89 \cdot 653\\ 9 \cdot 89 \cdot 643\\ 9 \cdot 89 \cdot 643\\ 9 \cdot 89 \cdot 623\\ 9 \cdot 89 \cdot 624\\ 9 \cdot 89 \cdot 594\\ 4 \cdot 9 \cdot 89 \cdot 594\\ 4 \cdot 9 \cdot 89 \cdot 594\\ 9 \cdot 89 \cdot 554\\ 4 \cdot 9 \cdot 89 \cdot 89 \cdot 554\\ 4 \cdot 9 \cdot 89 \cdot 89 \cdot 89 \cdot 89 \cdot 89 \cdot 89 \cdot 8</math></td> <td><math display="block">\begin{array}{c} \bar{9} \\ \bar{9} \\ 10 \\ 10 \\ 0 \\ \bar{9} \\ 10 \\ 10 \\ 10 \\ 10 \\ 10 \\ 10 \\ 10 \\ 1</math></td> <td>59 557 55 554 554 554 554 554 554 554 554</td> <td><math display="block">\begin{array}{c ccccccccccccccccccccccccccccccccccc</math></td>	$\begin{array}{c} \hline 0.10 & 715\\ 0.10 & 615\\ 0.10 & 663\\ 0.10 & 663\\ 0.10 & 682\\ 0.10 & 563\\ 0.10 & 563\\ 0.10 & 563\\ 0.10 & 563\\ 0.10 & 513\\ 0.10 & 433\\ 0.10 & 453\\ 0.10 & 453\\ 0.10 & 453\\ 0.10 & 453\\ 0.10 & 453\\ 0.10 & 453\\ 0.10 & 453\\ 0.10 & 453\\ 0.10 & 453\\ 0.10 & 453\\ 0.10 & 453\\ 0.10 & 453\\ 0.10 & 453\\ 0.10 & 453\\ 0.10 & 453\\ 0.10 & 453\\ 0.10 & 453\\ 0.10 & 453\\ 0.10 & 255\\ 0.10 & 103\\ 0.10 & 10$	$\begin{array}{c} 9 \cdot 89 \cdot 653\\ 9 \cdot 89 \cdot 643\\ 9 \cdot 89 \cdot 643\\ 9 \cdot 89 \cdot 623\\ 9 \cdot 89 \cdot 624\\ 9 \cdot 89 \cdot 594\\ 4 \cdot 9 \cdot 89 \cdot 594\\ 4 \cdot 9 \cdot 89 \cdot 594\\ 9 \cdot 89 \cdot 554\\ 4 \cdot 9 \cdot 89 \cdot 89 \cdot 554\\ 4 \cdot 9 \cdot 89 \cdot 89 \cdot 89 \cdot 89 \cdot 89 \cdot 89 \cdot 8$	$\begin{array}{c} \bar{9} \\ \bar{9} \\ 10 \\ 10 \\ 0 \\ \bar{9} \\ 10 \\ 10 \\ 10 \\ 10 \\ 10 \\ 10 \\ 10 \\ 1$	59 557 55 554 554 554 554 554 554 554 554	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
Log. Cos. d. Log. Cot. c. d. Log. Tan. Log. Sin. d. / P. P.	$\begin{array}{c} 366\\ 3789\\ 412\\ 434\\ 4467\\ 849\\ 51234\\ 5555\\ 555\\ 55\\ 55\\ 55\\ 55\\ 5\\ 5\\ 5\\ 5\\$	$\begin{array}{r} 9.79\ 510\\ 9.79\ 526\\ 9.79\ 526\\ 9.79\ 526\\ 9.79\ 557\\ 9.79\ 557\\ 9.79\ 557\\ 9.79\ 562\\ 9.79\ 665\\ 9.79\ 809\\ 9.79\ 856\\ 9.79\ 871\\ 9.79\ 887\\ 9.79$	16656 65656 56656 56656 56656 56656 5656 5656 5656 5656 5656 5656 5656 5656 5555	$\begin{array}{c} 9.90\ 2162\\ 9.90\ 2428\\ 9.90\ 2428\\ 9.90\ 29.90\ 29.90\\ 9.90\ 29.90\ 29.90\\ 9.90\ 3717\\ 9.90\ 39.90\ 3717\\ 9.90\ 39.90\ 3717\\ 9.90\ 423\\ 9.90\ 5255\\ 9.90\ 5756\\ 9.90\ 5756\\ 9.90\ 5756\\ 9.90\ 6562\\ 9.90\ 757\\ 9.90\ 757\\ 9.90\ 758\ 758\\ 9.90\ 758\ 758\ 758\ 758\ 758\ 758\ 758\ 758$	22222 222222 222222 222222 222222 222222	$\begin{array}{c} 0.09 & 784 \\ 0.09 & 758 \\ 0.09 & 758 \\ 0.09 & 768 \\ 0.09 & 680 \\ 0.09 & 680 \\ 0.09 & 680 \\ 0.09 & 672 \\ 0.09 & 623 \\ 0.09 & 577 \\ 0.09 & 551 \\ 0.09 & 551 \\ 0.09 & 525 \\ 0.09 & 473 \\ 0.09 & 447 \\ 0.09 & 447 \\ 0.09 & 395 \\ 0.09 & 447 \\ 0.09 & 395 \\ 0.09 & 447 \\ 0.09 & 395 \\ 0.09 & 240 \\ 0.09 & 240 \\ 0.09 & 214 \\ 0.09 & 163 $	$\begin{array}{c} 9 & 89 & 294 \\ 9 & 89 & 284 \\ 9 & 89 & 274 \\ 9 & 89 & 256 \\ 9 & 89 & 253 \\ 9 & 89 & 243 \\ 9 & 89 & 233 \\ 9 & 89 & 233 \\ 9 & 89 & 233 \\ 9 & 89 & 233 \\ 9 & 89 & 233 \\ 9 & 89 & 233 \\ 9 & 89 & 233 \\ 9 & 89 & 132 \\ 9 & 89 & 132 \\ 9 & 89 & 132 \\ 9 & 89 & 162 \\ 9 & 89 & 050 \\ \hline \end{array}$	$\begin{array}{c} 10\\ 10\\ 10\\ 10\\ 10\\ 10\\ 10\\ 10\\ 10\\ 10\\$	$\begin{array}{c} 24\\ 23\\ 22\\ 21\\ 19\\ 18\\ 17\\ 16\\ 15\\ 14\\ 13\\ 12\\ 11\\ 10\\ 9\\ 8\\ 7\\ 6\\ 5\\ 4\\ 3\\ 2\\ 1\\ 1\end{array}$	$\begin{array}{c} 10 & 10 & 9 \\ 6 [1 \cdot 0   1 \cdot 0   0 \cdot 9 \\ 7   1 \cdot 2   1 \cdot 1   1 \cdot 1 \\ 8   1 \cdot 4   1 \cdot 3   1 \cdot 2 \\ 9   1 \cdot 6   1 \cdot 5   1 \cdot 4 \\ 10   1 \cdot 7   1 \cdot 6   1 \cdot 6 \\ 20   3 \cdot 5   3 \cdot 3   3 \cdot 1 \\ 30   5 \cdot 2   5 \cdot 0   4 \cdot 7 \\ 40   7 \cdot 0   6 \cdot 6   6 \cdot 3 \\ 50   8 \cdot 7   8 \cdot 3   7 \cdot 9 \end{array}$
		Log. Cos.	d,	Log. Cot.	c. d.	Log. Tan.	Log. Sin.	d.	7	P. P.

128°

643

51°

## TABLE VII.-LOGARITHMIC SINES, COSINES

d.

 $10 \\ 10 \\ 10 \\ 10 \\ 10 \\ 10 \\ -$ 60

39° 1

Log. Sin.

 $\begin{array}{c} 9.79 \\ 887 \\ 9.79 \\ 903 \\ 9.79 \\ 918 \\ 9.79 \\ 934 \\ 9.79 \\ 949 \end{array}$ 

d.

 $1615 \\ 1515 \\$ 

9.90 837 9.90 863 9.90 888 9.90 914 9.90 940

AND COTANGENTS.

 $\begin{array}{c} \hline 0.09 \ 163 \ 9.89 \ 050 \ 0.09 \ 137 \ 9.89 \ 040 \ 0.09 \ 111 \ 9.89 \ 030 \ 0.09 \ 011 \ 9.89 \ 030 \ 0.09 \ 085 \ 9.89 \ 019 \ 0.09 \ 060 \ 9.89 \ 009 \ \end{array}$ 

Log. Tan. c. d. Log. Cot. Log. Cos.

			140°
	P. P		
	26	$2\overline{5}$	
6 7 8 9	$26 \\ 2 \cdot 6 \\ 3 \cdot 0 \\ 3 \cdot 4 \\ 3 \cdot 9 \end{bmatrix}$	25 2.5 3.0 3.4 3.8	
8	3 4	3.4	

4	9.79	949	15	<u>9.90</u>	940	25	0.09	060	9.89	009	10	56	
	9.79 9.79			9.90 9.90		26 26		034		3 999 3 989	10 10	55 54	
	9.79		15	9.90 9.91 9.91	017	$2\overline{5} \\ 26$	0.08	8982	9.8	8978	10	54 53	
	9.80					26 26	0.08	¦95 <u>6</u>	9 . 8	B 968	10 10	52	$26 \ 2\overline{5}$
	9.80 9.80			<u>9.91</u> 9.91	And the local databases	25		930		<u>8 958</u> 8 947	10	$\frac{51}{50}$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
11	9.80			$9.91 \\ 9.91$		26		879		8 937		49	8 3.4 3.4
12	9.80	073	16	9.91	$14\overline{6}$	25 26		853	9.8	8 927	10 10	48	9 3.9 3.8
$13 \\ 14$	9.80 9.80		15	9.91 9.91	198	25				8917 8906	10	47 46	$\begin{array}{cccccccccccccccccccccccccccccccccccc$
15	9.80	120	15	9.91	224	26				8 896	10	45	30 13.0 12.7
	9.80		181	9.91	250	$\frac{26}{25}$	0.08	750	9.8	8 886	$  10 \\ 10 \\ 10 \\$	44	$\begin{array}{c} 40 \\ 50 \\ 21 \cdot 6 \\ 21 \cdot 2 \\ \end{array}$
17 18	9 · 80 9 · 80		15	9.91 9.91	275 301	26		5724 5698		8 875 8 865	10	$\frac{43}{42}$	00/21.0/21.2
<u>19</u>	9.80		101	9.91	327	25		673		8 855		41	•
20	9.80		$1\overline{5}$ $1\overline{5}$	9.91	353	$\frac{26}{25}$	0.08	8 647	9.8	8 844	$ 10 \\ 10 \\ 10$	40	
$\frac{21}{22}$	9.80 9.80		15	9.91 9.91		26		$62\overline{1} \\ 59\overline{5}$		8 83 <u>4</u> 8 823	$1\overline{0}$	39 38	
23	9.80	$24\bar{3}$	$15 \\ 15 \\ 15$	9.91	430	25	0.08	3 570	9.8	8 813	$  10 \\ 10 \\ 10 \\  $	37	
24	9.80		15	9.91		25		3 544		8 803	10	36	
25 26	9.80 9.80		15	$9.91 \\ 9 91$		26 25		$351\overline{8}$ $349\overline{2}$		8 792 8 782	10	$\frac{35}{34}$	$16$ $1\overline{5}$ $15$
27	9.80	30 <u>5</u>	$15 \\ 15 \\ 15 \\ 15 \\ 15 \\ 15 \\ 15 \\ 15 \\$	9.91	533	25	0.08	3 467	9.8	8772	$  10 \\ 10 \\ 10 \\  $	33	6 1.6 1.5 1.5
28 29	9.80 9.80		15	9.91 9.91		25			9.8	8 76ī 8 751	10	32 31	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
30	9.80		$1\overline{5}$ $1\overline{5}$	9.91		26		3 3 8 9			1₫	$\frac{31}{30}$	9 2.4 2.3 $2.\overline{2}$
31	9.80	366	$15 \\ 15 \\ 15 \\ 15 \\ 15 \\ 15 \\ 15 \\ 15 \\$	9.91	636	25	0.01	3 3 6 4	9.8	8 730		29	$\begin{array}{cccccccccccccccccccccccccccccccccccc$
32 33	9.80 9.80		15	9.91 9.91		25		$3338 \\ 312$		8720 8709	ίŏ	28 27	$\begin{array}{cccccccccccccccccccccccccccccccccccc$
34	9.80		15	9.91	713	26	0.0	3 286	9.8	8 699	10	26	$\begin{array}{c} 40 \ 10 \cdot \overline{6} \ 10 \cdot \overline{3} \ 10 \cdot 0 \\ 50 \ 13 \cdot \overline{3} \ 12 \cdot 9 \ 12 \cdot 5 \end{array}$
35	9.80		$15 \\ 15$	9.91	739	25		3 261		8 688	$10 \\ 10 \\ 10$	25	00113-3112-9112-9
36 37	9 · 80 9 · 80	443	$15 \\ 15 \\ 15$	9.91 9.91	. 765 795	25	0.0	3 23 <u>5</u> 3 209	9.8	867 <u>8</u> 8667	10	$\frac{24}{23}$	
38	9 . 80	47 <u>3</u>	$15 \\ 15$	9.91	. 816	26	0.01	3 183	9.8	8 657	$  10 \\ 10 \\ 10 \\   10$	22	
<u>39</u>	9.80		15	Contraction of the local division of the loc	842	25		<u>3 158</u>		8 646	10	21	
40 41	9.80 9.80		15	$9.91 \\ 9.91 \\ 9.91$	867	26	0.0	$\frac{132}{3106}$	9.8	8 63 <u>6</u> 8 625	10	20 19	
42	9.80	$53\overline{4}$	$1\overline{5} \\ 15$	9.91	919	25	0.01	3 081	9.8	8 615	$ 10 \\ 10 \\ 10$	18	
43 44	9.80 9.80		15		945 970	25		3 055 3 029		$860\overline{4}8594$	110	$17 \\ 16$	11 10 10
±± 45	9.80		15		996	25		3 004		8 583	10	$\frac{10}{15}$	$6 1 \cdot 1 1 \cdot \overline{0} 1 \cdot 0$
46	9.80	595	$15 \\ 15$	9.92	2 0 2 2	2 <u>6</u> 25	0.0	7978	9.8	8 57 <u>3</u>	$10 \\ 10 \\ 10$	14	$\begin{array}{c} 7 \\ 1 \\ 3 \\ 1 \\ 4 \\ 1 \\ 4 \\ 1 \\ 4 \\ 1 \\ 3 \\ \end{array}$
47 48	9.80 9.80		15		$2\ 04\overline{7}\ 2\ 07\overline{3}$	26	0.0	795 <u>2</u> 7926	9.8	$856\overline{2}$ 8552	10	$13 \\ 12$	$9 1 \cdot 6 1 \cdot 6 1 \cdot 5$
49	9.80		15		2 099	25				8 541	10	11	$\begin{array}{c c} 10 & 1 \cdot \overline{8} & 1 \cdot \overline{7} & 1 \cdot \overline{6} \\ 20 & 3 \cdot \overline{6} & 3 \cdot 5 & 3 \cdot \overline{3} \end{array}$
50	9.80		$15 \\ 15$	9.92	$12\overline{4}$	25		7 875		8 531	$10 \\ 10 \\ 10$	10	305.55.25.0
51 52	9 · 80 9 · 80		15	9.92	$215\overline{0}$ 2176	25		$784\overline{9}7824$		8 520 8 510	10	9	30 5 · 5 5 · 2 5 · 0 40 7 · 3 7 · 0 6 · 6 50 9 · 1 8 · 7 8 · 3
53	9.80		$15 \\ 15$	9.92	2 20 <u>1</u>	25	0.07	7798	9.8	8499	$10 \\ 10 \\ 10$	7	50 9 . 1 8 . 7 8 . 3
54	9.80		15	9.92		25		7772		8 489	10	6	
55 56	9 · 80 9 · 80		15	9.92 9.92		25		7747 7721		8478 8467	11	54	
57	9.80	76Ī	15	9.92	304	26 25	0.07	695	9.8	8457		3	
58 59	9.80		$\frac{15}{15}$	9.92		25		7670 644		8 446 3 436	$10\\10$	2	
<u>59</u>	<u>9 · 80</u> 9 · 80		15	9.92 9.92		26	0.07				$1\overline{0}$	$\frac{1}{0}$	
50	Log.		d.		Cot.	c. d.				Sin.	d.	$\dot{\gamma}$	P. P.
-	, <u>.</u>	_					0		344				

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 TABLE VII.—LOGARITHMIC SINES, COSINES, TANGENTS,

 AND COTANGENTS.

40	• TAB	LE	VIILO			C SINES		SIN	ES, TANGENTS, 139°
	Log. Sin.	d.	Log. Tan. d	. d. 1 o	or. Cot	Log. Cos.	d.	1	P. P.
0 1 2 3 4	9.80 806 9.80 822 9.80 837 9.80 852 9.80 852 9.80 867	$1\overline{5} \\ 15 \\ 15 \\ 15 \\ 15 \\ 15 \\ 15 \\ 15 \\ $	$ \begin{array}{r} 9.9238\overline{1}\\ 9.92407\\ 9.9243\overline{2}\\ 9.9243\overline{2}\\ 9.9245\overline{8}\\ 9.92484 \end{array} $	25 25 26 0. 25 0.	07 618 07 593 07 567 07 541		$10 \\ 11 \\ 10 \\ 10 \\ 10 \\ 10 \\ 10 \\ 10 \\$	60 59 58 57 56	
5 6 7 8 9 10 11	9.80 882 9.80 897 9.80 912 9.80 927 9.80 942 9.80 957 9.80 957 9.80 972	$15 \\ 15 \\ 15 \\ 15 \\ 15 \\ 15 \\ 15 \\ 15 \\$	9.92509 9.92535 9.92561 9.92586 9.92612	$     \begin{array}{ccccccccccccccccccccccccccccccccc$	07 490 07 465 07 439 07 413 07 388 07 362 07 362	9 88 361 9 88 351 9 88 340 9 88 340 9 88 329	$     \begin{array}{c}       11 \\       10 \\       10 \\       11 \\       10 \\$	55 54 53 52 51 50 49	$\begin{array}{cccccccccccccccccccccccccccccccccccc$
$     \begin{array}{r}       11 \\       12 \\       13 \\       14 \\       15 \\       16 \\       16 \\       \end{array} $	$\begin{array}{c} 9.80 \ 987 \\ 9.81 \ 001 \\ 9.81 \ 016 \\ 9.81 \ 031 \\ 9.81 \ 046 \end{array}$	$15 \\ 14 \\ 15 \\ 15 \\ 15 \\ 15 \\ 15 \\ 15 \\ $	$9.92689 \\ 9.92714 \\ 9.92740 \\ 0.02$		07 31 <u>1</u> 07 28 <u>5</u> 07 259	9.88 297 9.88 287	$     \begin{array}{c}       11 \\       10 \\       10 \\       11 \\       10 \\       10 \\       11 \\       10 \\$	48 47 46 45 44	$\begin{array}{c c c} 9 & 3 \cdot 9 & 3 \cdot \overline{8} \\ 10 & 4 \cdot \overline{3} & 4 \cdot \overline{2} \\ 20 & 8 \cdot 6 & 8 \cdot 5 \\ 30 & 13 \cdot 0 & 12 \cdot \overline{7} \\ 40 & 17 \cdot 3 & 17 \cdot 0 \end{array}$
$     \begin{array}{r}       17 \\       18 \\       19 \\       20 \\       21     \end{array} $	$9.8106\overline{1}$ $9.8107\overline{6}$ 9.81091 9.81106 9.81121	15 15	$\begin{array}{r} 9 \cdot 92 \ 817 \\ 9 \cdot 92 \ 842 \\ 9 \cdot 92 \ 858 \\ \hline 9 \cdot 92 \ 894 \\ 9 \cdot 92 \ 919 \end{array}$	25000 25000 25000 255000	07 183 07 157 07 131 07 106 07 080	9.88 244 9.88 233 9.88 223 9.88 212 9.88 212 9.88 201	$1\overline{0}$ 11 $1\overline{0}$ 11 $1\overline{0}$ 11 $1\overline{0}$ 11	43 42 41 40 39	50 21 . 6 21 . 2
22 23 24 25 26 27	$9 \cdot 81 \ 136 \\ 9 \cdot 81 \ 150 \\ 9 \cdot 81 \ 165 \\ 9 \cdot 81 \ 180 \\ 9 \cdot 81 \ 195 \\ 9 \cdot 81 \ 210 $	$15 \\ 14 \\ 15 \\ 15 \\ 14 \\ 15 \\ 14 \\ 15 \\ 15$	9.92 971 9.92 996 9.93 022 9.93 047	$     \begin{array}{c}       26 \\       25 \\       25 \\       25 \\       25 \\       0 \\$	07 055 07 029 07 003 06 978 06 952 06 952	$\begin{array}{r} 9\cdot 88 \ 19\bar{0} \\ 9\cdot 88 \ 180 \\ 9\cdot 88 \ 169 \\ 9\cdot 88 \ 15\bar{8} \\ 9\cdot 88 \ 147 \\ 9\cdot 88 \ 137 \end{array}$	$11 \\ 10 \\ 11 \\ 10 \\ 11 \\ 10 \\ 11 \\ 10 \\$	38 37 36 35 34 33	$egin{array}{cccccccccccccccccccccccccccccccccccc$
28 29 30 31 32	9.81225 9.81239 9.81254 9.81269 9.81269 9.81284	$15 \\ 14 \\ 15 \\ 14 \\ 15 \\ 15 \\ 15 \\ 15 \\ $	$\begin{array}{c} 9.93 & 098 \\ \underline{9.93} & 124 \\ 9.93 & 150 \\ 9.93 & 175 \\ 9.93 & 201 \end{array}$	25 26 25 0 0 0 0 0 0 0 0 0 0 0 0 0	06 927 06 901 06 875 06 850 06 824 06 799	9.88 115 9.88 104 9.88 094 9.88 083	$     \begin{array}{c}             11 \\             10 \\           $	$     \begin{array}{r}       32 \\       31 \\       30 \\       29 \\       28     \end{array}   $	$\begin{array}{c} 1 & 1 & 1 & 1 & 1 & 1 \\ 7 & 1 & 8 & 1 & 7 & 1 & 1 \\ 8 & 2 & 0 & 2 & 0 & 1 & 9 \\ 9 & 9 & 2 & 3 & 2 & 2 & 2 & 2 \\ 10 & 2 & 6 & 2 & 5 & 2 & 4 \\ 20 & 5 & 1 & 5 & 0 & 4 & 8 \\ 30 & 7 & 7 & 7 & 5 & 0 & 4 & 8 \\ 40 & 10 & 3 & 10 & 0 & 9 & 6 \\ 40 & 10 & 0 & 10 & 0 & 9 & 6 \end{array}$
33 34 35 36 37 38	$9 \cdot 81 \ 299 \\ 9 \cdot 81 \ 313 \\ 9 \cdot 81 \ 328 \\ 9 \cdot 81 \ 343 \\ 9 \cdot 81 \ 358 \\ 9 \cdot 81 \ 372 \\ \end{array}$	$1\overline{4}$ 15 14 15 $1\overline{4}$ $1\overline{4}$ $1\overline{4}$	9.93 252 9.93 252 9.93 278 9.93 303 9.93 329 9.93 354		$\begin{array}{c} 06 & 77\overline{3} \\ 06 & 748 \\ 06 & 722 \\ 06 & 696 \\ 06 & 671 \\ 06 & 645 \\ 06 & 645 \end{array}$	9.88 029 9.88 018	10 11 11 10 11 11	27 26 25 24 23 22	40 10.3 10.6 9.6 50 12.9 12.5 12 <b>.1</b>
39 40 41 42 43 44	$\frac{9 \cdot 81 \ 387}{9 \cdot 81 \ 402} \\9 \cdot 81 \ 416 \\9 \cdot 81 \ 431 \\9 \cdot 81 \ 446 \\9 \cdot 81 \ 460$	$15 \\ 14 \\ 15 \\ 14 \\ 14 \\ 14 \\ 14 \\ 14 \\ $	9.93 405 9.93 431 9.93 456 9.93 482 9.93 508	2550.0 2550.0 2500.0 2500.0	06 620 06 594 06 569 06 543 06 518 06 492	9 · 87 99 <u>6</u> 9 · 87 985 9 · 87 974 9 · 87 963	$1\overline{0}\\11\\11\\11\\11\\1\overline{0}$	21 20 19 18 17 16	.11.10
45 46 47 48 49	9.81504 9.81519 9.81534	$14 \\ 14 \\ 15 \\ 14 \\ 14 \\ 17 \\ 17 \\ 17 \\ 17 \\ 17 \\ 17$	9.93 55 <u>9</u> 9.93 584 9.93 610 9.93 635		06 466 06 441 06 415 06 390 06 364	9.87931 9.87920 9.87909 9.87898	$     \begin{array}{c}       11 \\       11 \\       11 \\       10 \\       11 \\$	15 14 13 12 11	$\begin{array}{c} 6 1 \cdot 1 \\ 7 1 \cdot 3 1 \cdot 2 \\ 8 1 \cdot 4 1 \cdot 4 \\ 9 1 \cdot 6 1 \cdot 6 \\ 10 1 \cdot \overline{8} 1 \cdot \overline{7} \\ 20 3 \cdot \overline{6} 3 \cdot \overline{5} \\ \end{array}$
50 51 52 53 54 55	9.81 548 9.81 563 9.81 578 9.81 592 9.81 607	$1\overline{4} \\ 15 \\ 1\overline{4} \\ 1\overline{4} \\ 1\overline{4}$	9.93 686 9.93 686 9.93 712 9.93 737 9.93 763	25 0. 25 0. 25 0. 25 0. 25 0. 25 0. 25 0. 25 0.	06 33 <u>9</u> 06 313 06 288 06 262 06 237 06 211	9 · 87 87 <u>6</u> 9 · 87 86 <u>5</u> 9 · 87 854 9 · 87 844	$11 \\ 11 \\ 11 \\ 11 \\ 10 \\ 11 \\ 11 \\ 11 \\$	$     \begin{array}{c}       10 \\       9 \\       8 \\       7 \\       6 \\       5     \end{array} $	30 5 5 5 5 2 40 7 3 7 0 50 9 1 8 7
55 57 58 59 60	9.81 665	$14 \\ 14 \\ 14 \\ 14 \\ 15 \\ 17 \\ 17 \\ 17 \\ 17 \\ 17 \\ 17 \\ 17$	9.93814 9.93840 9.93865 9.93865	26 26 25 0.0	06 186 06 160 06 134 06 109	9 87 822 9 87 811 9 87 800	$11 \\ 11 \\ 11 \\ 11 \\ 11 \\ 11 \\ 11 \\ 11 $	$     \begin{array}{c}       5 \\       4 \\       3 \\       2 \\       1 \\       0     \end{array} $	ц.,
<u> </u>	Log. Cos.	d.		.d. Log		Log. Sin.	d.	<i>~</i>	P. P.

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TABLE VII.—LOGARITHMIC SINES, COSINES, TANGENTS, AND COTANGENTS.

41°	AND COTANGENTS.	138°
' Log. Sin. d	Log. Tan. c. d. Log. Cot. Log. Cos. d.	P. P.
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	$\begin{array}{c} \begin{array}{c} 1\\ 9& 9.4 & 0.44 \\ 9& 9.4 & 0.65 \\ 1& 25 \\ 1& 9& 9.4 & 0.65 \\ 1& 25 \\ 1& 9& 0.4 & 0.5 \\ 1& 25 \\ 1& 9& 0.4 & 0.5 \\ 1& 25 \\ 1& 9& 0.4 & 0.5 \\ 1& 25 \\ 1& 9& 0.4 & 0.5 \\ 1& 25 \\ 1& 9& 0.4 & 0.5 \\ 1& 25 \\ 1& 0& 0.5 \\ 1& 0& 0.5 \\ 1& 0& 0.5 \\ 1& 0& 0.5 \\ 1& 0& 0.5 \\ 1& 0& 0.5 \\ 1& 0& 0.5 \\ 1& 0& 0.5 \\ 1& 0& 0.5 \\ 1& 0& 0.5 \\ 1& 0& 0& 0& 0 \\ 1& 0& 0& 0& 0& 0 \\ 1& 0& 0& 0& 0& 0& 0\\ 1& 0& 0& 0& 0& 0& 0\\ 1& 0& 0& 0& 0& 0& 0\\ 1& 0& 0& 0& 0& 0& 0\\ 1& 0& 0& 0& 0& 0& 0\\ 1& 0& 0& 0& 0& 0& 0& 0\\ 1& 0& 0& 0& 0& 0& 0& 0\\ 1& 0& 0& 0& 0& 0& 0& 0\\ 1& 0& 0& 0& 0& 0& 0& 0& 0\\ 1& 0& 0& 0& 0& 0& 0& 0& 0\\ 1& 0& 0& 0& 0& 0& 0& 0& 0\\ 1& 0& 0& 0& 0& 0& 0& 0& 0\\ 1& 0& 0& 0& 0& 0& 0& 0& 0\\ 1& 0& 0& 0& 0& 0& 0& 0& 0\\ 1& 0& 0& 0& 0& 0& 0& 0& 0\\ 1& 0& 0& 0& 0& 0& 0& 0& 0\\ 1& 0& 0& 0& 0& 0& 0& 0& 0\\ 1& 0& 0& 0& 0& 0& 0& 0& 0& 0\\ 1& 0& 0& 0& 0& 0& 0& 0& 0& 0\\ 1& 0& 0& 0& 0& 0& 0& 0& 0& 0\\ 1& 0& 0& 0& 0& 0& 0& 0& 0& 0& 0\\ 1& 0& 0& 0& 0& 0& 0& 0& 0& 0& 0\\ 1& 0& 0& 0& 0& 0& 0& 0& 0& 0& 0\\ 1& 0& 0& 0& 0& 0& 0& 0& 0& 0& 0& 0\\ 1& 0& 0& 0& 0& 0& 0& 0& 0& 0& 0& 0\\ 1& 0& 0& 0& 0& 0& 0& 0& 0& 0& 0& 0& 0\\ 1& 0& 0& 0& 0& 0& 0& 0& 0& 0& 0& 0& 0& 0\\ 1& 0& 0& 0& 0& 0& 0& 0& 0& 0& 0& 0& 0& 0&$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$
$\begin{array}{c} 19 & 9.81 969 \\ \hline 200 9.81 983 9.1 \\ 21 9.81 983 9.1 \\ 22 9.82 012 1. \\ 23 9.82 040 \\ 1. \\ 24 9.82 040 \\ 1. \\ 25 9.82 055 \\ 1. \\ 26 9.82 055 \\ 1. \\ 26 9.82 055 \\ 1. \\ 27 9.82 083 1. \\ 1. \\ 28 9.82 098 \\ 1. \\ 29 9.82 121 \\ 1. \\ 30 9.82 126 \\ 1. \\ 33 9.82 140 \\ 1. \\ 33 9.82 140 \\ 1. \\ 34 9.82 145 \\ 1. \\ 35 9.82 197 \\ 1. \\ 35 9.82 240 \\ 1. \\ 38 9.82 240 \\ 1. \\ 38 9.82 240 \\ 1. \\ 39 9.82 254 \\ 1. \\ 39 9.82 254 \\ 1. \\ 39 9.82 260 \\ 1. \\ 39 9.82 254 \\ 1. \\ 39 9.82 260 \\ 1. \\ 39 9.82 260 \\ 1. \\ 39 9.82 254 \\ 1. \\ 39 9.82 283 \\ 1. \\ 1. \\ 30 9.82 283 \\ 1. \\ 1. \\ 1. \\ 1. \\ 1. \\ 1. \\ 1. \\ 1$	$\begin{array}{c} 9.94\ 426 \\ 9.94\ 426 \\ 125 \\ 9.94\ 426 \\ 125 \\ 9.94\ 426 \\ 125 \\ 10.05\ 574\ 9.87\ 555 \\ 11 \\ 39 \\ 139 \\ 139 \\ 139 \\ 139 \\ 139 \\ 139 \\ 139 \\ 139 \\ 139 \\ 139 \\ 139 \\ 139 \\ 139 \\ 139 \\ 130 \\ 110 \\ 120 \\ 130 \\ 110 \\ 120 \\ 110 \\ 120 \\ 130 \\ 110 \\ 120 \\ 110 \\ 110 \\ 120 \\ 110 \\ 110 \\ 1$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
$\begin{array}{c} 1 \\ 42 \\ 9 \\ 82 \\ 297 \\ 14 \\ 43 \\ 9 \\ 82 \\ 317 \\ 14 \\ 44 \\ 9 \\ 82 \\ 317 \\ 14 \\ 45 \\ 9 \\ 82 \\ 317 \\ 14 \\ 45 \\ 9 \\ 82 \\ 317 \\ 14 \\ 45 \\ 9 \\ 82 \\ 317 \\ 14 \\ 45 \\ 9 \\ 82 \\ 317 \\ 14 \\ 45 \\ 9 \\ 82 \\ 317 \\ 14 \\ 51 \\ 9 \\ 82 \\ 417 \\ 14 \\ 51 \\ 9 \\ 82 \\ 417 \\ 14 \\ 51 \\ 9 \\ 82 \\ 417 \\ 14 \\ 51 \\ 9 \\ 82 \\ 417 \\ 14 \\ 51 \\ 9 \\ 82 \\ 421 \\ 14 \\ 55 \\ 9 \\ 82 \\ 421 \\ 14 \\ 55 \\ 9 \\ 82 \\ 421 \\ 14 \\ 55 \\ 9 \\ 82 \\ 421 \\ 14 \\ 55 \\ 9 \\ 82 \\ 421 \\ 14 \\ 55 \\ 9 \\ 82 \\ 421 \\ 14 \\ 55 \\ 9 \\ 82 \\ 421 \\ 14 \\ 55 \\ 9 \\ 82 \\ 425 \\ 14 \\ 58 \\ 9 \\ 82 \\ 557 \\ 14 \\ 56 \\ 80 \\ 80 \\ 80 \\ 80 \\ 80 \\ 80 \\ 80 \\ 8$		$\begin{array}{c} 17 & 11 \\ 6 [1, \frac{1}{2}] 1, 1 \\ 7 [1, \frac{1}{2}] 1, 3 \\ 8 [1, 5] 1, 4 \\ 9 [1, 7] 1, 6 \\ 10 [1, 9] 1, 8 \\ 20 [3, 6] 3, 6 \\ 30 [5, \overline{7}] 5, 5 \\ 40 [7, 6] [7, 3] \\ 50 [9, 6] 9, 1 \end{array}$

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 TABLE VII.—LOGARITHMIC SINES, COSINES, TANGENTS,

 AND COTANGENTS.

42°	AND COTANGENTS.	137°
' Log. Sin.	d. Log. Tan. c. d. Log. Cot. Log. Cos. d.	P. P.
$\begin{array}{c} 0 & 9 & 82 & 551 \\ 1 & 9 & 82 & 565 \\ 1 & 9 & 82 & 565 \\ 1 & 9 & 82 & 565 \\ 1 & 9 & 82 & 565 \\ 1 & 9 & 82 & 565 \\ 1 & 9 & 82 & 565 \\ 1 & 9 & 82 & 565 \\ 1 & 9 & 82 & 565 \\ 1 & 9 & 82 & 565 \\ 1 & 9 & 82 & 565 \\ 1 & 9 & 82 & 565 \\ 1 & 9 & 82 & 565 \\ 1 & 9 & 82 & 565 \\ 1 & 9 & 82 & 565 \\ 1 & 9 & 82 & 565 \\ 1 & 9 & 82 & 643 \\ 1 & 9 & 82 & 643 \\ 1 & 9 & 82 & 643 \\ 1 & 9 & 82 & 643 \\ 1 & 9 & 82 & 643 \\ 1 & 9 & 82 & 643 \\ 1 & 9 & 82 & 643 \\ 1 & 9 & 82 & 643 \\ 1 & 9 & 82 & 643 \\ 1 & 9 & 82 & 643 \\ 1 & 9 & 82 & 643 \\ 1 & 9 & 82 & 643 \\ 1 & 9 & 82 & 643 \\ 1 & 9 & 82 & 643 \\ 1 & 9 & 82 & 746 \\ 1 & 9 & 82 & 746 \\ 1 & 9 & 82 & 746 \\ 1 & 9 & 82 & 746 \\ 1 & 9 & 82 & 746 \\ 1 & 9 & 82 & 786 \\ 1 & 9 & 82 & 786 \\ 1 & 9 & 82 & 786 \\ 1 & 9 & 82 & 786 \\ 1 & 9 & 82 & 786 \\ 1 & 9 & 82 & 786 \\ 1 & 9 & 82 & 786 \\ 1 & 9 & 82 & 786 \\ 1 & 9 & 82 & 786 \\ 1 & 9 & 82 & 836 \\ 1 & 9 & 82 & 836 \\ 1 & 9 & 82 & 982 \\ 1 & 9 & 82 & 982 \\ 1 & 9 & 82 & 982 \\ 1 & 9 & 82 & 982 \\ 1 & 9 & 82 & 982 \\ 1 & 9 & 82 & 982 \\ 1 & 9 & 82 & 982 \\ 1 & 9 & 82 & 982 \\ 1 & 9 & 82 & 982 \\ 1 & 9 & 82 & 982 \\ 1 & 9 & 82 & 982 \\ 1 & 9 & 82 & 982 \\ 1 & 9 & 82 & 982 \\ 1 & 9 & 82 & 982 \\ 1 & 9 & 83 & 023 \\ 1 & 9 & 83 & 023 \\ 1 & 9 & 83 & 023 \\ 1 & 9 & 83 & 023 \\ 1 & 9 & 83 & 023 \\ 1 & 9 & 83 & 023 \\ 1 & 9 & 83 & 023 \\ 1 & 9 & 83 & 023 \\ 1 & 9 & 83 & 023 \\ 1 & 9 & 83 & 023 \\ 1 & 9 & 83 & 023 \\ 1 & 9 & 83 & 024 \\ 1 & 9 & 83 & 106 \\ 1 & 1 & 9 & 83 & 106 \\ 1 & 1 & 9 & 83 & 106 \\ 1 & 1 & 9 & 83 & 106 \\ 1 & 1 & 9 & 83 & 215 \\ 1 & 9 & 83 & 229 \\ 1 & 1 & 1 & 1 \\ 1 & 1 & 1 & 1 & $	$\begin{array}{c} 4 \\ 4 \\ 9 \\ 9 \\ 9 \\ 9 \\ 9 \\ 4 \\ 4 \\ 9 \\ 9$	$\begin{array}{c} 25 & 25 \\ 6 & 2.5 \\ 7 & 3.0 \\ 2.9 \\ 7 & 3.0 \\ 2.9 \\ 8 & 3.4 \\ 3.9 \\ 9 \\ 3.8 \\ 3.7 \\ 10 \\ 4.2 \\ 4.1 \\ 3.0 \\ 12.7 \\ 12.5 \\ 40 \\ 17.0 \\ 16.6 \\ 1.4 \\ 1.3 \\ 1.6 \\ 1.2 \\ 1.2 \\ 1.2 \\ 20.8 \\ 1.6 \\ 1.2 \\ 1.2 \\ 1.2 \\ 20.8 \\ 1.6 \\ 1.2 \\ 1$
1-0D. 0301		1

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# TABLE VII.—LOGARITHMIC SINES, COSINES, TANGENTS, AND COTANGENTS.

43°	VII.—LOGA	AND COTANGEN		ES, TANGENIS, 136°
' Log. Sin. d.	Log. Tan. c. d.	Log. Cot. Log. Cos.	d.	· P. P.
$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	$\begin{array}{c} 9.9696\overline{5}\\ 9.96901\\ 25\\ 9.97016\\ 25\\ 9.9704\overline{1}\\ 25\\ 9.9704\overline{1}\\ 25\\ 9.9704\overline{1}\\ 25\\ 9.9704\overline{1}\\ 25\\ 9.97107\\ 25\\ 9.97117\\ 25\\ 9.97143\\ 25\\ 9.97168\\ 25\\ 2.5\\ 9.97132\\ 25\\ 9.97132\\ 25\\ 9.97132\\ 25\\ 9.97132\\ 25\\ 9.97132\\ 25\\ 9.97132\\ 25\\ 9.97132\\ 25\\ 9.97132\\ 25\\ 9.97132\\ 25\\ 9.97132\\ 25\\ 9.97132\\ 25\\ 25\\ 9.97132\\ 25\\ 25\\ 25\\ 25\\ 25\\ 25\\ 25\\ 25\\ 25\\ 2$	$\begin{array}{c} \hline 0.03 \ 03\overline{4} & 9.86 \ 41\overline{2} \\ 0.03 \ 009 \ 9.86 \ 401 \\ 0.02 \ 984 \ 9.86 \ 389 \\ 0.02 \ 95\overline{3} & 9.86 \ 37\overline{6} \\ 0.02 \ 93\overline{3} & 9.86 \ 37\overline{6} \\ 0.02 \ 93\overline{3} & 9.86 \ 37\overline{6} \\ 0.02 \ 90\overline{8} & 9.86 \ 35\overline{4} \\ 0.02 \ 85\overline{7} & 9.86 \ 342 \\ 0.02 \ 85\overline{7} & 9.86 \ 31\overline{8} \\ 0.02 \ 85\overline{2} & 9.86 \ 31\overline{8} \\ 0.02 \ 85\overline{6} & 9.86 \ 30\overline{6} \\ \end{array}$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$2\overline{5}$ 25 6  2.5  2.5
$\begin{array}{c} 10 \\ 9 \\ 83 \\ 513 \\ 11 \\ 9 \\ 83 \\ 527 \\ 13 \\ 9 \\ 83 \\ 540 \\ 13 \\ 9 \\ 83 \\ 554 \\ 13 \\ 9 \\ 83 \\ 554 \\ 13 \\ 14 \\ 9 \\ 83 \\ 554 \\ 13 \\ 15 \\ 9 \\ 83 \\ 554 \\ 13 \\ 15 \\ 9 \\ 83 \\ 554 \\ 13 \\ 15 \\ 9 \\ 83 \\ 554 \\ 13 \\ 15 \\ 9 \\ 83 \\ 567 \\ 13 \\ 13 \\ 15 \\ 9 \\ 83 \\ 567 \\ 13 \\ 13 \\ 15 \\ 9 \\ 83 \\ 567 \\ 13 \\ 13 \\ 15 \\ 9 \\ 83 \\ 567 \\ 13 \\ 13 \\ 15 \\ 10 \\ 13 \\ 10 \\ 13 \\ 10 \\ 13 \\ 10 \\ 13 \\ 10 \\ 10$	$\begin{array}{c} 9.97\ 219\\ 9.97\ 244\\ 9.97\ 269\\ 25\\ 9.97\ 295\\ 9.97\ 295\\ 9.97\ 320\\ 9.97\ 345\\ 9.97\ 370\\ 9.97\ 370\\ 9.97\ 320\\ 9.97\ 421\\ 9.97\ 421\\ 9.97\ 421\\ 9.97\ 426\\ $	$\begin{array}{c} 0.02\ 781 9.86\ 294 \\ 0.02\ 756 9.86\ 282 \\ 0.02\ 736 9.86\ 281 \\ 0.02\ 736 9.86\ 281 \\ 0.02\ 705 9.86\ 291 \\ 0.02\ 680 9.86\ 247 \\ 0.02\ 654 9.86\ 235 \\ 0.02\ 624 9.86\ 235 \\ 0.02\ 604\ 9.86\ 211 \\ 0.02\ 578\ 9.86\ 199 \\ 0.02\ 578\ 9.86\ 199 \\ 0.02\ 578\ 9.86\ 197 \ 9.86\ 197 \ 9.86\ 197 \ 9.86\ 197 \ 9.86\ 197 \ 9.86\ 197 \ 9.86\ 197 \ 9.86\ 197 \ 9.86\ 100\ 100\ 100\ 100\ 100\ 100\ 100\ 10$	$\begin{array}{c} 12 & 49 \\ 11 & 48 \\ 12 & 47 \\ 12 & 46 \\ 11 & 45 \\ 12 & 44 \\ 12 & 43 \\ 12 & 42 \\ 12 & 42 \\ 12 & 41 \\ 11 & 11 \\ \end{array}$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	$\begin{array}{c} 9 & 97 & 419 \\ 9 & 97 & 522 \\ 9 & 97 & 522 \\ 9 & 97 & 522 \\ 9 & 97 & 522 \\ 9 & 97 & 573 \\ 9 & 97 & 568 \\ 9 & 97 & 578 \\ 9 & 97 & 649 \\ 9 & 97 & 649 \\ 9 & 97 & 674 \\ 9 & 97 & 674 \\ 9 & 97 & 674 \\ 9 & 97 & 674 \\ 9 & 97 & 755 \\ 9 & 97 & 755 \\ 9 & 97 & 755 \\ 9 & 97 & 755 \\ 9 & 97 & 755 \\ 9 & 97 & 755 \\ 9 & 97 & 755 \\ 9 & 97 & 851 \\ 2 & 55 \\ 1 & 55 \\ 1 $	$\begin{array}{c} 0.02\ 528\ 9.86\ 176\\ 0.02\ 502\ 9.86\ 164\\ 0.02\ 477\ 9.86\ 152\\ 0.02\ 452\ 9.86\ 140\\ 0.02\ 452\ 9.86\ 152\\ 0.02\ 452\ 9.86\ 152\\ 0.02\ 452\ 9.86\ 152\\ 0.02\ 452\ 9.86\ 164\\ 0.02\ 376\ 9.86\ 104\\ 0.02\ 351\ 9.86\ 080\\ 0.02\ 351\ 9.86\ 080\\ 0.02\ 351\ 9.86\ 080\\ 0.02\ 275\ 9.86\ 068\\ 0.02\ 275\ 9.86\ 068\\ 0.02\ 275\ 9.86\ 068\\ 0.02\ 124\ 9.86\ 020\\ 0.02\ 174\ 9.86\ 000\\ 0.02\ 124\ 9.85\ 996\\ 0.02\ 123\ 9.85\ 984\\ 0.02\ 092\ 9.85\ 984\\ 0.02\ 092\ 9.85\ 984\\ 0.02\ 092\ 9.85\ 984\\ 0.02\ 092\ 9.85\ 984\\ 0.02\ 092\ 9.85\ 960\\ 0.02\ 123\ 9.85\ 960\ 0.02\ 120\ 9.85\ 960\ 0.02\ 120\ 9.85\ 960\ 0.02\ 120\ 9.85\ 960\ 0.02\ 120\ 9.85\ 960\ 0.02\ 120\ 9.85\ 960\ 0.02\ 120\ 9.85\ 960\ 0.02\ 120\ 9.85\ 960\ 0.02\ 100\ 0.02$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{array}{c} 9.97 \ 95\overline{2} \\ 9.97 \ 97\overline{8} \\ 9.98 \ 079 \ 978 \\ 9.98 \ 028 \ 255 \\ 9.98 \ 054 \\ 9.98 \ 074 \ 255 \\ 9.98 \ 074 \ 255 \\ 9.98 \ 10\overline{2} \ 255 \\ 9.98 \ 10\overline{2} \ 255 \\ 9.98 \ 10\overline{2} \ 255 \\ 9.98 \ 256 \ 255 \\ 9.98 \ 256 \ 255 \\ 9.98 \ 357 \ 255 \ 357$	$\begin{array}{c} 0.02 \ 04\overline{7} \ 9.85 \ 948\\ 0.02 \ 022 \ 9.85 \ 936\\ 0.01 \ 99\overline{6} \ 9.85 \ 912\\ 0.01 \ 97\overline{1} \ 9.85 \ 912\\ 0.01 \ 946 \ 9.85 \ 912\\ 0.01 \ 946 \ 9.85 \ 912\\ 0.01 \ 946 \ 9.85 \ 912\\ 0.01 \ 946 \ 9.85 \ 875\\ 0.01 \ 97\overline{1} \ 9.85 \ 875\\ 0.01 \ 87\overline{0} \ 9.85 \ 875\\ 0.01 \ 87\overline{0} \ 9.85 \ 875\\ 0.01 \ 87\overline{0} \ 9.85 \ 815\\ 0.01 \ 744 \ 9.85 \ 815\\ 0.01 \ 744 \ 9.85 \ 815\\ 0.01 \ 744 \ 9.85 \ 815\\ 0.01 \ 744 \ 9.85 \ 815\\ 0.01 \ 744 \ 9.85 \ 815\\ 0.01 \ 748 \ 9.85 \ 778\\ 0.01 \ 668 \ 9.85 \ 778\\ 0.01 \ 668 \ 9.85 \ 778\\ 0.01 \ 668 \ 9.85 \ 754\\ 0.01 \ 667 \ 9.85 \ 754\\ 0.01 \ 667 \ 9.85 \ 718\\ 0.01 \ 572 \ 9.85 \ 718\\ 0.01 \ 574 \ 9.85 $	$\begin{array}{c} 12 \\ 221 \\ 12 \\ 209 \\ 122 \\ 12 \\ 12 \\ 12 \\ 12 \\ 12 \\ 12 \\ $	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
60 9.84 177 Log. Cos. d	5.50 400	0.01 516 9.85 693 Log. Tan. Log. Sin.	12 0 d. /	P. P.

133°

648

46°

TABLE VII.—LOGARITHMIC SINES, COSINES, TANGENTS, AND COTANGENTS.

134°

44°

642

45°

### , Log. Vers. D D D D , Log. Exsec. Log. Vers. Log. Exsec. 01234 Õ - 00 8 6.18271 6.18278 $143\overline{5} \\ 1412 \\ 1389$ $1436\\1412$ 19707 2.62642 2.62642 .19714 1234 60206 60206 21126 3 · 22848 3 · 58066 3.22848.21119 35218 24987 1390 35218 3.58066 ·22516 ·23884 .22509 24987 1368 1368 23877 3.830543.8305419382 19382 $134\overline{6}$ 1347 567 4.02436.18272 $4.0243\overline{6}$ .18272 6.25223 6.25231 5 1583 13389 1326 1326 15836 26549 .26557 6 7 8 13389 1306 1306 .31662 .31662 .27856 .2786411598 11598 1286 1287 8 .43260 ·43260 $.2914\overline{2}$ .29151 10230 10230 1268 1268 õ .53490 .53491 ·30410 ·30419 ġ $915\overline{1} \\ 827\overline{8}$ 1250 1250 9151 10 4.62642 .70920 4.626426.31660 6.31669 10 $1232 \\ 1214$ 8279 1232 īī .70921 .32901 ·32892 11 7557 6952 7558 1215 $\overline{12}$ $\overline{12}$ .78478 .78478 .34107 $3411\bar{6}$ 6953 1198 1198 ī3 13 35305 35315 .85431 .85431 6437 1182 1182 6437 .91868 .91868 36487 .36497 $\overline{14}$ 14 599<u>2</u> 5605 599<u>3</u> 5605 1166 1166 6.37663 15 15 4.97860 4.97866.37653 $1150 \\ 1135$ $1151 \\ 1135$ 5.03466 38814 16 38803 16 5.03466526<u>6</u> 5266 4964 17 17 .08732 .08732 39938 39949 4964 1121 112118 18 13697 $41059 \\ 42165$ ·41070 ·13696 1106 1106 4696 4696 18393 18393 42177 19 19 109<u>3</u> 1078 $1093 \\ 1079$ 4455 4456 $\mathbf{20}$ 20 21 5.228485.228496.43258 6.43270 4238 4238 21 22 .27086 .27087 .44337 ·44349 1066 4040 1066 404<u>0</u> $\overline{22}$ ·31126 .31127.45403 .454153861 3861 $105\bar{2}$ 105<u>3</u> 23 .34987 .34988 ·46468 23 $.4645\overline{5}$ 3697 3697 $104\bar{0}$ $104\bar{0}$ 24 .38684 .38685 .47496 .47509 24 $354\overline{5}$ 1028 1028 $354\overline{5}$ 25 25 5.42230 5.422316.48524 6.48537 1016 1004 992 3406 1015 3407 26 ·45636 .45638 .49539 .49553 26 3278 3278 $100\bar{4}$ -48915 -52073 -55121 27 27 .48916 .50544 50557 3158 3159 993 28 28 .52075.51536 51550 981 3048 982 3048 $\tilde{2}\tilde{9}$ 29 .55123 .52518 52532 2944 970 970 2945 5.58066 30 30 5.58068 2848 2757 2672 6.53488 6.53503 960 2848 960 31 31 ·60914 .60916 . 54448 .54463 949 2758 950 32 32 .63672 .63674 .55397 .55413939 $267\bar{2}$ 939 33 ·66344 ·66346 .56336 ·56352 ·57281 33 2593 2593 929 929 34 .68937 .68940 34 .57265 2518 919 919 251735 5.71455 5.71457 35 6.58184 6.58201 2447 2379 2447 909 909 900 .73902 36 73904 .59093 ·59110 36 2380 900 37 37 ·76282 ·78598 ·76284 . 59993 .60011 $231\bar{6}$ 2316 891 891 882 38 78601 38 $.6088\overline{4}$ .60902 2256 882 $225\overline{6}$ 39 ·80854 ·80857 61766 39 $6178\bar{4}$ 2199 872 2199 $873 \\ 864$ 40 5.83053 5.83056 6.62639 40 6.62657 2145 2093 2043 2145864 ·85198 .85201 .63503 41 .63522 41 2093 855 847 856 $\overline{4}2$ ·8729] .87295 42 .64359 .64378 2044848 43 ·89335 .89338 ·65206 65226 43 1996 839 1997 839 44 .91332 .91335 .66045 44 .66065 83<u>1</u> 82<u>3</u> 815 1952 $195\overline{2}$ 83Ī 45 5.93284 5.93288 6.66876 45 6.66897 1909 823 1909 .95193 46 .95197 .67700 46 67720 1868 1868 81<u>6</u> 80<u>8</u> 47 .97061 .97065 ·68515 ·69323 68536 47 1829 808 1829 $\overline{48}$ 5.98890 5.98894 48 69345 1790 1791 800 800 $\overline{49}$ 6.00680 6.00685 70124 .70145 49 1755 793 1755 6.02435 794 50 6.02440 6.709176.70939 .71725 501720 786 1720 786 51 ·04155 .0416071703 51 1686 1687 779 779772772 $\overline{52}$ .05842 ·05847 ·07501 72482 72505 73277 52 $1654 \\ 1623$ $165\overline{4} \\ 162\overline{3}$ 772 53 .07496 53 73254 765 54 .09120 .0912574019 54 74043 1594 758 $159\bar{4}$ 759 55 6.10714 6.10719 6 · 74802 · 75554 · 76300 6.74777 752 745 739 55 1565 1565 75256 .12279·12284 75529 56 74<u>6</u> 73<u>9</u> 733 1537 1537 57 .13816 .13822 76275 57 $1511 \\ 1484$ 1511 58 .15327 .15333 770407777358 59 733 1485 59 .16811 .16818 77747 1460 $72\bar{6}$ 1460 727 60 6.1827] 6.18278 ē.78500 6.7847460 Log. Vers. D Log. Exsec $\boldsymbol{n}$ Log. Vers. $\overline{D}$ $\overline{D}$ Log. Exsec.

## TABLE VIII.—LOGARITHMIC VERSED SINES AND EXTERNAL 0° SECANTS. 1°

### , D Log. Vers. D Log. Exsec. D 1 D Log. Exsec. Log. Vers. $7.1374\bar{6}$ ō 7.13687 0 6.784746.78500 721 715 709 703 481 **48**Ī 721 714 14168 478 475 473 .14228 12 1 79195 ·79221 479 .14707 23 ·79909 .79937 .80646 ·14646 $\bar{4}\bar{7}\bar{6}$ 709 703 15122 ·15183 ·15657 34 ·80618 474 .15595 4 .81322 .81350 470 471 697 698 5 7.16066 5 6.82019 6.82048 7.16129 692 692 468 469 .16534 .82711 .82740 .16598 6 6 686 466 466 687 .17000 7 .83398 ·83427 .17064 7 463 460 464681 682 .17463 ·17528 8 .84079 ·84109 8 676 676 461 .84785 ·17923 ·17989 ĝ 9 •84755 45<u>8</u> 45<u>5</u> 45<u>3</u> 670 671 45<u>9</u> 10 6.85425 6.854577.18382 7.18448 10 66<u>5</u> 660 666 456 .18837 .86123 $\frac{11}{12}$ 11 .86091 .18905 66Ō 454 $\overline{12}$ 13.86751 ·86783 .19291 .19359 655 656 451 452·19742 .87407 .87439 .19811 13 448 650 651 449 14 ·88057 ·88090 .20191 .20260 14 446 447 646 <u>64</u> 6.88703 6.88737 7.20637 7.20707 15 15 445 442 440 641 444 64] .89378 ·21152 ·89344 ·89980 16 .21081 16 636 636 631 627 ·21523 ·21963 442 17 .90015 .21595 17 18 440 632 18 .90612 .90647 ·22035 437 438 628 91239 91275 22400 22473 ī9 19 $62\bar{2}$ 435 436 623 7.22909 6.91862 6.91898 7.22836 20 20 434 431 618 614 618 433 21 22 21 22 $.2334\overline{3}$ .92480 ·92516 .23269 613 431 .93093 .23700 .23775 .93131 609 429 429 610 23 .93703 .93741 24129 ·24204 23 24 25 26 27 605 605 426 427 24555 24 •94308 .94346 .24632 $42\overline{4}$ $42\overline{2}$ $42\bar{5}$ 601 601 6.94909 7.24980 7.25057 25 6.94948423 421 597 593 597 ·25402 25480 .95506 ·95545 422 420 418 416 26 592 .96139 .25823 .25902 27 .96099 419 589 589 .96728 28 ·26241 .26321 28 .96688 417 584 585 26738 29 29 ·97272 .97313 .26658 41<u>4</u> 41<u>2</u> 410 $\frac{415}{413}$ 581 581 6.97895 7.27072 7.27153 30 30 6.97853 577 57<u>7</u> 573 .27485 27567 31 ·98472 61 ·98430 $\overline{411}$ 574 32 33 ·27895 .27978 32 33 ·99046 .99004 409 569 570 409 28387 6.99573 6.99616 $.2830\overline{4}$ 407 $40\bar{6}$ 535 566 .28711 28795 34 **B**4 7.00139 7.00182 405 405 562 558 563 7.29200 35 35 7.007457.29116 7.00701 402 404559 $2960\bar{4}$ 36 36 37 .01259 .01304 29518 401 399 402 555 55<u>5</u> 551 29919 37 30006 .01860 $.0181\bar{4}$ 400 552 548 30406 38 38 .02412 30319 .02366 397 398 548 30716 30804 39 39 02960 02914 39<u>5</u> 393 396 545 544 40 7.31112 7.31201 40 7.03505 7.03458 394 $541 \\ 538$ 3150<u>5</u> 31897 .31595 541 41 41 .04047 03999 392 390 393 537 534 .31988 42 42 .04585 .04537 391 535 . 32379 43 32288 43 .05120 05071 389 53Î 388 531 ·32768 44 32676 44 05603 .05652 388 386 528 527 7.33156 45 45 7.06180 7.33063 385 384 382 380 7.06130 38<u>5</u> 383 525 521 518 515 525 ·33542 ·33926 46 33448 46 06655 .06706 522 47 47 33831 .07177 ·07228 382 519 **4**8 48 49 34213 .34309 .07695 .07747 380 516 49 .34689 08263 34593 .08211 379 378 $512 \\ 509$ $513 \\ 509$ 7.35069 50 50 7.34971 7.08776 7.08723 377 377 51 35348 $3544\overline{6}$ 51 09232 .09286 37<u>5</u> 37<u>3</u> 371 376 50<u>5</u> 50<u>5</u> 50<u>3</u> 500 50<u>7</u> 503 52 35822 52 53 35723 .09793 .09739 374 53 ·36196 .10297 36097 .10242 373 501 .36569 54 54 .10798 36468 .10743 371 498 370 497 55 7.36940 55 7.11297 7.36839 369 7.11240 368 495 495 37310 56 56 11792 37207 .11735 368 493 367 492 57 57 .37574 .37678 ·12227 .12285 366 366 48<u>9</u> 490 58 .38044 58 .12716 .12775 37940 365 364 486 487 59 .38409 59 $3830\bar{4}$ .13203 .13262 $36\overline{3}$ $48\overline{4}$ 362 484 60 7.38773 60 7.13746 7. 38667 7.13687D 7 DLog. Exsec. $\overline{D}$ Log. Vers. D Exsec. Log. Log. Vers

## TABLE VIII.—LOGARITHMIC VERSED SINES AND EXTERNAL 2° SECANTS. 3°

TABLE VIIILOGARI	THMIC VERSED SINES.	AND EXTERNAL SECANTS.
4°	5°	

чл ,	$\frac{4^{\circ}}{5^{\circ}}$										
	Lg. Vers.	D	Log. Exs.	D	Lg. Vers.	D	Log. Exs.	D	'	P. P.	
0 1 2 3 4	$ \begin{array}{r}       .39028 \\       .39387 \\       .39745 \\       .40102 \\       .40102 \end{array} $	61 59 58 56	7.3877 <u>3</u> .39134 .39495 .39854 .40211	36 <u>1</u> 360 359 357	7.58039 58328 58615 58902 59188	289 287 287 286	7.58204 .58494 .58783 .59071 .59358	290 289 288 287	0 1 2 3 4	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	
5 6 7 8 9	7.404573 .408103 .411633 .415133 .41863	553 52 50 49	7.40567 .40922 .41275 .41627 .41977	35 <u>6</u> 354 353 352 350	7.59473.59758.60041.60323.60604	285 284 283 282 281	7.59645.59930.60214.60498.60780	286 285 284 283 283 282 283	5 6 7 8 9	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	
10 11 12 13 14	$7.42211 \\ -42557 \\ 3.42903 \\ -43246 \\ 3.43589 $	48 45 43 43 2 4	7.42326.42673.43019.43364.43708	349 347 346 345 343	7.60885.61164.61443.61721.61998	280 279 279 277 277 277	7.61062.61342.61622.61901.62179	281 280 280 279 278 278 277	10 11 12 13 14	330         320         310           6         33.0         32.0         31.0           7         38.5         37.3         36.1           8         44.0         42.6         41.3           9         49.5         48.0         46.5	
15 16 17 18 19	$ \begin{array}{r} 7.43930 \\ .44270 \\ 3.44608 \\ .44946 \\ .45281 \\ 3\end{array} $	419 318 317 315 315 314	7.44050 .44390 .44730 .45068 .45405	342 340 339 338 338 337	7 · 62274 · 62549 · 62823 · 63096 · 63369	276 275 274 273 272	7 · 62456 · 62733 · 63008 · 63282 · 63556	276 275 274 274 274 273	15 16 17 18 19	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	
20 21 22 23 24	7.456163 .459493 .462813 .466123 .46941	332 320 29 28	7 · 45740 · 46075 · 46407 · 46739 · 47070	335 334 332 332 330 329	7.63641.63911.64181.64451.64451.64719	272 270 270 269 268 268 267	7.63829 .64101 .64372 .64643 .64643 .64912	273 272 271 270 269 269	20 21 22 23 24	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	
25 26 27 28 29	7.47270 .47597 .47922 .48247 .48570	27 25 24 23	7 · 47399 · 47727 · 4805 <u>4</u> · 4837 <u>9</u> · 48703	328 327 325 324	$7.6498\overline{6} \\ .65253 \\ .65519 \\ .65784 \\ .66048 $	$26\overline{6} \\ 266 \\ 265 \\ 26\overline{4} $	7.65181 .65449 .65716 .65982 .66247	268     267     266     265     265     264	25 26 27 28 29	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	
30 31 32 33 34	7.488923 .492133 .495333 .498523 .50169	22 21 20 18 17	$\begin{array}{r} 7.4902\overline{6} \\ .49348 \\ .49669 \\ .49989 \\ .50307 \end{array}$	323 322 321 319 318		263 263 261 261 260	7.66512 .66776 .67039 .67301 .67562	264 263 262 261 261	30 31 32 33 34	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	
35 36 37 38 39	7.50485 508003 511143 514273 51739	16 15 14 13 11	$7.5062\overline{4}$ .50941 .51256 .51569 .51882	$317 \\ 316 \\ 315 \\ 313 \\ 313 \\ 313 \\ 311 $		259 258 258 257 256	7 · 6782 <u>3</u> · 6808 <u>3</u> · 68342 · 6860 <u>1</u> · 68858	260 259 258 257 257	35 36 37 38 39	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	
40 41 42 43 44	7.52050 .52359 .52667 3 .52975 3 .53281	11 809 808 807 806	7.52194.52504.52814.53122.53429	310 309 308 307	7.68902 .69157 .69411 .69665 .69917	255 255 254 253 252	7.69115 .69371 .69627 .69881 .70135	$256 \\ 255 \\ 254 $	40 41 42 43 44	240         230         220           6         24.0         23.0         22.0           7         28.0         26.8         25.6           8         32.0         30.6         29.3	
45 46 47 48 49	7 · 53586 3 · 53890 3 · 54193 3 · 54495 3 · 54796	05 04 03 02 00	$7.5373\overline{5}$ .54041 .54345 .54648 .54950	306 305 304 303 302	.70671	252 251 250 250 249	7 · 70388 · 70641 · 70893 · 71144 · 71394	250	45 46 47 48 49	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	
50 51 52 53 54	7 · 55096 · 55395 · 55692 · 55989 · 56285	999 97 97 97 95	7.55251.55550.55849.56147.56444	30 <u>1</u> 299 299 298 298	$7.7141\overline{8} \\ .71666 \\ .71913 \\ .72159 \\ .72404$	$24\overline{8} \\ 247 \\ 247 \\ 246 \\ 245 \\ 2$	7 · 71644 · 71892 · 72141 · 72388 · 72635	250 248 248 247 246 246	50 51 52 53 54		
55 56 57 58 59	7 · 56580 22 · 56873 22 · 57166 22 · 57458 22 · 57458 22	295 293 293 292 292 290	7 · 56740 · 57035 · 57329 · 57621 · 57913	296 295 29 <u>4</u> 292 292	7 · 72649 · 72893 · 73137 · 73379 · 73621	245 244 243 242 242 242	7.7288 <u>1</u> .7312 <u>6</u> .7337 <u>1</u> .73615 .73859	$24\overline{6}$ 245 245 244 243 $24\overline{3}$	55 56 57 58 59	$\begin{array}{c} 21.0 \\ 7 \\ 24.5 \\ 23.0 \\ 24.5 \\ 23.0 \\ 24.5 $	
<u>60</u> /	$7.58039^2$	290 D	7 · 58204 Log. Exs.	291 D	<u>7 - 73863</u> Lg. Vers.	$\frac{24\overline{1}}{D}$	<u>7 · 74101</u> Log. Exs.	$\frac{24\overline{2}}{D}$	<u>60</u> '	50 175.0 166.6 158.3 P. P.	

TABLE VIII.-LOGARITHMIC VERSED SINES AND EXTERNAL SECANTS.

	6°		7	•	
Lg. Vers.	D Log. Exs. Di	Lg. Vers. D	Log. Exs. D	Ľ	P. P.
$\begin{array}{c}1 & .74104 \\2 & .74344 \\3 & .74583 \\4 & .74822 \end{array}$	$\begin{array}{c} 41\\ 40\\ 39\\ 39\\ 75066\\ 75066\\ 38\\ 775066\\ 75305\\ 241\\ 75066\\ 240\\ 238\\ 775305\\ 238\\ 238\\ 775305\\ 238\\ 238\\ 238\\ 238\\ 238\\ 238\\ 238\\ 238$	7 · 87238 · 87444 · 87650 · 87855 · 88060 7 · 99987 20	87978 20 87978 20 88185 20 88391 20	7 2 7 3 4	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
8 .75534 2 7 .75534 2 8 .75770 2 9 .76006	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	7.88264 20 .88468 20 .88672 20 .88875 20 .88875 20 .88977 20	89008 20 89212 20 89212 20 89416 20	07.89	20 60.0 3.1 3.0 30 90.0 4.7 4.5 40 120.0 6.3 6.0 50 150.0 7.9 7.5
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{array}{c} 3\frac{4}{2} & 7.76728 \\ 3\overline{3} & 76728 \\ 3\overline{3} & 76963 \\ 3\overline{3} & 77197 \\ 3\overline{2} & 771431 \\ 3\overline{2} & 77431 \\ 3$	89481 20 89682 20 89882 20 90082 10	$\begin{array}{c} 1 & \cdot 89823 \\ 0 & \cdot 90025 \\ 0 & \cdot 90228 \\ 0 & \cdot 90429 \\ 0 & \cdot 90429 \\ 0 \end{array}$	$     \begin{array}{c}       10 \\       11 \\       12 \\       12 \\       13 \\       14 \\       14 \\     \end{array} $	$\begin{array}{c c} \overline{8} & 8 & \overline{7} \\ 6 & 0 \cdot \overline{8} & 0 \cdot 9 \\ 7 & 1 \cdot 0 & 0 \cdot 9 & 0 \cdot 9 \\ 8 & 1 \cdot 1 & 1 \cdot 0 & 1 \cdot 0 \\ 9 & 1 \cdot 3 & 1 \cdot 2 & 1 \cdot 1 \\ 10 & 1 \cdot 4 & 1 \cdot 3 & 1 \cdot 2 \end{array}$
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{array}{c} 31\\ 3\overline{0}\\ 3\overline{0}\\ 77897\\ 23\overline{1}\\ 7812\overline{8}\\ 23\overline{1}\\ 30\\ 78360\\ 23\overline{1}\\ 7859\overline{0}\\ 23\overline{0}\\ 7859\overline{0}\\ 7859\overline{0}\\$	·90282 19 ·90481 19 ·90680 19 ·90878 19 ·91076 10		10 16 17 18 19 19	$\begin{array}{c} 10 & 1 \cdot \underline{4} \\ 20 & 2 \cdot \underline{3} \\ 20 & 2 \cdot \underline{3} \\ 2 \cdot \underline{2} \\ 4 \cdot \underline{2} \\ 4 \cdot \underline{2} \\ 4 \cdot \underline{3} \\ 5 \cdot \underline{3} \\ $
$\begin{array}{c c} 20 & 7.78534 \\ 21 & .78783 \\ 22 & .79010 \\ 23 & .79237 \\ 24 & .79463 \\ \end{array}$	28 -79050 229 27 -79279 228 -79507 228 -79507 228 -79735 228	$\begin{array}{r} 7.91273 \\ .91470 \\ 19 \\ .91667 \\ 19 \\ .91863 \\ 19 \\ .92058 \\ 10 \end{array}$	7.9163019 60.9182819 60.9202719 60.9222419 9242119 9242119	20 21 22 23 7 24	$\begin{array}{cccc} 7 & \overline{6} & 6 \\ 6 & 0 \cdot 7 & 0 \cdot \overline{6} & 0 \cdot 6 \\ 7 & 0 \cdot 8 & 0 \cdot 7 & 0 \cdot 7 \\ 8 & 0 \cdot 9 & 0 \cdot 8 & 0 \cdot 8 \\ 9 & 1 \cdot 0 & 1 \cdot 0 & 0 \cdot 9 \end{array}$
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{array}{c} 25 \\ 24 \\ 24 \\ 24 \\ 23 \\ 23 \\ 30864 \\ 30864 \\ 225 \\ 30864 \\ 225 \\ 30864 \\ 225 \\ 30864 \\ 225 \\ 30864 \\ 225 \\ 30864 \\ 224 \\ 225 \\ 30864 \\ 224 \\ 225 \\ 30864 \\ 224 \\ 225 \\ 30864 \\ 224 \\ 225 \\ 30864 \\ 224 \\ 225 \\ 30864 \\ 224 \\ 225 \\ 30864 \\ 224 \\ 225 \\ 30864 \\ 224 \\ 225 \\ 30864 \\ 224 \\ 225 \\ 30864 \\ 224 \\ 225 \\ 30864 \\ 224 \\ 225 \\ 30864 \\ 224 \\ 225 \\ 30864 \\ 224 \\ 225 \\ 30864 \\ 224 \\ 30864 \\ 225 \\ 30864 \\ 225 \\ 30864 \\ 225 \\ 30864 \\ 225 \\ 30864 \\ 225 \\ 30864 \\ 225 \\ 30864 \\ 225 \\ 30864 \\ 225 \\ 30864 \\ 225 \\ 30864 \\ 225 \\ 30864 \\ 225 \\ 30864 \\ 225 \\ 30864 \\ 225 \\ 30864 \\ 225 \\ 30864 \\ 225 \\ 30864 \\ 225 \\ 30864 \\ 225 \\ 30864 \\ 224 \\ 30864 \\ 224 \\ 30864 \\ 224 \\ 30864 \\ 224 \\ 30864 \\ 308$	7.92255 $9.92448$ $9.92642$ $9.92642$ $9.92836$ $9.93029$ $19.93029$ $19.93029$	5 92815 92815 93010 93206 93206 93206 93401	20 26 27 28 29	$\begin{array}{c} 10 & \overline{1} \cdot \overline{1} & \overline{1} \cdot \overline{1} & \overline{1} \cdot \overline{1} \\ 20 & 2 \cdot \overline{3} & 2 \cdot \overline{1} & 2 \cdot 0 \\ 30 & 3 \cdot 5 & 3 \cdot 2 & \overline{3} \cdot 2 \\ 40 & 4 \cdot 6 & 4 \cdot 3 & 4 \cdot 0 \\ 50 & 5 & 8 & 5 \cdot 4 & 5 \cdot 6 \end{array}$
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{array}{c} 22 \\ 21 \\ \cdot 81312 \\ 223 \\ \cdot 81535 \\ 222 \\ \cdot 81758 \\ 222 \\ \cdot 81980 \\ 222 \\ \cdot 81980 \\ 221 \\ \cdot 81980 \\ \cdot 81980$	$\begin{array}{r} 7.93222 \\ .93415 \\ 19 \\ .93607 \\ 19 \\ .93799 \\ 19 \\ .93990 \\ 10 \end{array}$		$     \begin{array}{c}       30 \\       4 \\       31 \\       32 \\       33 \\       34 \\       34     \end{array} $	$\begin{array}{cccccccccccccccccccccccccccccccccccc$
<b>35</b> <b>36</b> <b>36</b> <b>37</b> <b>38</b> <b>38</b> <b>38</b> <b>39</b> <b>39</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b> <b>30</b>	$\begin{array}{c} 19 & \cdot $	$\begin{array}{c} 7.94181 \\ .94371 \\ 190 \\ .94561 \\ 180 \\ .94751 \\ 180 \\ .94940 \\ 180 \end{array}$	$     \begin{array}{c}       7.94562 \\       \cdot 94754 \\       19 \\       \cdot 94946 \\       \cdot 95137 \\       19 \\       \cdot 95328 \\       19 \\       \cdot 95328 \\       10 \\     \end{array} $	35 36 37 38 39	$\begin{array}{c} 9 \\ 0 \cdot 8 \\ 0 \cdot 7 \\ 0 \cdot 7 \\ 0 \cdot 7 \\ 0 \cdot 7 \\ 0 \cdot 8 \\ 0 \cdot 7 \\ 0 \cdot 6 \\ 0 \cdot 7 \\ 0 \cdot 7 \\ 0 \cdot 7 \\ 0 \cdot 7 \\ 0 \cdot 6 \\ 0 \cdot 7 \\ 0 \cdot 7 \\ 0 \cdot 6 \\ 0 \cdot 7 \\ 0 \cdot 7 \\ 0 \cdot 6 \\ 0 \cdot 7 \\ 0 \cdot$
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{array}{c} 17 & \cdot 83518 & 218 \\ 16 & \cdot 83735 & 217 \\ 15 & \cdot 83952 & 217 \\ 15 & \cdot 83952 & 216 \\ 15 & \cdot 84169 & 216 \end{array}$	7.95129 .95317 18 .95505 18 .95693 18 .95880	$     \begin{array}{c}             37.95519 \\             95709 \\             196             95898 \\             96088 \\             186 \\             96276 \\             186             186           $	41 42 43 44	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
$\begin{array}{c} \textbf{45} & \textbf{7.84083} \\ \textbf{46} & \textbf{.84297} \\ \textbf{47} & \textbf{.84510} \\ \textbf{28} \\ \textbf{48} & \textbf{.84723} \\ \textbf{28} \\ \textbf{49} \\ \textbf{.84935} \\ \textbf{29} \end{array}$	$\begin{array}{c} 14 \\ 13 \\ 13 \\ 12 \\ 12 \\ 12 \\ 12 \\ 12 \\ 12$	7.96066 18 .96253 18 .96439 18 .96624 18 .96809 18	$     \begin{array}{c}             996465 \\             96653 \\             96841 \\             97028 \\             97215 \\             187 \\             97215 \\             187 \\             197215 \\             187 \\             197215 \\             187 \\             197215 \\             19$	45     46     47     48     49     49     4	$\begin{array}{c} 9 \\ 0 \cdot 5 \\ 0 \cdot 4 \\ 0 \cdot 4 \\ 0 \cdot 5 \\ 0 \cdot$
51 · 85359 2 52 · 85570 2 53 · 85780 2 54 · 85990	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{array}{c} 7.30394 \\ .97178 \\ 18 \\ .97362 \\ 18 \\ .97546 \\ 18 \\ .97729 \\ 19 \end{array}$	$ \begin{array}{c}             .97401 \\             .97587 \\             .97773 \\             .97958 \\             .98143 \\  $	50 51 52 53 54	$\begin{array}{c c} \mathbf{\overline{1}} & 1 & \mathbf{\overline{0}} \\ 6 \\ 0 \cdot \mathbf{\overline{1}} \\ 0 \cdot 2 \\ 0 \cdot 1 \\ 0 \cdot 0 \end{array}$
55       7.86199       2         56       .86408       2         57       .86616       2         58       .86824       2         59       .87031       2	$\begin{array}{c} 097 \cdot 86510 \\ 08 \cdot 86726 \\ 210 \\ 08 \cdot 86936 \\ 209 \\ 07 \cdot 87146 \\ 208 \\ \cdot 87354 \\ 208 \\ 07 \end{array}$	$\begin{array}{r} 7.97912 \\ .98094 \\ .98276 \\ .98458 \\ .98639 \\ 18 \\ .98639 \\ 18 \\ \end{array}$	$     \begin{array}{c}       7.98327 \\       98512 \\       98695 \\       98879 \\       99062 \\       99062 \\       183     \end{array} $	50 56 57 58 59	$\begin{array}{c} 9 \\ 0 \cdot \overline{2} \\ 0 \cdot 1 \\ 10 \\ 0 \cdot \overline{2} \\ 0 \cdot \overline{1} \\ 0 \cdot \overline{2} \\ 0 \cdot \overline{1} $
001.01230	$\frac{106}{D} \frac{7 \cdot 87563}{\text{Log. Exs.}} \frac{208}{D}$	7.98820 Lg. Vers. D	1.00244	60 (	40 1 . 0 0 . 5 0 . 3 50 1 . 2 0 . 8 0 . 4 P. P.

· 01234 56789 1011234 15	7.98820 99000 99180 99360 99539 7.998718 8.00075 .00253 .00431 8.000784 .00784 .00784 .00961 .01313 8.01438 8.01438 8.01438 8.01438 8.01663 .01838	180 180 179 179	Log, Exs. 7.99244 .99427 .99609 .99790 7.99971 8.00152 .00332 .00692 .00871 8.01050 .01229 .01407 .01585 .01763 8.01940	<b>D</b> 182 181 181 180 180 180 180 179 178 178 178 178 177	.09192 .09352 .09512 .09671	<b>D</b> 160 160 159 159 158 158 158 157 157 157	Log.Exs. 8.09569 .09732 .09894 .10056 .10217 8.10378 .10539 .10700 .10860 .11020 8.11180 .11340	<b>D</b> 162 162 162 161 161 161 160 160 160 160	· 01234 56789	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
5 6 7 8 9 10 11 12 13 14 15	.99000 .99180 .99360 .99539 .99539 .99539 .99539 .00253 .00253 .00253 .00253 .00431 8.00608 .00784 .00784 .00784 .00784 .01137 .01313 8.01488 .01663 .01838 .01838 .01838	$180 \\ 179 \\ 179 \\ 178 \\ 178 \\ 178 \\ 177 \\ 177 \\ 177 \\ 177 \\ 177 \\ 177 \\ 177 \\ 177 \\ 177 \\ 177 \\ 177 \\ 177 \\ 175 \\ 175 \\ 175 $	.99427 .99609 .99790 7.99971 8.00152 .003322 .005122 .00692 .00871 8.01050 .01229 .01407 .01585 .01763	182 181 180 180 180 180 179 179 178 178	.09192 .09352 .09671 8.09830 .09983 .10148 .10306 .10464 8.10622 .10779 .10936	$160 \\ 160 \\ 159 \\ 159 \\ 159 \\ 158 \\ 158 \\ 158 \\ 157 $	$\begin{array}{r} .09732\\ .09894\\ .10056\\ .10217\\ \overline{8}.1037\overline{8}\\ .10539\\ .10539\\ .10700\\ .10860\\ .11020\\ \overline{8}.11180\end{array}$	$     \begin{array}{r}       162 \\       161 \\       161 \\       161 \\       160 \\       $	1 2 3 4 5 6 7 8 9	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$
5 6 7 8 9 10 11 12 13 14 15	99360 99539 7.99718 7.99897 8.00075 .00253 .00431 8.00608 .00784 .00961 .01137 .01313 8.01488 .01663 .01838 .01838	$179 \\ 179 \\ 179 \\ 178 \\ 178 \\ 178 \\ 177 \\ 178 \\ 177 \\ 176 \\ 176 \\ 176 \\ 176 \\ 176 \\ 176 \\ 175 \\ 175 \\ 175 $	.99790 7.99971 8.00152 .00332 .00512 .00692 .00871 8.01050 .01229 .01407 .01585 .01763	181 180 180 180 179 179 178 178	.09352 .09671 8.09830 .09983 .10148 .10306 .10464 8.10622 .10779 .10936	$     \begin{array}{r}       160 \\       159 \\       159 \\       158 \\       158 \\       158 \\       157 \\       157 \\       157 \\       157 \\     \end{array} $	$\begin{array}{r} .10056\\ .10217\\ \hline 8.10378\\ .10539\\ .10539\\ .10700\\ .10860\\ .11020\\ \hline 8.11180\end{array}$	$162 \\ 161 \\ 161 \\ 161 \\ 160 \\ 100 $	3 4 5 6 7 8 9	$\begin{array}{c c c c c c c c c c c c c c c c c c c $
5 6 7 8 9 10 11 12 13 14 15		$179 \\ 178 \\ 178 \\ 177 \\ 177 \\ 177 \\ 176 \\ 176 \\ 176 \\ 176 \\ 176 \\ 176 \\ 175 $	$\begin{array}{r} 8.00152\\.00332\\.00512\\.00692\\.00871\\8.01050\\.01229\\.01407\\.01585\\.01763\\\end{array}$	180 180 180 179 179 178 178	$\begin{array}{r} 8.09830\\ .09989\\ .10148\\ .10306\\ .10464\\ 8.10622\\ .10779\\ .10936\\ \end{array}$	$     \begin{array}{r} 159 \\       158 \\       158 \\       158 \\       158 \\       157 \\       157 \\       157 \\       157 \\     \end{array} $	$     \begin{array}{r}       8.1037\overline{8} \\       .10539 \\       .10700 \\       .10860 \\       .11020 \\       8.11180 \\       \hline       8.11180 \\     \end{array} $	$161 \\ 161 \\ 160 \\ 100 $	5 6 7 8 9	20 60.0 56.6 53.3 30 90.0 85.0 80.0
6 7 9 10 11 12 13 14 15	00431 8.00608 .00784 .00961 .01137 <u>.01313</u> 8.01488 .01663 .01838	$178 \\ 177 \\ 176 \\ 176 \\ 176 \\ 176 \\ 176 \\ 176 \\ 176 \\ 175 \\ 175 \\ 175 $	$\begin{array}{r} .00871 \\ 8.01050 \\ .01229 \\ .01407 \\ .01585 \\ .01763 \end{array}$	180 180 179 179 178 178	$\begin{array}{r} .0998\bar{9}\\ .10148\\ .1030\underline{6}\\ .10464\\ \overline{8.10622}\\ .1077\underline{9}\\ .10936\end{array}$	$158 \\ 158 \\ 158 \\ 157 $	.10539 .10700 .10860 .11020 8.11180	$16\overline{0} \\ 16\overline{0} \\ 160 \\ 160 \\ 160 \\ 160 \\ 160 \\ 160 \\ 160 \\ 160 \\ 160 \\ 160 \\ 160 \\ 160 \\ 100 $	6 7 8 9	20 60.0 56.6 53.3 30 90.0 85.0 80.0
8 9 10 11 12 13 14 15	00431 8.00608 .00784 .00961 .01137 <u>.01313</u> 8.01488 .01663 .01838	$178 \\ 177 \\ 176 \\ 176 \\ 176 \\ 176 \\ 176 \\ 176 \\ 176 \\ 175 \\ 175 \\ 175 $	$\begin{array}{r} .00871 \\ 8.01050 \\ .01229 \\ .01407 \\ .01585 \\ .01763 \end{array}$	$179 \\ 179 \\ 178 $	$.1030\overline{6}$ .10464 8.10622 .10779 .10936	$158 \\ 157 $	.10860 .11020 8.11180	160 160	9	$\begin{array}{c} 40 120\cdot 0 113\cdot 3 106\cdot 6\\ 50 150\cdot 0 141\cdot 6 133\cdot 3\\ \end{array}$
$     \begin{array}{c}       11 \\       12 \\       13 \\       14 \\       15     \end{array} $	$\begin{array}{r} 8.00608 \\ .00784 \\ .00961 \\ .01137 \\ .01313 \\ \hline 8.01488 \\ .01663 \\ .01838 \\ .01838 \end{array}$	17 <u>6</u> 176 176 176 175 175	$\begin{array}{r} 8.0105\bar{0} \\ .01229 \\ .01407 \\ .01585 \\ .01763 \end{array}$	178	.10779 .10936	$157 \\ 157$	8.11180	160	10	
$12 \\ 13 \\ 14 \\ 15$	$\begin{array}{r} .00961\\ .01137\\ .01313\\ \hline 8.01488\\ .01663\\ .01838\\ .00012\end{array}$	176 176 175 175	01407 01585 01763	$178 \\ 178 \\ 177 $	.10936	1157		1108	10 11	150 140
$\frac{14}{15}$	$     \underbrace{\begin{array}{r} \cdot 01313 \\ 8 \cdot 01488 \\ \cdot 01663 \\ \cdot 01838 \\ 00012 \end{array}} $	175 175	.01763	1177		157	.11499	159	$\hat{12}$ 13	$\begin{array}{c ccccc} 6 & 15 \cdot 0 & 14 \cdot 0 \\ 7 & 17 \cdot 5 & 16 \cdot 3 \\ 8 & 20 \cdot 0 & 18 \cdot 6 \end{array}$
10	·01663 ·01838			177	.11250	156 156	•1181ē	150	14	9 22.5 21.0
$\frac{16}{17}$	00010		.02117 .0229 <u>3</u>	11 00	$     \begin{array}{r}       8 \cdot 11406 \\       \cdot 11562 \\       \cdot 11718 \\       \cdot 11718     \end{array} $	$156 \\ 155$			15 16	20 50.0 46.6
18	.02186	$174 \\ 174$	•02469	176 175	.11873	155	.12133 .12291 .12448 .12605	157 157	17	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
$\frac{19}{20}$	8.02359	$17\overline{3} \\ 17\overline{3}$	$\frac{.02645}{8.02820}$	1.72	8.12184	155	8 · 12762	157 157	$\frac{19}{20}$	$50 125.0 116.\overline{6}$
22	.02706	$173 \\ 172$	.0299 <u>5</u> .03170	175	$.1233\overline{8}$ $.1249\overline{2}$	154	.1307	156	44	$\begin{array}{cccccccccccccccccccccccccccccccccccc$
$23 \\ 24$	02078	172	·03345 ·03519	174	12647	153	1338	155		8 1 · 2 1 · 2 1 · L
25 26	8.03222 .03394	$172 \\ 171 \\ 171 \\ 171$	8.03692 .03866	1110	$8.12954 \\ .13107$	1100	8.1354 .1369	1100		$\begin{array}{c}91.\overline{4}1.\overline{3}1.3\\101.\underline{6}1.51.4\\002\end{array}$
27 28	00796	$171 \\ 171 \\ 170 $	·04039 ·04212	173	·13260	1102	.13854	159	27	$\begin{array}{c} 9 & 1.4 \\ 10 & 1.6 & 1.5 \\ 1.5 & 1.4 \\ 20 & 3.1 & 3.0 \\ 2.8 \\ 30 & 4.7 & 4.5 \\ 40 & 6.3 & 6.0 \\ 50 & 7.9 & 7.5 \\ 7.1 \end{array}$
29 30	03906	170	04384 8.04556	172	.13565	$15\overline{2}$ 152	.1416	154	29	50 7.9 7.5 7.1
31 32	·04246	$\begin{array}{c} 170 \\ 169 \end{array}$	·04728 ·04899	171	.13869	1101	.1447	티는운종	1 21	8 7 7 610-810-710-7
33 34	01505	$169 \\ 169$	·05070 ·05241	はた	1 1 1 70	$151 \\ 151$	1/773	5 1 5 5	33	$\begin{array}{c} 6 & 0 \cdot \overline{7} & 0 \cdot \overline{7} \\ 7 & 0 \cdot \overline{9} & 0 \cdot 9 & 0 \cdot 8 \\ 8 & 1 \cdot \overline{0} & 1 \cdot 0 & 0 \cdot \overline{9} \\ \end{array}$
35	8.04922	$16\bar{8} \\ 168$	8.05411	170	$8.1447\overline{4}$	151	8.1508		35	91.31.91.4
36 37	·05258	$168 \\ 167$	$.0558\overline{1}$ $.0575\overline{1}$	170	.14775	150	.1523	5152	37	202.62.52.5
38 39	05593	167	.05921 .06090	169	.14920	149	.15694	152	39	$\begin{array}{c} 10 & 1 \cdot 3 & 1 \cdot 2 & 1 \cdot 1 \\ 20 & 2 \cdot 6 & 2 \cdot 5 & 2 \cdot 3 \\ 30 & 4 \cdot 0 & 3 \cdot 7 & 3 \cdot 5 \\ 40 & 5 \cdot 3 & 5 \cdot 0 & 4 \cdot 6 \\ 50 & 6 \cdot 6 & 6 \cdot 2 & 5 \cdot 8 \end{array}$
40 41	•000020	$167 \\ 166 $	8.06259 .06427	1100	15374	149	.1599	152 151 151	41	<u>6</u> 6
42 43	·06093 ·06259	$160 \\ 166 \\ 165$	·06595 ·06763	1100	•15523 •15672	149	.1614		42 43	$\begin{array}{c} 6 & 0 \cdot \overline{\underline{6}} & 0 \cdot 6 \\ 7 & 0 \cdot \overline{7} & 0 \cdot 7 \\ 8 & 0 \cdot \overline{8} & 0 \cdot 8 \end{array}$
$\frac{44}{45}$	$\frac{.0642\overline{4}}{8.0658\overline{9}}$	165	·06931 8·07098	167		148	1040	150	44	
46 47	.06754	$165 \\ 165 $	·07265		$.1611\overline{6}$	148			46	101.11.0
48 49		$\begin{array}{c} 164 \\ 164 \end{array}$	07500	100	16/12	117.6	17050	) 149	1 4 8	$ \begin{array}{c} 20   2 \cdot \underline{1}   2 \cdot 0 \\ 30   3 \cdot \underline{2}   3 \cdot 0 \\ 40   4 \cdot \overline{3}   4 \cdot 0 \\ 50   5 \cdot 4   5 \cdot 0 \\ \overline{5}  5 \end{array} $
50	$8.0741\bar{1}$	$164 \\ 163$	8.07929	165	8.16706	147	8.17349	149	50	5015.415.0
51 52	.07738	$163 \\ 162$	.00090	$165 \\ 164$	·16999	14	17640	149	51 52 53	$\overline{5}$ $\overline{5}$ $6 0\cdot\overline{5} 0\cdot\overline{5}$
53 54	·07900 ·08063	$16\bar{2}$	08580		17291	1	17949	148	54	70.60.6
55 56	8.08225 .08387	$16\bar{2} \\ 16\bar{1} \\ 16\bar{1} \\ 162$	.00311		.17582	$145 \\ 145 $	8.18091 .18238		55 56	90.80.7
57 58	.08549 .08710	161	.09081	169	•17728	145	.1858		57 58	2011.811.6
<u>59</u> 60	$\frac{.08871}{8.09031}$	160	$\frac{.09407}{8.09569}$	1160	8.18162	144	18080	140	<u>59</u> 60	$\begin{array}{c} 30 & 2 & \overline{7} & 2 \cdot 5 \\ 40 & 3 \cdot 6 & 3 \cdot \overline{3} \\ 50 & 4 \cdot 6 & 4 \cdot 1 \end{array}$
7	Lg. Vers.	$\overline{D}$	Log.Exs.		Lg. Vers.	$\overline{D}$	Log.Exs.	in the second second	1	P. P.

TABLE VIII.-LOGARITHMIC VERSED SINES AND EXTERNAL SECANTS

TABLE	VIIILO	GARITHMIC V	VERSED	SINES	AND	EXTERNAL SECANTS.
, Y	10°		11°			

-

	10	<b>)</b>	11	Ľ		
'	Lg. Vers. D	Log. Exs. D	Lg. Vers. D	Log. Exs.		P. P.
0 1 2 3 4	$\begin{array}{r} 8.18162\\ \cdot 1830\overline{6}\\ 14\overline{4}\\ \cdot 1845\overline{0}\\ 144\\ \cdot 1859\overline{4}\\ 143\\ \cdot 18738\\ 143\end{array}$	$ \begin{array}{c}       .18973 \\       .19120 \\       .19266 \\       .19411 \\       .19411   \end{array} $	$ \begin{array}{r}     26348 \\     26679 \\     13 \\     26810 \\     26941 \\     13 \end{array} $	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{c c} 13\overline{3} & 0 \\ 13\overline{3} & 1 \\ 133 & 2 \\ 133 & 2 \\ 133 & 3 \\ 133 & 4 \end{array}$	130 120
56789	$\begin{array}{r} 143\\8\cdot 18881\\143\\\cdot 19024\\142\\\cdot 19167\\142\\\cdot 19309\\142\\\cdot 19452\\142\end{array}$	$\begin{array}{r} 8.19557\\ 145\\ .19702\\ 19702\\ 145\\ .19847\\ 145\\ .19992\\ 145\\ .20137\\ 144\end{array}$	$\begin{array}{r} 8 \cdot 27071 \\ \cdot 27201 \\ \cdot 27331 \\ \cdot 27461 \\ \cdot 27590 \\ 12 \end{array}$	$\begin{array}{c} 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 $	$\begin{array}{c ccccc} 133 \\ 132 \\ 132 \\ 6 \\ 132 \\ 7 \\ 132 \\ 132 \\ 9 \end{array}$	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$
$10 \\ 11 \\ 12 \\ 13 \\ 14$	$\begin{array}{r} 8.19594 \\ 142 \\ .19736 \\ 142 \\ .19878 \\ 142 \\ .20019 \\ 141 \\ .20160 \\ 141 \\ \end{array}$	$\begin{array}{r} 8.20281\\ \cdot 2042\overline{5} \\ 144\\ \cdot 2056\overline{9} \\ 144\\ \cdot 2071\overline{3} \\ 14\overline{3}\\ \cdot 20857 \\ 142\end{array}$	$\begin{array}{r} 8.27719 \\ .27849 \\ .27977 \\ 12 \\ .28106 \\ 12 \\ .28235 \\ 12 \end{array}$		$ \begin{array}{c} 132\\13\overline{1}\\13\overline{1}\\131\\131\\131\\131\\131\\131\\14\\131\\15\end{array} $	$\begin{array}{cccccccccccccccccccccccccccccccccccc$
15 16 17 18 19	$     \begin{array}{r}             20301 \\             20442 \\             20582 \\             140 \\             20723 \\             140 \\             20863 \\             140         \end{array}     $	21143 143 21143 143 21286 142 21428 142 21571 142	$ \begin{array}{r}       28305 12 \\       28491 12 \\       28619 12 \\       28747 12 \\       28875 12   \end{array} $	$     \begin{array}{c}       3 \\             29336 \\             \cdot 29467 \\             \cdot 29597 \\             \cdot 29727         \end{array}     $	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{array}{c} 6 & 0 \cdot \overline{4} & 0 \cdot 4 & 0 \cdot \overline{3} \\ 7 & 0 \cdot 5 & 0 \cdot 4 & 0 \cdot 4 \\ 8 & 0 \cdot 6 & 0 \cdot 5 & 0 \cdot 4 \\ 9 & 0 \cdot 7 & 0 \cdot 6 & 0 \cdot 5 \\ 10 & 0 \cdot 7 & 0 \cdot 6 & 0 \cdot 6 \end{array}$
20 21 22 23 24	$\begin{array}{r} 8.21003\\ \cdot 2114\overline{2} \\ 13\overline{9}\\ \cdot 21282 \\ 139\\ \cdot 21421 \\ 139\\ \cdot 21560 \\ 12\overline{6} \\ 13\overline{9} $	$\begin{array}{r} 0 \cdot 21713 \\ \cdot 21855 \\ 141 \\ \cdot 21996 \\ 141 \\ \cdot 22138 \\ 141 \\ \cdot 22279 \\ 141 \end{array}$	$\begin{array}{r} 29129 \\ 29129 \\ 129256 \\ 29383 \\ 12 \\ 29510 \\ 12 \\ 12 \\ 12 \\ 12 \\ 12 \\ 12 \\ 12 \\ $	$     \begin{array}{r}         29987 \\             \cdot 29987 \\             \cdot 30117 \\             \cdot 30246 \\             \cdot 30375 \\             \cdot 30375 \\         \end{array} $	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{array}{c} 20 & 1 \cdot \underline{5} & 1 \cdot \overline{3} & 1 \cdot \overline{1} \\ 30 & 2 \cdot \underline{2} & 2 \cdot \underline{0} & 1 \cdot \overline{7} \\ 40 & 3 \cdot \underline{0} & 2 \cdot \underline{6} & 2 \cdot \overline{3} \\ 50 & 3 \cdot \overline{7} & 3 \cdot \overline{3} & 2 \cdot 9 \end{array}$
25 26 27 28 29	$\begin{array}{r} 13\overline{8} \\ \cdot 21837 \\ \cdot 21975 \\ \cdot 21975 \\ \cdot 22113 \\ \cdot 22251 \\ \cdot 22251 \\ 137 \\ \cdot 22251 \\ 130 \\ \cdot 22251 \\ \cdot 2251 \\ \cdot 2$	$\begin{array}{c} 140 \\ \cdot 22561 \\ \cdot 22701 \\ \cdot 22701 \\ \cdot 22842 \\ \cdot 22982 \\ 140 \\ \cdot 22982 \\ 140 \\ \cdot 22982 \\ 140 \\ \cdot 22982 \\ \cdot 22982 \\ \cdot 200 \\ \cdot 200$	$\begin{array}{r} 29763 \\ 29763 \\ 12 \\ 29889 \\ 12 \\ 30015 \\ 12 \\ 30140 \\ 10 \\ 10 \\ 10 \\ 10 \\ 10 \\ 10 \\ 10 $	30633 30633 30762 30890 31019	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$
30 31 32 33 34	$22526 \\ 137 \\ 22663 \\ 137 \\ 22800 \\ 136 \\ 22800 \\ 137 \\ 12937 \\ 127 \\ 137 \\ 12937 \\ 137 \\ 127 $	$ \begin{array}{r}             23262 \\             \cdot 23262 \\             139 \\             \cdot 23401 \\             139 \\             \cdot 23540 \\             139 \\             \cdot 23679 \\             139         \end{array} $	$     \begin{array}{r}       30391 \\       30391 \\       30516 \\       125 \\       30642 \\       30766 \\       124     \end{array} $	·31275 ·31402 ·31530 ·31657	$\begin{array}{c} 128 & 30 \\ 127 & 31 \\ 127 & 32 \\ 127 & 33 \\ 127 & 34 \\ 197 & 34 \end{array}$	$ \begin{array}{c} 10 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ $
35 36 37 38 39	$ \begin{array}{r}       23209 \\       23346 \\       23481 \\       23617 \\       136     \end{array} $	$ \begin{array}{r}         23957 \\             23957 \\             24095 \\             24234 \\             24234 \\             138 \\             24372 \\             138 \\             24372 \\             138 \\             24372 \\             137         $	8-30891 31015 3124 31264 31388 291511 124 124 124 124 124 124 124 124 124 1	32039 32165 32292	$\begin{array}{c} 127 & 35 \\ 127 & 36 \\ 126 & 37 \\ 126 & 38 \\ 126 & 39 \\ 126 & 40 \end{array}$	$\begin{array}{c} 2  \mathbf{\overline{1}} \\ 6 0\cdot \underline{2} 0\cdot \mathbf{\overline{1}} \\ 7 0\cdot \underline{2} 0\cdot 2 \end{array}$
40 41 42 43 44	$8 \cdot 23752 \\ 135 \\ \cdot 23888 \\ 135 \\ \cdot 24023 \\ 135 \\ \cdot 24158 \\ 135 \\ \cdot 24292 \\ 134 \\ \cdot 24292 \\ \cdot 2429 \\ \cdot 2429$	$ \begin{array}{r}         24509 \\             24647 \\             137 \\             24922 \\             137 \\             25059 \\             137 \\             125059 \\             137 \\             125059 \\             137 \\             125059 \\             137 \\             125059 \\             137 \\             125059 \\             137 \\             125059 \\            1$		· 32544 · 32544 · 32670 · 32796 · 32922	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	$ \begin{array}{c} 6 \left[ \begin{matrix} 0 \\ \end{array} \\ 2 \\ 7 \\ 0 \\ 2 \\ 0 \\ 2 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0$
45 46 47 48 49	$ \begin{array}{r}       3.24420 \\       24561 \\       134 \\       24695 \\       133 \\       24828 \\       133 \\       24962 \\       133 \\       136   \end{array} $	$ \begin{array}{r}         25135113\overline{6} \\         2533213\overline{6} \\         2546\overline{8} 13\overline{6} \\         2560413\overline{6} \\         2574\overline{6} 136     \end{array} $			$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	
50 51 52 53 54	$\begin{array}{r} 8 \cdot 2509\overline{5} \\ \cdot 2522\overline{8} \\ \cdot 2522\overline{8} \\ \cdot 2536\overline{1} \\ \cdot 2536\overline{1} \\ \cdot 25494 \\ \cdot 25494 \\ \cdot 25627 \\ \cdot 25627 \\ \cdot 132 \\ \cdot 132 \\ \cdot 25627 \\ \cdot 132 \\ \cdot $	$\begin{array}{c} 136\\ 8 \cdot 25876\\ \cdot 26012\\ \cdot 26012\\ 135\\ \cdot 26147\\ 135\\ \cdot 26282\\ 135\\ \cdot 26417\\ 135\\ \cdot 26417\\ 135\\ \cdot 26417\\ 135\\ \cdot 26417\\ 134\\ \end{array}$	$ \begin{array}{c}             32861 \\             32983 \\             33104 \\             3225 \\             33225 \\             12         \end{array} $		$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{c} 6 0.1 0.0\\ 7 0.1 0.0\\ 8 0.1 0.0\\ 9 0.1 0.1\\ 10 0.1\\ 20 0.3 0.1\\ 30 0.5 0.2\\ 40 0.6 0.3\\ 50 0.6\\ 6 0.4\\ \end{array}$
55 56 57 58 59	$\begin{array}{r} 8.25759 \\ .25891 \\ .26023 \\ .26155 \\ .26286 \\ .26286 \\ 131 \\ .26286 \\ 131 \\ .26286 \\ 131 \end{array}$	$\begin{array}{r} 8.26352\\ \cdot 2668\overline{6}\\ \cdot 26821\\ \cdot 26921\\ \cdot 26955\\ \cdot 27089\\ \cdot 27089$	8 · 33347 12 · 33468 120 · 33588 120 · 33709 120 · 33829 120 · 33829 120	$ \begin{array}{r}             34417 \\                                    $	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	30 0.5002 40 0.60.3 50 0.8 0.4
<u>60</u> /	$\frac{3 \cdot 2641\overline{7}}{\text{Lg. Vers.}} \frac{131}{D}$	$\frac{8 \cdot 27223}{\text{Log, Exs,}} \frac{134}{D}$	$\frac{8 \cdot 33950}{\text{Lg. Vers.}} \frac{12}{D}$	0.04000	$\frac{123}{D} \frac{60}{\prime}$	P. P.

1	ABLE	VIII	-LOGARITHMIC	VERSED	SINES AND	EXTERNAL	SECANTS.

1A	TABLE VIII.—LOGARITHMIC VERSED SINES AND EXTERNAL SECANTS.         12°       13°										
,	Lg. Vers.	D	Log. Exs.	D	Lg. Vers.	D	Log. Exs.	D	'	P. P.	
U 1 2 3 4	$\begin{array}{r} 8.33950 \\ .34070 \\ .34190 \\ .3430\overline{9} \\ .34429 \end{array}$	120 120 119 120 120 119	8 · 34909 · 35032 · 35155 · 35277 · 35399	$     \begin{array}{r}       123 \\       122 \\       122 \\       122 \\       122 \\       122 \\       122 \\       122 \\       \end{array} $	$\begin{array}{r} 8.40875 \\ .40985 \\ .41096 \\ .41206 \\ .41317 \end{array}$	$11\overline{0}$ $11\overline{0}$ $11\overline{0}$ $11\overline{0}$ $11\overline{0}$ $11\overline{0}$	$\begin{array}{r} 8.4200\overline{2} \\ .42116 \\ .42229 \\ .42343 \\ .42456 \end{array}$	$     \begin{array}{r} 11\overline{3} \\     113   \end{array} $	0 1 2 3 4	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	
5 6 7 8 9	$     \begin{array}{r}       8.34549 \\       \cdot 34668 \\       \cdot 34787 \\       \cdot 34906 \\       \underline{\cdot 35025}     \end{array} $	119 119 119 119 119 118	·35887	$122 \\ 121 \\ 122 \\ 122 \\ 121 $		110 110 109 110 109	$\begin{array}{r} 8.4256\overline{9} \\ .42682 \\ .42795 \\ .42908 \\ .43021 \end{array}$	$113 \\ 113 \\ 113 \\ 113 \\ 112 \\ 112 \\ 112$	5 6 7 8 9	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	
$10 \\ 11 \\ 12 \\ 13 \\ 14$	$ \begin{array}{r} 8.3514\overline{3} \\ .35262 \\ .35380 \\ .3549\overline{8} \\ .35616 \\ \end{array} $	$11\overline{8}$ 118 118 118 118 117	·36251 ·36372 ·36493 ·36614	$121 \\ 121 \\ 120 \\ 121 \\ 121 \\ 120 \\ 121 \\ 100 $	.42413	109 109 109 109 109	$     \begin{array}{r}       8 \cdot 4313\overline{3} \\       \cdot 43246 \\       \cdot 43358 \\       \cdot 43470 \\       \cdot 43582 \\       \hline     \end{array} $	$11\overline{2}$ 112 112 112 112 112	$     \begin{array}{r}       10 \\       11 \\       12 \\       13 \\       14     \end{array}   $	$\begin{array}{c} 117 \ 116 \ 115 \\ 6 \ 11 \cdot 7 \ 11 \cdot 6 \ 11 \cdot 5 \\ 7 \ 13 \cdot 6 \ 13 \cdot 5 \ 13 \cdot 4 \\ 8 \ 15 \cdot 6 \ 15 \cdot 4 \ 15 \cdot 3 \\ 9 \ 17 \cdot 5 \ 17 \cdot 4 \ 17 \cdot 2 \\ 9 \ 17 \cdot 5 \ 17 \cdot 4 \ 17 \cdot 2 \end{array}$	
15 16 17 18 19	·36086 ·36204	118 117 117 117 117	*36734 •36855 •36975 •37095 •37215	120 120 120 120	·42630 ·42739 ·42847 ·42956	108 109 108 108 108	$     \begin{array}{r}             8 \cdot 43694 \\             \cdot 43805 \\             \cdot 43917 \\             \cdot 44028 \\             \cdot 44139 \\             \hline         \end{array}     $	$   \begin{array}{c}     111 \\     111 \\     111 \\     111 \\     111 \\     111 \\     111 \\   \end{array} $	15 16 17 18 19	10 19.5 19.3 19.1 20 39.0 38.6 38.3 30 58.5 58.0 57.5 40 78.0 77.3 76.6 50 97.5 96.6 95.8	
20 21 22 23 24	·36554 ·36671 ·36787	$   \begin{array}{r}     11\overline{6} \\     117 \\     116 \\     116 \\     116 \\     11\overline{6} \\     11\overline{6}   \end{array} $	·37454 ·37574 ·37693 ·37812	$11\overline{9} \\ 11\overline{9} \\ 119 \\ 119 \\ 119 \\ 119 \\ 119 \\ 110 $		108 108 108 107 107	8.44251 .44362 .44473 .44583 .44694	$     \begin{array}{c}       111 \\       111 \\       110 \\       110 \\       110 \\       110 \\       11\overline{0}   \end{array} $	20 21 22 23 24	$\begin{array}{c} 114 \ 113 \ \ 112 \\ 6   11 \cdot 4   11 \cdot 3   11 \cdot 2 \\ 7   13 \cdot 3   13 \cdot 2   13 \cdot 0 \\ 8   15 \cdot 2   15 \cdot 0   14 \cdot 9 \\ 9   17 \cdot 1   16 \cdot 0   16 \cdot 8 \end{array}$	
25 26 27 28 29	·37135 ·37251 37866	$     \begin{array}{r}       116 \\       116 \\       115 \\       115 \\       115 \\       115 \\     \end{array} $	8.37931 ·38050 ·38169 ·38287 ·38406	$11\overline{8}$ 119 $11\overline{8}$ $11\overline{8}$ 118	.43817 .43924 .44031	107 107 107 107 107	$\begin{array}{r} 8.4480\overline{4} \\ .44915 \\ .45025 \\ .45135 \\ .45245 \end{array}$	$   \begin{array}{r}     110 \\     110 \\     110 \\     109 \\     110 \\     110   \end{array} $	27 28 29	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	
30 31 32 33 34	·37712	$115 \\ 115 \\ 115 \\ 115 \\ 115 \\ 115 \\ 115 \\ 115 \\ 114$	8.38524 ·38642 ·38760 ·38878 ·38995	$     \begin{array}{r}       118 \\       118 \\       118 \\       117 \\       117 \\       117 \\     \end{array} $	$     \begin{array}{r}             8 \cdot 44138 \\             \cdot 44245 \\             \cdot 44351 \\             \cdot 44458 \\             \underline{\cdot 44564} \\             8 \cdot 44670 \\         \end{array} $	107 106 106 106 106	8 · 45355 · 45465 · 45574 · 45684 · 45793 3 · 45902	110 109 109 109 109	30 31 32 33 34 35	$\begin{array}{c} 111 \ 110 \ 109 \\ 6 & 11 \cdot 1 & 11 \cdot 0 \\ 7 & 12 \cdot 9 & 12 \cdot 8 \\ 8 & 14 \cdot 8 & 14 \cdot 6 & 14 \cdot 5 \\ 9 & 16 \cdot 6 & 16 \cdot 5 & 16 \cdot 3 \end{array}$	
35 36 37 38 39 40	$3817\overline{1}$ 38286 38400 38514	$11\frac{4}{114}$ 114 114 114 114	· 39230 · 39347 · 39464 · 39581	$117 \\ 117 \\ 117 \\ 117 \\ 117 \\ 117 \\ 116 $	.44776 .44882 .44988 .45093	$106 \\ 105 \\ 106 \\ 105 $	4601 <u>1</u> 46120 46229 46338 3.46446	109 109 108 109 109	36 37 38 39	$\begin{array}{c} 9 & 16 \cdot \overline{6} & 16 \cdot 5 & 16 \cdot \overline{3} \\ 10 & 18 \cdot 5 & 18 \cdot \overline{3} & 18 \cdot \overline{1} \\ 20 & 37 \cdot 0 & 36 \cdot \overline{6} & 36 \cdot \overline{3} \\ 30 & 55 \cdot 5 & 55 \cdot 0 & 54 \cdot 5 \\ 40 & 74 \cdot 0 & 73 \cdot \overline{3} & 72 \cdot \overline{6} \\ 50 & 92 \cdot 5 & 91 \cdot 6 & 90 \cdot 8 \end{array}$	
41 42 43 44 45	·38741 ·38855 ·38969 ·39082	$11\overline{3}$ 114 113 113 113 113	·39814 ·39931 ·40047 ·40163	$116 \\ 116 $	$     \cdot 4530\overline{4} \\     \cdot 4540\overline{9} $	$10\overline{5}$ 105 105 105 105 105	$\begin{array}{r} \cdot 46555 \\ \cdot 46663 \\ \cdot 46771 \\ \cdot 46879 \\ \hline 8 \cdot 46987 \end{array}$	108 108 108 108 108	41 42 43 44 45	$\begin{array}{c} 108 \ 107 \ 106 \\ 6 10.8 10.7 10.6 \\ 7 12.6 12.5 12.3 \\ 8 14.4 14.2 14.1 \\ 9 16.2 16.0 15.9 \\ 10 18.0 17.8 17.6 \\ 0 05 \ $	
	·39308 ·39421 ·39534 39645	$     \begin{array}{r}       113 \\       113 \\       112 \\      1$	·4051 ·40626 ·40742	115 115 115 115 115 115	·45829 ·45934	$10\overline{4}$ 105 104 104 104 104	·47095 ·47202 ·47310 ·47417 8·47525	$10\overline{7} \\ 108 \\ 107 \\ 1$	$     \begin{array}{r}       46 \\       47 \\       48 \\       49 \\       50     \end{array} $	10 18.0 17.8 17.6 20 36.0 35.6 35.3 30 54.0 53.5 53.0 40 72.0 71.3 70.6 50 90.0 89.1 88.3	
51 52 53 54 55	· 39871 · 39983 · 40095 · 40207	112 112 112		$115 \\ 115 \\ 115 \\ 115 \\ 114 $	$     \begin{array}{r}                                     $	$104 \\ 104 \\ 103 \\ 104 \\ 103 \\ 104 \\ 103 \\ 103 \\ 103 \\ 103 \\ 103 \\ 103 \\ 103 \\ 103 \\ 103 \\ 103 \\ 103 \\ 103 \\ 104 \\ 103 \\ 104 $	$     \begin{array}{r}                                     $	$107 \\ 107 \\ 107 \\ 106 \\ 107 $	51 52 53 54 55	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	
56 57 58 59 <b>60</b>	·40541 ·40652 ·40764	$11\overline{1}$ $11\overline{1}$ $11\overline{1}$ $11\overline{1}$ $11\overline{1}$ $11\overline{1}$		$11\overline{4} \\ 11\overline{4} \\ 114 $	-46869 -46972 -47076 -47179	103 103 103 103 103 103	·48166 ·48273 ·48379 ·48485 8 · 48591	$10\overline{6} \\ 10\overline{6} \\ 1$	56 57 58 59 60	$\begin{array}{c} 9 & 115 \cdot \overline{7} & 15 \cdot 6 \\ 1 & 0 & 15 \cdot 7 & 15 \cdot 6 \\ 1 & 0 & 17 \cdot 5 & 17 \cdot 3 & 0 \cdot 1 \\ 2 & 0 & 35 \cdot 0 & 34 \cdot 6 & 0 \cdot 1 \\ 3 & 0 & 52 \cdot 5 & 52 \cdot 0 & 0 \cdot 2 \\ 4 & 0 & 70 \cdot 0 & 69 \cdot 3 & 0 \cdot 3 \\ 5 & 0 & 87 \cdot 5 & 86 \cdot 6 & 0 \cdot 4 \end{array}$	
<del>90</del>	Lg. Vers.	D	Log. Exs.		Lg. Vers.	D	Log. Exs.	$\overline{D}$	-	P. P.	

14°						15°			
,		Log.Exs.	D	Lg. Vers.	D	Log.Exs.	D	'	P. P.
01234	$\begin{array}{r} 8.47282 \\ .47384 \\ 103 \\ .47487 \\ 103 \\ .47590 \\ .47692 \\ 103 \\ .47692 \\ 103 \\ .47692 \\ 103 \\ .47692 \\ 103 \\ .47692 \\ 103 \\ .47692 $	·48897 ·48803 ·48909 ·49014	106 10 <u>6</u> 10 <u>5</u> 10 <u>5</u> 10 <u>5</u>	8.53242 .53338 .53434 .53530 .53625	965 955 95 95 95 95		99 99 99 99 99	01234	<b>103 102 101</b> 6/10.3/10.2/10.1 7/12.0/11.9/11.8
5 6 7 8 9 10	.47897 102 .47897 102 .47999 102 .48101 102 .48203 103	·49225 ·49331 ·49436 ·49541	105 105 105 105 105	8.53721 .53816 .53911 .54007 .54102 8.54197	95 95 95 95 95	• 55342 • 55342 • 555441 • 55539 • 55638 8 • 55736	99 98 98 88 88 88 88 88 88 88 88 88 88 8	5 6 7 8 9 10	8 13.7 13.6 13.2 9 15.4 15.3 15.1 10 17.1 17.0 16.8 20 34.3 34.0 33.6 30 51.5 51.0 50.5 40 68.6 68.0 67.3 50 85.8 85.0 84.1
$11 \\ 12 \\ 13 \\ 14 \\ 15 \\ 15 \\ 10 \\ 11 \\ 10 \\ 10 \\ 10 \\ 10$		•49750 •49855 •49960 •50064	$10\overline{4} \\ 10\overline{5} \\ 10\overline{4} \\ 1$	.54291 .54386 .54481 .54575 8.54670	94 95 94 94 94 94 94	.55834 .55933 .56031 .56129 8.56226	98 98 98 98 98 97	$     \begin{array}{c}       11 \\       12 \\       13 \\       14 \\       15     \end{array} $	$\begin{array}{c} 40085 \cdot 0085 \cdot 0081 \cdot 3 \\ 50085 \cdot 8085 \cdot 0084 \cdot 1 \\ 100  99  98 \\ 610 \cdot 00  9 \cdot 90  9 \cdot 8 \end{array}$
16 17 18 19	$\begin{array}{r} 0 \cdot 40011 \\ \cdot 48912 \\ 101 \\ \cdot 49013 \\ 100 \\ \cdot 49114 \\ 101 \\ \cdot 49215 \\ 8 \cdot 49315 \\ 100 \\ \end{array}$	• 50273 • 50377 • 50481 • 50585	104 104 104 104 103	•54764 •54858 •54952 •55046 8•55140	94 94 94 94 94	·56324 ·56422 ·56519 ·56617 8·56714	98 97 97 97 97	16     17     18     19     20	$\begin{array}{c} 5 & 5 & 5 & 5 & 5 \\ 7 & 11 & 6 & 11 & 5 & 11 & 4 \\ 8 & 13 & 3 & 13 & 2 & 13 & 0 \\ 9 & 15 & 0 & 14 & 8 & 14 & 7 \\ 10 & 16 & 6 & 16 & 5 & 16 & 3 \\ 20 & 33 & 3 & 33 & 0 & 32 & 6 \end{array}$
20 21 22 23 24 25	$\begin{array}{r} 0.49315 \\ .49415 \\ 100 \\ .49516 \\ 100 \\ .49616 \\ 100 \\ .49716 \\ 100 \\ 8.49816 \\ 100 \end{array}$	·50792 ·50896 ·50999 ·51102	104 103 103 103 103	• 55234 • 55328 • 55421 • 55515 8 • 55608	93 94 93 93 93 93	·56812 ·56909 ·57006 ·57103 8·57200	97 97 97 97 97	21 22 23 24 25	$\begin{array}{c} 30 50 \cdot \underline{0} 49 \cdot 5 49 \cdot \underline{0} \\ 40 66 \cdot \underline{6} 66 \cdot 0 65 \cdot \underline{3} \\ 50 83 \cdot \underline{3} 82 \cdot 5 82 \cdot \underline{6} \end{array}$
26 27 28 29 30	$\begin{array}{c} \cdot 49916 \\ \cdot 49916 \\ \cdot 50015 \\ \cdot 50115 \\ \cdot 50215 \\ \hline 8 \cdot 50314 \\ 9 \\ \hline 8 \cdot 50314 \\ 9 \\ \hline \end{array}$	.51309 .51412 .51514 .51514 .51617	$     \begin{array}{r}       103 \\       102 \\       102 \\       103 \\       102 \\       102 \\       \end{array} $	·55701 ·55795 ·55888 ·55981 8·56074	9 <u>3</u> 93 93 93 93	·57296 ·57393 ·57490 ·57586 8·57682	96 97 96 96 96	26 27 28 29 30	$\begin{array}{c} 97 & 96 & 95 \\ 6 & 9.7 & 9.6 & 9.5 \\ 7 & 11.3 & 11.2 & 11.1 \\ 8 & 12.9 & 12.8 & 12.6 \\ 9 & 14.5 & 14.4 & 14.2 \\ 10 & 16.1 & 16.0 & 15.8 \\ 20 & 32.3 & 32.0 & 31.6 \\ 20 & 32.3 & 32.0 & 31.6 \\ \end{array}$
31 32 33 34	• 50413 95 • 50512 95 • 50611 95 • 50710 95 • 50809 95	•51925 •52027 •52129	102 102 102 102 102	• 56166 • 56259 • 56352 • 56444 8 • 56536	922 932 92 92 92 92 92	·57779 ·57875 ·57971 ·57971 ·58067 8·58163	96 96 96 96 96 96	31 32 33 34 35	$\begin{array}{c} 1010 \cdot 110 \cdot 0 & 110 \cdot 0 \\ 20 & 32 \cdot 3 & 32 \cdot 0 & 31 \cdot 6 \\ 30 & 48 \cdot 5 & 48 \cdot 0 & 47 \cdot 5 \\ 40 & 64 \cdot 6 & 64 \cdot 0 & 63 \cdot 3 \\ 50 & 80 \cdot 8 & 80 \cdot 0 & 79 \cdot 1 \end{array}$
35 36 37 38 <u>39</u> 40	·50908 93 ·51006 93 ·51105 93 ·51203 93	•52333 •52435 •52537 •52638 •52638	$     \begin{array}{r}       102 \\       101 \\       $	• 56629 • 56721 • 56813 • 56905 8 • 56997	92 92 92 92	.58259 .58354 .58450 .58546 8.58641	96 95 95 95 95	36 37 38 39 40	$\begin{array}{cccccccccccccccccccccccccccccccccccc$
41 42 43 44 45	$ \begin{array}{r} \cdot 5139\overline{9} \\ \cdot 5149\overline{7} \\ \cdot 5159\overline{5} \\ \cdot 51693 \\ 9 \\ \cdot 51791 \\ 9 \\ \cdot 51693 \\ 9 \\ \cdot 51791 \\ 9 \\ \cdot 51693 \\ 9 \\ \cdot 51791 \\ 0 \\ \cdot 51791 \\ \cdot 517$	·52841 ·52943 ·53044 ·53145	101 101 101 101	•57089 •57180 •57272 •57363 8•57455	92 91 91 91 91	•58736 •58832 •58927 •59022 8•59117	9 <u>5</u> 95 95 95 95	$     \begin{array}{r}       41 \\       42 \\       43 \\       \underline{44} \\       45     \end{array} $	$\begin{array}{c}9 14.1 13.9 13.8\\10 15.6\\15.5 15.5 15.3\\20 31.3 31.0 30.6\\30 47.0 46.5 46.0\end{array}$
46 47 48 49 50			$     \begin{array}{r}       101 \\       101 \\       100 \\       100 \\       100 \\       100 \\       \hline     \end{array} $	•57546 •57637 •57728 •57819 8 • 57910	91 91 91 91 91	.59211 .59306 .59401 .59495 8.59590	94 95 94 94 94 94	$     \begin{array}{r}       46 \\       47 \\       48 \\       49 \\       50     \end{array} $	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
51 52 53 54 55	$ \begin{array}{c} \cdot 5237\overline{4} \\ \cdot 5247\overline{1} \\ \cdot 52568 \\ \cdot 52665 \\ 9 \\ \cdot 52665 \\ 9 \\ \cdot 5276\overline{1} \\ 9 \\ \end{array} $		$100 \\ 100 $	• 58001 • 58092 • 58182 • 58273 8 • 58363	90 91 90 90 90	•59684 •59779 •59873 •59967 8•60061	94 94 94 94	51 52 53 54 55	$\begin{array}{c} 10.6 \\ 10.5 \\ 0.0$
56 57 58 59 60		$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	100 99 100 99 99	•58453 •58544 •58634 •58724 8•58814	90 90 90 90 90	.60155 .60249 .60342 .60436 8.60530	94 9 <u>4</u> 93 94 93	56 57 58 59 60	30 45.5 45.0 0.2 40 60.6 60.0 0.3 50 75.8 75.0 0.4
	Lg. Vers. D		D	Lg. Vers.	D	Log.Exs.	D	1	P. P.

# TABLE VIII.—LOGARITHMIC VERSED SINES AND EXTERNAL SECANTS.

# **PABLE VIII.—LOGARITHMIC VERSED** SINES AND EXTERNAL SECANTS. 16° 17°

-	10					1.7				
<u> </u>	Lg. Vers.	D	Log.Exs.	D	Lg. Vers.	D	Log.Exs.	D	<u>·</u>	P. P.
01234	8.58814 .58904 .58993 .59083 .59173	90 89 90 89 89 89	8.60530 .60623 .60716 .60810 .60903	93 93 93 93 93 93	$8.6404\overline{3} \\ .64128 \\ .64212 \\ .64296 \\ .64381 \\ .6441 \\ .6441 \\ .6441 \\ .6441 \\ .6441 \\ .6441 \\ .6441 \\ .6441 \\ .6441$	84 84 84 84 84 84 84	8.65984 .66072 .66160 .66248 .66336	88 88 88 88 88 88	01234	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
56789	8.59262 .59351 .59441 .59530 .59619 8.59708	8 <u>9</u> 89 89 89 89	$     \begin{array}{r}       8 \cdot 6099\overline{6} \\       \cdot 6108\overline{9} \\       \cdot 61182 \\       \cdot 61275 \\       \cdot 61368 \\       \hline       8 \cdot 6146\overline{6}   \end{array} $	93 9 <u>3</u> 92 93 93 93	8.64465 .64549 .64633 .64717 .64801 8.64901	84 84 84 84 83	$     \begin{array}{r}       8.66425 \\       .66512 \\       .66600 \\       .66688 \\       .66776 \\       8.66863 \\     \end{array} $	87 88 88 87 87 87	5 67 9	1015.515.315.12031.030.630.53046.546.045.54062.061.360.65077.576.675.8
$10 \\ 11 \\ 12 \\ 13 \\ 14 \\ 15 $		89 8 <u>9</u> 88 89 88 89 88	8.61460 .61553 .61645 .61738 .61830 8.61922	922 922 92 92 92	8.64884 .64968 .65052 .65135 .65218 8.65302	83 84 83 83 83 83	·66951 ·67039 ·67126 ·67213 8·67301	88 87 87 87 87	$     \begin{array}{r}       10 \\       11 \\       12 \\       13 \\       14 \\       15     \end{array} $	$\begin{array}{c} 90 & 89 & 88 \\ 6 & 9 \cdot 0 & 8 \cdot 9 & 8 \cdot 8 \\ 7 & 10 \cdot 5 & 10 \cdot 4 & 10 \cdot 2 \\ 8 & 12 \cdot 0 & 11 \cdot 8 & 11 \cdot 7 \\ 9 & 13 \cdot 5 & 13 \cdot 3 & 13 \cdot 2 \\ 10 & 15 \cdot 0 & 14 \cdot 8 & 14 \cdot 6 \end{array}$
$     \begin{array}{r}       16 \\       17 \\       18 \\       \underline{19} \\       20     \end{array} $	·60240 ·60328 ·60417 ·60505 8·60593	88 88 88 88 88 88	•62014 •62106 •62198 •62290 8•62382	92 92 92 92 92 91 92	•65385 •65468 •65551 •65634 8•65717	8 <u>3</u> 83 83 83 83	•67388 •67475 •67562 <u>•67649</u> 8•67736	87 87 87 87 87 87 86	$     \begin{array}{r}       16 \\       17 \\       18 \\       19 \\       20     \end{array} $	$\begin{array}{c} 20   30 \cdot 0   29 \cdot \overline{6}   29 \cdot \overline{3} \\ 30   45 \cdot 0   44 \cdot 5   44 \cdot 0 \\ 40   60 \cdot 0   59 \cdot \overline{3}   58 \cdot \overline{6} \\ 50   75 \cdot 0   74 \cdot \overline{1}   73 \cdot \overline{3} \end{array}$
21 22 23 24 25		88 88 87 87 87 87	•6247 <u>4</u> •62565 •6265 <u>7</u> •62748 8•62840	91 91 91 91 91 91	•65800 •65883 •65965 <u>•6604</u> 8 8•66131	83 82 82 83 83 82 82 82 82	•67822 •67909 •67996 •68082 8•68169	87 86 86 86 86 86	21 22 23 24 25	$\begin{array}{c} 87 & 86 & 85 \\ 6 & 8.7   & 8.6   & 8.5 \\ 7 & 10.1 & 10.0   & 9.9 \\ 8 & 11.6 & 11.4 & 11.3 \\ 9 & 13.0 & 12.9 & 12.7 \\ 10 & 14.5 & 14.3 & 14.1 \end{array}$
26 27 28 29 30	$\begin{array}{r} \cdot 61119 \\ \cdot 61207 \\ \cdot 61294 \\ \underline{\cdot 61381} \\ 8 \cdot 61469 \end{array}$	87 87 87 87 87 87 87		91 91 91 90 90	$     \begin{array}{r}                                     $	82 82 82 82 82 82 82 82	•68255 •68341 •68428 •68514 8•68600	86 86 86 86 86	26 27 28 29 30	$\begin{array}{c} 20   29 \cdot 0   28 \cdot 6   28 \cdot 3 \\ 30   43 \cdot 5   43 \cdot 0   42 \cdot 5 \\ 40   58 \cdot 0   57 \cdot 3   56 \cdot 6 \\ 50   72 \cdot 5   71 \cdot 6   70 \cdot 8 \end{array}$
31 32 33 <u>34</u> 35	$ \begin{array}{r} \cdot 61556\\\cdot 61643\\\cdot 61730\\\underline{\cdot 61816}\\8\cdot 61903\end{array} $	87 87 86 87 86		91 90 90 90 90	•66624 •66706 •66788 •66870 8•66951	82 82 82 8 <u>1</u> 8 <u>1</u>	•68686 •68772 •68858 •68944 8•69029	85 86 86 85 85	31 32 33 34 35	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
36 37 38 <u>39</u> 40	•61990 •62076 •62163 •62249 8•62336	866 866 866 866 866 866		90 90 90 90 90	$     \begin{array}{r}                                     $	82 81 81 81 81	•69115 •69201 •69286 •69372 8•69457	855 855 855 855	36 37 38 39 40	$\begin{array}{c} 10 & 10 & 0 & 10 & 0 & 0 \\ 20 & 28 & 0 & 27 & 6 & 27 & 3 \\ 30 & 42 & 0 & 41 & 5 & 41 & 0 \\ 40 & 56 & 0 & 55 & 3 & 54 & 6 \\ 50 & 70 & 0 & 69 & 1 & 68 & 3 \end{array}$
41 42 43 <u>44</u> 45	•62422 •62508 •62594 •62680 8•62766	86 86 86 86 86	64289 64379 64469 64559 $8 \cdot 64649$	90 90 89 90 89 89		81 81 81 81 81 81	•69542 •69627 •69712 •69798 8•69883	85 85 85 85 85 85	$     \begin{array}{r}       41 \\       42 \\       43 \\       44 \\       45 \\       45 \\     \end{array} $	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
$     \begin{array}{r}       46 \\       47 \\       48 \\       \underline{49} \\       50     \end{array} $	•62852 •62937 •63023 •63108 8•63194	8555 855 855 855	•64738 •64828 •64917 •65006 8•65096	89 89 89 89 89 89	•67845 •67926 •68007 •68087 8•68168	80 81 80 80 80 80	•69967 •70052 •70137 •70222 8 • 70306	85 85 84 84 84 84	46 47 48 49 50	$\begin{array}{c} 10 \ 13 \cdot 5 \ 13 \cdot 3 \ 13 \cdot 1 \\ 20 \ 27 \cdot 0 \ 26 \cdot 6 \ 26 \cdot 3 \\ 30 \ 40 \cdot 5 \ 40 \cdot 0 \ 39 \cdot 5 \\ 40 \ 54 \cdot 0 \ 53 \cdot 3 \ 52 \cdot 6 \\ 50 \ 67 \cdot 5 \ 66 \cdot 6 \ 65 \cdot 8 \end{array}$
51 52 53 54 55	$\begin{array}{r} \cdot 63279 \\ \cdot 63364 \\ \cdot 63449 \\ \underline{\cdot 63534} \\ 8 \cdot 63519 \end{array}$	85 85 85 85	•65185 •65274 •65363 •65452 8•65541	89 89 89 89 89 89 89	•68248 •68329 •68409 •68489 8•68569	80 80 80 80 80 80 80	•70391 •70475 •70560 •70644 8•70728	844 84 84 84 84 84 84	51 52 53 54 55	0 6 0.0 7 0.0 8 0.0 9 0.1
56 57 58 59 60	•63704 •63789 •63874 •63959	85 85 84 85 84 85 84	·65629 ·65718 ·65807 ·65895 8·65984	88 89 88 88 88 88 88	•68650 •68730 •68810 •68889 8•68969	80 80 80 79 80	·70813 ·70897 ·70981 <u>·71065</u> 8·71149	84 84 84 84 84	56 57 58 59 60	$ \begin{array}{c} 10 \\ 0 \\ 0 \\ 1 \\ 20 \\ 0 \\ 1 \\ 30 \\ 0 \\ 2 \\ 4 \\ 0 \\ 0 \\ 3 \\ 1 \\ 1 \\ 1 \\ 1 \\ 1 \\ 1 \\ 1 \\ 1 \\ 1 \\ 1$
~	Lg. Vers.	D	Log.Exs.	D	Lg. Vers.	D	Log.Exs.	D	<i>′</i>	P. P.

$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	a.			18°			1	L9°			
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	'	Lg. Vers.	D	Log.Exs.	D	Lg. Vers.	D	Log. Exs.	D	·	P. P.
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	0 1 2 3 4	·69049 ·69129 ·69208	8 <u>0</u> 79 79	·71232 ·71316 ·71400	84 83 84	8.73625 .73700 .73775 .73851 .73926	75 75 75	•76137 •76217 •76297	80 79 79	$\frac{1}{2}$	84, 83, 82
$ \begin{array}{c} 108.69763 \\ 112 \\ .698421 \\ .79079 \\ .72150 \\ .72231 \\ .70079 \\ .72316 \\ .72231 \\ .72231 \\ .72231 \\ .72231 \\ .72231 \\ .72316 \\ .74250 \\ .77224 \\ .77224 \\ .77224 \\ .77224 \\ .77224 \\ .77224 \\ .77224 \\ .77224 \\ .77224 \\ .77224 \\ .77224 \\ .77224 \\ .77225 \\ .77241 \\ .77225 \\ .77241 \\ .77225 \\ .77241 \\ .77225 \\ .77242 \\ .77225 \\ .77247 \\ .77225 \\ .77247 \\ .77225 \\ .77247 \\ .77225 \\ .77247 \\ .77225 \\ .77247 \\ .77225 \\ .77247 \\ .77225 \\ .77247 \\ .77225 \\ .77247 \\ .77225 \\ .77247 \\ .77225 \\ .77247 \\ .77225 \\ .77247 \\ .77225 \\ .77247 \\ .77225 \\ .77247 \\ .77225 \\ .77247 \\ .77225 \\ .77247 \\ .77447 \\ .77247 \\ .77247 \\ .77447 \\ .77$	6 7 8	·69446 ·69526 ·69605	79 79 79 79 79	·71651 ·71734 ·71817	8 <u>3</u> 8 <u>3</u> 83	$     \begin{array}{r}       8 \cdot 7400 \overline{1} \\       \cdot 7407 \overline{6} \\       \cdot 7415 \overline{1} \\       \cdot 7422 \overline{6}     \end{array} $	75 75 75 75	·76536 ·76615 ·76694	79 79 79 79 79	6 7 8	7 9.8 9.7 9.5 8 11.2 11.0 10.9
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	$11 \\ 12 \\ 13$	·69842 ·69921 ·70000	79 79 78 78	.72067 .72150 .72233	83 83 83 83	.74451 .74526 .74600	74 75 74 74 74	·76932 ·77011 ·77090	79 79 79 79 79	$     \begin{array}{c}       11 \\       12 \\       13     \end{array}   $	$\begin{array}{c} 30 42\cdot 0 41\cdot 5 41\cdot 0\\ 40 56\cdot 0 55\cdot 3 54\cdot 6\\ 50 70\cdot 0 69\cdot 1 68\cdot 3\end{array}$
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	15 16 17 18 19	8.70157 .70236 .70314 .70393 .70471	78 78 78 78 78 78	8 · 72399 · 72481 · 72564 · 72647 · 72729	82 83 82 82 82	8 • 74749 • 74824 • 74898 • 74973 • 75047	74 74 74 74	·77327 ·77406 ·77485 ·77563	7 <u>9</u> 78 79 78	16 17 18 19	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	21 22 23 24	·70628 ·70706 ·70784 ·70862	78 78 78 78 78	•72894 •72977 •7305 <u>9</u> •73141	82 82 82	·75195 ·75269 ·75343 ·75417	74 74 74 74 74	·77720 ·77799 ·77877 ·77956	79 78 78	21 22 23 24	2027.026.626.5 3040.540.039.5 4054.053.352.6 5067.566.665.3
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	26 27 28 29	·71018 ·71096 ·7117 <u>4</u> ·71251	77 78 77 77	·73306 ·73388 ·73470 ·73551	82 82 82 81 82 81	•75565 •75639 •75712 •75786	73 74 73 73 73 74	•78112 •78191 •78269 •78347	7 <u>8</u> 78 78 78	26 27 28 29	78 77 76 6 7.8 7.7 7.6 7 9 1 9 0 8 9
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	31 32 33 34	.71406     .71484     .71561     .71639     .		·73797 ·73878 ·73960	81 81	•75933 •76006 •76080 •76153	7 <u>3</u> 73 73	•78503 •78581 •78659 •78736	78 7 <u>8</u> 77	31 32 33 34	$\begin{array}{c} 10 \ 13 \cdot 0 \ 12 \cdot \underline{8} \ 12 \cdot \underline{6} \\ 20 \ 26 \cdot 0 \ 25 \cdot \underline{6} \ 25 \cdot \overline{3} \\ 30 \ 39 \cdot 0 \ 38 \cdot \underline{5} \ 38 \cdot \underline{0} \\ 40 \ 52 \cdot 0 \ 51 \cdot \underline{3} \ 50 \cdot \underline{6} \\ 50 \ 65 \cdot 0 \ 64 \cdot 1 \ 63 \cdot \overline{3} \end{array}$
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	36 37 38 39	·71793 ·71870 ·71947 ·72024	77 77 77 77	$ \begin{array}{r} \cdot 74123 \\ \cdot 74204 \\ \cdot 74286 \\ \cdot 74367 \\ \end{array} $	8 <u>1</u> 81 81 81	•76300 •76373 •76446 •76519	73 73 73	•78892 •78969 •79047 •79124		36 37 38 39	6 7.5 7.4 7.3
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{array}{c} 41\\ 42\\ 43\\ 44 \end{array}$	•72178 •72255 •7233 <u>1</u> •72408	77 76 77 76	·74529 ·74610 ·74691 ·74772	81 81 80 81	•76664 •76737 •76810 •76883	7 <u>3</u> 72 73	•79279 •79357 •79434 •79511	77 77	41 42 43 44	$\begin{array}{c} 9 \\ 10 \\ 12 \\ 10 \\ 12 \\ 12 \\ 12 \\ 12 \\ 12$
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	46 47 48 49	·72561 ·72637 ·72714 ·72790	7 <u>6</u> 7 <u>6</u> 76	·74934 ·75014 ·75095 ·75175	80 80 80	·77028 ·77100 ·77173 ·77245	72 72 72 72	.7966 <u>5</u> .79742 .7981 <u>9</u> .79896	77 77 77	46 47 48 49	$50162 \cdot 5161 \cdot 6160 \cdot 8$
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	51 52 53 54	·72942 ·73018 ·73094 ·73170	76 76 76	•75336 •75417 •75497 •75577	80 80 80 80 80	•77390 •77462 •77534 •77606	72 72 72	·80050 ·80126 ·80203 ·80280	77 76 77 76 76	51 52 53 54	7 8.4 8.3000 8 9.6 9.40.0 9 0.8 0.6 0.1 10 12.0 11.8 0.1 20 24.0 23.6 0.1 20 24.0 23.6 0.1
<u>8.78037</u> 8.78037 - 8.80738 - 60	56 57 58 59	•73322 •73398 •73473 •73549	7 <u>6</u> 7 <u>5</u> 75 76	•75738 •75818 •75898 •75978	80 80 80 80	•77750 •77822 •77893 •77965	72 72 71 72	-80433 -80509 -80586 -80662	7 <u>6</u> 7 <u>6</u> 76 76	56 57 58 59	40148.0147.30.3 40148.0147.30.3 50160.0159.110.4
			D		-		-		_	<u>ov</u>	P. P.

TABLE VIII.—LOGARITHMIC VERSED SINES AND EXTERNAL SECANTS.

TABLE VIIILOGARITHMIC	VERSED	SINES	AND	EXTERNAL	SECANTS.
20°	21°				

20%			21				
	Log. Exs. D	-0	D	Log. Exs.	D	<u>_</u>	P. P.
$\begin{array}{c} 0 \\ 0 \\ 1 \\ 78108 \\ 2 \\ 78180 \\ 71 \\ 78180 \\ 71 \\ 78251 \\ 71 \\ 3 \\ 78323 \\ 71 \\ 71 \\ 78323 \\ 71 \end{array}$	8.8073 <u>8</u> .80814 .80891 .80967 .80967 .81043	·82434 ·82502	6 <u>8</u> 68 68 68	8.85214 .85287 .85360 .85433 .85506	73 7 <u>3</u> 72 73	0 1 2 3 4	. 76 . 75 . 74
$\begin{array}{c} \overline{} \\ \overline{} \end{array} \\ \overline{} \\ \overline{} \\ \overline{} \\ \overline{} \\ \overline{} \\ \overline{}$	$\begin{array}{r} 8.81119 \\ .81195 \\ .81271 \\ .81346 \\ .81422 \\ .81422 \\ .61422 \\ .8142 \\ .8142 \\$	8·82569	67 68 68 67 68	8 · 85579 • 85651 • 85724 • 85797 • 85869	73 72 73 73 72 72 72	56789	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	8.81498 .81573 .81573 .81649 .81649 .81725 .75	8 · 82908 · 82976 · 83043 · 83111	67 67 67 67 67	8.85942 .86014 .86087 .86159	72121212 72272 72	10 11 12 13	20 25-3 25-0 21-6 30 38-0 37-5 37-0 40 50-6 50-0 49-3 50 63-3 62-5 61-6
$\begin{array}{c} 1 \pm & 7305 \pm \\ 15 & 8.79105 & 70 \\ 16 & .79175 & 70 \\ 17 & .79246 & 71 \\ 18 & .79317 & 70 \\ 19 & .79387 & 70 \end{array}$	$\begin{array}{r} 1313000\\ \hline 8\cdot81876\\ \cdot81951\\ \cdot82026\\ \cdot82102\\ \cdot82102\\ \cdot82177\\ 75\end{array}$	<u>.83178</u> 8.83246 .83313 .83380 .83447 .83515	67 67 67 67 67	<u>- 86231</u> 8 · 86304 · 86376 · 86448 · 86520 · 86592	72 72 72 72 72 72 72	14 15 16 17 18 19	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
$\begin{array}{c} \textbf{20} & \textbf{8} \cdot 79458 & 70\\ \textbf{21} & \cdot 79528 & 70\\ \textbf{22} & \cdot 79598 & 70\\ \textbf{23} & \cdot 79669 & 70\\ \textbf{24} & \cdot 79739 & 70\\ \end{array}$	8.82252 75 .82327 75 .82402 75 .92477 74 .32552 75	8 · 83582 · 83649 · 83716 · 83783 · 83850	67 67 67 67 67 67	8 • 86664 • 86736 • 86808 • 86808 • 86880 • 86952	72 72 72 72 72 71 72	20 21 22 23 24	$\begin{array}{c} 1012 \cdot 112 \cdot 011 \cdot 3 \\ 2024 \cdot 324 \cdot 023 \cdot 6 \\ 3036 \cdot 536 \cdot 035 \cdot 5 \\ 4048 \cdot 648 \cdot 047 \cdot 3 \\ 5060 \cdot 860 \cdot 059 \cdot 1 \end{array}$
29 0.173809 70 26 .79879 70 27 .79949 70 28 .80019 70 .80089 70			67 66 67 66 66 66	8 · 87024 • 87095 • 87167 • 87239 • 87310	72 71 72 71 71 71 71	25 26 27 28 29 30	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{array}{r} \cdot \cdot$	-84383 -84449 -84515	66 66 66 66	8 · 87382 · 87453 · 87525 · 87596 · 87668	7 <u>1</u> 7 <u>1</u> 7 <u>1</u> 7 <u>1</u> 7 <u>1</u> 7 <u>1</u> 7 <u>1</u>	31 32 33 34	$\begin{array}{cccccccccccccccccccccccccccccccccccc$
36         •80577         69           37         •80647         69           38         •80716         69           39         •80786         69	8-83373 -83447 -83521 -83595 74 -83595 74 -83670	·84780 ·84846	66 66 66 66	8-87739 -87810 -87881 -87953 -88024	71 71 71 71 71	35 36 37 38 39	67 66 65
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	8.83744 .83818 74 .83892 74 .83966 73 .84039	8 • 84912 • 84978 • 85044 • 85110 • 85176	66 66 66 66 65	8 · 88095 · 88166 · 88237 · 88308 · 88378	71 71 71 70 70 71	40 41 42 43 44	$\begin{matrix} 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 7 & 7 & 8 & 7 & 7 & 7 & 6 \\ 8 & 8 & 9 & 8 & 8 & 8 & 8 \\ 9 & 10 & 0 & 9 & 9 & 9 & 9 & 7 \\ 10 & 11 & 1 & 11 & 0 & 10 & 8 \\ 20 & 22 & 3 & 22 & 0 & 21 & 6 \\ 30 & 33 & 5 & 33 & 0 & 32 & 5 \\ 40 & 44 & 6 & 44 & 0 & 43 & 3 \\ 50 & 55 & 8 & 55 & 0 & 54 & 1 \end{matrix}$
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$ \begin{array}{r}             84187 \\             \cdot 84187 \\             \cdot 84261 \\             \cdot 84334 \\             84408 \\             73         \end{array} $	8 · 85242 • 85308 • 85373 • 85439 • 85505	66 65 65 66	8.8844 <u>9</u> .88520 .8859 <u>1</u> .8866 <u>1</u> .88732	7 <u>1</u> 70 70 71	45 46 47 48 49	0 000
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{array}{c} 10 \pm 20 \\ \hline & 8 + 84481 \\ \hline & 84555 \\ \cdot 84628 \\ \cdot 84702 \\ \cdot 84775 \\ \hline & 73 \\ \cdot 84775 \\ \hline & 77 \\ \end{array}$	8 · 85570 • 85626 • 85701 • 85766 • 85832	655555 66566 66566 65666	8.83°03 .88873 .88944 .89014 .89085	70 70 70 70 70 70 70 70	50 51 52 53 54	70.0 80.0 90.1 100.1 200.1
51         8.81888         68           55         8.81888         68           56         .81956         68           57         .82025         68           58         .82093         68           59         .82161         69	8 · 84848 73 · 84922 73 · 84995 73 · 85068 73 · 85141 72	.00100	65 65 65 65 65 65 65	8.8915 <u>5</u> .8922 <u>5</u> .89295 .89366 .89436	70 70 70 70 70 70	55 56 57 58 59	300.2 400.3 500.4
60 8.82229 68 Lg. Vers. D	8.80214	8.86223 Lg. Vers.		8.89506 Log.Exs.	D	<u>60</u> /	P. P.

TABLE VIIILOGARITHMIC VERSED SINES	SAND	EXTERNAL SECANTS.
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990	

 $23^{\circ}$ 

		2	~			7	3			
•	Lg. Vers.	D	Log.Exs.	D	Lg. Vers.	D	Log. Exs.	D	1	P. P.
0 1 2 3 4	8.86223 .86287 .86352 .86417 .86482	64 65 65 65	8.8950 <u>6</u> .8957 <u>6</u> .8964 <u>6</u> .89716 .89786	70 70 70 69	8.90034 .90096 .90158 .90220 .90282	62 62 62 62	8.93631 .93699 .93766 .93833 .93901	67 67 67 67	01234	70, 69, 68
5 6 7 8 9	8.86547 .86612 .86676 .86741 .86805	64 65 64 64 64 64 64	8.89356 .89926 .89995 .90065 .90135	70 70 69 70 69	8.90344 .90406 .90467 .90529 .90529	62 62 61 62 61	8.93968 .94035 .94102 .94170 .94237	67 67 67 67 67	5 6 7 8 9	$ \begin{array}{c} 6 & 7 \cdot 0 \\ 7 & 8 \cdot 1 \\ 8 & 9 \cdot 3 \\ 9 \cdot 2 \\ 9 & 10 \cdot 5 \\ 10 \cdot 1 \\ 10 \cdot 1 \\ 20 & 23 \cdot 3 \\ 20 & 23 \cdot 3 \\ 23 \cdot 3 & 23 \cdot 0 \\ 23 \cdot 3 & 23 \cdot 0 \\ 22 \cdot 6 \end{array} $
10 11 12 13 14	8.86870 .86934 .86999 .87063 .87127	64444 644 644	8.90205 .90274 .90344 .90413 .90483	70 69 69 69 69 69	8.90652 .90714 .90776 .90837 .90899	61 62 61 61 61	8.94304 .94371 .94438 .94505 .94572	67 67 67 67 67	10 11 12 13 14	$\begin{array}{c} 30 & 35 \cdot 0 & 34 \cdot 5 & 34 \cdot 0 \\ 40 & 46 \cdot 6 & 46 \cdot 0 & 45 \cdot 3 \\ 50 & 58 \cdot 3 & 57 \cdot 5 & 56 \cdot 6 \end{array}$
15 16 17 18 19	8.87192 .87256 .87320 .87384 .87448	64 64 64 64 64 64 64	8.90552 .90622 .90691 .90760 .90830	6 <u>9</u> 6 <u>9</u> 6 <u>9</u> 6 <u>9</u> 6 <u>9</u> 6 <u>9</u> 69	8.90960 .91021 .91083 .91144 .91205	61 61 61 61 61 61	8 · 94638 · 94705 · 94772 · 94839 · 94905	66 67 66 67 66 66 66	15 16 17 18 19	$\begin{array}{cccccccccccccccccccccccccccccccccccc$
20 21 22 23 24	-87576 -87640 -87704 -87768	64 64 64 63 64	8.90899 .90968 .91037 .91106 .91175	69 69 69 69 69	8.91267 .91328 .91389 .91450 .91511	61 61 61 61 61	8.94972 .95039 .95105 .95172 .95238	67 66 66 66 66 66	20 21 22 23 24	$\begin{array}{c} 10 & 11 & 1 & 11 & 10 & 10 & 18 \\ 20 & 22 & 3 & 22 & 0 & 21 & 6 \\ 30 & 33 & 5 & 33 & 0 & 32 & 5 \\ 40 & 44 & 6 & 44 & 0 & 43 & 3 \\ 50 & 55 & 8 & 55 & 0 & 54 & 1 \end{array}$
25 26 27 28 29	8-87832 -87895 -87959 -88023 -88086	664030 6636 63 63	$\begin{array}{r} 8.9124\overline{4} \\ .9131\overline{3} \\ .91382 \\ .91451 \\ .91520 \end{array}$	69 68 69 69 69 68	8.91572 .91633 .91694 .91755 .91815	61 61 61 60 61	8.9530 <u>5</u> .9537 <u>1</u> .95437 .95504 .95570	66 66 66 66	25 26 27 28 29	$\begin{array}{cccccccccccccccccccccccccccccccccccc$
30 31 32 33 34	8-88150 -88213 -88277 -88340 -88404	63 3 3 633 3 3 63	8.91588 .91657 .91726 .91794 .91863	69 68 68 68 68 68 69	8.91876 .91937 .91997 .92058 .92119	60 60 61 60 60 60	8.95636 .95703 .95769 .95835 .95901	66 66 66 66	$30 \\ 31 \\ 32 \\ 33 \\ 34$	$ \begin{array}{c} 9 \\ 9 \\ 6 \\ 6 \\ 7 \\ 7 \\ 8 \\ 7 \\ 7 \\ 7 \\ 7 \\ 7 \\ 7 \\ 7$
35 36 37 38 39	8-88467 -88530 -88593 -88656 -88720	63 63 63 63 63 63 63	8.91932 .92000 .92068 .92137 .92205	688 688 688 688 688 68 68 68 68	$8.9217\overline{9}$ .92240 $.9230\overline{0}$ .92361 .92421	60 60 60 60 60 60 60 60	8.95967 .96033 .96099 .96165 .96231	66 66 66 66	35 36 37 38 39	61 60 59 6 6.1 6.0 5.9 7 7.1 7.0 6.9
40 41 42 43 44	8-88783 -88846 -88909 -88971 -89034	63 6 <u>3</u> 62 63	8.92274 .92342 .92410 .92478 .92546	68 68 68 68 68 68	8.92487 .92542 .92602 .92662 .92722	60 60 60 60	8.96297 .96362 .96428 .96494 .96560	66 65 66 65 66	$40 \\ 41 \\ 42 \\ 43 \\ 44$	$ \begin{array}{c} 8 \\ 8 \\ 8 \\ 10 \\ 10 \\ 10 \\ 10 \\ 10 \\ 10$
45 46 47 48 49	8.29097 .89160 .89223 .89285 .89348	63 62 63 62 62 62	8.92615 .92683 .92751 .92819 .92887	68 68 68 68	8 · 92782 · 92842 · 92902 · 92962 · 93022	60 60 60 60 60	8.96625 .96691 .96757 .96822 .96888	655 665 655 655 655 655	45 46 47 48 49	ō
50 51 52 53 54	$\begin{array}{r} 8 \cdot 89411 \\ \cdot 89473 \\ \cdot 89536 \\ \cdot 89598 \\ \cdot 89660 \end{array}$	6312121212 662662 662662	8.92955 .93022 .93090 .93158 .93226	68 67 68 67 68	8.93082 .93142 .93202 .93261 .93221	60 59 60 50 50 50 50	$     \begin{array}{r}       8 \cdot 9695\overline{3} \\       \cdot 97018 \\       \cdot 97084 \\       \cdot 97149 \\       \cdot 97214     \end{array} $	6 <u>5</u> 6 <u>5</u> 6 <u>5</u> 65 65	50 51 52 53 54	60.0 70.0 80.0 90.1 100.1 200.1
55 56 57 58 59	8.89723 .89785 .89847 .89910 .89972	622 622 622 622 622 622 622 622 622 622	8.9329 <u>3</u> .93361 .93429 .93496 .93564	67 68 67 67 67	8.9338 <u>1</u> .9344 <u>0</u> .93500 .93560 .93619	5990999 50555	$\begin{array}{r} 8.97280 \\ .97345 \\ .97410 \\ .97475 \\ .97540 \end{array}$	65 65 65 65 65	55 56 57 58 59	200.2 400.3 500.4
<u>60</u>	8.00034	62	<u>8.93631</u>	67	8.93679	59	<u>8.97606</u>	65	<u>60</u>	
_	Lg. Vers.	D	Log.Exs.	D	Lg. Vers.	D	Log.Exs.	D	1	P. P.

661

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## TABLE VIII.-LOGARITHMIC VERSED SINES AND EXTERNAL SECANTS.

10	TABLE VIII.—LOGARITHMIC VERSED SINES AND EXTERNAL SECANTS. $24^{\circ}$ $25^{\circ}$									
,	Lg. Vers.	D	Log.Exs.	D	Lg. Vers.	D	Log. Exs.	D	'	P. P.
·         0         1         2         3         4         5         6         7         8         9         10         11         12         3         4         15         6         7         8         9         10         11         12         13         14         15         16         17         18         19         20         10         12         12         14         15         16         17         18         19         20	$\begin{array}{c} Lg, Vers, \\ \hline 8.93679 \\ -93738 \\ -93738 \\ -93738 \\ -93738 \\ -93916 \\ -93916 \\ -94034 \\ -94034 \\ -94153 \\ -94212 \\ 8.94212 \\ 8.94271 \\ -94389 \\ -94389 \\ -94389 \\ -94388 \\ -94468 \\ -94683 \\ 8.94506 \\ 8.94506 \\ 8.94506 \\ 8.94800 \\ 8.9480 \\ 8.94800 \\ 8.$	<b>D</b> 55555555555555555555555555555555555	Log. Exs. 8 - 97606 977671 -97736 97865 8 - 97995 -97995 -97995 -97995 -97995 -97995 -97995 -98190 8 - 98254 -98319 -983819 -983813 8 - 982513 8 - 985513 8 - 985513 8 - 98577 -98642 -98706 -98706 -98706 -988355	55554 555455 141414554 141414444 66666 6666666666666666666666	8.97170 97227 97284 97384 97398 8.97455 97561 97565 97651 8.97738 97795 97861 8.97796 97808 97964 8.98020 97864 8.98020 97864 8.98020 98133 981300 98246	<b>D 55577767766666766666666666666666666666</b>	$\begin{array}{c} \mbox{Log, Exs.}\\ 9.0143, 01505, 01568, 01631, 01568, 01631, 01694, 01962, 01962, 01962, 01942, 01942, 01942, 01942, 01942, 01942, 02195, 02257, 02257, 02257, 02257, 02257, 02257, 02257, 02257, 02257, 02257, 02257, 02257, 02257, 02257, 022569, 026$	66666666666666666666666666666666666666	0 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19	$\begin{array}{cccccccccccccccccccccccccccccccccccc$
$\begin{array}{c} 201 \\ 222$	$\begin{array}{r} 94917\\ 94917\\ 94976\\ 95034\\ 95038\\ 95019\\ 95268\\ 95268\\ 953268\\ 953268\\ 9553268\\ 95553\\ 95551\\ 95559\\ 95617\\ 95569\\ 95675\\ 8.9573\\ 95567\\ 95567\\ 95567\\ 8.9573\\ 95657\\ 8.9573\\ 95657\\ 8.9573\\ 95657\\ 8.9573\\ 95657\\ 8.9573\\ 95657\\ 95657\\ 8.9573\\ 95657\\ 95657\\ 95657\\ 8.9573\\ 95657\\ 95657\\ 95657\\ 8.9573\\ 95657\\ 95575\\ 955$	<u></u>	8 98899 99028 99029 99156 8 99226 99156 8 99226 99284 99294 99294 99294 99205 99205 99205 99205 99205 99205 99205 99205 99205 99205 99005 100005 10005 10005 10005 10000		8 98302 98410 98420 98527 98527 986527 986527 98639 98639 98639 98639 98805 98805 98805 98805 98805 98805 98805 98874 98974 990305 8 99141 990305 8 99141 990305 990305 8 99141 990305 99030 990000 99030 9900000000	ସସପ ସସସସର ସସସସର ଜଣ୍ୟସର ସସସେପ ସ୍ଥ୍ୟପ୍ରଥିବି ହେଇଥିବି ସେଥିବିତ ସସସ ସସାସସାଦ ସାସାସସାରା ସାସାସାରେ ସା ସାର୍ପସାର୍ଚ୍ଚ ଚିର୍ନେଚ୍ଚର ହାରିଚନ୍ଦ୍ରର	$\begin{array}{r} 9 \cdot 02693\\ \cdot 02755\\ \cdot 0280\\ \cdot 02912\\ \cdot 02942\\ \cdot 02942\\ \cdot 03066\\ \cdot 03128\\ \cdot 03102\\ \cdot 03066\\ \cdot 03128\\ \cdot 03102\\ \cdot 03252\\ \cdot 03315\\ \cdot 03425\\ \cdot 0425\\ \cdot 04421\\ \cdot 04423\\ \cdot 04425\\ \cdot 04405\\ \cdot 04605\\ \cdot 046$	622222 622222 622 62222 622 62222 622 6	$\begin{array}{c} 20\\ 211\\ 223\\ 24\\ 255\\ 267\\ 28\\ 2\\ 333\\ 35\\ 334\\ 355\\ 366\\ 7\\ 38\\ 39\\ 401\\ 423\\ 4\\ 45\\ 46\\ 47\\ 8\\ 49\\ 50\\ 52\\ \end{array}$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
53 54 55 56 57 58 59 60	.96770 .96827 8.96885 .96942 .96999 .97056 .97113	57 57 57 57 57 57 57 57 57 57 57	01002 01065 9.01128 01191 01254 01317 01380 9.01443 Log, Exs,	63 63 63 63 63 63 63 63 7	$\begin{array}{c} .0013\overline{6}\\ .0019\overline{1}\\ 9.0024\overline{6}\\ .0030\overline{1}\\ .0035\overline{6}\\ .00411\\ .0046\overline{6}\\ 9.0052\overline{0}\\ Lg. Vers, \end{array}$	55 55 55 55 55 54 55 54 55 54 54	04727 04788 9.04850 04911 04972 05033 05093 9.05154 Log.Exs.	61 61 61 61 60 61 61	53 54 55 56 57 58 59 60	P. P.

TABLE VIIILOGARITHMIC	VERSED SINES ANI	D EXTERNAL SECANTS.
260	27°	

	26°				27°							
,	Lg. Vers.	D	Log.Exs.	D	Lg. Vers.	D	Log.Exs.	D		P. P.		
0 1 2 3 4 5	9.00520 .00575 .00630 .00684 .00739 9.00794	55 54 54 54 55 55 55 55 55	9.05154.05215.05276.05337.053389.05458	$     \begin{array}{r}       61 \\       61 \\       60 \\       61 \\       60 \\       61 \\       61     \end{array} $	9.03740 .03792 .03845 .03898 .03950 9.04002	52 52 532 52 52 52 52 52	9.08752 .08811 .08870 .08929 .08988 9.09047	59 59 59 59 59 59 59	0 1 2 3 4 5	61 60 59 6 6.1 6.0 5.9 7 7.1 7.0 6.9		
6 7 8 9 10	·00848 ·00903 ·00957 ·01011 9·01066	54 54 54 54 54	$ \begin{array}{r} \cdot 0551\bar{9} \\ \cdot 05580 \\ \cdot 0564\bar{0} \\ \underline{\cdot 05701} \\ 9 \cdot 05762 \end{array} $	60 60 60 61	$\begin{array}{r} \cdot 04055 \\ \cdot 04107 \\ \cdot 04160 \\ \underline{\cdot 04212} \\ 9 \cdot 04264 \end{array}$	512121 51212 51212 51212 51212	·09106 ·09164 ·09223 ·09282 9·09341	58 59 59 58	6 7 8 9 10	$\begin{array}{cccccccccccccccccccccccccccccccccccc$		
11 12 13 14	.01120 .01174 .01229 .01283 9.01337	54 54 54 54 54 54	$0582\overline{2}$ 05883 05943 06004 $9.0606\overline{4}$	60 60 60 60 60	04317 04369 04421 04473 9.04525	52 52 52 52	·09400 ·09458 ·09517 <u>·09576</u> 9·09634	59 58 59 58 58 58 58	$     \begin{array}{c}       11 \\       12 \\       13 \\       \underline{14} \\       15     \end{array} $			
15 16 17 18 19	$0.0139\overline{1}$ $0.0144\overline{5}$ $0.0149\overline{9}$ 0.01554	54 54 54 54 54 54	·06124 ·06185 ·06245 ·06305	60 60 60 60 60	·04577 ·04630 ·04682 ·04734 9·04786	52 52 52 52 52 52 52 52	·09693 ·09752 ·09810 ·09869 9·09927	58 59 58 58 58 58	$     \begin{array}{r}       15 \\       16 \\       17 \\       18 \\       19 \\       20 \\     \end{array} $	58 57 6 5.8 57 7 6.7 5.6 8 7.7 7.6 9 8.7 8.5 10 9.6 9.6 20 19.3 19.0 30 29.0 28.6 40 38.6 38.0 50 48.3 47.5		
20 21 22 23 24	·01662 ·01715 ·01769 ·01823 9·01877	54 53 54 54 54 54	·06426 ·06486 ·06546 ·06606	60 60 60 60 60	·04837 ·04889 ·04941 ·04993 9·05045	52 52 52 51	$     \begin{array}{r}             .09986 \\             .10044 \\             .10102 \\             .10161 \\             9.10219 \\         \end{array} $	555588 5555555555555555555555555555555	21 22 23 24 25	30 129 • 0 28 • 5 40 38 • 6 38 • 0 50 48 • 3 47 • 5		
25 267 29 20 20 20 20 20 20 20 20 20 20 20 20 20	0.01877 0.01931 0.01985 0.02038 0.02092 9.02146	5343 543 555 555 535 535	·06727 ·06787 ·06847 ·06907 9·06967	60 60 60 60 60	·05097 ·05148 ·05200 ·05252 9·05303	52 51 52 52 52 51		58 58 58 58 58	26 27 28 29 30	55 54 6 5.5 54 7 6.4 6.3 8 7.3 7.8 9 8.2 8.1		
31 32 33 34	·02199 ·02253 ·02307 ·02360	54 53 53 53	·07027 ·07087 ·07146 ·07206	60 6 <u>0</u> 59 60 60	·05355 ·05407 ·05458 ·05510	52 51 51 51 51	$     \begin{array}{r}         & \cdot 10569 \\         & \cdot 10627 \\         & \cdot 10685 \\         & \cdot 10743     \end{array}   $	58 58 58 58 58 58	31 32 33 34	6 5.5 5.4 7 6.4 6.3 8 7.3 7.8 9 8.2 8.1 10 9.1 5.3 20 18.3 18.0 30 27.5 27.0 40 36.6 36.0 50 45.8 45.0		
85 86 87 88 89	9.02414 0.02467 0.02521 0.02574 0.02627	533 533 533 533 533 533 533 533 533	9.07266 .07326 .07386 .07445 .07505	59 60 59 60 59	9.05561 .05613 .05664 .05715 .05767	51 51 51 51 51 51 51	9.10801 .10859 .10917 .10975 .11033	58 58 58 58 58	35 36 37 38 39	53 52 6  5.3  5.2 7  6.2  6.0		
40 41 42 43 44	$9.02681 \\ .02734 \\ .02787 \\ .02840 \\ .02894 \\ $	53 53 53 53 53 53	9.07565 .07624 .07684 .07743 .077803	59 59 59 59 59 60 59	$9.0581\overline{8}$ .05869 .05921 .05972 .06023	51 51 51 51 51	$9.1109\overline{1}$ .11149 .11207 .11265 .11323	58 57 58 58 58	$     \begin{array}{r}       40 \\       41 \\       42 \\       43 \\       44 \\       \hline       44     \end{array} $	6 5.3 5.3 7 6.2 6.0 8 7.0 6.9 9 7.9 7.8 10 8.8 8 2017.6 17.3 30 26.5 26.0 40 35.3 34.6 50 44.1 43.3		
45 46 47 48 49	9.02947 0.03000 0.03053 0.03106 0.03159	53 53 53 53 53 53	$\begin{array}{r}9.07863\\.07922\\.07981\\.08041\\.08100\end{array}$	599 599 599 599 599 59 59 59 59 59	9.06074 .06125 .06176 .06227 .06279	51 51 51 51	9.11380/11438/11438/11496/11554/11611/	58 58 57 57	45 46 47 48 49	F1 A		
50 51 52 53 54	$9.03212 \\ 0.03265 \\ 0.03318 \\ 0.03371 \\ 0.03423 \\ \hline{}$	53 53 53 53 53 53 53 53	9.08160 .08219 .08278 .08338 .08397	59 59 59 59 59 59 59 59 59	$\begin{array}{r}9.06330\\.06380\\.06431\\.06431\\.06482\\.06533\end{array}$	51 50 51 51 51 51	9.11669.11727.11784.11842.11899	58 57 57 57 57 57 58	50 51 52 53 54	7 5.9 0.0 8 6.8 0.0 9 7.6 0.1 10 8.5 0.1		
55 56 57 58 59	$\begin{array}{r}9.0347\overline{6}\\.03529\\.03582\\.03634\\.03687\end{array}$	53 53 53 53 53 53 53 53 53 53 53 53 53 5	$\begin{array}{r} 9.0845\bar{6} \\ .0851\bar{5} \\ .08574 \\ .08634 \\ .08693 \end{array}$	59 59 59 59 59 59	9.06584 .06635 .06686 .06736 .06787	51 50 51 50 51 50	9.11957 .12015 .12072 .12129 .12187	58 57 57 57 57 57 57	55 56 57 58 59	2017.00.1 3025.80.2 4034.00.3 5042.50.4		
<u>60</u>	9.03740 Lg. Vers.	$\overline{D}$	9 · 08752 Log. Exs.	D	<u>9 - 06838</u> Lg. Vers.	$\overline{D}$	<u>9 · 12244</u> Log. Exs.	D	<u>60</u> ′	P. P.		

TABLE VIIILOGARITHMIC	VERSED SINES.	AND EXTERNAL	SECANTS.
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28°

**29°** 

-	28-					^	·9·					
1	Lg. Vers.	D	Log.Exs.	D	Lg. Vers.	D	Log.Exs.	D	'	P. P.		
01234	9.06838 .06888 .06939 .06990 .07040	50 51 50 50	$9.1224\bar{4} \\ .12302 \\ .1235\bar{9} \\ .12416 \\ .12474$	57 57 57 57 57	9.09823 .09872 .09920 .09969 .10018	49 48 49 48	9.15641 .15697 .15752 .15808 .15864	56 55 56 55	0 1 2 3 4	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$		
56789	9.07091 .07141 .07192 .07242 .07293	50 50 50 50 50 50	9.12531.12588.12645.12703.12703.12760	57 57 57 57 57 57	9.10067 .10115 .10164 .10213 .10261	49 48 49 49 49 49	$\begin{array}{r} 9.15920 \\ .15975 \\ .16031 \\ .16087 \\ .16142 \end{array}$	56 55 55 55 55 55	5 6 7 8 9	6         0.5         0.5         0.5           10         9.6         9.5         9.4           20         19.1         19.0         18.8           30         28.7         28.5         28.2           40         38.3         38.0         37.6           50         47.9         47.5         47.1		
10 11 12 13 14	9.07343 .97393 .07444 .07494 .07544	50 50 50 50 50	9.12817.12874.12931.12988.12988.13045	57 57 57 57 57	$9.10310 \\ .10358 \\ .10407 \\ .10455 \\ .10504$	444444	$\begin{array}{r} 9.1619\overline{8} \\ .16254 \\ .1630\overline{9} \\ .16365 \\ .16420 \end{array}$	565555 55555	10 11 12 13 14	$\begin{array}{cccccccccccccccccccccccccccccccccccc$		
15 16 17 18 19	9.0759 <u>4</u> .0764 <u>4</u> .07695 .07745 .07795	50 50 50 50 50 50	9.13102.13159.13216.13273.13330	57 57 57 56 57	$9.1055\overline{2} \\ .10601 \\ .10649 \\ .10697 \\ .10746$	48 48 48 48 48 48 48	9.16476.16531.16587.16642.16698	555555 555555	15 16 17 18 19	$\begin{array}{c} 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 $		
20 21 22 23 24	9.07845 .07895 .07945 .07995 .08045	50 50 50 50 50	9.13387.13444.13500.13557.13614	57 57 56 57 56	9.10794 .10842 .10890 .10939 .10987	48 48 48 48 48 48	9.16753 .16808 .16864 .16919 .16974	55 55 55 55 55 55 55	20 21 22 23 24	$\begin{array}{cccccccccccccccccccccccccccccccccccc$		
25 26 27 28 29	$\begin{array}{r} 9.08095 \\ .08145 \\ .08195 \\ .08244 \\ .08294 \end{array}$	50 50 50 49 50	$9.13671 \\ .13727 \\ .13784 \\ .13841 \\ .13897$	57 56 57 56 56	$\begin{array}{r} 9.11035 \\ .11083 \\ .11131 \\ .11179 \\ .11227 \end{array}$	48 48 48 48 48	9.17029 .17085 .17140 .17195 .17250	555 555 555 555	25 26 27 28 29	$\begin{array}{c c c c c c c c c c c c c c c c c c c $		
30 31 32 33 34	$9.08344 \\ .08394 \\ .08443 \\ .08493 \\ .08543$	49 50 49 49 50	$\begin{array}{r} 9.1395\overline{4} \\ .14011 \\ .14067 \\ .14124 \\ .14180 \end{array}$	57 566 566 566	$9.1127\overline{5} \\ .1132\overline{3} \\ .11371 \\ .11419 \\ .11467$	48 48 48 47 48	9.17305 .17361 .17416 .17471 .17471 .17526	5555 5555 555	30 31 32 33 34	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$		
35 36 37 38 39	9.08592 .08642 .08691 .08741 .08790	4999999 499999	$9.14237 \\ .14293 \\ .14350 \\ .14406 \\ .14462$	5666 5566 556	9.11515 .11562 .11610 .11658 .11706	48 47 48 48 47	9.17581 .17636 .17691 .17746 .17801	55 55 55 55 55	35 36 37 38 39	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$		
40 41 42 43 44	9.08840 .08889 .08939 .08988 .09087	49 49 49 49 49 49	9.14519 .14575 .14631 .14688 .14688 .14744	5 <u>6</u> 56 56 56 56	9.11754.11801.11849.11849.11897.11944	48 47 47 48 47	9.17856 .17910 .17965 .18020 .18075	55 54 55 55 54 54	40 41 42 43 44	$\begin{array}{cccccccccccccccccccccccccccccccccccc$		
45 46 47 48 49	9.09087 .09136 .09185 .09234 .09284	49 49 49 49 49 49	$\begin{array}{r} \hline 9.14800 \\ \cdot 14856 \\ \cdot 14913 \\ \cdot 14969 \\ \cdot 15025 \end{array}$	56 56 56 56 56	9.11992 .12039 .12087 .12134 .12182	47 47 47 47 47 47	$9.18130 \\ .18185 \\ .18239 \\ .18294 \\ .18349$	55 55 54 55 54 55 4	45 46 47 48 49	$\begin{array}{c} 9 & 7 \cdot 4 & 7 \cdot 3 \\ 10 & 8 \cdot 2 & 8 \cdot 1 & 8 \cdot 1 \\ 20 & 16 \cdot 5 & 16 \cdot 3 & 16 \cdot 1 \\ 30 & 24 \cdot 7 & 24 \cdot 5 & 24 \cdot 2 \\ 40 & 33 \cdot 0 & 23 \cdot 0 & 32 \cdot 3 \\ 50 & 41 \cdot 2 & 40 \cdot 3 & 40 \cdot 4 \end{array}$		
50 51 52 53 54	$\begin{array}{r} & 0.09333 \\ 0.09382 \\ 0.09431 \\ 0.09480 \\ 0.09529 \end{array}$	49 49 49 49 49	9.15081 .15137 15193 15249 .15305	56 56 56 56 56	$\begin{array}{r} & -12229 \\ \hline 9.12229 \\ .12277 \\ .12324 \\ .12371 \\ .12419 \end{array}$	47 47 47 47 47	9.1840 <u>3</u> .18458 .1851 <u>3</u> .18567 .18622	545 554 544 554 554 554 554 554 555 555	50 51 52 53 54	$\begin{array}{cccccccccccccccccccccccccccccccccccc$		
55 56 57 58 59	9.09578 .09627 .09676 .09725 .09774	49 49 4 <u>9</u> 48 49	$\begin{array}{r} 9.1536\overline{1} \\ .15417 \\ .15473 \\ .15529 \\ .15585 \end{array}$	56 56 56 56 55 55	$\begin{array}{r} \hline 9.12466\\ \cdot 12513\\ \cdot 12560\\ \cdot 12608\\ \cdot 12655\\ \end{array}$	47 47 47 47 47	9 · 18676 • 18731 • 18786 • 18840 • 18894	54 55 54 54 54	55 56 57 58 59	$\begin{array}{c c c c c c c c c c c c c c c c c c c $		
<u>60</u>	9.09823 Lg. Vers.	49 D	9.15641 Log.Exs.	56 D	<u>9 · 12702</u> Lg. Vers.	47 D	<u>9 · 18949</u> Log.Exs.	54 D	<u>60</u> '	20 24 0 23 7 23 5 40 32 0 31 6 31 3 50 40 0 39 6 39 1 P, P,		

TABLE VIIILOGARITHMIC	VERSED SINES AND	EXTERNAL SECANTS.
30°	31°	

1	30°		31°				
' Lg. Vers.	D Log. Exs.	D Lg. Vers.	D Log. Exs.	D'	P. P.		
	$\begin{array}{r} 4\overline{7} & 9.18949 \\ 4\overline{7} & .19003 \\ 4\overline{7} & .19058 \\ 4\overline{7} & .19112 \\ 4\overline{7} & .19167 \end{array}$	$\begin{array}{c} 5\overline{\underline{4}}\\ 5\overline{\underline{4}}\\ 5\overline{\underline{4}}\\ 5\overline{\underline{4}}\\ 5\overline{\underline{4}}\\ 5\overline{\underline{4}}\\ 5\overline{\underline{4}}\\ -15619\\ -15665\end{array}$	22388	$\begin{array}{cccc} 5\overline{3} & 0 \\ 5\overline{3} & 1 \\ 5\overline{3} & 2 \\ 5\overline{3} & 5\overline{3} \\ 5\overline{3} & 4 \end{array}$	54, 54, 53		
$\begin{array}{c} 5 & 9 \cdot 1293\overline{7} \\ 6 & \cdot 1298\overline{4} \\ 7 & \cdot 1303\overline{1} \\ 8 & \cdot 1307\overline{8} \\ 9 & \cdot 1312\overline{5} \end{array}$	$\begin{array}{c} 47\\ 47\\ 47\\ 47\\ 47\\ 47\\ 19275\\ 19329\\ 47\\ 19384\\ 47\\ 19438\\ \end{array}$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{array}{r} 45 \\ 45 \\ 45 \\ 45 \\ 45 \\ 45 \\ 45 \\ 22600 \\ 45 \\ 22653 \end{array}$	53 53 53 53 53 7 53 53 8 9	$\begin{array}{cccccccccccccccccccccccccccccccccccc$		
$\begin{array}{c} 10 \\ 9.13172 \\ 11 \\ 13219 \\ 12 \\ 13266 \\ 10010 \end{array}$	$\begin{array}{c} 47\\ 46\\ 47\\ 47\\ 47\\ 47\\ 46\\ 47\\ 46\\ 19601\\ 46\\ 19655\\ 19709\\ \end{array}$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	53 10	50145+4145+0144+6		
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{array}{c} 47\\ 46\\ 47\\ 47\\ 47\\ 47\\ 46\\ 46\\ 46\\ 19925\\ 46\\ 19979\\ 46\\ 19979\\ \end{array}$	$\begin{array}{c} 54\\ 54\\ 54\\ 54\\ 54\\ 54\\ 54\\ 54\\ 54\\ 54\\$	$\begin{array}{c cccccc} 45 & 9 \cdot 22971 \\ 45 & \cdot 23024 \\ 45 & \cdot 23076 \\ 45 & \cdot 23129 \\ 45 & \cdot 23189 \\ 45 & \cdot 23189 \end{array}$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{array}{c} 53 & 5\overline{2} & 52 \\ 6 & 5 \cdot 3 & 5 \cdot 2 & 5 \cdot 2 \\ 7 & 6 \cdot 2 & 6 \cdot 1 & 6 \cdot 0 \\ 8 & 7 \cdot 0 & 7 \cdot 0 & 7 \cdot 0 \\ 9 & 7 \cdot 9 & 7 \cdot 9 & 7 \cdot 8 \\ 10 & 8 & 8 & 8 & 7 & 8 \cdot 6 \\ 20 & 17 \cdot 6 & 17 \cdot 5 & 17 \cdot 3 \\ 20 & 17 \cdot 6 & 17 \cdot 5 & 17 \cdot 3 \\ \end{array}$		
$\begin{array}{r} 21 & \cdot 13086 \\ 22 & \cdot 13733 \\ 23 & \cdot 13779 \\ 24 & \cdot 13826 \end{array}$	$\begin{array}{c} 47 \\ 46 \\ 46 \\ 46 \\ 46 \\ 46 \\ \cdot 20141 \\ \cdot 20195 \\ \cdot 20249 \\ \end{array}$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	52 21 53 22 52 23 53 24	$\begin{array}{c} 20 17\cdot \overline{6} 17\cdot \overline{5} 17\cdot \overline{3}\\ 30 26\cdot \overline{5} 26\cdot 2 26\cdot 0\\ 40 35\cdot \overline{3} 35\cdot 0 34\cdot \overline{6}\\ 50 44\cdot 1 43\cdot 7 43\cdot \overline{3}\\ \end{array}$		
25 9.13872 26 .13919 27 .13965 28 .14011 29 .14058	$\begin{array}{c} 4\bar{6} \\ 20518 \end{array}$	$\begin{array}{r} 54 \\ 54 \\ 54 \\ 54 \\ 53 \\ 53 \\ 16748 \\ 16793 \end{array}$	$\begin{array}{r} 45 & \cdot 23436 \\ 45 & \cdot 23551 \\ 45 & \cdot 23603 \\ 45 & \cdot 23656 \\ 44 & \cdot 23709 \\ 45 & \cdot 23709 \end{array}$	522 26 522 27 522 28 53 29	$\begin{array}{cccccccccccccccccccccccccccccccccccc$		
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{array}{r} 4\overline{6} & 9 \cdot 20572 \\ \cdot 20626 \\ \cdot 20680 \\ \cdot 20733 \\ 4\overline{6} \\ \cdot 20787 \end{array}$	$5\overline{3}$ 9.16838 54 16882 53 16927 54 16972 57 17017	$\begin{array}{r} 4\overline{4} & 5 \cdot 23761 \\ 4\overline{4} & \cdot 23814 \\ 4\overline{5} & \cdot 2386\overline{6} \\ 4\overline{4} & \cdot 23919 \\ 4\overline{5} & \cdot 2397\overline{1} \end{array}$	52 52 52 52 52 32 32 52 33 52 34	10 7.9 7.8 7.7 20 15.8 15.6 15.5 30 23.7 23.5 23.2 40 31.6 31.3 31.0 50 39.6 39.1 38.7		
$\begin{array}{r} 35 & 9 \cdot 14336 \\ 36 & \cdot 14382 \\ 37 & \cdot 14428 \\ 38 & \cdot 14474 \\ 39 & \cdot 14520 \end{array}$	$\begin{array}{c} 46 \\ 9.20841 \\ \cdot 20894 \\ 46 \\ \cdot 20948 \\ \cdot 21002 \\ 46 \\ \cdot 21055 \end{array}$	$\begin{array}{c} 5\overline{3} & 9 \cdot 17061 \\ 5\overline{3} & \cdot 17106 \\ 5\overline{3} & \cdot 17151 \\ 5\overline{3} & \cdot 1719\overline{5} \\ 5\overline{3} & \cdot 1719\overline{5} \end{array}$	$\begin{array}{c c} & -26074 \\ \hline & 44 \\ 44 \\ 45 \\ 45 \\ 44 \\ 44 \\ -24128 \\ 44 \\ -24128 \\ 44 \\ -24233 \\ 44 \\ -24285 \\ \hline \end{array}$	522 36 522 37 522 38 52 39	$46 \ 4\overline{5} \ 45$		
$\begin{array}{r} 409.14366 \\ 41 & \cdot 14612 \\ 42 & \cdot 14658 \\ 43 & \cdot 14704 \\ 44 & \cdot 14750 \end{array}$		$\begin{array}{r} 5\overline{3} & -172 + 172 + 172 + 172 + 172 + 172 + 1732 + 1732 + 1732 + 17373 + 17418 + 17462$	$\begin{array}{c} 4\frac{4}{4} & \cdot 24138 \\ 4\frac{4}{4} & \cdot 24390 \\ 4\frac{4}{4} & \cdot 24442 \\ 4\frac{4}{4} & \cdot 24442 \\ 4\frac{4}{4} & \cdot 24495 \end{array}$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$ \begin{array}{c} 6 \\ 6 \\ 7 \\ 7 \\ 5 \\ 3 \\ 3 \\ 5 \\ 3 \\ 5 \\ 3 \\ 3 \\ 5 \\ 3 \\ 3$		
$\begin{array}{r} 45 & 5.14790 \\ 46 & .14842 \\ 47 & .14888 \\ 48 & .14934 \\ 49 & .14980 \end{array}$		$\begin{array}{c} 5\overline{3} \\ 17596 \\ 5\overline{3} \\ 17640 \\ 5\overline{3} \\ 17684 \end{array}$	$\begin{array}{c c} 4\overline{4} & & & & \\ \hline 9 \cdot 24547 \\ 4\overline{4} & & & & \\ 4\overline{4} & & & & \\ 24756 \end{array}$	52 52 52 52 46 52 47 52 48 52 48 52 49	44 6 4 4 4 4		
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$46 + 21750 \\ 45 + 21803 \\ -21857 \\ 45 + 21857 \\ -21857 $	$\begin{array}{c} 53\\ 53\\ 53\\ 53\\ 53\\ 53\\ 53\\ 53\\ 53\\ 53\\$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{array}{c} 52 \\ 52 \\ 52 \\ 52 \\ 52 \\ 52 \\ 52 \\ 52 $	$\begin{array}{cccccccccccccccccccccccccccccccccccc$		
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{array}{c} 46 \\ 9 \cdot 21910 \\ \cdot 21963 \\ 45 \\ \cdot 22016 \\ 45 \\ \cdot 22070 \\ \cdot 22123 \end{array}$	$\begin{array}{c} 53\\ 53\\ 53\\ 53\\ 53\\ 53\\ 53\\ 53\\ 53\\ 53\\$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{array}{c} 3 \\ 10 \\ 7 \\ 20 \\ 14 \\ 8 \\ 14 \\ 6 \\ 22 \\ 22 \\ 22 \\ 22 \\ 0 \\ 3 \\ 5 \\ 5 \\ 37 \\ 1 \\ 36 \\ 6 \end{array}$		
009.15483	<b>D</b> Log. Exs.	53 9.18170 D Lg. Vers.	$\frac{44}{D} \frac{9.2532\overline{8}}{\text{Log.Exs.}}$	$\frac{52}{D}$ $\frac{60}{\prime}$	P. P.		

<b>A'</b>	A'ABLE VIII.—LOGARITHMIC VERSED SINES AND EXTERNAL SECANTS. 32° 33°											
,	Lg. Vers.		Log.Exs.	D	Lg. Vers.	D	Log.Exs.		1	P. P.		
<b>1123457891112345789111234156789111234156789101111111111111</b>	9.18170           .18214           .18214           .18214           .18214           .18302           .183302           .183304           .18346           9.18390           .18434           .18454           .18526           .18556           9.18610           .18654           .18785           9.18872           .18876           .18050           .18050           .18050           .19000           .19177           .19221           9.19221           9.19221           9.19221           9.19221           9.19235           .19335	44444 444444 44444 44444 44444 44444 4444	$\begin{array}{r} 9.25328\\ -25328\\ -25380\\ -25484\\ -25536\\ -25484\\ -25536\\ -25588\\ -25588\\ -25588\\ -25588\\ -25588\\ -25588\\ -25588\\ -25588\\ -25899\\ -25847\\ -25899\\ -25847\\ -25899\\ -26052\\ -26052\\ -26052\\ -26052\\ -26052\\ -26518\\ -26570\\ 9.26570\\ -26578\\ -26578\\ -26578\\ -26578\\ -26572\\ -26578\\ -26572\\ -26578\\ -26572\\ -26578\\ -26572\\ -26572\\ -26578\\ -26572\\ -26578\\ -26572\\ -26578\\ -26572\\ -26578\\ -26572\\ -26578\\ -26572\\ -26578\\ -2657$		$\begin{array}{r} \hline 9.2077\overline{1}\\ 20814\\ 20856\\ 20899\\ 20942\\ 9.20942\\ 9.20947\\ 21065\\ 21027\\ 21065\\ 21027\\ 21056\\ 21027\\ 21056\\ 21239\\ 21324\\ 21324\\ 21326\\ 9.21236\\ 9.21236\\ 21324\\ 21326\\ 21326\\ 21577\\ 9.21620\\ 21652\\ 21577\\ 9.21620\\ 2176\\ 2178\\ 9.21872\\ 2178\\ 9.21872\\ 21914\\ 21956\\ 21872\\ 21914\\ 21856\\ 21872\\ 21872\\ 21872\\ 21914\\ 21856\\ 21872\\ 21872\\ 21872\\ 21914\\ 21856\\ 21872\\ 21872\\ 21872\\ 21872\\ 21886\\ 2188$	422 422 422 422 422 422 422 422 422 422	9.28412 .28463 .28564 .28564 .28564 .28564 .28665 9.28665 9.28665 .28778 .28768 .28870 .28970 .29072 .29072 .29072 .292375 9.29426 .29375 9.29426 .295777 .295777 .295777 .295777 .295777 .295777 .295777	55100000000000000000000000000000000000	0 12334 567789 10112134 1567789 2022234 256728 2222324 256728	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$		

9.29930 .29980

.30030

9.3018<u>1</u> .3023<u>1</u> .30282 .3038<u>2</u> .3038<u>2</u>

9.30432 .30482 .30533 .30583

. 30633

9 · 30683 · 30733 · 30783 · 30783 · 30833 · 30883

 $\begin{array}{r} 9.3093\overline{3} \\ .3098\overline{3} \\ .3103\overline{3} \\ .3108\overline{3} \\ .3113\overline{3} \end{array}$ 

9.31183.31233 .31283 .31333 .31333 .31383

Log.Exs.

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P. P.

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30

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4.4 5.1 5.8

 $\begin{array}{c} \mathbf{5} & \mathbf{5} \cdot \mathbf{8} \\ \mathbf{9} & \mathbf{6} \cdot \mathbf{6} \\ \mathbf{10} & \mathbf{7} \cdot \mathbf{2} \\ \mathbf{20} & \mathbf{14} \cdot \mathbf{6} \\ \mathbf{14} \cdot \mathbf{5} \\ \mathbf{30} & \mathbf{22} \cdot \mathbf{0} \\ \mathbf{21} \cdot \mathbf{7} \\ \mathbf{40} & \mathbf{29} \cdot \mathbf{3} \\ \mathbf{29} \cdot \mathbf{0} \\ \mathbf{50} & \mathbf{36} \cdot \mathbf{6} \\ \mathbf{36} \cdot \mathbf{2} \end{array}$ 

 $\begin{array}{c} 4\overline{2} \\ 4 \cdot \overline{2} \\ 4 \cdot \overline{9} \\ 5 \cdot \overline{6} \end{array}$ 4.2 4.2 4.9

 $\begin{array}{r}
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 28.3 \\
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41 41

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D

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9. g. Vers.

.19395

.19438

9.19698

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.19870

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9 · 20343 · 20386 · 20429 · 20472

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2077]

9.20129

9.19914

9.19481

 $4\overline{3} \\ 4\overline{3}$ 

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43

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42

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 $\boldsymbol{D}$ 

.26776

.26827

·26930 ·26981

·27032 ·27084

9 · 27135 · 27186 · 27238 · 27289 · 27340

9 · 27391 · 27443 · 27494 · 27545 · 27596

·27647 ·27698 ·27749 ·27800 ·27852

9.27903

.27954

·28005 ·28056

.28107

9 · 28157 • 28208 • 28259 • 28310 • 28361

9.28412

Log. Exs.

9.26878

·21830 ·21872 ·21914 ·21956

9.22040 .22082 .22124 .22166 .22208

9 · 22250 · 22292 · 22334 · 22376 · 22417

9 · 22459 · 22501 · 22543 · 22584 · 22626

9 · 22668 · 22709 · 22751 · 22792 · 22834

9 · 22876 · 22917 · 22959 · 23000 · 23042

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9.23290

Lg. Vers.

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'	Lg. Vers.	D	Log.Exs.	D	Lg. Vers.	D	Log.Exs.	D	1	P. P.
· 01234 56789 011334	Lg, Vers. 9.23290 23331 23372 23414 23455 9.23496 23537 235579 23661 9.23702 23743 23784 23825 23826	$\begin{array}{c} 4\overline{1} \\ 41 \\ 41 \\ 41 \\ 41 \\ 41 \\ 41 \\ 41 \\ $	Log. Exs., 9.31432 .31532 .31532 .31582 .31582 .31681 .31781 .31781 .31881 .31883 .31883 .31883 .31880 .31980 .31980 .32029 .32029 .32129	$\begin{array}{c} 50\\ 50\\ 9\\ 4\\ 5\\ 4\\ 5\\ 4\\ 5\\ 4\\ 5\\ 4\\ 5\\ 4\\ 5\\ 9\\ 5\\ 4\\ 9\\ 5\\ 4\\ 9\\ 5\\ 5\\ 5\\ 4\\ 9\\ 5\\ 5\\ 5\\ 4\\ 9\\ 5\\ 5\\ 5\\ 5\\ 5\\ 5\\ 5\\ 5\\ 5\\ 5\\ 5\\ 5\\ 5\\$		$\begin{array}{r} 40 \\ 40 \\ 40 \\ 40 \\ 40 \\ 40 \\ 39 \\ 40 \\ 40 \\ 39 \\ 40 \\ 40 \\ 39 \\ 40 \\ 40 \end{array}$	Log. Exs. 9.34395 .34444 .34492 .34541 .34590 9.34639 .34638 .34737 .34785 .34784 9.34883 .34883 .34832 .34832 .34830 .340200 .340200000000000000000000000000000000000	49 49 49 49 49 49 49 49 49 49 49 49 49 4	, 0 1 2 3 4 5 6 7 8 9 10 11 12 13 14	$\begin{array}{cccccccccccccccccccccccccccccccccccc$
15 16 17 18 19 20 21 22 23 24 25 27 28	$\begin{array}{r} \hline 9 \cdot 23907 \\ \cdot 23948 \\ \cdot 23983 \\ \cdot 24030 \\ \cdot 24030 \\ \cdot 24071 \\ \hline 9 \cdot 24112 \\ \cdot 24153 \\ \cdot 24154 \\ \cdot 24235 \\ \cdot 24275 \\ \hline 9 \cdot 24316 \\ \cdot 24357 \\ \cdot 24398 \\ \cdot 24438 \\ \cdot 2448 \\ \cdot 2448 \\$	$\begin{array}{c} 41\\ 41\\ 41\\ 41\\ 40\\ 40\\ 41\\ 40\\ 40\\ 41\\ 40\\ 40\\ 41\\ 40\\ 40\\ 40\\ 40\\ 40\\ 40\\ 40\\ 40\\ 40\\ 40$	$\begin{array}{r} 9.32178\\ \cdot 32228\\ \cdot 32277\\ \cdot 32327\\ \cdot 32327\\ \cdot 32327\\ \cdot 32476\\ \cdot 32476\\ \cdot 32476\\ \cdot 32575\\ \cdot 32575\\ \cdot 32673\\ \cdot 32673\\ \cdot 32772\\ \cdot 32772\\ \cdot 3282772\\ \cdot 328222\end{array}$	49999999999999999999999999999999999999	$\begin{array}{r} \hline 9.26330\\ .26370\\ .26409\\ .26449\\ .26449\\ .26568\\ .26568\\ .26668\\ .26647\\ \hline 9.26726\\ .26766\\ .26806\\ .26845\\ \end{array}$	39090999909999999999999999999999999999	9.35127 .35175 .35224 .35273 .35321 9.35370 .35419 .35516 .35564 9.35661 9.35661 .355663 .35661 .355663 .35663	498988 898888 44444444444444444444444444	15 16 17 18 19 20 21 22 23 24 25 26 27 28	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
29 30 31 32 33 34 35 36 37 38 39 40 41 42 43	24479 9.24520 24561 24601 24642 24642 24682 9.24723 9.24723 24764 24804 24845 24885 9.24926 24986 24906 25007 250047	$\begin{array}{c} 4\bar{0} \\ 4\bar{1} \\ 4\bar{0} \\$	<u>-32871</u> 9.32920 .32970 .33019 .33069 <u>.33118</u> 9.33167 .33216 .33266 .33315 <u>.33364</u> 9.33413 .33463 .33463 .33512 .33551	499 499 499 499 499 499 499 499 499 499	$\begin{array}{r} \underline{.26885}\\ \underline{9.26924}\\ \underline{.26964}\\ \underline{.27082}\\ \underline{.27082}\\ \underline{.27082}\\ \underline{.27082}\\ \underline{.27082}\\ \underline{.27082}\\ \underline{.27239}\\ \underline{.27236}\\ \underline{.27238}\\ \underline{.27357}\\ \underline{.27386}\\ \underline{.27386}\\ \underline{.2734557}\\ \underline{.2734557}\\ \underline{.27485}\\ \underline{.2748557}\\ \underline{.274855757}\\ \underline{.27485757}\\ \underline{.27485757}\\ \underline{.274855757}\\ .2748575$	00000000000000000000000000000000000000		44888888888888888888888888888888888888	$\begin{array}{c} 29\\ 30\\ 31\\ 32\\ 33\\ 3\\ 3\\ 3\\ 3\\ 3\\ 3\\ 3\\ 3\\ 3\\ 3\\ 3\\ 3$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
44 45 46 47 48 49 551 552 554 556 558	25087 9 25128 25168 25209 25249 25289 9 25329 25370 25410 25410 25490 9 25531 25591 25591 25611 25651	$\begin{array}{c} 40 \\ 40 \\ 40 \\ 40 \\ 40 \\ 40 \\ 40 \\ 40 $	<u>- 33610</u> 9 3365 <u>9</u> 33708 33758 33856 9 33905 33954 34003 34003 34052 - 34100 9 34150 - 34199 34248 34248	49 49 49 49 49 49 49 49 49 49 49 49 49 4	<u>27475</u> 9.27514 27553 27593 27631 <u>27631</u> <u>27670</u> 9.27709 27749 27788 27882 27886 9.27982 27984 27982 27982 28021	3 3 3 3 3 3 3 3 3 3 3 3 3 3	<u>36533</u> 9.36581 9.36629 36629 36678 36726 <u>36774</u> 9.36822 36870 36919 369697 <u>37015</u> 9.37063 <u>37115</u> 377207	48 48 48 48 48 48 48 48 48 48 48 48 48 4	$\begin{array}{c c} 44\\ 45\\ 46\\ 47\\ 48\\ 9\\ 50\\ 52\\ 53\\ 5\\ 55\\ 5\\ 5\\ 5\\ 5\\ 5\\ 5\\ 5\\ 5\\ 5\\ 5\\ 5$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
59 60	<u>·25691</u> <u>9·25731</u> Lg. Vers.	40 40 D	<u>.34346</u> 9.34395 Log.Exs.	49 49 D	28060 9 28099 Lg. Vers.	39 39 D	<u>- 37255</u> 9 - 37303 Log.Exs.	48 48 D	<u>59</u> 60 ′	30 19.2 40 25.6 50 32.1 P. P.

	36	5			3	7-			
' Lg. Vers		Log.Exs.	D	Lg. Vers.	D	Log. Exs.	D	1	P. P.
0 9.2809 1 .2813 2 .2817 3 .2881 4 .2825	8 38 7 38 6 39 5 39	9.37303 .37352 .37400 .37448 .37496	$4\overline{8} \\ 48 \\ 48 \\ 48 \\ 48 \\ 48 \\ 48 \\ 48 \\ $	9.30398 .30436 .30474 .30511 .30549	37 38 37 37	$9.4016\overline{3}$ .40210 .40258 .40305 .40352	47 47 47 47	0 1 2 3 4	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
59.2829 6.2833 7.2837 8.2841 9.2844	3 38 3 39 2 38 1 39 3 39 3 9 3 9 3 9 3 9 3 9 3 9 3 9 3 9	9.37544 .37592 .37640 .37687 .37735	48 48 48 47 48	9.30587 .30624 .30662 .30700 .30737	38 37 37 37 38 37	9 · 40399 • 40447 • 40494 • 40541 • 40588	47 47 47 47 47	5 6 7 8 9	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	7 6 4 3 3 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8	9.37783 .37831 .37879 .37927 .37975 9.38023	48 48 48 48 47 48	9.30775 .30812 .30850 .30887 .30925 9.30962	377 377 377 377 377 377 377	9.40635 .40682 .40730 .40777 .40824 9.40871	47 47 47 47 47 47	10 11 12 13 14 15	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
$\begin{array}{c} 16 \\ \cdot 2871 \\ 17 \\ \cdot 2875 \\ 18 \\ \cdot 2879 \\ \underline{19} \\ \cdot 2883 \\ 20 \\ 9 \\ \cdot 2887 \end{array}$	9 38 7 38 6 39 38 39 38 39 38	.38071 .38119 .38166 .38214 9.38262	48 48 47 48 47	.31000 .31037 .31075 .31075 .31112 9.31150	37 37 37 37 37 37 37	.40918 .40965 .41012 .41059 9.41106	47 47 47 47 47 47	16 17 18 19 20	20 15.8 15.6 30 23.7 23.5 40 31.6 31.3 50 39.6 39.1
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$     \begin{array}{c}       38 \\       08 \\       38 \\       38 \\       38 \\       7 \\       38 \\ $		48 47 48 47 48	·31187 ·31224 ·31262 ·31299	37 37 37 37 37	$ \begin{array}{r} \cdot 4115\overline{3} \\ \cdot 41200 \\ \cdot 41247 \\ \cdot 41294 \\ \end{array} $	47 47 47 47 47	21 22 23 24	46 6  4.6 7  5.4 8  6.2 9  7.0
25 9 2906 26 2910 27 2914 28 2918 29 2921	3888818 3888818 388818 3	9.38501 .38548 .38596 .38644 .38692	47 48 47 48	$\begin{array}{r}9.3133\overline{6}\\.31374\\.31411\\.3144\underline{8}\\.3144\underline{8}\\.31485\end{array}$	37 37 37 37 37 37 37	$\begin{array}{r}9.41341\\.41383\\.41435\\.41435\\.41482\\.41529\end{array}$	47 47 47 47	25 26 27 28 29	10, 7.7 20, 15.5 30, 23.2 40, 31.0 50, 38.7
<b>30</b> 9 · 2925 31 · 2929 32 · 2933 33 · 2937 34 · 2941	75 38 38 38 38 38 38 38 38 38 38 38 38 38	9.38739 .3878 <u>7</u> .3883 <u>4</u> .38882 .38930	47 47 47 48 47 47	$\begin{array}{r}9.31523\\.31560\\.31597\\.31634\\.31671\end{array}$	37 37 37 37	.41700	47 47 4 <u>7</u> 46	30 31 32 33 34	$\begin{array}{c} 39 & 3\overline{8} \\ 6 & 3 \cdot 9 & 3 \cdot \overline{8} \\ 7 & 4 \cdot 5 & 4 \cdot 5 \\ 8 & 5 \cdot 2 & 5 \cdot \overline{1} \\ 9 & 5 \cdot \overline{8} & 5 \cdot 8 \end{array}$
35         9 · 2944           36         · 2948           37         · 2959           38         · 2956           39         · 2960	8 38 7 38 5 38 3 38	9.38977 .39025 .39072 .39120 .39168	47 47 48 47 47 47	9.31708 .31746 .31783 .31783 .31820 .31857	37 37 37 37	$     \begin{array}{r}             9.41810 \\             \cdot 41857 \\             \cdot 41904 \\             \cdot 41951 \\             \underline{.41998} \\             \underline{.41998}         $	47 46 47 47	35 36 37 38 39	10 6.5 6.4 20 13.0 12.8 30 10.5 19.2 40 26.0 25.6 50 32.5 32.1
40 9 · 2963 41 · 2963 42 · 2973 43 · 2975 44 · 2975	9 38 7 38 5 38 4 38	$\begin{array}{r}9.3921\overline{5}\\.3926\underline{3}\\.39310\\.3935\underline{8}\\.39405\end{array}$	48 47 47 47 47	.31968	37 37 37 37 37	42044 4209] 42138 42188 42188 4228]	47 46 47 46	40 41 42 43 44	$\begin{array}{c} 38 & 37 \\ 6 & 3 \cdot 8 & 3 \cdot 7 \\ 7 & 4 \cdot 4 & 4 \cdot 4 \\ 5 \cdot 0 & 5 \cdot 0 \end{array}$
45 9.298 46 .298 47 .299 48 .299 49 .299	8 38 6 38 4 38 2 38	9.39453 .39500 .39548 .39595 .39642	47 47 47 47 47 47	·32190 ·32227	37	• 42272 • 42323 • 42372 • 42418 • 42465	40 47 46 47	45 46 47 48 49	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
$\begin{array}{c} 50 & 9.3003 \\ 51 & .3003 \\ 52 & .3003 \\ 53 & .3013 \\ 54 & .3013 \end{array}$	57 38 55 38 33 38 1 38		47 47 47 47 47 47	9.32263 .32300 .32337 .32374 .32374 .32411	37 36 37	4251 4255 4260 42652 42652 42698	40     41     42     46     46     46     46     46     46     46	$50 \\ 51 \\ 52 \\ 53 \\ 54$	$ \begin{array}{c} \overline{50} 31.\overline{6} 31.\overline{2}\\ 37 & 3\overline{6}\\ 6  3.7  & 3.\overline{6}\\ 7  & 4.3\\ 8  & 4.\overline{9}\\ 4.\overline{8}\\ 4.\overline{8} \end{array} $
55 9.3020 56 .3024 57 .3021 58 .303 59 .303	17 37 35 38 35 37 36 38	9.39927 .39974 .40021 .40069 .40116	47 47 47 47 47	9.32447 .32484 .32521 .32558 .32594	36 37 36 37 36 37 36	$     \begin{array}{r}             42740 \\             42792 \\             42838 \\             42885 \\             42931 \\         \end{array}     $	4 <u>1</u> 4 <u>6</u> 4 <u>6</u>	55 56 57 58 59	$\begin{array}{c} 0 & 5 \cdot 5 \\ 10 & 6 \cdot 1 \\ 20 & 12 \cdot 3 & 12 \cdot 1 \\ 30 & 18 \cdot 5 & 18 \cdot 5 \\ 40 & 24 \cdot 6 & 24 \cdot 3 \\ 50 & 18 & 50 \cdot 4 \end{array}$
<u>60 9 . 303</u> <u> </u>		9 · 40163 Log. Exs.	47 D	9 3263 <u>1</u> Lg. Vers.	37 D	<u>9.42978</u> Log.Exs.	40 D	<u>60</u> ´	<u>50130-8130-4</u> P. P.

TA	TABLE VIII.—LOGARITHMIC VERSED SINES AND EXTERNAL SECANTS.         38°       39°									
,	Lg. Vers.	Д	Log.Exs.	D	Lg. Vers.	D	Log.Exs.	D		P. P.
0 1 2 3 4	$\begin{array}{r} 9.3263\bar{1}\\.32668\\.3270\underline{4}\\.3274\bar{1}\\.32778\end{array}$	36 36 37 36	9.42978.43024.43071.43118.43164	46 47 46 46	$\begin{array}{r} 9.34802\\ .34837\\ .34873\\ .34873\\ .34909\\ .34944\end{array}$	35 36 35 35 35 35 35 35	$\begin{array}{r} 9.45752 \\ .45797 \\ .45843 \\ .45889 \\ .45935 \end{array}$	45 46 46 46	0 1 2 3 4	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
5 6 7 8 9	$9.3281\overline{4} \\ .32851 \\ .32888 \\ .32924 \\ .32961$	366 3766 366 366 36	9.43211.43257.43304.43350.43396	4 <u>6</u> 4 <u>6</u> 4 <u>6</u> 4 <u>6</u> 4 <u>6</u> 4 <u>6</u>	9.34980 .35016 .35051 .35087 .35122	36 36 35 5 5 5 5 35 5 35 35 35	9.45981 .46027 .46073 .46118 .46164	45 46 45 45 46 46	5 6 7 8 9	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
$10 \\ 11 \\ 12 \\ 13 \\ 14 \\ 14 \\ 14 \\ 10 \\ 10 \\ 10 \\ 10 \\ 10$	$ \begin{array}{r} \cdot 33034\\ \cdot 33070\\ \cdot 33107\\ \cdot 33143\end{array} $	366 366 366 366 36 36	9.43443 .43489 .43536 .43582 .43629 .43629	466 466 466 466 466	$9 \cdot 35158 \\ \cdot 35193 \\ \cdot 35229 \\ \cdot 35264 \\ \cdot 35300 \\ \hline 2 \cdot 3500 \\ \hline 2$	3555 355 355 355 355 355 355 355 355 35	9.46210.46256.46302.46347.46393	45 46 45 46 45	10 11 12 13 14	$\begin{array}{cccccccccccccccccccccccccccccccccccc$
15 16 17 18 <u>19</u>	9.33180 .33216 .33252 .33289 .3325	36 36 36 36 36 36	9.43675 .43721 .43768 .43814 .43861	46 46 46 46 46	$9.3533\overline{5} \\ .35370 \\ .35406 \\ .35441 \\ .35477 \\ .3577 $	35 35 35 35 35 35 35	9.46439 .46485 .46530 .46576 .46622	46 45 46 45 46	15 16 17 18 19	10 7.6 7.6 2015.315.1 3023.022.7 4030.630.3 5038.337.9
20 21 22 23 24	-33398 -33434 -33470 -33507	36 36 36 36 36 36 36	9.43907 .43953 .43999 .44046 .44092 .44092	46 46 46 46 46 46	9.35512 .35547 .35583 .35618 .35653	35 35 35 35 35 35	9.46668 .46713 .46759 .46805 .46850	45 45 46 45 45 45	20 21 22 23 24	45 6 4.5 7 5.2 8 6.0 9 6.7
25 26 27 28 29	9.3354 <u>3</u> .3357 <u>9</u> .33615 .33652 .33688	36 36 36 36 36 36 36 36	$9.4413\overline{8} \\ .44185 \\ .44231 \\ .44277 \\ .44323 \\ .4432 \\ .4442 \\ .4432 \\ .4432 \\ .4432 \\ .4432 \\ .4432 \\ .4432 \\ .4432 \\ .443$	46 46 46 46 46	9.35689.35724.35759.35794.35829	35 35 35 35 35 35	9.46896 .46942 .46987 .47033 .47078	4 <u>6</u> 4 <u>5</u> 4 <u>5</u> 4 <u>5</u> 4 <u>5</u> 4 <u>6</u>	25 26 27 28 29	$ \begin{array}{c} 10 & 7.5 \\ 20 & 15.0 \\ 30 & 22.5 \\ 40 & 30.0 \\ 50 & 37.5 \\ \end{array} $
30 31 32 33 34	·33760 ·33796 ·33833 ·33869	36 36 36 36 36 36	9.44370 .44416 .44462 .44508 .44554		9.35865 .35900 .35935 .35970 .36005	35 35 35 35 35 35	9.47124 .47170 .47215 .47261 .47306	45 45 45 45 45 46	30 31 32 33 34	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
35 36 37 38 39	9.33905.33941.33977.34013.34049	36 36 36 36 36 36	9.44601 .44647 .44693 .44739 .44785	46 46 46 46 46	9.36040 .36076 .36111 .36146 .36181	35 35 35 35 35 35	$9.4735\overline{2} \\ .47398 \\ .4744\overline{3} \\ .4744\overline{3} \\ .47489 \\ .4753\overline{4}$	45 45 45 45	35 36 37 38 <u>39</u>	$\begin{array}{c} 5 & 5 & 5 & 5 \\ 10 & 6 & 1 \\ 20 & 12 \cdot 3 & 12 \cdot 1 \\ 20 & 12 \cdot 3 & 12 \cdot 1 \\ 30 & 18 \cdot 5 & 18 \cdot 2 \\ 40 & 24 \cdot 6 & 24 \cdot 3 \\ 50 & 30 \cdot 8 & 30 \cdot 4 \end{array}$
40 41 42 43 44	9.34085.34121.34157.34193.34229	36 36 36 36 36	$9.4483\overline{1}$ .44877 .44924 .44970 .45016	46 46 46 46 46	9.36216 .36251 .36286 .36321 .36356	35 35 35 35 35 85	$\begin{array}{r}9.47580\\ \cdot 47625\\ \cdot 47671\\ \cdot 47716\\ \underline{}.47716\end{array}$	4 <u>5</u> 4 <u>5</u> 4 <u>5</u> 4 <u>5</u> 4 <u>5</u> 4 <u>5</u> 4 <u>5</u>	$\begin{array}{c} 40 \\ 41 \\ 42 \\ 43 \\ 44 \end{array}$	$\begin{array}{cccc} 36 & 3\overline{5} \\ 6 & 3 \cdot 6 & 3 \cdot \overline{5} \\ 7 & 4 \cdot 2 & 4 \cdot \overline{1} \\ 8 & 4 \cdot 8 & 4 \cdot \overline{7} \end{array}$
45 46 47 48 49	9.34265 .34301 .34337 .3437 <u>3</u> .34408	36 36 3 <u>6</u> 3 <u>5</u> 35	9.45062 .45108 .45154 .45200 .45246	46 46 46 46 46	9.36391 .36426 .36461 .36495 .36530	35 35 34 35 35 35	9.47807.47852.47898.47943.47989.47989	45 45 45 45 45 45	45 46 47 48 49	$\begin{array}{c} 9 & 5.4 & 5.3 \\ 10 & 6.0 & 5.9 \\ 20 & 12.0 & 11.8 \\ 30 & 18.0 & 17.7 \\ 40 & 24.0 & 23.6 \end{array}$
50 51 52 53 54	$\begin{array}{r} 9.3444\bar{4} \\ .34480 \\ .34516 \\ .34552 \\ .34587 \end{array}$	36 35 36 35	9.45292 .45338 .45384 .45430 .45476	$     \begin{array}{r}       46 \\       46 \\       46 \\       46     \end{array} $	9.36565 .36600 .36635 .36670 .36705	35 35 35 35 35 35 35 35 35	$9.4803\overline{4} \\ .48080 \\ .48125 \\ .48170 \\ .48216$	45 45 45 45 45 45 45	50 51 52 53 54	$\begin{array}{c} \bar{5}0 3\bar{0},\bar{0} \bar{2}\bar{9},\bar{6} \\ , 35 & 3\bar{4} \\ \bar{6} 3,5 3,\bar{4} \\ 7 4,1 4,0 \\ 8 4,\bar{6} 4,6 \\ 9 5,2 5,2 \end{array}$
55 56 57 58 59	9.34623 .34659 .34695 .34730 .34766	36 35 36 35 36 36	9.45522 .45568 .45614 .45660 .45706	46 46 46 46 46	9 36739 36774 36809 36844 36878	35 34 3 <u>5</u> 34	9 · 48261 · 48306 · 48352 · 48397 · 48442	$45 \\ 45 \\ 45 \\ 45 \\ 45$	55 56 57 58 59	$\begin{array}{c} c & 4 \cdot 6 \\ 9 & 5 \cdot 2 \\ 10 & 5 \cdot 8 \\ 20 & 11 \cdot 6 \\ 30 & 17 \cdot 5 & 17 \cdot 2 \\ 40 & 23 \cdot 3 & 23 \cdot 0 \end{array}$
<u>60</u>	9.34802 Lg.Verst	35 D	9.45752 Log.Exs.	46 D	9.36913 Lg. Vers.	35 D	9 · 48488 Log.Exs.	$\frac{4\overline{5}}{D}$	<u>60</u> ′	50129.1128.7 P. P.

# $\tilde{T}$ ABLE VIII.—LOGARITHMIC VERSED SINES AND EXTERNAL SECANTS.40°41°

<u>′</u>	Lg. Vers.	D	Log.Exs.	D	Lg. Vers.	D	Log.Exs.	D	•	P. P.
0 1 2 3 4	9.36913 .36948 .36982 .37017 .37052	34 34 35 35 34	9.48488 .48533 .48578 .48624 .48669	45 45 45 45	9.38968 .39002 .39035 .39069 .39103	34 33 34 33 33	9.51190 .51235 .51279 .51324 .51369	$45 \\ 44 \\ 45 \\ 44 \\ 44$	0 1 2 3 4	45 45
5 6 7 8	9.3708 <u>6</u> .37121 .37156 .37190	345 354 34 34 34 34	$9.4871\overline{4}$ .48759 .48805 .48850	45 45 45 45 45	9.39137.39170.39204.39238	34 33 33 34 33 33 33 33	$9.51414 \\ .51458 \\ .51503 \\ .51548$	4 <u>5</u> 44 4 <u>5</u> 44 44	5 6 7 8	$\begin{array}{cccccccccccccccccccccccccccccccccccc$
$\frac{9}{10}$ $\frac{11}{12}$ $\frac{12}{13}$	.37225 9.37259 .37294 .37328 .37363	34444 33333333333333333333333333333333	$     \underbrace{ \frac{.48895}{9.48940} }_{.48986} \\ .48986 \\ .49031 \\ .49076 $	45 45 45 45 45	<u>.39271</u> 9.39305 .39339 .39372 .39406	34 34 33 33 33 33 33 33 33 33 33 33 33 3	<u>.51592</u> 9.51637 .51682 .51726 .51771	45 44 44 45 44	9 10 11 12 13	10 7.6 7.5 20 15.1 15.0 30 22.7 22.5 40 30.3 30.0 50 37.9 37.5
14 15 16 17 18 19	<u>.37397</u> 9.37432 .37466 .37501 .37535 .37570	5 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3	$      .49121 \\ 9.49166 \\ .49211 \\ .49257 \\ .49302 \\ .49347 \\ .49347 \\ $	45 45 45 45 45 45	<u>-39439</u> 9-39473 -39507 -39540 -39574 -39607	34 34 33 33 33 33 33 33 33	$     \begin{array}{r} \cdot 51816 \\         9 \cdot 5186 \\         \overline{0} \\         \cdot 5190 \\         \cdot 5195 \\         \cdot 5195 \\         \cdot 51994 \\         \cdot 52039     \end{array} $	44 45 45 44 44 44	14 15 16 17 18 19	$\begin{array}{cccccccccccccccccccccccccccccccccccc$
20 21 22 23 24	9 · 37604 · 37639 · 37673 · 37707 · 37742	344 344 344 34 3 3 3 3 3 3 3 3 3 3 3 3	9.49392 .49437 .49482 .49527 .49572	45 45 45 45 45	9.39641 .39674 .39708 .39708 .39741 .39774	00000000000000000000000000000000000000	9.52084 .52128 .52173 .52217 .52262	45 44 44 44 44	$   \begin{array}{c}     10 \\     20 \\     21 \\     22 \\     23 \\     24   \end{array} $	$\begin{array}{cccccccccccccccccccccccccccccccccccc$
	9.37776 .37810 .37845 .37879 .37913	34 34 34 34 34 34 34 34	9.49618 .49663 .49708 .49753 .49798	45 45 45 45 45 45 45	$\begin{array}{r}9.39808\\.39841\\.39875\\.39875\\.39908\\.39941\end{array}$	101030303 0 0 0 0 0 0 0 0 0 0 0 0	9.52306 .52351 .52396 .52440 .52485	45 44 44 44 44	25 26 27 28 29	$\begin{array}{cccccccccccccccccccccccccccccccccccc$
31 32 33 34	9.37947 .37982 .38016 .38050 .38084	34 34 34 34 34 34 34	9.49843 .49888 .49933 .49978 .50023	45 45 45 45 45 45	9.39975 .40008 .40041 .40075 .40108	1010 00100 00 00100 00 00100 00	9 · 52529 · 52574 · 52618 · 52663 · 52707	44 44 44 44 44	30 31 32 33 34	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
36 37 38 39	$9.3811\overline{8}$ .38153 .38187 .38221 .38255	34 34 34 34 34 34 34	9.50068 .50113 .50158 .50203 .50248	45 45 45 45	$\begin{array}{r} 9.40141\\ .40175\\ .40208\\ .40241\\ .40274\end{array}$	33 33 33 33 33 33 33 33 33 33	9 · 52752 · 52796 · 52841 · 52885 · 52930	44 44 44 44	35 36 37 38 39	$\begin{array}{cccc} 34 & 3\overline{3} \\ 6 & 3 \cdot 4 & 3 \cdot \overline{3} \\ 7 & 3 \cdot 9 & 3 \cdot 9 \end{array}$
40 41 42 43 44	9 · 38289 · 38323 · 38357 · 38391 · 38425	34 34 34 34	9 · 50293 · 50338 · 50383 · 50427 · 50472	45 45 45 44 45	$\begin{array}{r}9.4030\overline{7}\\.40341\\.40374\\.4040\overline{7}\\.4040\overline{7}\\.40440\end{array}$	3 <u>3</u> 33 33 33 33 33 33 33 33 33 33	9.52974 .53018 .53063 .53107 .53152	44 44 44 44 44	44	$\begin{array}{c} 8 & 4 \cdot \overline{5} & 4 \cdot \overline{4} \\ 9 & 5 \cdot 1 & 5 \cdot 0 \\ 10 & 5 \cdot \overline{6} & 5 \cdot 6 \\ 20 & 11 \cdot 3 & 11 \cdot \overline{1} \\ 30 & 17 \cdot 0 & 16 \cdot \overline{7} \\ 40 & 22 \cdot \overline{6} & 22 \cdot 3 \\ 50 & 28 \cdot 3 & 27 \cdot 9 \end{array}$
45 46 47 48 49	9.38459 .38493 .38527 .38561 .38561 .38595	34 34 34 34 34	9.50517 .50562 .50607 .50652 .50652 .50697	45 45 4 <u>5</u> 44 45	$9.4047\overline{3} \\ .40506 \\ .40540 \\ .40573 \\ .40606$	3 <u>3</u> 33 33 33 33	9 - 53196 - 53240 - 53285 - 53329 - 53374	44 44 44 44	45 46 47 48 49	50 22:3 27.9 33 6  3.3
50 51 52 53 54	9.38629 .38663 .38697 .38731 .38765	34 34 3 <u>4</u> 33 34	9.50742 .50787 .50831 .50876 .50921	45 45 44 45 45	9 · 40639 · 40672 · 40705 · 40738 · 40771	33 33 33 33 33 33	$\begin{array}{r} 9.53418 \\ .53462 \\ .53507 \\ .53551 \\ .53595 \end{array}$	44 44 44 44	50 51 52 53 54	7 3.8 8 4.4 9 4.9 10 5.5 20 11.0
	9.38799 .3883 <u>3</u> .3886 <u>6</u> .38900 .38934	34 34 33 34 33	9.50966 .51011 .51055 .51100 .51145	$4\overline{4} \\ 45 \\ 44 \\ 45 \\ 45 \\ 45 \\ 45 \\ -$	9 · 40804 · 40837 · 40870 · 40903 · 40936	33 33 33 33 33	9 · 53640 · 53684 · 53728 · 53773 · 53817	$44 \\ 44 \\ 44 \\ 44 \\ 44 \\ 44$	55 56 57 58 59	30 16 · 5 40 22 · 0 50 27 · 5
	9.38968 Lg. Vers.	34 D	9.51190 Log.Exs.	44 D	9.40969 Lg. Vers.	33 D	9.53861 Log.Exs.	$\frac{4\overline{4}}{D}$	<u>60</u> ′	P. P.

42°
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**43°** 

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$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	,	Lg. Vers.	D	Log.Exs.	D	Lg, Vers,	D	Log.Exs.	D	'	P. P.
$ \begin{array}{c} 13 \\ 14 \\ -41426 \\ 15 \\ 9 \\ -41446 \\ 15 \\ 9 \\ -41446 \\ 13 \\ 16 \\ -41443 \\ 33 \\ -5456 \\ 18 \\ -41483 \\ 33 \\ -5456 \\ 32 \\ -5456 \\ 34 \\ -4148 \\ 33 \\ -5456 \\ 32 \\ -5456 \\ 34 \\ -4148 \\ 33 \\ -5456 \\ 32 \\ -5466 \\ -41 \\ -4336 \\ 33 \\ -5456 \\ 32 \\ -5466 \\ -44 \\ -4346 \\ -4346 \\ -4346 \\ -57723 \\ -57723 \\ -57723 \\ -44 \\ -4376 \\ -57723 \\ -57723 \\ -44 \\ -4376 \\ -57723 \\ -57723 \\ -44 \\ -4376 \\ -57723 \\ -57723 \\ -44 \\ -4436 \\ -57723 \\ -57723 \\ -44 \\ -44 \\ -4436 \\ -57723 \\ -57723 \\ -44 \\ -44 \\ -44 \\ -57723 \\ -57781 \\ -45 \\ -57781 \\ -44 \\ -44 \\ -23 \\ -57781 \\ -57781 \\ -44 \\ -44 \\ -23 \\ -57781 \\ -57781 \\ -44 \\ -44 \\ -23 \\ -57781 \\ -44 \\ -44 \\ -23 \\ -57781 \\ -57781 \\ -44 \\ -24 \\ -23 \\ -57781 \\ -57781 \\ -57781 \\ -57781 \\ -57781 \\ -44 \\ -24 \\ -23 \\ -57781 \\ -57781 \\ -57781 \\ -44 \\ -24 \\ -23 \\ -57781 \\ -57781 \\ -57781 \\ -57781 \\ -44 \\ -24 \\ -23 \\ -57781 \\ -57781 \\ -57781 \\ -44 \\ -24 \\ -23 \\ -57781 \\ -57781 \\ -57781 \\ -57781 \\ -44 \\ -24 \\ -23 \\ -57781 \\ -57781 \\ -57781 \\ -57781 \\ -57781 \\ -44 \\ -24 \\ -23 \\ -57781 \\ -57781 \\ -44 \\ -24 \\ -25 \\ -57781 \\ -44 \\ -24 \\ -25 \\ -57781 \\ -57781 \\ -57781 \\ -57781 \\ -57781 \\ -57781 \\ -57781 \\ -57781 \\ -57781 \\ -57781 \\ -57781 \\ -57781 \\ -57781 \\ -57781 \\ -57781 \\ -57781 \\ -57781 \\ -44 \\ -24 \\ -28 \\ -57781 \\ -57781 \\ -57781 \\ -57781 \\ -44 \\ -28 \\ -57781 \\ -44 \\ -28 \\ -57781 \\ -$	$   \begin{array}{c}     1 \\     2 \\     3 \\     4 \\     5 \\     6 \\     7 \\     8 \\     9 \\     10 \\     11   \end{array} $	$\begin{array}{r} 9.40969\\ -41001\\ -41034\\ -41067\\ -41100\\ 9.41133\\ -41166\\ -41199\\ -41231\\ -41264\\ 9.41297\\ \end{array}$	123333 12333123 33333 233332 1233 33333 123331233 1233 33333 123331233 1233	$\begin{array}{r} 9.53861\\ \cdot 53906\\ \cdot 53990\\ \cdot 53994\\ \cdot 54038\\ 9.54038\\ \cdot 54127\\ \cdot 54127\\ \cdot 54215\\ \cdot 542215\\ \cdot 542304\\ 9.54304\\ \cdot 54348\end{array}$	$\begin{array}{r} 4\bar{4} \\ 4\bar{4} \\$	$\begin{array}{r} \hline 9.42918\\ .42950\\ .42982\\ .43014\\ .43046\\ \hline 9.43048\\ .43110\\ .43142\\ .43174\\ .43174\\ .43206\\ \hline 9.43238\\ .43270\\ \hline \end{array}$	32 32 32 32 32 32 32 32 32 32 32 32 32 3	$\begin{array}{c} 9.56505\\ .56549\\ .56637\\ .56680\\ 9.56724\\ .56680\\ 9.56724\\ .56812\\ .56812\\ .56812\\ .56899\\ 9.56943\\ .56987\end{array}$	$\begin{array}{r} 4\overline{3} \\ 44 \\ 43 \\ 44 \\ 43 \\ 44 \\ 43 \\ 44 \\ 43 \\ 44 \\ 43 \\ 44 \\ 4$	$ \begin{array}{r}1\\2\\3\\4\\5\\6\\7\\9\\10\\11\end{array} $	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
$\begin{array}{c} \frac{42}{25} & \frac{-9.1787}{9} & \frac{37}{32} & \frac{9}{9} & \frac{54966}{55010} & \frac{47}{44} & \frac{9.43717}{9} & \frac{31}{31} & \frac{157590}{557633} & \frac{43}{44} & \frac{25}{25} \\ \frac{43}{25} & \frac{3}{9} & \frac{3}{550154} & \frac{44}{44} & \frac{43779}{9} & \frac{31}{31} & \frac{557783}{57783} & \frac{43}{43} & \frac{28}{28} \\ \frac{41917}{322} & \frac{41852}{322} & \frac{32}{550126} & \frac{44}{44} & \frac{43842}{43842} & \frac{31}{577831} & \frac{557784}{43} & \frac{43}{228} & \frac{7}{7} & \frac{3}{3.8} & \frac{3}{3.2} \\ \frac{39}{21} & \frac{41917}{322} & \frac{55142}{55235} & \frac{44}{44} & \frac{43877}{43397} & \frac{31}{31} & \frac{557784}{557861} & \frac{44}{43} & \frac{3}{30} & \frac{9}{9} & \frac{4.9}{4.9} & \frac{4.9}{4.9} \\ \frac{55235}{32} & \frac{55275}{5442} & \frac{44}{4} & \frac{439874}{43937} & \frac{31}{51} & \frac{557861}{557861} & \frac{44}{43} & \frac{3}{30} & \frac{10}{10} & \frac{5}{5.5} & \frac{5}{5.4} \\ \frac{44}{23937} & \frac{3}{31} & \frac{5}{577905} & \frac{43}{43} & \frac{32}{32} & \frac{3}{31} & \frac{10}{10} & \frac{5}{5.5} & \frac{5}{5.4} \\ \frac{34}{22047} & \frac{32}{32} & \frac{555275}{55275} & \frac{44}{4} & \frac{43999}{9} & \frac{31}{51} & \frac{557861}{579492} & \frac{43}{43} & \frac{33}{32} & \frac{3}{20} & \frac{3}{11} & \frac{10}{558277} \\ \frac{55451}{44} & \frac{440026}{331} & \frac{3}{11} & \frac{558127}{58827} & \frac{43}{43} & \frac{3}{32} & \frac{3}{60} & \frac{3}{22} & \frac{3}{31} \\ \frac{36}{35} & \frac{422241}{322} & \frac{555451}{32} & \frac{44}{4} & \frac{44032}{331} & \frac{3}{58167} & \frac{58123}{43} & \frac{43}{40} & \frac{3}{22} & \frac{3}{11} \\ \frac{58227}{58277} & \frac{44}{4} & \frac{44027}{331} & \frac{3}{58167} & \frac{58123}{43} & \frac{43}{40} & \frac{3}{22} & \frac{3}{11} \\ \frac{58227}{331} & \frac{58237}{43} & \frac{43}{43} & \frac{4}{41} & \frac{3}{20} & \frac{3}{1} & \frac{3}{12} \\ \frac{58227}{42241} & \frac{3}{32} & \frac{555759}{5958} & \frac{44}{4} & \frac{44223}{331} & \frac{3}{1} & \frac{588326}{58428} & \frac{43}{43} & \frac{4}{43} & \frac{4}{43} & \frac{4}{43} \\ \frac{422241}{322} & \frac{556759}{5958} & \frac{44}{4} & \frac{44237}{331} & \frac{3}{1} & \frac{588326}{58428} & \frac{43}{43} & \frac{4}{43} & \frac{4}{44} & \frac{4}{42} \\ \frac{42237}{322} & \frac{556871}{556871} & \frac{4}{4} & \frac{44237}{331} & \frac{3}{1} & \frac{588326}{58428} & \frac{43}{43} & \frac{4}{43} & \frac{4}{42} \\ \frac{42241}{322} & \frac{556871}{32} & \frac{4}{4} & \frac{4427}{331} & \frac{588326}{43} & \frac{43}{43} & \frac{4}{43} & \frac{4}{43} & \frac{4}{43} & \frac{4}{43} \\ \frac{42226}{322} & \frac{556871}{56$	$     \begin{array}{r}       12 \\       13 \\       14 \\       15 \\       16 \\       17 \\       18 \\       19 \\       20 \\       \end{array} $	$\begin{array}{r} \cdot 41395 \\ \underline{\cdot 41428} \\ 9 \cdot 41461 \\ \underline{\cdot 41493} \\ \underline{\cdot 41526} \\ \underline{\cdot 41559} \\ \underline{\cdot 41591} \\ 9 \cdot 41624 \end{array}$	332 332 332 332 3 3 3 3 3 3 3 3 3 3 3 3	$\begin{array}{r} .54392\\ .54436\\ .54480\\ 9.54525\\ .54569\\ .54613\\ .54657\\ .54701\\ 9.54745\\ \end{array}$	$\begin{array}{c} 44 \\ 44 \\ 4\bar{4} \\ 44 \\ 4\bar{4} \end{array}$	$\begin{array}{r} .43302 \\ .43334 \\ .43365 \\ 9 .43397 \\ .43429 \\ .43461 \\ .43493 \\ .43525 \\ 9 .43557 \end{array}$	32 31 32 32 32 32 32 32 32 32 32 32	57031 57075 57118 9.57162 57206 57250 57250 572337 9.57381	$\begin{array}{c} 44\\ 43\\ 44\\ 43\\ 44\\ 43\\ 44\\ 43\\ 44\\ 43\\ 43$	$     \begin{array}{r}       12 \\       13 \\       14 \\       15 \\       16 \\       17 \\       18 \\       19 \\       20 \\       \end{array} $	$\begin{array}{cccccccccccccccccccccccccccccccccccc$
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	22 23 24 25 26 27 28 29 30	$\begin{array}{r} \cdot 41689\\ \cdot 41722\\ \cdot 41754\\ \hline 9 \cdot 41787\\ \cdot 41819\\ \cdot 41852\\ \cdot 41852\\ \cdot 41885\\ \cdot 41917\\ \hline 9 \cdot 41950\end{array}$	3 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	.54834 .54878 .54922 9.54966 .55010 .55054 .55098 .55142 9.55186	44 44 44 44 44 44 44 44	.43620 .43652 .43684 9.43715 .43747 .43747 .43779 .43810 .43842 9.43874	31 32 31 32 31 31 32 31 32 31	.57468 .57512 .57556 9.57599 .57643 .57643 .57687 .57730 .57774 9.57818	43 44 43 43 44 43 44 31 34 43 44 31 34 43 31 34 43 31 34 43 31 34 43 31 34 43 31 34 43 31 34 43 31 34 43 31 34 43 31 34 43 31 34 43 31 31 31 31 31 31 31 31 31 31 31 31 31	22 23 24 25 26 27 28 29 30	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	32 33 34 35 36 37 38 39	$\begin{array}{r} .4201\bar{4}\\ .42047\\ .42079\\ \hline 9.42112\\ .4214\bar{4}\\ .42177\\ .42209\\ .4224\bar{1}\\ \end{array}$	3 101010 010 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3	.55275 .55319 .55363 9.55407 .55451 .55495 .55539 .55583	44 44 44 44 44 44 44 44 44	$\begin{array}{r} .43937\\ .43969\\ .44000\\ 9.44032\\ .44064\\ .44095\\ .44127\\ .44158\end{array}$	$     \begin{array}{c}       31 \\       32 \\       31 \\$	.57905 .57949 .57992 9.58036 .58079 .58123 .58167 .58210 9.58254	443 433 443 443 433 443 433	32 33 34 35 36 37 38 39	$\begin{array}{c} 20   11.0   10.\overline{8} \\ 30   16.5   16.\overline{2} \\ 40   22.0   21.6 \\ 50   27.5   27.1 \\ \end{array}$ $\begin{array}{c} 32  3\overline{1} \\ 6   3.2   3.1 \\ 7   3.7 \\ 3.7 \\ 3.7 \\ 3.4 \end{array}$
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	41 42 43 44 45 46 47 48 49	$\begin{array}{r} \cdot 4230\bar{6}\\ \cdot 4233\bar{8}\\ \cdot 42371\\ \underline{\cdot 42403}\\ 9\cdot 4243\bar{5}\\ \cdot 42467\\ \cdot 42500\\ \cdot 4253\underline{2}\\ \cdot 42564\end{array}$	3212 322 322 322 322 322 322 322 322 322	55671 55715 55759 55803 55847 55890 55934 55978 56022	44 44 44 43 44 44 44 44	$\begin{array}{r} .4422\overline{1} \\ .44253 \\ .44284 \\ .44316 \\ 9.4434\overline{7} \\ .44379 \\ .44379 \\ .44410 \\ .44442 \\ .44473 \end{array}$	31 31 31 31 31	$\begin{array}{r} .5829\overline{7}\\ .58341\\ .58385\\ .58428\\ 9.58428\\ 9.58472\\ .58515\\ .58559\\ .58602\\ .58646\end{array}$	443 43 43 43 43 43 33 33 33 33 33 33 33	41 42 43 44 45 46 47 48 49	$\begin{array}{c}9 & 4.8 \\ 10 & 5.3 \\ 20 & 10.6 \\ 10.5 \\ 20 & 10.6 \\ 10.5 \\ 30 & 16.0 \\ 15.7 \\ 40 & 21.3 \\ 21.0 \\ 50 & 26.6 \\ 26.2 \\ 31 \\ 6l & 3.1 \end{array}$
00[9.42918] = [9.565005] = [9.44818] = [9.59124] = [00]	51 52 53 54 55 56 57 58 59	$\begin{array}{r} \cdot 42629 \\ \cdot 42661 \\ \cdot 42693 \\ \hline 9 \cdot 42725 \\ \hline 9 \cdot 42757 \\ \cdot 42789 \\ \cdot 42822 \\ \cdot 42824 \\ \cdot 42886 \end{array}$	32 32 32 32 32 32 32 32 32 32	$\begin{array}{r} \cdot 5611\bar{0} \\ \cdot 56154 \\ \cdot 56198 \\ \cdot 56242 \\ 9 \cdot 56286 \\ \cdot 56330 \\ \cdot 56374 \\ \cdot 56417 \\ \cdot 56461 \end{array}$	$ \begin{array}{r} 44\\ 43\\ 44\\ 44\\ 44\\ 44\\ 43\\ 44\\ 43\\ 44\\ 43\\ 44\\ 45\\ 44\\ 45\\ 44\\ 45\\ 44\\ 45\\ 44\\ 45\\ 44\\ 45\\ 44\\ 45\\ 44\\ 45\\ 44\\ 45\\ 44\\ 45\\ 44\\ 45\\ 44\\ 45\\ 44\\ 45\\ 45$	$\begin{array}{r} \cdot 4453\underline{6}\\ \cdot 44567\\ \cdot 44599\\ \cdot 44630\\ \hline 9\cdot 44661\\ \cdot 44693\\ \cdot 44724\\ \cdot 44755\\ \cdot 44787\end{array}$	31 31 31 31 31 31 31 31 31 31	$\begin{array}{r} \cdot 58733\\ \cdot 58776\\ \cdot 58820\\ \cdot 58864\\ 9\cdot 58907\\ \cdot 58951\\ \cdot 58994\\ \cdot 59037\\ \cdot 59081\\ \end{array}$	443 433 433 433 433 433 433 433 433	51 52 53 54 55 56 57 58 59	$\begin{array}{cccc} 7 & 3 \cdot 6 \\ 8 & 4 \cdot 1 \\ 9 & 4 \cdot 6 \\ 10 & 5 \cdot 1 \\ 20 & 10 \cdot 3 \\ 30 & 15 \cdot 5 \\ 40 & 20 \cdot 6 \end{array}$
							-	Contraction of the local division of the loc	_	<u>00</u>	P. P.

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,	Lg. Vers.	D	Log.Exs.	D	Lg. Vers.	D	Log.Exs.	D	,	P. P.	
01234 56789 0112	$\begin{array}{r} 9.44818\\ .44849\\ .44840\\ .44912\\ .44943\\ 9.44974\\ .45005\\ .45005\\ .45005\\ .45005\\ .45068\\ .45069\\ .9.45160\\ 9.45161\\ .05162\\ \end{array}$	31 31 31 31 31 31 31 31 31 31 31	$9.5912\overline{4}$ $5912\overline{4}$ 59211 59255 592985 593429 593429 59472 59515 9.59559 59602	4444 4444 4444 444 444 444 444	$\begin{array}{r} 9.46671\\ .46701\\ .46732\\ .46762\\ .46763\\ .46823\\ .46823\\ .46884\\ .46914\\ .46945\\ 9.46975\\ 9.46975\\ 9.46975\\ .47005\end{array}$	300 300 300 300 300 300 300 300 300 300	$\begin{array}{c} 9\cdot 6172\overline{2}\\ \cdot 6176\overline{5}\\ \cdot 61808\\ \cdot 61852\\ \cdot 61895\\ 9\cdot 61938\\ \cdot 61981\\ \cdot 62024\\ \cdot 62067\\ \hline 62110\\ 9\cdot 621536\\ \cdot 621536\\ \cdot 62239 \\ \hline \end{array}$	$\begin{array}{r} 43\\ 43\\ 43\\ 43\\ 43\\ 43\\ 43\\ 43\\ 43\\ 43\\$	0 1 2 3 4 5 6 7 8 9 10 11	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	
$ \begin{array}{c} 12\\13\\14\\15\\16\\17\\18\\19\\20\end{array} $	$\begin{array}{r} .4519\overline{2} \\ .45223 \\ .45254 \\ 9.4528\overline{5} \\ .45316 \\ .45348 \\ .45379 \\ .45410 \\ 9.45441 \end{array}$	31 31 31 31 31 31 31 31 31	59646 59689 59732 9.59776 59819 59863 59906 59949 9.59993	43 43 43 43 43 43 43 43 43 43 43 43 43 4	$\begin{array}{r} .4703\underline{6} \\ .4706\underline{6} \\ .47096 \\ \hline 9.47127 \\ .47157 \\ .47187 \\ .47218 \\ .47248 \\ \hline 9.47278 \\ \hline 9.47278 \\ \end{array}$	30 30 30 30 30 30 30 30 30 30 30 30	·62282 ·62326 9.62369 ·62412 ·62455 ·62498 ·62541 9.62584	43 43 43 43 43 43 43 43 43 43 43	$     \begin{array}{r}       12 \\       13 \\       14 \\       15 \\       16 \\       17 \\       18 \\       19 \\       20 \\       \end{array} $	42 6 4.2 7 4.9 8 5.6 9 6.4 10 7.1 2014	
21 22 23 24 25 26 27 28	$\begin{array}{r} .45472 \\ .45503 \\ .45534 \\ .45565 \\ 9 .45595 \\ .45626 \\ .45657 \\ .45688 \end{array}$	31 31 30 31 31 31 31 31 31	$\begin{array}{r} 60036\\ 60079\\ 60123\\ 60166\\ 9.60209\\ 60253\\ 60296\\ 60339\\ \end{array}$	43 43 43 43 43 43 43 43 43 43 43 43	$\begin{array}{r} .47308\\ .47339\\ .47369\\ .47399\\ \hline 9.47429\\ .47459\\ .47459\\ .47450\\ .47520\\ .47550\\ \end{array}$	30 30 30 30 30 30 30 30 30 30	$\begin{array}{r} \cdot 62627\\ \cdot 62670\\ \cdot 62713\\ \cdot 62756\\ 9\cdot 62799\\ \cdot 62842\\ \cdot 62885\\ \cdot 62928\end{array}$	43 43 43 43 43 43 43 43 43 43	21 22 23 24 25 26 27 28	$\begin{array}{c} 30 21\cdot\underline{2}\\ 40 28\cdot3\\ 50 35\cdot4\\ \mathbf{3\overline{1}}, 31\\ 6 3\cdot\overline{1} 3\cdot1\\ 6 3\cdot\overline{1} 3\cdot\overline{1} 3\cdot1\\ 6 3\cdot\overline{1} 3\cdot1\\ 6 3\cdot\overline{1} 3\cdot$	
29 30 31 32 33 34 35	$     \underbrace{ .45719 \\ 9.45750 \\ .45781 \\ .45812 \\ .45843 \\ .45873 \\ 9.45904 } $	31 30 31 3 <u>1</u> 30 31 30 31 31	$\begin{array}{r} \cdot 60383\\ \hline 9\cdot 60426\\ \cdot 60469\\ \cdot 60512\\ \cdot 60556\\ \cdot 60599\\ \hline 9\cdot 60642\\ \end{array}$	43 43 43 43 43 43 43 43 43 43	$9.4758\bar{0} \\ .4761\bar{0} \\ .4764\bar{0} \\ .4764\bar{0} \\ .4767\bar{0} \\ .4770\bar{0} \\ 9.47731$	30 30 30 30 30 30 30 30	$\begin{array}{r} \cdot 62971 \\ 9 \cdot 63014 \\ \cdot 63057 \\ \cdot 63100 \\ \cdot 63143 \\ \cdot 63186 \\ 9 \cdot 63229 \end{array}$	43 43 43 43 43 43 43 43	29 30 31 32 33 34 35	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	
36 37 38 <u>39</u> 40 41 42 43 44	$\begin{array}{r} .4593\overline{5} \\ .45966 \\ .45997 \\ .46027 \\ \hline 9.4605\overline{8} \\ .46089 \\ .46089 \\ .46120 \\ .4615\overline{0} \\ .4618\overline{1} \end{array}$	30 31 30 31 30 31 30 31 30 31	60685 60729 60772 60815 9.60858 60902 60945 60988 60988 61031	43 43 43 43 43 43 43 43 43 43 43	.47761 .47791 .47821 .47851 9.47881 .47911 .47911 .47941 .47971 .48001	30 30 30 30 30 30 30 30 30	$\begin{array}{r} \cdot 63272 \\ \cdot 63315 \\ \cdot 63358 \\ \cdot 63401 \\ \hline 9 \cdot 63443 \\ \cdot 63486 \\ \cdot 63529 \\ \cdot 63572 \\ \cdot 63615 \\ \hline \end{array}$	$\begin{array}{c} 43 \\ 43 \\ 43 \\ 42 \\ 43 \\ 43 \\ 43 \\ 43 \\$	36 37 38 39 40 41 42 43 44	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	
45 46 47 48 49 50 51	·46396	30 30 31 30 30 30 30 30 30 30	$\begin{array}{r} 9.61075\\ .61118\\ .61161\\ .61204\\ .61247\\ 9.61247\\ 9.61291\\ .61334\\ .61377\end{array}$	43 43 43 43 43 43 43 43 43 43	$\begin{array}{r} 9.48031\\ .48061\\ .48090\\ .48120\\ .48120\\ .48150\\ 9.48180\\ .48210\\ .48210\\ \end{array}$	30 30 30 30	$\begin{array}{r} 9.6365\overline{8}\\ .63701\\ .63744\\ .63787\\ .63830\\ 9.63873\\ .63915\\ .63915\end{array}$	42 43 43 43 43 42 42	45 46 47 48 49 50 51	50 25.4(25.0 29 6  2.9 7  3.4 8  3.9	
52 53 55 55 56 57 58 59	$\begin{array}{r} \cdot 46426\\ \cdot 46457\\ \cdot 46487\\ \cdot 46487\\ 9\cdot 46518\\ \cdot 46549\\ \cdot 46579\\ \cdot 46610\\ \cdot 46640\end{array}$	30 30 31 30 30 30 30 30 30	$\begin{array}{r} \cdot  61420 \\ \cdot  61463 \\ \hline 9 \cdot 61506 \\ \cdot  61550 \\ \cdot  61593 \\ \cdot  61636 \\ \cdot  61679 \end{array}$	43 43 43 43 43 43 43 43 43 43 43	$\begin{array}{r} \cdot 48240 \\ \cdot 48270 \\ \cdot 48300 \\ 9 \cdot 48329 \\ \cdot 48359 \\ \cdot 48389 \\ \cdot 48389 \\ \cdot 48419 \\ \cdot 48449 \\ \cdot 48449 \\ \end{array}$	30 30 29 30 30 29 30 30 30	$\begin{array}{r} \cdot 63958 \\ \cdot 64001 \\ \cdot 64044 \\ \hline 9 \cdot 64047 \\ \cdot 64130 \\ \cdot 64130 \\ \cdot 64173 \\ \cdot 64216 \\ \cdot 64258 \end{array}$		52 53 54 55 56 57 58 59	$\begin{array}{c} 9 & 4.4 \\ 10 & 4.9 \\ 20 & 9.8 \\ 30 & 14.7 \\ 40 & 19.6 \\ 50 & 24.6 \end{array}$	
<u>60</u>	9.46671	7	$9 \cdot 6172\overline{2}$	40	9.48478	23 D	<u>9.6430</u> 1	$\frac{1}{D}$	<u>60</u>	P. P.	

672

Log.Exs.

D

Lg. Vers.

D

Log.Exs.

Lg. Vers.

9 D

P. P.

D

**46°** 

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,	Lg. Vers.	D	Log.Exs.	D	Lg. Vers.	D	Log, Exs.	D	<u>i</u>	P. P.
0 1 2 3 4	9 · 48478 • 48508 • 48538 • 48568 • 48597	30 29 30 29	9.64301 .64344 .64387 .64430 .64473	43 42 43 43	9.50243 .50272 .50301 .50330 .50359	29 29 29 29	9 · 66864 · 66907 · 66950 · 66992 · 67035	42 43 42 42	0 1 2 3 4	$\begin{array}{ccc} 43 & \mathbf{4\overline{2}} \\ 6 & 4.3 & 4.2 \end{array}$
5 6 7 8 9	$9.4862\overline{7}$ .48657 .4868 <u>6</u> .48716 .48746	30 29 29 30 29 30 29	$9.6451\frac{5}{64558}$ $.64558$ $.64601$ $.64644$ $.64687$	$4\bar{2}$ 43 43 42 42 43	9.50388 .50417 .50446 .50475 .50504	29 29 29 29 29	9.67077 .67120 .67162 .67205 .67248	$42 \\ 43 \\ 42$	5 6 7 8 9	$\begin{array}{c} 6 & 4 \cdot 3 & 4 \cdot \overline{2} \\ 7 & 5 \cdot 0 & 4 \cdot 9 \\ 8 & 5 \cdot 7 & 5 \cdot 6 \\ 9 & 6 \cdot 4 & 6 \cdot 4 \\ 10 & 7 \cdot \overline{1} & 7 \cdot 1 \\ 20 & 14 \cdot \overline{3} & 14 \cdot \overline{1} \end{array}$
10 11 12 13 14	-48805 -48835 -48864 -48894	29 309 29 29 29 29 29 29	9 · 64729 · 64772 · 64815 · 64858 · 64901	$4\overline{2}$ 43 43 42 43 43	9.50533 .50562 .50591 .50619 .50648	29 29 29 28 29	9.67290 .67333 .67375 .67418 .67460	42 42 42 42 42 42 42 42 42	10 11 12 13 14	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
15 16 17 18 19	-48923 -48953 -48983 -49012 -49042	29 30 29 29 29 29	9.6494 <u>3</u> .64986 .65029 .65072 .65114	$4\overline{2} \\ 43\overline{2} \\ 43\overline{2} \\ 43\overline{2} \\ 4\overline{2} \\ 4$	9.50677 .50706 .50735 .50764 .50793	29 2 <u>9</u> 28 29 29	9 · 67503 · 67546 · 67588 · 67631 · 67673	$4\overline{2}$ 43 42 42 42 42 42	15 16 17 18 19	42 6 4 · 2 7 4 · 9 8 5 · 6 9 6 · 3
20 21 22 23 24	·49101 ·49130 ·49160 ·49189	29 29 29 29 29 29 29 29	9.65157 .65200 .65243 .65285 .65328	43 42 43 42 43	9.50821 .50850 .50879 .50908 .50937	28 29 29 28 29	9.6771 <u>6</u> .67758 .6780 <u>1</u> .6784 <u>3</u> .67886	422222222 4222222 4222222 422222 422222 422222 42222 42222 42222 42222 42222 42222 42222 42222 42222 42222 42222 42222 42222 422 42 4	20 21 22 23 24	10 7.0 20 14.0 30 21.0 40 28.0 50 35.0
25 26 27 28 29	·49278 ·49307 ·49336	29 29 29 29	$\begin{array}{r} 9.65371 \\ .65414 \\ .65456 \\ .65499 \\ .65542 \end{array}$	43 42 43 42	9.50965 .50994 .51023 .51052 .51080	28 29 28 29 28 29 28	9.67928 .67971 .68013 .68056 .68098	4212121212 4221212 4221212	25 26 27 28 29	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
30 9 31 32 33 34	·49300 ·49395 ·49425 ·49454 ·49483	29 29 29	9.65585 .65627 .65670 .65713 .65755	42 43 42 42	$9.5110\overline{9}$ .51138 .51167 .51195 .51224	29 28 28	9.68141 .68183 .68226 .68268 .68311	42 42 42 42 42 42 42 42 42 42 42	30 31 32 33 34	$\begin{array}{c ccccc} 9 & 4.5 & 4.4 \\ 10 & 5.0 & 4.9 \\ 20 & 10.0 & 9.8 \\ 30 & 15.0 & 14.7 \\ 40 & 20.0 & 19.6 \\ \hline \end{array}$
35 9 36 37 38 39	·49571 ·49601 ·49630	29 29 29 29	9.65798 .65841 .65884 .65926 .65969	43 42 42 42	$\begin{array}{r} 9.51253 \\ .51281 \\ .51310 \\ .51338 \\ .51367 \end{array}$	29 28 28 28 28 29	9 • 68353 • 68396 • 68438 • 68481 • 68523	421212121212121212121212121212121212121	35 36 37 38 39	50 25.0 24.6 29 28 6  2.9  2.8 7  3.4  3.3
40 9 41 42 43 44	· 49059 · 49689 · 49718 · 49747 · 49776	29 29	9-66012 -66054 -66097 -66140 -65182	42 43 42	$\begin{array}{r} 9.51396 \\ .51424 \\ .51453 \\ .51481 \\ .51510 \end{array}$	28 28 28 28	9 - 68566 - 68608 - 68651 - 68693 - 68735	$\begin{array}{c} 4\bar{2} \\ 4\bar{2} \\$	40 41 42 43 44	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$
45 9 46 47 48 49	-49806 -49835 -49864 -49893 -49922	29 29 29	9.66225 .66268 .66310 .66353 .66396	42 42 43	9.51539 .51567 .51596 .51624 .51653	208 28 28 28 28	9 · 68778 • 68820 • 68863 • 68905 • 68948	421212121212121212121212121212121212121	45 46 47 48 49	30 14.514.2 40 19.319.0 50 24.1 23.7
50 9 51 52 53 54	-49952 -49981 -50010 -50039 -50068	2 <u>9</u> 29 29	9 · 66438 · 66481 · 66523 · 66566 · 66609	42 43 42	9.51681 .51710 .51738 .51767 .51795	288 288 288 288 288 288 288 288 288 288	9.68990 .69033 .69075 .69117 .69160	42 42 42 42 42 42 42 42 42	50 51 52 53 54	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$
55 9 56 57 58 59	· 50126 · 50125 · 50155 · 50185 · 50214	2 <u>9</u> 2 <u>0</u> 29	$9 \cdot 6665\overline{1} \\ \cdot 66694 \\ \cdot 66737 \\ \cdot 66779 \\ \cdot 66822$	43 42 42 42	9.51823 .51852 .51880 .51909 .51937	2888 288 288 288 288 288 288 288 288 28	9.69202 .69245 .69287 .69380 .69372	$\begin{array}{c} 4\overline{2} \\ 42 \\ 42 \\ 42 \\ 42 \\ 42 \\ 42 \\ 42 \\ $	55 56 57 58 59	200 14.0 40 18.6 50 23.3
_	. 90743		9.66864 Log.Exs.	42 77	9.51965 Lg. Vers.	28 D	9.69414 Log.Exs.	$\frac{4\overline{2}}{D}$	<u>60</u> '	P. P.
				1	-3				1	

**48°** 

 $49^{\circ}$ 

48	49	
· Lg. Vers. D Log. Exs. D		. <i>D</i> ′ P. P.
$\begin{array}{c} 0 & 9 \cdot 5196\bar{5} \\ 1 & \cdot 51994 \\ 2 & \cdot 5202\bar{2} & 2\bar{8} \\ 3 & \cdot 5205\bar{0} & 2\bar{8} \\ 4 & \cdot 5207\bar{9} \\ 4 & \cdot 5207\bar{9} \\ - & \cdot 69584 \\ 4 \end{array} \left. \begin{array}{c} 9 \cdot 6941\bar{4} \\ - & 6945\bar{7} \\ - & 69584 \\ 4 \\ - & 5207\bar{9} \\ - & - \\ - & 69584 \\ 4 \end{array} \right.$		$ \begin{array}{cccccccccccccccccccccccccccccccccccc$
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$5.54060 \ 27 \ .72630 \ .72630 \ .54118 \ 27 \ .72672 \ .54145 \ 27 \ .72714 \ .54173 \ .72756$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
$\begin{array}{c} \hline 20 & 9 & 52531 \\ 21 & 52531 \\ 22 & 52537 \\ 23 & 52637 \\ 23 & 52615 \\ 23 & 52615 \\ 28 & 70347 \\ 4 \\ 24 & 52643 \\ 28 & 70389 \\ 4 \\ 24 & 52643 \\ 28 & 70431 \\ 4 \\ 24 \\ 24 \\ 52643 \\ 28 \\ 70431 \\ 4 \\ 52643 \\ 28 \\ 70431 \\ 4 \\ 52643 \\ 28 \\ 70431 \\ 4 \\ 52643 \\ 4 \\ 52643 \\ 52644$	$\begin{array}{c} 4\\ 9 \cdot 5420\overline{0} & \begin{array}{c} 27\\ 7 \\ 54228\\ \cdot 54255\\ \cdot 54283\\ 27\\ \cdot 72825\\ 7295$	9 42 20 1 42 21 3 42 22 5 42 23 5 42 23
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$		$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	54967 = 27 $7389554912 = 27$ $7389554939 = 27$ $7393854967 = 27$ $7398054967 = 27$ $7398074022$	
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{array}{c} 2\\ 2\\ \hline 9.55157\\ 2\\ \hline 55184\\ 2\\ \hline 55211\\ 2\\ \hline 55265\\ 2\\ \hline 55265\\ 2\\ \hline 55265\\ 2\\ \hline 74401\\ -55265\\ 2\\ \hline 74401\\ -74444 \end{array}$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$
$\begin{array}{c} 60 \\ 9 \cdot 5364\overline{8} \\ \mathbf{Lg}, \text{Vers.} \end{array} \begin{array}{c} 28 \\ \mathbf{D} \end{array} \begin{array}{c} 9 \cdot 71954 \\ \text{Log. Exs.} \end{array} \begin{array}{c} 4 \\ 0 \end{array}$	$29.5529\overline{2}279.74486$	

TABLE VIIILOGARITEMI	C VERSED SINES AND EXTERNAL SECANTS.
50°	51°

_	50°						51°			
	Lg. Vers.	D	Log.Exs.	D	Lg. Vers.	D	Log.Exs	D	<u>'</u>	P. P.
01234	9.55292 .55319 .55347 .55374 .55401	27 27 27 27 27	9.74486 .74528 .74570 .74612 .74654	42 42 42 42	9.56900 .56926 .56953 .56979 .57005	2 <u>6</u> 2 <u>6</u> 2 <u>6</u> 2 <u>6</u> 2 <u>6</u> 2 <u>6</u>	9.77012 .77055 .77097 .77139 .77181	$4\overline{2} \\ 42 \\ 42 \\ 42 \\ 42 \\ 42 \\ 42 \\ 42 \\ $	0 1 2 3 4	17.10
56789	9.55428 .55455 .55482 .55509 .55536	27 27 27 27 27 27 27 27	9.74696 .74739 .74781 .74823 .74865	42 42 42 42 42 42 42 42 42	9.57032 .57058 .57085 .57111 .57138	200 200 200 200 200 200 200 200 200 200	9.77223 .77265 .77307 .77349 .77391	$     \begin{array}{r}       42 \\$	56789	42 6 4.2 7 4.9 8 5.6 5.6 9 6.4 6.3 10 7.1 7.0
$10 \\ 11 \\ 12 \\ 13 \\ 14 \\ 14 \\ 14 \\ 10 \\ 10 \\ 10 \\ 10 \\ 10$	9.55563 .55590 .55617 .55644 .55671	27 27 27 27 27 27	9.74907 .74949 .74991 .75033 .75076	42 42 42 42 42 42	9.57164.57190.57217.57243.57269	266 266 26 26 26 26	9.77433 .77475 .77517 .77560 .77602	42 42 42 42 42 42	$   \begin{array}{c}     10 \\     11 \\     12 \\     13 \\     14 \\     14   \end{array} $	$\begin{array}{c} 10 & 7 \cdot 1 \\ 20 & 14 \cdot \overline{1} & 14 \cdot 0 \\ 30 & 21 \cdot \overline{2} & 21 \cdot 0 \\ 40 & 28 \cdot \overline{3} & 28 \cdot 0 \\ 50 & 35 \cdot 4 & 35 \cdot 0 \end{array}$
15 16 17 18 19	9.55698 .55725 .55751 .55778 .55805	27 26 27 27 27 27	9.75118 .75160 .75202 .75244 .75286	42 42 42 42 42 42	9.57296 .57322 .57348 .57375 .57401	26 26 26 26 26 26	9.77644 .77686 .77728 .77770 .77812		15 16 17 18 19	27 27 6  2.7  2.7
20 21 22 23 24	9.55832 .55859 .55886 .55913 .55940	27 26 27 27 27 26	9.75328 .75370 .75413 .75455 .75497	42 42 42 42 42	9.57427 .57454 .57480 .57506 .57532	26 26 26 26 26 26	9.77854 .77896 .77938 .77980 .77980 .78022	42 42 42 42 42 42	20 21 22 23 24	$\begin{array}{cccccccccccccccccccccccccccccccccccc$
25 26 27 28 29	9.55906 .55993 .56020 .56047 .56074	27 27 26 27	9.75539 .75581 .75623 .75665 .75707	42 42 42 42 42 42 42 42 42	9.57559 .57585 .57611 .57637 .57664	26 26 26 26 26 26 26	9.78064 .78107 .78149 .78191 .78233	$4\overline{2}$ 42 42 42 42 42 42	25 26 27 28 29	30 13.7 13.5 40 18.3 18.0 50 22.9 22.5
30 31 32 33 34	9.56101 .56127 .56154 .56181 .56208	26 27 26 27	9.75750 .75792 .75834 .75876 .75918	42 42 42 42 42	9.57690 .57716 .57742 .57768 .57794	2 <u>6</u> 26 26 26 26	9.78275 .78317 .78359 .78401 .78443	42 42 42 42 42 42 42	30 31 32 33 34	26 26 6 2.6 2.6 7 3.1 3.0
35 36 37 38 39	9.56234 .56261 .56288 .56315 .56311	26 27 26 27 26 27 26 27 26 26	9.75960 .76002 .76044 .76086 .76128	42 42 42 42	9.57821 .57847 .57873 .57899 .57925	26 26 26 26 26 26	9.78485 .78527 .78569 .78611 .78653		35 36 37 38 39	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
40 41 42 43 44	9.56368 .56395 .56421 .56448 .56475	27 26 26 27 26 27 26 27 26	9.76171 .76213 .76255 .76297 .76339	42 42 42 42 42 42 42	9.57951 .57977 .58003 .58029 .58055	26 26 26 26 26 26 26	9.78696 .78738 .78780 .78822 .78864	42 42 42 42 42 42 42	$\begin{array}{c} 40 \\ 41 \\ 42 \\ 43 \\ 44 \\ \end{array}$	30 13.2 13.0 40 17.6 17.3 50 22.1 21.6
45 46 47 48 49	9.56501 .56528 .56554 .56581 .56608	2667 2276 26 20 20 20 20	9.7638 <u>1</u> .7642 <u>3</u> .7646 <u>5</u> .76507 .7654 <u>9</u>	$     \begin{array}{r}       42 \\$	9.58082 .58108 .58134 .58160 .58186	26 26 26 26 26 26	9.78906 .78948 .78990 .79032 .79074	42 42 42 42 42 42 42 42	45 46 47 48 49	6 2.5 7 3.0 8 3.4
50 51 52 53 54	9.56634 .56661 .56687 .56714 .56741	226 226 27 26 27	9.76592 .76634 .76676 .76718 .76760	42 42 42 42 42 42 42	9.58212 .58238 .58264 .58290 .58316	26 26 26 26 26 26	9.79116 .79158 .79200 .79242 .79285	42 42 42 42 42 42	50 51 52 53 54	9 3.8 10 4.2 20 8.5 30 12.7 40 17.0
55 56 57 58 59	9.56767 .56794 .56820 .56847 .56873	1226161616	9.76802 .76344 .76896 .76928 .76970	42 42 42 42 42 42 42	9.58342 .58367 .58393 .58419 .58445	25 26 26 26 26 26	9.79327 .79369 .79411 .79453 .79495	42 42 42 42 42 42 42	55 56 57 58 59	50 21.2
<u>60</u>	9 · 56900 Lg. Vers.	D	<u>9.77012</u> Log.Exs.	$\overline{D}$	<u>9 - 58471</u> Lg. Vers.	$\overline{D}$	9.79537 Log.Exs.	D	<u>60</u>	P. P.
-			-				- 1			

TABLE VIIILOGARITHMIC	VERSED SINES AND	DEXTERNAL SECANTS.
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53°

),	1. V.	7		ъ	1. v	n		2		D D
-	Lg. Vers.		Log.Exs.	<b>D</b>	Lg. Vers.		Log.Exs.	D		P. P.
0 1	9.5847 <u>1</u> .58497	$\frac{26}{25}$	9.79537 .7957 <u>9</u>	$4\overline{2}$ 42	9.60008 .60034	25	9.82062 .82104	$4\overline{2}$ 42	0.	
23	·58523 ·58549	26	·7962 <u>1</u> ·7966 <u>3</u>	42	60059 60084	$25 \\ 25 \\ 25 \\ 31 \\ 32 \\ 32 \\ 32 \\ 33 \\ 34 \\ 34 \\ 34 \\ 34$	$\cdot 8214\overline{6} \\ \cdot 8218\overline{8}$	42	23	
4	.58575	26	.79705	42 42	.60110	$\overline{25}$ 25	-82230	42	_4	
5 6	9.5860 <u>1</u> .5862 <u>6</u>	2 <u>6</u> 25	$9.7974\overline{7} \\ .7978\overline{9}$	42	9.60135 .60160	25	9.82272 .82315	$\frac{42}{42}$	5 6	
7	·5865 <u>2</u>	$\frac{26}{26}$	·7983ī	$\frac{42}{42}$	.60185	$\frac{25}{25}$	·82357	$\frac{42}{42}$	7	
8 9	-58678 -58704	$2\overline{5}$	.79874 .79916	42	$60211 \\ 60236$	25	.82399 .82441	42	8 9	42 · 42 61 4 · 2 4 · 2
10	9.58730	$\frac{26}{25}$	9.79958	$\frac{42}{42}$	9.60261	25 25	9.82483	$4\bar{2}$ 42	$\overline{10}$	7 4.9 4.9
$\frac{11}{12}$	·58755 ·58781	26	.80000 .80042	42	·60286 ·60312	25	·82525 ·82567	42	$11 \\ 12$	8 5·6 5·6 9 6·4 6·3
13	•58807	26 25	.80084	$\frac{42}{42}$	·6033 <u>7</u>	2 <u>5</u> 25	·82609	42 42	13	10 7.1 7.0
$\frac{14}{15}$	<u>.58833</u> 9.58859	26	$\frac{.80126}{9.80168}$	42	$\frac{.60362}{9.60387}$	25	<u>.82651</u> 9.82694	$4\overline{2}$	$\frac{14}{15}$	$     \begin{array}{c}       20 \\       20 \\       30 \\       21 \\       21 \\       21 \\       21 \\       0     \end{array} $
16	·58884	$2\overline{5}$ 26	·80210	42 42	.60412	$\frac{25}{25}$	·82736	42 42	16	30 21 · 2 21 · 0 40 28 · 3 28 · 0 50 35 · 4 35 · 0
17 18	.58910 .58936	$2\overline{5}$	·80252 ·80294	42	·60438 ·60463	2 <u>5</u> 25	·82778 ·82820	42	17 18	00100.4100.0
19	.58962	26 25	<u>.80336</u>	42 42	·60488	25 25	·82862	$4\overline{2}$ 42	19	
20 21 22	9.58987 .59013	2 <u>5</u> 25	$9.8037\overline{8} \\ .80420$	42	9.6051 <u>3</u> .6053 <u>8</u>	25	9.82904 .82946	42	<b>20</b> 21	
22	·59039	$\frac{26}{25}$	·80463	$\frac{42}{42}$	.60563	25 25	·82988	$\frac{42}{42}$	22	
$\frac{23}{24}$	·59064 ·59090	26	·80505 ·80547	42	·60589 ·60614	25	·83031 ·83073	42	23 24	
25	9.59116	$2\overline{5} \\ 2\overline{5}$	9.80589	42 42	9.60639	25	9.83115	42 42	25	_
$\frac{26}{27}$	$.5914\overline{1}$ $.5916\overline{7}$	26	·80631 ·80673	42	·60664 ·60689	25 25	·83157 ·83199	$4\overline{2}$	26 27	26 25 6  2·6  2·5 7  3·0  3·0
28	•5919 <u>3</u>	25 25	·8071 <u>5</u>	42 42	.60714	25	·83241	42	28	7 3.0 3.0
29	$\frac{.59218}{9.59244}$	25	<u>.80757</u> 9.8079 <u>9</u>	42	60739	25	<u>-83283</u> 9-83325	42	$\frac{29}{30}$	8 3.4 3.4 9 3.9 3.1
30 31	·59270	26	•8084 <u>1</u>	42 42	9.60764 .60789	25 25	.83368	42 42	31	$\begin{array}{cccccccccccccccccccccccccccccccccccc$
32 33	·59295 ·59321	255	-80883 -80925	42	·60814 ·60839	25	·83410 ·83452	42	32 33	3013.012.7
$33 \\ 34$	.59346		.80968	42	.60864	25 25	83494	42	34	$4017.\overline{3}17.0$ 5021.621.2
35	9.59372 .59397	25 25	9.81010 .81052	42 42	$9.60889 \\ .60914$	25	9 · 83536 · 83578	42 42	35 36	00121-0121-2
36 37	·59423	$26 \\ 25 \\ 25 \\ 31 \\ 32 \\ 32 \\ 32 \\ 33 \\ 34 \\ 34 \\ 34 \\ 34$	.81094	42 42	·60939	25 25	↓ 83620	42 42	37	
38 39	.59449 .59474	25	·81136 ·81178	42	· 60964 · 60989	25	-83663 -83705	42	38 39	
<del>33</del> 40	9.59500	25	9.81220	42 42	9.61014	25 25	9.83747	$\frac{42}{42}$	40	
41	·59525	$25 \\ 25$	.81262	42	· 61039	25	.83789 .83831	42	$\frac{41}{42}$	-1
42 43	·59551 ·59576	2 <u>5</u> 2 <u>5</u> 25	$.81304 \\ .81346$	42 42	.61064 .61089	25 25	·83873	42 42	43	
<u>44</u>	.59602		<u>·81388</u>	42	<u>.61114</u>	25	83916	42	44	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
45 46	9.59627 .59653	25 25 25	$9.81430 \\ .81473$	42	$9.6113\overline{9}$ .6116 <u>4</u>	25 25	9.83958 .84000	42 42	45 46	7 2.9 2.8 8 3.3 3.2 9 3.7 3.7 10 4.1 4.1
47	·59678	2 <u>5</u> 25	·81515	42 42	· 61189	24	·84042 ·84084	42	47 48	8 3.3 3.2 9 3.7 3.7
48 49	·59704 ·59729	25	·81557 ·81599	42	·61214 ·61239	25	·84.26	42	49	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
50	$9.5975\bar{4}$	25 25 25	9.81641	$\frac{42}{42}$	9.61264	25 2 <u>5</u>	9.84168	42 42	50	$30 12 \cdot 5 12 \cdot \overline{2}$
51 52	·59780 ·59805	25	·81683 ·81725	42	·61289 ·61313	24	·84211 ·84253	$\frac{42}{42}$	51 52	$4016.\overline{6}16.\overline{3}$ 5020.820.4
53	.59831	25 25	·8176 <u>7</u>	42 42	·61338 ·61363	25 25	·84295 ·84337	42	53 54	
54 55	<u>.5985ē</u> 9.5988ī	25	<u>·81809</u> 9·81851	$\frac{42}{42}$	$\frac{.61363}{9.61388}$	25	9.84379	42	55	
56	.59907	2 <u>5</u> 2 <u>5</u>	·81894	42	.61413	$2\bar{4} \\ 25$	·84422	$4\bar{2} \\ 42$	56	
57 58	·59932 ·59958	25	·81936 ·81978	42	$61438 \\ 61462$	$2\bar{4}$ 25	•84464 •84506	$\frac{42}{42}$	57 58	
59	.59983	25 25	<u>·82020</u>	42 42	<u>.61487</u>	25	<u>·84548</u>	42 42	59	
<u>60</u>		<b>D</b>	9 · 82062 Log.Exs.		$\frac{9 \cdot 6151\overline{2}}{\text{Lg. Vers.}}$	D	9.84590 Log.Exs.	D	<u>60</u>	P. P.
_	Lg. Vers.	10	LOBIEXSI		L.B. Veisi		LOSILASI	<u> </u>	I	1

54°							55°			
,	Lg. Vers.	D	Log.Exs.	D	Lg. Vers.	D	Log.Exs.	D	1	P. P.
$, \ \left[ 0 \\ 1 \\ 2 \\ 3 \\ 4 \\ 5 \\ 6 \\ 7 \\ 8 \\ 9 \\ 1 \\ 1 \\ 1 \\ 1 \\ 1 \\ 1 \\ 1 \\ 1 \\ 1$	$ \begin{array}{c} Lg, Vers, \\ g, 61512\\ & 61537\\ & 61562\\ & 61611\\ & 61685\\ & 61611\\ & 61685\\ & 61710\\ & 61685\\ & 61710\\ & 61784\\ & 61838\\ & 61838\\ & 61838\\ & 61838\\ & 61982\\ & 9.61784\\ & 61838\\ & 61982\\ & 9.61888\\ & 61982\\ & 9.61282\\ & 9.62066\\ & 620252\\ & 620252\\ & 622066\\ & 622052\\ & 622052\\ & 622052\\ & 622052\\ & 62252\\ & 6$	়ে বিতিষিত বিতিষ্ঠিয়ে তাৰ্বাবিতাৰ তাৰাৰাৰ্বিত বিৰিধিতাৰ বিবিবিধাৰাৰ বিবিবিধাৰা বিবিবিধাৰ বিবিধাৰণ বি	Log. Exs. 9.84590 84632 84632 84675 84759 9.84075 847759 9.84071 84759 9.84071 84759 9.84071 84928 845599 845561 8455661 845567 845567 845567 8455788 8455788 8455788 845578 8455788 8455788 8455788	$\square \boxed{\begin{array}{ c c c c c c c c c c c c c c c c c c $	$\begin{array}{c} Lg, Vers, \\ g: 62294 \\ 63008 \\ 63008 \\ 63032 \\ 63032 \\ 63032 \\ 63032 \\ 63032 \\ 63154 \\ 63154 \\ 63154 \\ 63154 \\ 63226 \\ 63225 \\ 63225 \\ 63225 \\ 63225 \\ 63225 \\ 63225 \\ 63225 \\ 63225 \\ 63225 \\ 63225 \\ 63225 \\ 63225 \\ 63225 \\ 63225 \\ 63323 \\ 63323 \\ 63347 \\ 63347 \\ 63345 \\ 63347 \\ 63345 \\ 63345 \\ 63355 \\ 63355 \\ 635540 \\ $	D 24444 144444 44444 44444 44444 44444 44444 4444	Log, Exs, 9.87125 87125 87125 87209 87222 87294 9.87336 9.87336 9.87421 87453 87590 9.87548 87590 9.87548 87590 9.87548 87590 87675 87675 87717 9.87548 87590 9.87748 87929 9.87971 88014 88014 88014 88014 88014 88353 9.88353 9.88353 9.88352 88348 883480 88353 9.88353 9.88352 88352 9.88352 88353 9.88352 88353 9.88352 88353 9.88352 88353 9.88352 88353 9.88353 9.88353 9.88352 88353 9.88352 88353 9.88353 9.88353 9.88352 88353 9.88353 9.88353 9.88353 9.88352 88353 9.883552 88353 88480 9.88353 9.88353 9.88353 9.88353 9.88352 88353 88480 9.88353 9.88353 9.88352 88353 88480 9.88353 883552 88353 883552 88353 883552 88353 883552 883552 883553 883552 883553 8835555 8835555 8835555 88355555 8835555 88355555555	$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	, 0123456789011123415678901223345678901233456789012334567890012334567890012334567890012334567890012334567890012334567890012334567890012334567890012334567890001233456789000000000000000000000000000000000000	P. P. 42 42 6 4.2 4.2 7 4.9 4.9 8 5.6 5.6 9 6.4 6.3 10 7.1 14.0 30 $21.221.0$ 40 $28.328.0$ 50 $35.435.0$ 8 $3.37$ 9 $3.7$ 10 4.1 4.0 30 $21.221.0$ 40 $28.328.0$ 50 $35.435.0$ 8 $3.37$ 9 $3.7$ 10 4.1 4.1 20 $4.1$ 4.1 20 $4.1$ 4.1 20 $4.2$ 8 $3.37$ 9 $3.7$ 10 4.1 4.1 20 $4.1$ 4.1 20 $4.1$ 4.1 20 $4.2$ 4.1 20 $4.1$ 4.1 20 $4.1$ 4.1 20 $4.1$ 4.1 20 $4.1$ 4.1 20 $4.1$ 4.1 20 $4.1$ 20 $4.1$
<u>,60</u>	9.62984 Lg. Vers.	24 D	9.87125 Log.Exs.	$\frac{4\overline{2}}{D}$	9 · 64425 Lg. Vers.	24 D	<u>9 89668</u> Log. Exs.	$4\overline{2}$ <b>D</b>	<u>60</u> ′	P. P.
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<b>1</b> A	TABLE VIII.—LOGARITHMIC VERSED SINES AND EXTERNAL SECANTS. 56° 57°											
	Lg. Vers.	D	Log.Exs.	D	Lg. Vers.	D	Log.Exs.	D		P. P.		
01234 56789	$\begin{array}{r} 9.64425\\ .64443\\ .64472\\ .64496\\ .64520\\ 9.64543\\ .64567\\ .64591\\ .64614\\ .64638\\ \end{array}$	$\begin{array}{c} 23\\ 24\\ 23\\ 24\\ 23\\ 24\\ 23\\ 23\\ 23\\ 24\\ 23\\ 24\\ 23\\ 24\\ 24\\ 23\\ 24\\ 24\\ 24\\ 24\\ 24\\ 24\\ 24\\ 24\\ 24\\ 24$	9.89668 .89711 .89753 .89838 9.89838 9.89881 .89923 .89966 .90008 .90051	$\begin{array}{c} 4\overline{2}\\ 4\overline$	$\begin{array}{r} 9.6583\overline{5}\\ .65859\\ .6580\overline{5}\\ .6590\overline{5}\\ .6592\overline{8}\\ .6592\overline{8}\\ .65952\\ .65975\\ .65975\\ .65978\\ .66021\\ .66044\end{array}$	23 23 23 23 23 23 23 23 23 23 23 23 23 2	$\begin{array}{c} 9.9222\overline{4}\\.92267\\.92310\\.92353\\.92395\\.92395\\.92481\\.92481\\.92524\\.92566\\.92609\\.92609\end{array}$	$\begin{array}{r} 43\\ 42\\ 43\\ 42\\ 42\\ 43\\ 42\\ 43\\ 42\\ 43\\ 43\\ 43\\ 43\\ 43\\ 43\\ 43\\ 43\\ 43\\ 43$	01234 56789	$\begin{array}{cccccccccccccccccccccccccccccccccccc$		
10 11 12 13 14 15 16 17 18 19	$\begin{array}{r} 9.64662\\ .64685\\ .64709\\ .64733\\ .64756\\ 9.64780\\ .64804\\ .64804\\ .64827\\ .64851\\ .64875\end{array}$	1313 41313 4131313 4131313 4131313 4131313 4131313 4131313 4131313 413131313	9.9009 <u>4</u> .90136 .90179 .90221 .90264 9.90306 .90349 .90391 .90434 .90476	4320202020202020202020202020202020202020	$\begin{array}{r} 9.66068\\.66091\\.66114\\.66137\\.66160\\9.66183\\.66207\\.66230\\.66233\\.66276\\.66276\\.9.66293\\.6622$	233233 23323 23323 23333 23333 2333 23	9.92652 .92695 .92737, .92780 .92823 9.92828 9.92826 .92909 .92994 .92994 .93037 9.93080	42 43 42 43 42 43 42 43 42 43 42 43 42 43 42 43 42 43	10 11 12 13 14 15 16 17 18 19 20	$\begin{array}{c} 0 & 5 \cdot 0 & 4 \cdot 6 \\ 8 & 5 \cdot 7 & 5 \cdot 6 \\ 9 & 6 \cdot 4 & 6 \cdot 4 \\ 10 & 7 \cdot 1 & 7 \cdot 1 \\ 20 & 14 \cdot 3 & 14 \cdot 1 \\ 30 & 21 \cdot 5 & 21 \cdot 2 \\ 40 & 28 \cdot 6 & 28 \cdot 3 \\ 50 & 35 \cdot 8 & 35 \cdot 4 \end{array}$		
$\begin{array}{c} \textbf{20} \\ \textbf{21} \\ \textbf{223} \\ \textbf{24} \\ \textbf{25} \\ \textbf{26} \\ \textbf{27} \\ \textbf{29} \\ \textbf{31} \\ \textbf{333} \\ \textbf{356} \\ \textbf{378} \\ \textbf{367} \\ \textbf{386} \\ 38$	$\begin{array}{c} 9.\ 64898\\ 649925\\ 649425\\ 64945\\ 649425\\ 64942\\ 649925\\ 64992\\ 9.\ 65040\\ 65040\\ 65040\\ 65087\\ 65134\\ 65204\\ 65224\\ 65225\\ 65275\\ 665275\\ 66225\\ 662$	ରୁ ଅନ୍ତର ସ୍ଥାର ସହାର ସେହାର ସେହାର ସେହାର ଅଭିସାରାରୀ ସାହାରାହାର ସେହାର ସେହାର ସେହାର	$\begin{array}{c} 0.0561\\ -0.0604\\ -9.0647\\ -9.0647\\ -9.0649\\ -9.0774\\ -9.0689\\ -9.0774\\ -9.0800\\ -9.0774\\ -9.0800\\ -9.0945\\ -9.094\\ -9.$	$\begin{array}{c} 1 \\ 4 \\ 4 \\ 4 \\ 4 \\ 4 \\ 4 \\ 4 \\ 4 \\ 4 \\$	$\begin{array}{c} .663225\\ .66324508\\ .66324508\\ .66324508\\ .66324508\\ .66324508\\ .663288\\ .66438\\ .664438\\ .666438\\ .666438\\ .666507\\ .665507\\ .665508\\ .666522\\ .666522\\ .666688\\ .666688\\ .666681\\ .66714\\ .66$	23 23 23 23 23 23 23 23 23 23 23 23 23 2	93123 93208 93208 93251 9.98294 938251 9.98294 93837 93422 9.93465 9.93508 9.93594 9.93594 9.93594 9.93594 9.93594 9.93765 9.93765 9.93808	$\begin{array}{c} 4\underline{3}\\ 4\underline{2}\\ 43\\ 43\\ 4\underline{2}\\ 43\\ 4\underline{3}\\ 42\\ 43\\ 43\\ 43\\ 43\\ 43\\ 43\\ 43\\ 43\\ 42\\ 43\\ 43\\ 42\\ 43\\ 43\\ 42\\ 43\\ 43\\ 42\\ 43\\ 42\\ 43\\ 43\\ 42\\ 43\\ 43\\ 42\\ 43\\ 43\\ 42\\ 43\\ 43\\ 42\\ 43\\ 43\\ 42\\ 43\\ 43\\ 42\\ 43\\ 43\\ 43\\ 42\\ 43\\ 43\\ 43\\ 42\\ 43\\ 43\\ 43\\ 42\\ 43\\ 43\\ 43\\ 43\\ 43\\ 43\\ 43\\ 43\\ 43\\ 43$	20 21 22 23 24 25 26 27 28 29 30 31 32 33 34 35 36 37 38 39	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$		
<b>39</b> <b>40</b> <b>41</b> <b>42</b> <b>44</b> <b>44</b> <b>44</b> <b>44</b> <b>44</b> <b>44</b> <b>44</b>	$\begin{array}{r} \underline{65345}\\ 9, \underline{65368}\\ 0, \underline{65368}\\ 0, \underline{65368}\\ 0, \underline{6542}\\ 9, \underline{65462}\\ 9, \underline{65462}\\ 9, \underline{65509}\\ 0, \underline{655592}\\ 0, \underline{655592}\\ 0, \underline{65579}\\ 9, \underline{65579}\\ 0, \underline{65696}\\ 0, \underline{65719}\\ 0, \underline{65772}\\ 0, \underline{657765}\\ 0, \underline{657782}\\ 0, \underline{65782}\\ 0, \underline{65782}\\ 0, \underline{65782}\\ 0, \underline{65782}\\ 0, \underline{65782}\\ 0, \underline{65782}\\ 0, \underline{65812}\\ 0, \underline{65812}$		91328 9.91371 91414 91456 91541 9.91544 915584 91712 91712 91705 91712 91705 91712 91705 91712 91883 91926 91968 9.92011 92052 92096 92189	$\begin{array}{c} 4\overline{2}\\ 4\overline{3}\\ 4\overline{2}\\ 4\overline$	$\begin{array}{r} 66737\\ 9.667783\\ .66703\\ .668251\\ .668251\\ 9.668274\\ .66827\\ .66943\\ .66943\\ .66943\\ .66943\\ .66946\\ 9.667032\\ .67034\\ .67057\\ .67034\\ .67142\\ .67149\\ .671494\\ .67194\end{array}$	233233 233223 23323 23323 23323 23323 23323 23323 23332 233232 23332 23322 2332 23322 23322 23322 23322 23322 23322 23322 23322 23322 23322 23322 23322 2332 232	$\begin{array}{r} .93894\\ .93894\\ .938037\\ .93980\\ .94023\\ .94066\\ .94109\\ .94151\\ .94134\\ .94237\\ .94280\\ .94237\\ .94280\\ .94237\\ .94280\\ .94452\\ .94452\\ .94455\\ .94455\\ .94455\\ .94657\\ .94677\\ .9467710\\ .94770\\ .94750\\ .9470$	$\begin{array}{r} 43\\ 43\\ 43\\ 43\\ 43\\ 43\\ 43\\ 43\\ 43\\ 43\\$	39           40           41           42           43           44           45           44           45           50           51           52           53           54           55           56           57           58	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$		
<u>60</u>		23 D	9.92224 Log.Exs.	$\frac{4\overline{2}}{D}$	9.67217 Lg. Vers.	$\frac{2\overline{2}}{D}$	9.94796 Log.Exs.	43 D	<u>60</u> '	P. P.		
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TABLE VIIILOGARITHMI	C VERSED SIN	ES AND EXTERN	AL SECANTS.
TABLE VIIILOGARITHMI	J VERSED SIN	ES AND EXTERN	AL SECANTS.

58°

**59°** 

•	Lg. Vers.	D	Log.Exs.	D	Lg. Vers.	D	Log. Exs.	D	'	P. P.
0 1 2 3 4	9.67217 .67240 .6726 <u>3</u> .6728 <u>5</u> .67308	23 23 22 23	9.9479 <u>6</u> .9483 <u>9</u> .94882 .94925 .94968	43 43 43 43	9.68571 .6859 <u>3</u> .6861 <u>5</u> .68637 .68660	22 22 22 22 22	9.97387 .97430 .97473 .97517 .97560	43 43 43 43	0 1 2 3 4	
6 7 8 9	9.67331 .67354 .67376 .67399 .67422	22 23 23 23 23 23 23 23 23 23	9.9501 <u>1</u> .95054 .95097 .95140 .95183	43 43 43 43 43	$9.6868\overline{2} \\ .68704 \\ .68727 \\ .68749 \\ .68771$	22 22 22 22 22 22 22 22 22 22 22 22 22	9.97603 .97647 .97690 .97734 .97777	433333 4433 433 433 433 433 433 433 433	5 6 7 8 9	$\begin{array}{cccccccccccccccccccccccccccccccccccc$
10 11 12 13 14	9.67445 .67467 .67490 .67513 .67535	23212 222 2322 2322 2322	9.9522 <u>6</u> .95269 .95313 .95356 .95399	43 4 <u>3</u> 43 43 43	9.68793 .68816 .68838 .68860 .68882		9.97820 .97864 .97907 .97951 .97994	43 43 13 13 13 13 13 13 13 13 13 13 13 13 13	10 11 12 13 14	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
15 16 17 18 19	9.67558 .67581 .67603 .67626 .67649	23 23 23 23 23 23 23 23 23 23 23 23 23 2	9.05442 .95485 .95528 .95571 .95614	43 43 43 43 43	9 · 68905 · 68927 · 6894 <u>9</u> · 6897 <u>1</u> · 68993		9.98038 .98081 .98125 .98168 .98211	433 433 433 433 433 433	15 16 17 18 19	43
20 21 22 23 24	9.67671 .67694 .67717 .67739 .67762	2223222	9.95557 .95700 .95744 .95787 .95830	43 43 43 43 43	9.69016 .69038 .69060 .69082 .69104	22 22 22 22 22 22 22 22 22 22 22 22 22	9.98255 .98298 .98342 .98365 .98429	43333333	20 21 22 23 24	$ \begin{array}{c} 6 & 4 \cdot 3 \\ 7 & 5 \cdot 0 \\ 8 & 5 \cdot 7 \\ 9 & 6 \cdot 4 \\ 10 & 7 \cdot 1 \\ 20 & 14 \cdot 3 \end{array} $
25 26 27 28 29	9.67784 .67807 .67830 .67852 .67855	2223222	9.9587 <u>3</u> .9591 <u>6</u> .9595 <u>9</u> .96002 .96046	$43 \\ 43 \\ 43 \\ 43 \\ 43 \\ 43 \\ 43 \\ 43 \\$	9.69126 .69149 .69171 .69193 .69215	22 22 22 22 22 22 22	9.98472 .98516 .98559 .98603 .98647	4333 433 43 43 43 43 43	25 26 27 28 29	20 14.3 30 21.5 40 28.6 50 35.8
30 31 32 33 34	9.67897 .67920 .67942 .67965 .67987	2222222	9.96089 .96132 .96175 .96218 .96218 .96261	43 43 43 43 43	9.69237 .69259 .69281 .69303 .69325	22 22 22 22 22 22	9.08690 .98734 .98777 .98821 .98864	4333333 44433 4444 444	30 31 32 33 34	23 22 6  2·3  2·2
	9.68010 .68032 .68055 .68077 .68100	222222	9.96305 .96348 .96391 .96434 .96478	$4\overline{3} \\ 4\underline{3} \\ 43$	$9.6934\overline{7} \\ .69369 \\ .69392 \\ .69414 \\ .69436$	22 22 22 22 22 22 22	9.98908 .98952 .98095 .99039 .99082	4343333 443333 43	35 06 37 38 39	$\begin{array}{cccccccccccccccccccccccccccccccccccc$
_	$9.6812\overline{2}$ .68145 .68167 .68190 $.6821\overline{2}$	222222	9.96521 .96564 .96607 .96650 .96694	43 4 <u>3</u> 4 <u>3</u> 4 <u>3</u> 4 <u>3</u>	9.69458 .69480 .69502 .69524 .69546	22 22 22 22 22 22	9.99126 .99170 .99213 .99257 .99300	434 <u>13</u> 13 44 <u>3</u> 13 43 43 43	$     \begin{array}{r}       40 \\       41 \\       42 \\       43 \\       44     \end{array} $	30 11.5 11.2 40 15.3 15.0 50 19.1 18.7
	9.68235 .68257 .68280 .68302 .68324	222222222222222222222222222222222222222	9.96737 .96780 .96824 .96867 .96910	43 43 43 43 43 43	9.69568 .69590 .69612 .69634 .69656	22 22 22 22 22 22	9.99344 .99388 .99431 .99475 .99519	44 <u>13</u> 13 433 44 <u>13</u> 43	45 46 47 48 49	22.2.2.1 6 2.2.2.5 7 2.2.5 8 2.3.5 8 2.5.5 8 2
	9.68347 .68369 .68392 .68414 .68436	2222 2222 2222 2222 2222 2222	9.96953 .96997 .97040 .97083 .97127	43 43 43 43 43 43	9.69678 .69700 .69721 .69743 .69765	22 22 21 22 22	9.99562 .99606 .99650 .99694 .99737	43 44 43 44 3 44 3	$     \begin{array}{r}       10 \\       50 \\       51 \\       52 \\       53 \\       54 \\     \end{array} $	$\begin{array}{c} & & & & & & & & & & & & & & & & & & &$
55 56 57 58 59	9.68459 .68481 .68503 .68526 .68548	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	9.97170 97213 97257 97300 97343	$\begin{array}{r} 43 \\ 43 \\ 43 \\ 43 \\ 43 \\ 43 \end{array}$	$   \begin{array}{r}         & 0.03703 \\             9.69787 \\             .69809 \\             .69831 \\             .69853 \\             .69875 \\         \end{array}   $	$22 \\ 22 \\ 22 \\ 21 \\ 22 \\ 21 \\ 22 \\ 22 \\$	9.99781 .99825 .99868 .99912 9.99956	443 43 44 43 44 3	55 56 57 58 59	40 14.614.3 50 18.3  <b>17.9</b>
	9.68571 Lg. Vers.	$\frac{2\overline{2}}{D}$	9.97387 Log. Exs.	$\frac{4\overline{3}}{D}$	9.69897 Lg. Vers.	22 D	10.00000 Log. Exs.	44 D	<u>60</u> /	P. P.
_	-51 10131	-	LOGICASI	1~	Les versi		LOGI LASI	-		1.1.

60°

61°

<u>'</u>	Lg. Vers.	D	Log. Exs.	D	Lg. Vers.	D	Log. Exs.	D	<u>·</u>	P. P.
0 1 2 3 4	9.69897 .69919 .69940 .69962 .69984	$22 \\ 21 \\ 22 \\ 22 \\ 22 \\ 22 \\ 22 \\ 22 \\$	$\begin{array}{r} 10.00000 \\ \cdot 00044 \\ \cdot 00087 \\ \cdot 00131 \\ \cdot 00175 \end{array}$	$\begin{array}{c} 44 \\ 43 \\ 44 \\ 43 \\ 43 \end{array}$	9.71197 .71218 .71289 .71261 .71282	$21 \\ 21 \\ 21 \\ 21 \\ 21 \\ 21 \\ 21 \\ 1$	10.02639 .02684 .02728 .02772 .02772 .02816	44 44 44 44	0 1 2 3 4	
56789	9.70006 .70028 .70050 .70072 .70093	22 21 22 22 21 21	10.00219 .00262 .00306 .00350 .00394	44 43 44 43 43	9.71304 .71325 .71346 .71368 .71389	$2\overline{1} \\ 2\overline{1} \\ 21 \\ 21 \\ 2\overline{1} \\ 2\overline{1} \\ 2\overline{1}$	10.02861 .02905 .02949 .02994 .02994 .03038	44 44 44 44 44	5 6 7 8 9	$\begin{array}{cccccccccccccccccccccccccccccccccccc$
10 11 12 13 14	9.70115 .70137 .70159 .70181 .70202	22 21 22 22 21 21	10.00438 .00482 .00525 .00569 .00613	44 43 44 44	9.71411 .71432 .71453 .71475 .71475 .71496	$21 \\ 21 \\ 21 \\ 21 \\ 21 \\ 21 \\ 21 \\ 21 \\$	$   \begin{array}{r}     10.0308\overline{2} \\     .03127 \\     .03171 \\     .03215 \\     .03260   \end{array} $	44 44 44 44 44 44	10 11 12 13 14	9 6.7 6.7 10 7.5 7.4 20 15.0 14.8 36 22.5 22.2 40 30.0 29.6 50 37.5 37.1
15 16 17 18 19	9.70224 .70246 .70268 .70289 .70311	22 21 22 21 22 21 22	10.00657 .00701 .00745 .00789 .00833	44 43 44 44 44	9.71517 .71539 .71560 .71581 .71603	$21 \\ 21 \\ 21 \\ 21 \\ 21 \\ 21 \\ 21 \\ 21 \\$	$   \begin{array}{r}     10.03304 \\     .03348 \\     .03393 \\     .03437 \\     .03481   \end{array} $	44 44 44 44	15 16 17 18 19	• 44 43
20 21 22 23 24	9.70333 .70355 .70376 .70398 .70420	21 22 21 22 21 22	10.00876 .00920 .00964 .01008 .01052	43 44 44 44 44	9.71624 .71645 .71667 .71688 .71688 .71709	$2\overline{1} \\ 21 \\ 21 \\ 21 \\ 21 \\ 21 \\ 21 \\ 21 \\ $	10.03526 .03570 .03615 .03659 .03704	44 44 44 44 44	20 21 22 23 24	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
25 26 27 28 29	9.70441 .70463 .70485 .70507 .70528	21 22 21 22 21 22 21	10.01096 .01140 .01184 .01228 .01272	44 44 44 44 44	9.71730 .71752 .71773 .71794 .71815	$21 \\ 21 \\ 21 \\ 21 \\ 21 \\ 21 \\ 21 \\ 21 \\$	10.03748 .03793 .03837 .03881 .03926	44 44 44 44 44	25 26 27 28 29	20   14 · 6   14 · 5 30   22 · 0   21 · 7 40   29 · 3   29 · 0 50   36 · 6   36 · 2
30 31 32 33 34	9.70550 .70572 .70593 .70615 .70636	$21 \\ 22 \\ 21 \\ 21 \\ 21 \\ 21 \\ 21 \\ 21 \\$	$\begin{array}{r} 10.0131\overline{6} \\ .0136\overline{0} \\ .0140\overline{4} \\ .0144\overline{8} \\ .0144\overline{8} \\ .0149\overline{2} \end{array}$	44 44 44 44 44	9.71837 .71858 .71879 .71900 .71922	$     \begin{array}{c}       2\overline{1} \\       21 \\       21 \\       21 \\       21 \\       21 \\       21 \\       21 \\       \end{array} $	10.03970 .04015 .04059 .04104 .04149	44 44 44 44 45	30 31 32 33 34	22 21 6  2.2  2.1
35 36 37 38 39	9.70658 .70680 .70701 .70723 .70745	$22 \\ 21 \\ 21 \\ 21 \\ 21 \\ 22 \\ 22 \\ 22 \\$	10.01536 .01580 .01624 .01668 .01668 .01712	44 44 44 44 44	9.71943 .71964 .71985 .72006 .72028	$     \begin{array}{c}       21 \\        21 \\        21 \\       21$	10.04193 .04238 .04282 .04327 .04371	44 44 44 44 44 44	35 36 37 38 39	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
40 41 42 43 44	9.70766 .70788 .70809 .70831 .70852	$21 \\ 21 \\ 21 \\ 21 \\ 21 \\ 21 \\ 21 \\ 21 \\$	10.01756 .01800 .01844 .01889 .01933	44 44 44 44 44	9.72049 .72070 .72091 .72112 .7213	21 21 21 21 21 21	$   \begin{array}{r}     10.04416 \\     .04461 \\     .04505 \\     .04550 \\     .04594 \\   \end{array} $	44 45 44 44 44 44	$     \begin{array}{r}       40 \\       41 \\       42 \\       43 \\       44     \end{array} $	30 11 .0 10 .7 40 14 .6 14 .3 50 18 .3 17 .9
45 46 47 48 49	9.70874 .70896 .70917 .70939 .70960	22 21 21 21 21 21	10.01977 .02021 .02065 .02109 .02153	44 44 44 44 44	9.72154 .72176 .72197 .72218 .72239		10.0463 .04684 .04728 .04778 .04778	45 44 44 44 45	45 46 47 48 49	<b>21</b> 6  2 · <u>1</u> 7  2 · <u>4</u>
50 51 52 53	9.70982 .71003 .71025 .71046	$\begin{array}{c}2\overline{1}\\2\overline{1}\\2\overline{1}\\2\overline{1}\\2\overline{1}\\2\overline{1}\end{array}$	10.02197 .02242 .02286 .02330	44 44 44 44	9.72280 .72281 .72302 .72323 .72323 .72344	$     \begin{array}{c}       2\overline{1} \\       21 \\       21 \\       21 \\       21 \\       21 \\       21 \\       21   \end{array} $	10.04862 .04907 .04952 .04952	44 45 44 44 45	50 51 52 53 54	8 2 - 9 9 3 · 1 10 3 · 5 20 7 · 0 30 10 · 5 40 14 · 0
54 55 56 57 58 59	$\begin{array}{r} \cdot 71068\\ 9.71089\\ \cdot 71111\\ \cdot 71132\\ \cdot 71154\\ \cdot 71175\end{array}$	$21 \\ 21 \\ 21 \\ 21 \\ 21 \\ 21 \\ 21 \\ 21 \\$	$     \begin{array}{r} \cdot 0237\overline{4} \\     10 \cdot 0241\overline{8} \\     \cdot 02463 \\     \cdot 02507 \\     \cdot 02551 \\     0250\overline{5}1   \end{array} $	44 44 44 44	9.72344 9.72385 .72386 .72408 .72429 .72429 .72450	21 21 21 21 21 21	$\begin{array}{r} .05041 \\ 10.05086 \\ .05131 \\ .05175 \\ .05220 \\ .05265 \end{array}$	44 45 44 45	55 56 57 58 59	40 14.0 50 17.5
<u>60</u>		21	02595 10.02639 Log. Exs.	44 D	9.72450 9.72471 Lg. Vers.	21 D	10.05310 Log. Exs.	45 D	<u>60</u> /	P. P.
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TABLE VIII.-LOGARITHMIC VERSED SINES AND EXTERNAL SECANTS.

		52°		63°						
			Log. Exs.							
01	9.72471 .72492	$21 \\ 21$	10.05310 .05354	$\frac{4\overline{4}}{45}$	9.73720 .73740	$2\overline{0}$ $2\overline{0}$	$10.0801\overline{5}$ .08061	$4\overline{5}$ 45	0	

012	9.72471 .72492 .72513	$21 \\ 21 \\ 21 \\ 21$	10.05310 .05354 .05399	44 45 45	9.73720 .73740 .73761	$2\overline{0}$ $2\overline{0}$ 21	10.08015 .08061 .0810 <u>6</u>	$4\overline{5} \\ 45 \\ 45 \\ 45 \\ 45 \\ 100 \\ $	$     \begin{array}{c}       0 \\       1 \\       2     \end{array} $	
34	·72534 ·72555	$     \begin{array}{c}       21 \\       21 \\       21     \end{array} $	$0544\overline{4}$ 05489	$45 \\ 44 \\ 45$	·73782 ·73802 9·73823	$20^{21}_{20}$ $20^{20}_{20}$	·08151 -08197	45	3	$\begin{array}{ccc} \mathbf{4\overline{6}} & 46 \\ 6 & 4 \cdot 6 \\ 4 \cdot 6 \\ 4 \cdot 6 \end{array}$
5 6 7	9.72576 .72597 .72618	$21 \\ 21 \\ 21 \\ 21$	10.05534 .05579 .05623	$45 \\ 44 \\ 45$	·73843 ·73864	20 20 20	10.08242 .08288 .08333	45 45 45 45	5 6 7	$\begin{array}{cccccccccccccccccccccccccccccccccccc$
89	•72639 •72660		·05668 .05713	45 45 45	·73884 ·73905	$\frac{20}{21}$ $2\overline{0}$	$ \begin{array}{r} \cdot 08379 \\ - 08424 \\ \end{array} $	45	8	$10 7.\overline{7} 7.\overline{6}$ $20 15.5 15.\overline{3}$
10 11 12	9.7268 <u>1</u> .7270 <u>1</u> .7272 <u>2</u>	$2ar{0}$ 21	10.05758 .05803 .05848	44 45	9 · 73926 · 73946 · 73967	$2\overline{0}$ $2\overline{0}$	$10.08470 \\ .08515 \\ .08561$	4 <u>5</u> 4 <u>5</u> 4 <u>5</u>	$10 \\ 11 \\ 12$	$\begin{array}{c} 30 & 23 \cdot 2 & 23 \cdot 0 \\ 40 & 31 \cdot 0 & 30 \cdot 6 \\ 50 & 38 \cdot 7 & 38 \cdot 3 \end{array}$
13 14	·7274 <u>3</u> ·72764	$21 \\ 21 \\ 21 \\ 21$	·05893 ·05938	45 45	·73987 ·74008	20 20 20	·08606 ·08652	4 <u>5</u> 4 <u>5</u> 4 <u>5</u>	13 14	
15 16	9.72785 .72806	$21 \\ 21 \\ 21 \\ 21$	$10.05983 \\ .06028$	$45 \\ 45 \\ 44$	$9.7402\overline{8}$ .74049	20 20 20	$10.0869\overline{7}$ .08743	45 4 <u>6</u> 4 <u>5</u> 4 <u>5</u>	15 16	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
17 18 19	•72827 •72848 •72869	$2\overline{0}$ 21	•0607 <u>2</u> •0611 <u>7</u> •06162	45 45	·74069 ·74090 ·74110	20 20	·08789 ·08834 ·08880	45	17 18 19	8 6.0 6.0 9 6.8 6.7
<b>20</b> 21	9.72890	$21 \\ 21 \\ 20$	$10.0620\overline{7}$ .06252	$\frac{45}{45}$	$9.74131 \\ .74151$	20 20 20	$10.08926 \\ .08971$	4 <u>6</u> 4 <u>5</u> 45	20 21	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
22 23 24	72931 72952 72973	$     \begin{array}{c}       20 \\       21 \\       21     \end{array}   $	·06297 ·06342 ·06387	45 45	.74172 .74192 .74213	20 20 20	·09017 ·09062 ·09108	$4\overline{5}$ 46	22 23 24	30 22 · 7 22 · 5 40 30 · 3 30 · 0 50 37 · 9 37 · 5
25 26	9.72994 .73015	$21 \\ 20 \\ 21$	$10.0643\overline{2}$ .06477	45 45	9.74233 .74254	20 20 20	10.09154 .09200	$45 \\ 46 \\ 45$	25 26	44
27 28 29	.73036 .73057 .73077	$\frac{21}{21}$ 20	•06522 •06568 •06613	4 <u>5</u> 45 45	.74274 .74294 .74315	20 20 20	·09245 ·09291 ·09337	45 45 46	27 28 29	$\begin{array}{c ccccc} 6 & 4 & \overline{4} \\ 7 & 5 & 2 \\ 8 & 5 & 9 \end{array}$
30 31	9.7309 <u>8</u> .73119	$\frac{21}{21}$	10.06658 .06703	$\frac{45}{45}$	9.74315 9.74335 .74356	20 20	10.09382 .09428	45 46	$\frac{29}{30}$ 31	9 6.7 10 7.4
32 33	·73140 ·7316 <u>1</u>	$2\bar{0} \\ 2\underline{1} \\ 2\bar{0}$	·06748 ·06793	45 4 <u>5</u> 45	·74376 ·74396	20 20 20	·09474 ·09520	4 <u>6</u> 45 46	32 33	$ \begin{array}{c} 20 \\ 14 \\ 30 \\ 22 \\ 40 \\ 29 \\ 6 \end{array} $
34 35 36	.73181 9.73202 73223	$\begin{array}{c} 21\\ 2\underline{1} \end{array}$	06838 10.06883 .06928	$\frac{45}{45}$	$\frac{.74417}{9.74437}$ .74458	20 20	·09566 10·09611 ·09657	$4\overline{5}$ $4\overline{6}$	34 35 36	50 37.1
37 38	·73223 ·73244 ·73265	$2\overline{0} \\ 2\underline{1} \\ 2\overline{0}$	.06974 .07019	45 45 45	·74478 ·74498	20 20 20	·09703 ·09749	$\frac{46}{45}$	37 38	$\begin{array}{ccc} 21 & \mathbf{2\overline{0}} \\ 6 & 2 \cdot \underline{1} & 2 \cdot \overline{0} \end{array}$
$\frac{39}{40}$ 41	.73285 9.73306 .73327	21 20	0.07064 10.07109 .07154	45 4 <u>5</u>	$     \frac{.74519}{9.74539} \\ .74559 $	20 20	09795 10.09841	4 <u>6</u> 45	$\frac{39}{40}$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
42 43	·73348 ·73368	$21 \\ 20 \\ 21$	·07200 ·07245	45 45 45	·74580 ·74600	20 20 20	·09886 ·09932 ·09978	46 46 46	41 42 43	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
44	$\frac{.73389}{9.73410}$	$2\overline{0}$ $2\overline{0}$	07290 10.07335	$4\overline{5}$	$\frac{\cdot 7462\overline{0}}{9 \cdot 7464\underline{1}}$	20 20 20	$\frac{.10024}{10.10070}$	46 46	44 45	$\begin{array}{c} 30 & 10 \cdot 5 & 10 \cdot 2 \\ 40 & 14 \cdot 0 & 13 \cdot 6 \\ 50 & 17 \cdot 5 & 17 \cdot 1 \end{array}$
46 47 48	.73430 .73451 .73472	21 20	·07380 ·07426 ·0747 <u>1</u>	45 45 45	·74661 ·74681 ·74702	$\frac{20}{20}$	$.1011\overline{6}$ $.1016\overline{2}$ .10208	$\frac{46}{45}$	46 47 48	
<u>49</u> 50	$\frac{.73493}{9.73513}$	$\begin{array}{c} 21\\ 2\overline{0}\\ 2\overline{0}\end{array}$	$   \frac{.07516}{10.07562} $	45 45 4 <u>5</u>	$\frac{.74722}{9.74742}$	$20 \\ 2\overline{0} \\ 20$	$\frac{.10254}{10.10300}$	46 46 46	$\frac{\tilde{49}}{50}$	20 6 2.0 7 2. <u>3</u> 8 2.6
51 52 53	·73534 ·73555 ·73575	$\frac{21}{20}$	·07607 ·07652 ·07697	45 45	·74762 ·74783 ·74803	20 20	$ \begin{array}{r} \cdot 10346 \\ \cdot 10392 \\ \cdot 10438 \end{array} $	$\begin{array}{c} 46 \\ 46 \end{array}$	51 52 53	9 3.0
54 55	<u>.73596</u> 9.7361 <u>7</u>	$2\overline{0} \\ 21 \\ 2\overline{0}$	<u>·07743</u> 10·07788	45 45	·74803 ·74823 9·74844	20 20	10438 10438 10484 $10 \cdot 10530$	46 46	54 55	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$
56 57 58	·73637 ·73658 ·73679	$2\overline{0}$ 21	·07834 ·07879	45 45 45	·74864 ·74884	$\frac{20}{20}\\20$	·10576 ·10622	46 46 46	56 57	$ \begin{array}{c} 30 & 10 \cdot \underline{0} \\ 40 & 13 \cdot \underline{3} \\ 50 & 16 \cdot 6 \end{array} $
59 60	•73699	20 20	$0792\overline{4}$ 07970 $10.0801\overline{5}$	45 45	$     \begin{array}{r} \cdot 7490\overline{4} \\ \cdot 7492\overline{4} \\ 9 \cdot 74945 \end{array} $	20 20	$.1066\overline{8}$ .10714 $10.1076\overline{0}$	46 46	58 59 60	
-	Lg. Vers.	D	Log. Exs.	D	Lg. Vers.	D	Log. Exs.	D	<u>"'</u>	P. P.

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TABLE VIII.—LOGARITHMIC	VERSED SINES AND	EXTERNAL SECAN
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,	Lg. Vers.	D	Log.Exs.	D	Lg. Vers.	D	Log.Exs.	D		P. P.
0 1 2 3 4	9.74945 .74965 .74985 .75005 .75026 9.75046	20 20 20 20 20 20 20	$   \begin{array}{r}     10.1076\overline{0} \\     .10807 \\     .10853 \\     .10899 \\     .10945 \\     10.1099\overline{1}   \end{array} $	$4\overline{6} \\ 46 \\ 4\overline{6} \\ 4\overline{6} \\ 46 \\ 46 \\ 46 \\ 46 \\ 46 \\ 46 \\ 46 \\ $	$9.7614\overline{6} \\.76166 \\.76186 \\.76206 \\.76225 \\9.7624\overline{5}$	$1\overline{9}$ 20 20 19 20 20	$   \begin{array}{r}     10.13551 \\     .13598 \\     .13645 \\     .13692 \\     .13739 \\     10.13785   \end{array} $	47 47 47 47 47 47	0 1 2 3 4 5	48 47 6  4·8  4·7
5 67 8 9	·75066 ·75086 ·75106 ·75126	20 20 20 20 20 20	$ \begin{array}{r} \cdot 1103\overline{7} \\ \cdot 11084 \\ \cdot 11130 \\ \cdot 11176 \\ \end{array} $	$     \frac{46}{46}     46     46     46   $	-76265 -76285 -76304 -76324	$1\overline{9} \\ 20 \\ 1\overline{9} \\ 20 \\ 20 \\ 20 \\ 20 \\ 20 \\ 20 \\ 20 \\ 2$		47 47 47 47 47	6 7 8 9	$\begin{array}{c} 6 & 4 \cdot 8 & 4 \cdot 7 \\ 7 & 5 \cdot 6 & 5 \cdot 5 \\ 8 & 6 \cdot 4 & 6 \cdot 3 \\ 9 & 7 \cdot 2 & 7 \cdot 1 \\ 10 & 8 \cdot 0 & 7 \cdot 9 \\ 20 & 16 \cdot 0 & 15 \cdot 8 \\ 20 & 16 \cdot 0 & 15 \cdot 8 \\ \end{array}$
$10 \\ 11 \\ 12 \\ 13 \\ 14 \\ 14 \\ 14 \\ 10 \\ 10 \\ 10 \\ 10 \\ 10$	9.75147 .75167 .75187 .75207 .75227	20 20 20 20 20 20 20	$ \begin{array}{r} 10.11222\\ .11269\\ .11315\\ .11361\\ .11407 \end{array} $	46 46 46 46 46	9 · 76344 76364 • 76384 • 76403 • 76423	19 20 19 20 19 20 19	$10.14021 \\ .14068 \\ .14115 \\ .14162 \\ .14210$	47 47 47 47 47 47	10 11 12 13 14	$\begin{array}{c} 30 \\ 40 \\ 32 \cdot 0 \\ 31 \cdot 6 \\ 50 \\ 40 \cdot 0 \\ 39 \cdot 6 \end{array}$
$15 \\ 16 \\ 17 \\ 18 \\ 19$	9.75247 .75267 .75287 .75308 .75328	20 20 20 20 20 20 20	$10.11454 \\ .11500 \\ .11546 \\ .11593 \\ .11639$	46 46 46 46 46 46 46	9 · 76443 · 76463 · 76482 · 76502 · 76522	19 20 19 19 20 19	$10.14257 \\ \cdot 14304 \\ \cdot 14351 \\ \cdot 14398 \\ \cdot 14445 \\ \end{array}$	47 47 47 47 47 47 47	15 16 17 18 19	$\begin{array}{cccccccccccccccccccccccccccccccccccc$
20 21 22 23 24	9.75348 .75368 .75388 .75408 .75428	20 20 20 20 20 20 20	$10.11685 \\ .11732 \\ .11778 \\ .11825 \\ .11871 \\ \end{array}$	466 466 466 466 46	9.76541.76561.76581.76600.76620	19 20 19 19 20 19 20 19	$10.14493 \\ .14540 \\ .14587 \\ .14634 \\ .14682$	47 47 47 47 47 47	20 21 22 23 24	$\begin{array}{c} 10 & 15 \cdot 6 \\ 20 & 15 \cdot 6 \\ 30 & 23 \cdot 5 & 23 \cdot 2 \\ 40 & 31 \cdot 3 & 31 \cdot 0 \\ 50 & 39 \cdot 1 & 38 \cdot 7 \end{array}$
25 26 27 28 29	9 · 75448 · 75468 · 75488 · 75508 · 75528	20 20 20 20	$\begin{array}{r} 10.1191\overline{7} \\ .11964 \\ .1201\overline{0} \\ .12057 \\ .1210\overline{3} \end{array}$	46 46 46 46	9.76640 .76659 .76679 .76699 .76718	$1\overline{9} \\ 20 \\ 1\overline{9} \\ 1\overline{9} \\ 1\overline{9}$	$\begin{array}{r} 10.14729 \\ .14776 \\ .14823 \\ .14871 \\ .14871 \\ .14918 \end{array}$	47 47 47 47	25 26 27 28 29	$ \begin{array}{c}     46 \\     6 \\     7 \\     5 \\     3 \\     8 \\     6 \\     1 \end{array} $
30 31 32 33 34	9.75548 .75568 .75588 .75588 .75608 .75628	20 20 20 20 20 20	$10.12150 \\ .12196 \\ .12243 \\ .12289 \\ .12336$	46666 4666 466	9 · 76738 · 76758 · 76777 · 76797 · 76817	20 19 19 19 20	10.14965.15013.15060.15108.15155	47 47 47 47 47 47	30 31 32 33 34	9 6.9 10 7.6 20 15.3 30 23.0 40 30.6 50 38.3
35 36 37 38 39	9 · 75648 · 75668 · 75688 · 75708 · 75728	20 20 20 20 20 20	10.12383.12429.12476.12522.12522.12569	47 46 46 46 46 46	9 · 76836 · 76856 · 76875 · 76895 · 76915	19 19 19 20 19	$\begin{array}{r} 10.1520\bar{2} \\ .15250 \\ .15297 \\ .15297 \\ .15345 \\ .15392 \end{array}$	47 47 47 47 47	35 36 37 38 39	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
40 41 42 43 44	9 · 75748 · 75768 · 75788 · 75808 · 75828	20 20 20 20 19	$\begin{array}{r} 10.1261\underline{6}\\ .1266\underline{2}\\ .12709\\ .1275\underline{6}\\ .1280\underline{2}\end{array}$	47 46 47 46 47 46	9 · 76934 · 76954 · 76973 · 76993 · 76993 · 77012	$1\overline{9}$ $1\overline{9}$ $1\overline{9}$ $1\overline{9}$ $1\overline{9}$ $1\overline{9}$ 20	$10.15440 \\ .15487 \\ .15535 \\ .15582 \\ .15630 \\ \end{array}$	47	$     \begin{array}{r}       40 \\       41 \\       42 \\       43 \\       44     \end{array}   $	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
45 46 47 48 49	9.75848 .75868 .75888 .75908 .75928	20 20 20 20 20	10.12849 .12896 .12942 .12989 .12989 .13036	46 47 46 47 46 47 40	9.77032 .77052 .77071 .77091 .77110	20 19 19 19 19	$10.15678 \\ .15725 \\ .15773 \\ .15773 \\ .15820 \\ .15868 \\$	48	45 46 47 48 49	40 13 . 8 13 . 3 50 17 . 1 16 . 6 19 6 1 . 9
50 51 52 53 54		$1\overline{9} \\ 20 \\ 20 \\ 20 \\ 1\overline{9} \\ 1\overline{9} \\ 0$	$10.13083 \\ .13130 \\ .13176 \\ .13223 \\ .13270 \\$	47 4 <u>7</u> 46 47 46	9.77130 .77149 .77169 .77188 .77208	$19 \\ 19 \\ 19 \\ 19 \\ 19 \\ 19$	10.15916.15963.16011.16059.16105	47 48 47 47	50 51 52 53 54	7 2.3 8 2.6 9 2.9 10 3.2
55 56 57 58 59	9.76047 .76067 .76087 .76106	20 20 20 19 20	$     \begin{array}{r}       10.13317 \\       .13364 \\       .13411 \\       .13457 \\       .13504     \end{array} $	46	9 · 77227 · 77247 · 77266 · 77286 · 77286 · 77305	$19 \\ 19 \\ 19 \\ 19 \\ 19 \\ 19 \\ 19 \\ 19 \\$	$\begin{array}{r} 10.1615\overline{4} \\ .16202 \\ .16250 \\ .16298 \\ .16345 \end{array}$	48 47 48 48 47	55 56 57 58 59	$\begin{array}{c c} 20 & 6.5 \\ 30 & 9.7 \\ 40 & 13.0 \\ 50 & 16.2 \end{array}$
<u>60</u> /		20	10.13551 Log.Exs.	47 D	9 · 77325 Lg. Vers	$1\bar{9}$	10.16393 Log. Exs.	1 10	$\frac{60}{7}$	P. P.

TABLE VIIILOGARITHMIC VERSI	D SINES ANI	) EXTERNAL SECANTS.
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66°

67°

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	Lg. Vers.	D	Log.Exs.	D	Lg. Vers.	D	Log. Exs.	D	•	P. P.
O 123 4 567 89 011234 567 89 01234 567 89 0123 38 38 56	9.77325 .77344 .77363 .77383 .77342 9.77420 9.77420 9.77420 .77480 .77480 9.77519 .77557 .77557 .77557 .77557 .77557 .77654 .77654 .77654 .77659 9.77712 .77750 9.77721 .77750 .777809 .777800 .7777800 .777800 .777800 .7778000 .77778000 .7778000 .7778000 .77780000	D         100000         0000000         000000         000000	10.16393 .16441 .16489 .16537 .16587 .16587 .16587 .16587 .16587 .16728 .16728 .16728 .16920 .1706 .1706 .1706 .1706 .1706 .1706 .17127 .17305 10.17353 .17401 .17449 .17546 10.17594 .17690 .17787 10.17835 .17832 .17832 .17832 .17980 .18929 .18929 .17980 .18929 .18929 .17980 .18929 .18929 .18929 .17980 .18929 .18929 .18929 .17885 .178	44444 44444 44444 44444 44444 44444 4444	9.78481 .78500 .78519 .78575 .78575 .78575 .78575 .78614 .78652 9.78671 .78652 9.78670 .78709 9.78747 9.78747 9.78747 .78804 .78904 .78904 .78904 .78904 .78904 .78904 .78904 .78904 .78904 .78904 .79905 .79905 .79904 .79905 .79904 .79905 .79904 .79905 .79904 .79905 .79904 .79905 .79904 .79905 .79904 .79905 .79	19 19 19 19 19 19 19 19 19 19 19 19 19 1	Log. Exs. 10.19293 .19342 .19391 .19439 .19438 .19438 .19586 .19635 .19635 .19635 .19635 .19635 .19636 .19636 .19733 10.19782 .19831 .19830 .19929 10.20028 .200777 .20175 .20224 .20274 .20274 .20274 .20274 .20275 .20427 .20427 .20427 .20427 .20427 .20427 .20427 .20569 .20618 .20618 .20618 .20717 10.20767 .20865 .20915 .20964 10.21014 .21063	D 9998999999999999999999999999999999999	, 012334 56789 0111234 56789 000000000000000000000000000000000000	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
367 378 39 40 412 43 44 456 47 48 9 50 512 53 55 55 55 55 55 55 55 55 55 55 55 55	780421 780450 78050 978078 978078 978174 978155 78155 78155 78155 78155 78213 782251 782251 782250 978285 78309 78328 78309 78385 78345 78404 78	$\begin{array}{c} 19\\ 19\\ 19\\ 19\\ 19\\ 19\\ 19\\ 19\\ 19\\ 19\\$	18174 18174 18272 18271 10.18319 18368 18368 184165 18514 10.18562 18619 18659 18708 18805 18805 18805 18951 19000 10.19049 19049 19146 19243	4888 888888889889889889889889889889889889	. 79164 .79163 .79202 9.79220 9.79220 9.79220 9.79220 .79226 .793352 .79352 .79352 .79352 .79409 9.79426 .79446 .79446 .79446 .79446 .79503 9.79521 .79540 .79540 .795578 .795	$\begin{array}{c} 19\\ 19\\ 19\\ 18\\ 19\\ 19\\ 18\\ 19\\ 19\\ 18\\ 19\\ 19\\ 18\\ 18\\ 18\\ 18\\ 18\\ 18\\ 18\\ 18\\ 18\\ 18$	$\begin{array}{r} .21063\\ .21113\\ .21162\\ .21212\\ .21212\\ .21212\\ .21311\\ .21460\\ .21460\\ .21460\\ .21659\\ .21659\\ .21659\\ .21659\\ .21759\\ .21858\\ .21908\\ .21908\\ .21908\\ .22088\\ .22088\\ .22088\\ .22188\\ .22208\\ .22288\\ .2288\\ .28888\\ .28888\\ .28888\\ .28888\\ .28888\\ .28888\\ .28888\\ $	445 4445 900 900 900 900 900 900 900 900 900 90		$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
17	Lg. Vers.	$\overline{D}$	Log. Exs.	$\overline{D}$	Lg. Vers.		Log. Exs.	D	ŕ	P. P.
1 1000		_			and the second se	_		_		

68°

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**69°** 

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•	Lg, Vers,	D	Log.Exs.	D	Lg. Vers.	D	Log.Exs.	D	·	P. P.
01234	9.79615 •79634 •79653 •79671 •79690	18 19 18 18	$10.22258 \\ \cdot 22308 \\ \cdot 22358 \\ \cdot 22408 \\ \cdot 22458 \\ \cdot 2$	50 50 50 50	9.80728 .80747 .80765 .80783 .80802	$1\overline{8} \\ 1\overline{8} \\ 18 \\ 18 \\ 1\overline{8} \\ 1\overline$	10 · 25295 · 25347 · 25398 · 25449 · 25501	5 <u>1</u> 5 <u>1</u> 5 <u>1</u> 5 <u>1</u>	$     \begin{array}{c}       0 \\       1 \\       2 \\       3 \\       4     \end{array} $	$\begin{array}{c ccccc} 53 & 5\overline{2} \\ 6 & 5 \cdot 3 & 5 \cdot \overline{2} \\ 7 & 6 \cdot 2 & 6 \cdot \overline{1} \\ 8 & 7 \cdot \overline{0} & 7 \cdot 0 \\ 9 & 7 \cdot \overline{9} & 7 \cdot 9 \\ 10 & 8 \cdot \overline{8} & 8 \cdot \overline{7} \end{array}$
5 6 7 8 9	9.79709 .79727 .79746 .79765 .79783	19 18 19 18 18	10.22508 22558 22608 22658 22658 22708	50 50 50 50 50	9.80820 .80839 .80857 .80875 .80894	$1\frac{8}{18}$ $1\frac{8}{18}$ $1\frac{8}{18}$ $1\frac{8}{18}$	10.25552 25604 25655 25707 25758	51 51 51 51 51	5 6 7 8 9	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
10 11 12 13 14	9.79802 .79821 .79839 .79858 .79858 .79877	19 18 19 19 19	10.22759 .22809 .22859 .22909 .22909 .22960	50 50 50 50 50	9.80912 .80930 .80949 .80967 .80985	$18 \\ 18 \\ 18 \\ 18 \\ 18 \\ 18 \\ 18 \\ 18 \\$	10.25810 .25861 .25913 .25964 .25016	51 51 51 51 51	10 11 12 13 14	$\begin{array}{cccccccccccccccccccccccccccccccccccc$
15 16 17 18 <u>19</u>	9.79895 .79914 .79933 .79951 .79970	18 19 19 18 18	$10.23010 \\ \cdot 23060 \\ \cdot 23110 \\ \cdot 23161 \\ \cdot 23211 \\ \end{array}$	50 50 50 50 50 50 50	9.81003 .81022 .81040 .81058 .81077	18     18     18     18     18     18     18     18     1	$10.2606\overline{7} \\ .2611\overline{9} \\ .26171 \\ .2622\overline{2} \\ .2627\overline{4}$	51 52 51 52 51 52 52 51	15 16 17 18 19	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
20 21 22 23 24	9.79988 .80007 .80026 .80044 .80063	18 19 18 18 18 18	10.23262 .23312 .23362 .23413 .23463	50 50 50 50 50	9.81095 .8111 <u>3</u> .81131 .81150 .81168	$     \begin{array}{c}       18 \\$	$\begin{array}{r} 10.26326\\ \cdot 26378\\ \cdot 26429\\ \cdot 26481\\ \cdot 26533\end{array}$	52 51 52 52	20 21 22 23 24	$\begin{array}{cccc} 51 & 5\overline{0} \\ 6 & 5 \cdot 1 & 5 \cdot \overline{0} \\ 7 & 5 \cdot 9 & 5 \cdot 9 \\ 8 & 6 \cdot 8 & 6 \cdot \overline{7} \\ 9 & 7 \cdot 6 & 7 \cdot 6 \end{array}$
25 26 27 28 29	9.80081 .80100 .80119 .80137 .80156	1819181818181	10.23514 .23564 .23615 .23666 .23716	50 50 50 50 50	9.81186 .81204 .81223 .81241 .81259	$1\overline{8} \\ 18 \\ 18 \\ 18 \\ 18 \\ 18 \\ 18 \\ 18 \\ $	10.26585 .26637 .26689 .26741 .26793	52 51 52 52 52	25 26 27 28 29	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
30 31 32 33 34	9.80174 .80193 .80211 .80230 .80248	18 18 18 18 18 18 18 18	10.23767 .23817 .23868 .23919 .23969	50 50 51 50 50 50	9.81277 .81295 .81314 .81332 .81350	$     \begin{array}{r}       18 \\       18 \\       18 \\       18 \\       18 \\       18 \\       18 \\     \end{array} $	10.26845.26897.26949.27001.27053	52 52 52 52 52 52	30 31 32 33 34	50 6  5.0 7  5.8 8  6.6
35 36 37 38 39	9.80267 .80286 .80304 .80323 .80341	19 18 18 18 18 18 18	$10.24020 \\ .24071 \\ .24122 \\ .24172 \\ .2423$	51 50 51 50 51 50	9.8136 81386 .81405 .81423 .81441	18 18 18 18 18	10.27105.27157.27209.27261.27314	52 52 52 52 52 52	35 36 37 38 39	$\begin{array}{c} 9 & 7 \cdot 5 \\ 10 & 8 \cdot 3 \\ 20 & 16 \cdot 6 \\ 30 & 25 \cdot 0 \\ 40 & 33 \cdot 3 \end{array}$
40 41 42 43 44	9.80360 .80378 .80397 .80415 .80434	1888	$10.2427\overline{4} \\ .24325 \\ .24376 \\ .24427 \\ .24427 \\ .24478 \\$	51 50 51 51 51 51	9.81459 .81477 .81495 .81513 .81532	$1\overline{8} \\ 18 \\ 18 \\ 18 \\ 18 \\ 18 \\ 18 \\ 18 \\ $	10.27366.27418.27470.27523.27523.27575	52 52 52 52 52 52 52 52 52	$     \begin{array}{r}       40 \\       41 \\       42 \\       43 \\       44     \end{array} $	$50 41.\overline{6}$ $19  1\overline{8}$ $6  \ 1.9  \ 1.\overline{8}$ $7  2.2  2.\overline{1}$ $8  \ 2.\overline{5}  \ 2.4$
45 46 47 48 49	9.80452 .80470 .80489 .80507 .80526	18 18 18 18 18 18 18	10.24529 .24580 .24631 .24682 .24733	51 51 51 51 51	9.81550 .81568 .81586 .81604 .81604 .81622	18 18 18 18 18	10 · 22627 • 27680 • 27732 • 27785 • 2785 • 27837	52121212 55255 552	45 46 47 48 49	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
50 51 52 53 54	9.80544 .80563 .80587 .80600 .80618	$1\overline{8}$ $1\overline{8}$ $1\overline{8}$ $1\overline{8}$ $1\overline{8}$ $1\overline{8}$ $1\overline{8}$	10.24784 .24835 .24886 .24937 .24988	51 51 51 51 51 51	9.81640 .81658 .81676 .81695 .81713	18 18 18 18 18	10.27890 .27942 .27995 .28047 .28100	5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	50 51 52 53 54	18 6 1.8 7 2.1
55 56 57 58 59	9.80636 .80655 .80673 .80692 .80710	18 18 18 18 18 18 18	10.25039 .25090 .25142 .25193 .25244	51 51 51 51 51 51	9.81731 .81749 .81767 .81785 .81803	18 18 18 18 18	10 · 28152 · 28205 · 28258 · 28310 · 28363	53 53 52 52 53 52 53 53 53	55 56 57 58 59	8 2·4 9 2·7 10 3·0 20 6·0 30 9·0 40 12·0
<u>60</u> /	<u>9.80728</u> Lg. Vers.	$1\overline{8}$ <b>D</b>	10.25295 Log.Exs.	51 D	9.81821 Lg. Vers.	18 D	10.28416 Log.Exs.	$\frac{5\overline{2}}{D}$	<u>60</u> '	50 15.0 P. P.
_									-	Construction of the second sec

'ABLE	VIIILOGARITHMIC	VERSED SINES ANI	D EXTERNAL SECANTS.
	70°	71°	

-			70*		71°					
-	Lg. Vers.	D	Log. Exs.	D	Lg. Vers.	D	Log. Exs.	D	<u>′</u>	P. P.
01234 5678	9.81821 .81839 .81857 .81875 .81893 9.81911 .81929 .81947 .81947 .81965	18 18 18 18 18 18 18 18	$10.28416 \\ .28469 \\ .28521 \\ .28574 \\ .28627 \\ 10.28680 \\ .28733 \\ .28786 \\ .28736 \\ .28839 \\ \end{array}$	53 52 53 53 53 52 53 53 53 53 53	9.82894 .82911 .82929 .82947 .82964 9.82982 .83000 .83017 .83035	$1\frac{7}{17}$ 18 17 18 17 18 17 18 17 18	$10.3162\bar{9} \\ .31684 \\ .31738 \\ .31793 \\ .3184 \\ \overline{10.31902} \\ .31905 \\ .32011 \\ .32066 \\ \end{array}$	5444 5555 5555 55555 55555	012345678	$\begin{array}{cccccccccccccccccccccccccccccccccccc$
9 10 11 12 13 14 15 16 17 18	.81983 9.82001 .82019 .82037 .82055 .82073 9.82091 .82109 .82109 .82127 .82145	18 18 18 18 18 18 18 17 18 17 18	28892 -28892 10.28945 -28998 -29051 -29104 -29157 10.29210 -29263 -29316 -29370	53 53 53 53 53 53 53 53 53 53 53 53 53 5	$\begin{array}{r} .83053\\ \underline{.83053}\\ 9.83070\\ \underline{.83088}\\ .83106\\ \underline{.83123}\\ \underline{.83141}\\ 9.83159\\ \underline{.83194}\\ .83211\end{array}$	$1\overline{7}$ 17	$\begin{array}{r} .32120\\ .32120\\ 10.32175\\ .32230\\ .32339\\ .32339\\ .32394\\ 10.32449\\ .32504\\ .32558\\ .32613\end{array}$	54454554 55555555555555555555555555555	9 10 11 12 13 14 15 16 17 18	$50 47 \cdot 1 46 \cdot \overline{6}$ $5\overline{5}  55$ $6   5 \cdot \overline{5}   5 \cdot 5$ $7   6 \cdot 5   6 \cdot 4$ $8   7 \cdot 4   7 \cdot 3$ $9   8 \cdot 3   8 \cdot 2$ $10   9 \cdot 2   9 \cdot 1$ $20  18 \cdot 5  18 \cdot 3$ $30  27 \cdot 7  27 \cdot 5$ $40  37 \cdot 0  36 \cdot \overline{6} $
19 20 21 22 23 24 25 26 27 28	<u>.82163</u> 9.82181 .82199 .82217 .82255 .82252 9.82270 .82288 .82306 .82324	18 18 18 18 17 18 18 18 18 18 18 18 17	$\begin{array}{r} .29423 \\ \hline 10.29476 \\ .29529 \\ .29529 \\ .29636 \\ .29689 \\ \hline 10.29743 \\ .29796 \\ .29796 \\ .29795 \\ .29903 \\ \end{array}$	5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	<u>.83223</u> 9.83247 .83264 .83282 .83299 <u>.83317</u> 9.83335 .83352 .83352 .83370 .83387	$   \begin{array}{r} 18 \\     1\overline{7} \\      1\overline{7} \\   $	$\begin{array}{r} \underline{32668} \\ 10\cdot32723 \\ \underline{32778} \\ \underline{32833} \\ \underline{32833} \\ \underline{32944} \\ 10\cdot329949 \\ \underline{339054} \\ \underline{33109} \\ \underline{33164} \\ \end{array}$	55555555555555555555555555555555555555	19 20 21 22 23 24 25 26 27 28	$50 46\cdot \overline{2} 45\cdot \overline{8}$ $5\overline{4}  5\overline{4}$ $6   5\cdot \overline{4}   5\cdot 4$ $7   6\cdot \overline{3}   6\cdot 3$ $8   7\cdot 2   7\cdot 2$ $9   8\cdot 2   8\cdot 1$ $10   9\cdot 1   9\cdot 0$ $20   8\cdot 1  18\cdot 0$ $30   27\cdot \overline{2}   27\cdot 0$ $40   36\cdot 3   36\cdot 0$
29 30 31 32 33 34 35 36 37 38	<u>82342</u> 9.82360 82378 82396 8241 <u>3</u> 82431 9.82449 82467 82485 82485 82485 82503	18 18 18 17 18 17 18 17 18 17 18 17	$\begin{array}{r} .29957\\ 10.30010\\ .30064\\ .30117\\ .3017\\ .30225\\ 10.30278\\ .30332\\ .30332\\ .30386\\ .30440\end{array}$	55555555555555555555555555555555555555	<u>83405</u> 9 · 83422 · 83440 · 83458 · 83475 · 83493 9 · 83510 · 83528 · 83545 · 83563	$1\overline{7}$ $1\overline{7}$ $1\overline{7}$ $1\overline{7}$ $1\overline{7}$ $1\overline{7}$ $1\overline{7}$ $1\overline{7}$ $1\overline{7}$ $1\overline{7}$ $1\overline{7}$ $1\overline{7}$	.33220 10.33275 .33330 .33385 .33496 10.33552 .33607 .33663 .33718	ରୁ ପ୍ରକ୍ରମ ସ୍ଥାରମ୍ଭର ଅଭାରାସାରା ସାସାରାମ୍ବର ସ୍ଥାର	29 30 31 32 33 34 35 36 37 38	$50145 \cdot 4145 \cdot 0$ $53 53$ $6  5 \cdot 3  5 \cdot 3$ $7  6 \cdot 2  6 \cdot 2$ $8  7 \cdot 1  7 \cdot 0$ $9  8 \cdot 0  7 \cdot 9$ $10  8 \cdot 9  8 \cdot 8$ $20  17 \cdot 8  17 \cdot 6$ $30  26 \cdot 7  26 \cdot 5$
39 40 41 42 43 44 45 46 47 48 49	<u>82520</u> 9.82538 82556 82574 82592 <u>82609</u> 9.82627 82645 82645 82681 82681 82681 82695	18 18 17 18 17 18 17 18 17 18 17 18 17	.30493 10.30547 .30601 .30655 .30709 .30763 10.30817 .30871 .30925 .30979 .31033	54 53 54 54 54 54 54 54 54 54 54 54 54 54 54	<u>83580</u> 9.83598 83615 83633 83650 <u>83668</u> 9.83685 83703 83720 83727 83755	$1\frac{7}{17}$ $1\frac{7}{17}$ $1\frac{7}{17}$ $1\frac{7}{17}$ $1\frac{7}{17}$ $1\frac{7}{17}$ $1\frac{7}{17}$	$\begin{array}{r} .33774 \\ 10.33829 \\ .33885 \\ .33996 \\ .34052 \\ 10.34108 \\ .34164 \\ .34220 \\ .34275 \\ .34231 \\ \end{array}$	55555555555555555555555555555555555555	39 40 41 42 43 44 45 46 47 48 49	$\begin{array}{c} 40135 \cdot 6135 \cdot 3 \\ 50144 \cdot 6144 \cdot 1 \\ 5\overline{2} \\ 6 \\ 7 \cdot 6 \\ 7 \cdot 7 \\ 7 \cdot 9 \\ 10 \\ 10 \\ 10 \\ 10 \\ 10 \\ 10 \\ 10 \\ $
50 51 52 53 55 55 55 55 55 55 55 55 55 55 55 55	9.82716 .82734 .82752 .82769 .82787 9.82805 .82840 .82840 .82856 .82856 .82876 9.82894 Lg. Vers	$ \begin{array}{c} 18\\17\\18\\17\\18\\17\\18\\17\\18\\17\\18\\17\\18\\17\\18\\D\end{array} $	10.31087 .31141 .31195 .31249 .31303 10.31358 .31412 .31466 .31521 .31575 10.31629 Log. Exs	54454 54455555555555555555555555555555	9 · 83772 83700 83807 · 83825 · 83842 9 · 83852 · 83842 9 · 83854 · 83894 · 83912 · 83929 9 · 83946 Lg, Vers,	$   \begin{array}{c}     1\overline{7} \\      1\overline{7} \\     1$	10.34387 .34493 .34555 .34555 .34611 10.34667 .34723 .34780 .34780 .34892 10.34948 Log. Exs.	56 56 56 56 56 56 56 56 56 56 56 56 56 5	<b>50</b> <b>51</b> <b>52</b> <b>53</b> <b>56</b> <b>57</b> <b>58</b> <b>59</b> <b>60</b>	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$

TABLE VIII.—LOGARITHMIC VERSED SINES AND EXTERNAL SECANTS         72°       73°									
		<i>i</i>	(						
' Lg. Vers.	D	Log.Exs.	$\mathcal{D}$	Lg. Vers.	D	Log. Exs.	D	'	P. P. '
$\begin{array}{c} 0 & 9.8394\bar{6} \\ 1 & .83964 \\ 2 & .8398\bar{1} \\ 3 & .83999 \\ 4 & .84016 \\ 5 & 9.8403\bar{3} \\ 6 & .8405\underline{1} \end{array}$	$17 \\ 17 \\ 17 \\ 17 \\ 17 \\ 17 \\ 17 \\ 17 \\$	$10.3494\bar{8} \\ .35005 \\ .35061 \\ .35117 \\ .35174 \\ 10.3523\bar{0} \\ .35286 \\ .35286 \\ \end{array}$	56666 5566 5555 556	$\begin{array}{r} 9.8498\bar{0}\\ .8499\bar{7}\\ .85014\\ .8503\bar{1}\\ .85049\\ 9.85066\\ .85083\end{array}$	$17 \\ 17 \\ 17 \\ 17 \\ 17 \\ 17 \\ 17 \\ 17 \\$	$\begin{array}{r} 10.38387\\ .38445\\ .38504\\ .38562\\ \underline{.38621}\\ 10.38679\\ .38738\end{array}$	55555555555555555555555555555555555555	01234 56	$\begin{array}{c} 61 & 60 \\ 6 & 6 \cdot 1 & 6 \cdot 0 \\ 7 & 7 \cdot 1 & 7 \cdot 0 \\ 8 & 8 \cdot 1 & 8 \cdot 0 \\ 9 & 9 \cdot 1 & 9 \cdot 1 \\ 10 & 10 \cdot 1 & 10 \cdot 1 \\ 20 & 20 \cdot 3 & 20 \cdot 1 \\ 30 & 30 \cdot 5 & 30 \cdot 2 \\ 40 & 40 \cdot 6 & 40 \cdot 3 \\ 50 & 50 \cdot 8 & 50 \cdot 4 \end{array}$
7 .84068 8 .84085 9 .84103	$17 \\ 17 \\ 17 \\ 17 \\ 17 \\ 17 \\ 17 \\ 17 \\$	·35343 ·35399 ·35456	56 57 5 <u>6</u>	.85100 .85117 <u>.85134</u>	17 17 17 17	·38796 ·38855 ·38914	59 58 59	7 8 9	
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	17 17 17 17 17	10.35513.35569.35626.35683.3573910.35796	56 57 57 56 57	9.85151 .85168 .85185 .85202 .85219	17 17 17 17 17	$ \begin{array}{r} 10.38973 \\ .39031 \\ .39090 \\ .39149 \\ .39208 \\ 10.0000 \\ \end{array} $	58 59 59 58 59 58 59	$     \begin{array}{c}       10 \\       11 \\       12 \\       13 \\       14 \\       15     \end{array} $	60 59 6 6.0 5.9 7 7.0 6.9 8 8.0 7.9 9 9.0 8.9
15         9.84207           16         .84224           17         .84241           18         .84259           19         .84276           20         9.84293	$17 \\ 17 \\ 17 \\ 17 \\ 17 \\ 17 \\ 17 \\ 17 \\$	10.35796 -35853 -35910 -35967 -36023 10.36080	56 57 57 56 57	9.85236 .85253 .85270 .85287 <u>.85304</u> 9.85321	17 17 17 17 17	10.39267.39326.39385.39444.39503	59 59 59 59 59 59 59 59	15 16 17 18 19	10 10.0 9.9 20 20.0 19.8 30 30.0 29.7 40 40.0 39.6 50 50.0 49.6
$\begin{array}{cccc} 21 & \cdot 8431\bar{0} \\ 22 & \cdot 84328 \\ 23 & \cdot 8434\bar{5} \\ \underline{24} & \cdot 8436\bar{2} \end{array}$	17 17 17 17 17 17	$ \begin{array}{r} \cdot 3613\overline{7} \\ \cdot 3619\overline{4} \\ \cdot 3625\overline{1} \\ \cdot 3630\overline{8} \end{array} $	57 57 57 57 57 57	-85338 -85355 -85372 -85389	$17 \\ 17 \\ 17 \\ 17 \\ 17 \\ 16 \\ 1\overline{6}$	10.39562 .39621 .39681 .39740 .39799	59 59 59 59 59 59 59 59 59	20 21 22 23 24	$\begin{array}{c} 59 & 58 \\ 6 & 5 \cdot 9 & 5 \cdot 8 \\ 7 & 6 \cdot 9 & 6 \cdot 8 \\ 8 & 7 \cdot 8 & 7 \cdot 8 \\ 9 & 8 \cdot 8 & 8 \cdot 8 \\ 10 & 9 \cdot 8 & 9 \cdot 7 \\ 20 & 19 \cdot 6 & 19 \cdot 5 \\ 20 & 19 \cdot 6 & 19 \cdot 5 \\ \end{array}$
$\begin{array}{c} 25 \\ 9 \cdot 84380 \\ 26 \\ \cdot 84397 \\ 27 \\ \cdot 84414 \\ 28 \\ \cdot 84431 \\ \underline{29} \\ \cdot 84449 \\ \underline{29} \\ \cdot 844449 \\ \underline{29} \\ \cdot 844449 \\ \underline{29} \\ \cdot 84444 \\ \underline{29} \\ \cdot 844$	$     \begin{array}{r}       17 \\$	10.36366.36423.36480.36537.36594	57 57 57 57 57	9.85405 .85422 .85439 .85456 .85473	17 17 17 17 17	10.39859.39918.39977.40037.40096	5999999 59999 599 599 599 599 599 599 5	25 26 27 28 29	9 8.8 8.8 10 9.8 9.7 20 19.6 19.5 30 29.5 29.2 40 39.3 39.0 50 49.1 48.7
<b>30</b> 9.84466 <b>8</b> 1 .84483 32 .84500 33 .84517 34 .84535	17 17 17 17 17	10.36652 .36709 .36766 .36824 .36881	57 57 57 57 57 57	9.85490 .85507 .85524 .85541 .85558	17 16 17 17 17	$10.40156 \\ .40216 \\ .40275 \\ .40335 \\ .40395 \\ .40395$	60 59 59 60 59	30 31 32 33 34	58 57 6 5.8 5.7 7 6.7 8 7.7 7 6.7
35         9.84552           36         .84569           37         .84586           38         .84603           39         .84620           40         9.84638	17 17 17 17 17 17	$   \begin{array}{r}     10.36938 \\     .36996 \\     .37054 \\     .37111 \\     \underline{.37169} \\     10.27208 \\   \end{array} $	57 58 57 57 57 57	9 · 85575 · 85592 · 85608 · 85625 · 85642	1 <u>7</u> 16 17 17 17	$10.4045\overline{4} \\ .4051\overline{4} \\ .40574 \\ .40634 \\ .40694 \\ 10.40754 \\ .40694 \\ 10.40754 \\ 10$	60 59 60 60 60	35 36 37 38 39 40	9 8.7 8.6 10 9.6 9.6 20 19.3 19.1 30 29.0 28.7 40 38.6 38.3 50 48.3 47.9
$\begin{array}{cccc} 41 & \cdot 84655 \\ 42 & \cdot 84672 \\ 43 & \cdot 84689 \\ 44 & \cdot 84706 \end{array}$	$17 \\ 17 \\ 17 \\ 17 \\ 17 \\ 17 \\ 17 \\ 1\overline{7}$	$   \begin{array}{r}     10.37226 \\     .37284 \\     .37342 \\     .37399 \\     .37457 \\     .37457 \\   \end{array} $	57 58 57 58 58	9.85659 .85676 .85693 .85710 .85726	16 17 17 16 17	$   \begin{array}{r}     10.40754 \\     .40814 \\     .40874 \\     .40934 \\     .40994 \\     10.41057   \end{array} $	60 60 60 60 60	40 41 42 43 44 45	57 56 6 5.7 5.6 7 6.6 6.6 9 7.6 7.5
$\begin{array}{ccc} 46 & .84741 \\ 47 & .84758 \\ 48 & .84775 \\ \underline{49} & .84792 \end{array}$	17 17 17 17 17	$   \begin{array}{r}     10.37515 \\     .37573 \\     .37631 \\     .37689 \\     .37747 \\   \end{array} $	57 58 58 58 58 58	9.8574 <u>3</u> .85760 .85777 .85794 .85811	17 16 17 17 17	$10.4105\frac{4}{.41114}$ $.41174$ $.41235$ $.41295$ $10.4125$	60 60 60 60 60	46 47 48 49	$\begin{array}{c c c} 9 & 8 \cdot \overline{5} & 8 \cdot 5 \\ 10 & 9 \cdot 5 & 9 \cdot 4 \\ 20 & 19 \cdot 0 & 18 \cdot \overline{8} \\ 30 & 28 \cdot 5 & 28 \cdot 2 \\ 40 & 38 \cdot 0 & 37 \cdot \overline{6} \\ 50 & 47 \cdot 5 & 47 \cdot 1 \end{array}$
$\begin{array}{c} {\bf 50} 9.8480 \bar{9} \\ 51 \\ 52 \\ .8482 \bar{6} \\ 52 \\ .84844 \\ 53 \\ .84861 \\ .84878 \\ \end{array}$	17 17 17 17 17 17	10.37805.37863.37921.37979.38037	58 58 58 58 58 58 58	9-85827 -85844 -85861 -85878 -85895	$17 \\ 17 \\ 16 \\ 17 \\ 16 \\ 17 \\ 1\overline{6}$	$10.4135\overline{5} \\ .41416 \\ .41476 \\ .41537 \\ .4159$	60 60 60 60 60 60 60	50 51 52 53 54	$\begin{array}{cccccccccccccccccccccccccccccccccccc$
55         9.84895           56         .84912           57         .84929           58         .84946           59         .84963	$17 \\ 17 \\ 17 \\ 17 \\ 17 \\ 17 \\ 17 \\ 17 \\$	$10.3809\overline{5} \\ .38153 \\ .38212 \\ .38270 \\ .38328 \\ .38328 \\ \end{array}$	5888 5588 558 588 588 588 588 588 588 5	9.85911 .85928 .85945 .85962 .85979	17 17 16 17 16	$10.41658 \\ .41719 \\ .41779 \\ .41840 \\ .41901$		55 56 57 58 59	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
60 9.84980 , Lg. Vers.		10.38387 Log.Exs.		9 . 85995 Lg. Vers,		10 · 41962 Log. Exs.	<b>D</b>	<u>60</u> ′	50 14.6 14.1 13.7 P. P.

= C

	)	7	′ <b>4°</b>		75°					
·	Lg. Vers.	D	Log. Exs.	D	Lg. Vers.	D	Log. Exs.	D	·	P. P.
01234 5	9.85995 .86012 .86029 .86046 .86062 9.86079	$17 \\ 16 \\ 17 \\ 16 \\ 17 \\ 16 \\ 17 \\ 17 \\ $	10.41962.42022.42083.42144.4220510.42266	$     \begin{array}{c}       6\overline{0} \\       61 \\       61 \\       61 \\       61 \\       61     \end{array} $	9.86992 .87009 .87025 .87042 .87058 9.87074	$1\overline{6} \\ 1\overline{6} \\ 16$	10.45693.45756.45820.45884.4594710.46011	6 <u>3</u> 6 <u>3</u> 6 <u>4</u> 6 <u>3</u> 6 <u>4</u> 6 <u>4</u>	0 1 2 3 4 5	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
6 7 8 9	-86096 -86113 -86129 -86146	$16 \\ 17 \\ 16 \\ 17 \\ 16 \\ 17 \\ 16 \\ 16 \\ $	.42327     .42388     .42450     .42511	61 61 61 61	·87091 ·87107 ·87124 ·87140	16 16 16 16 16	$ \begin{array}{r} \cdot 46075 \\ \cdot 46139 \\ \cdot 46203 \\ \cdot 46267 \\ \end{array} $	64 64 64 64 64	6 7 8 9	$\begin{array}{c} 20 & 22 \cdot \overline{3} & 22 \cdot \overline{1} & 22 \cdot 0 \\ 30 & 33 \cdot \overline{5} & 33 \cdot 2 & 33 \cdot 0 \\ 40 & 44 \cdot \overline{6} & 44 \cdot 3 & 44 \cdot 0 \\ 50 & 55 \cdot 8 & 55 \cdot 4 & 55 \cdot 0 \end{array}$
10 11 12 13 14	9.86163 .86179 .86196 .86213 .86230	16 17 16 17 16	10.42572.42633.42695.42756.42756.42817	$61 \\ 61 \\ 61 \\ 61 \\ 61 \\ 61 \\ 61 \\ 61 \\$	9.87157 .87173 .87189 .87206 .87222	16 16 16 16 16	$   \begin{array}{r}     10.46331 \\     .46395 \\     .46460 \\     .46524 \\     .46588 \\   \end{array} $	64 64 64 64 64	$10 \\ 11 \\ 12 \\ 13 \\ 14 \\ 15$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$
15 16 17 18 19	9.86246 .86263 .86280 .86296 .86313	16 17 16 16 16	10.42879.42940.43002.43063.43125	61 61 62 61	9.87239 .87255 .87271 .87288 .87304	16 16 16 16	10.46652.46717.46781.46846.46910	644 644 64 64 64	15 16 17 18 19	$\begin{array}{c} 10 & 10 \cdot 9 & 10 \cdot \overline{3} & 10 \cdot \overline{7} \\ 20 & 21 \cdot \overline{3} & 21 \cdot \overline{6} & 21 \cdot \overline{5} \\ 30 & 32 \cdot \overline{7} & 32 \cdot \underline{5} & 32 \cdot 2 \\ 40 & 43 \cdot \overline{6} & 43 \cdot \underline{3} & 43 \cdot 0 \\ 50 & 54 \cdot \overline{6} & 54 \cdot \overline{1} & 53 \cdot \overline{7} \end{array}$
20 21 22 23 24	9.86330 .86346 .86363 .86380 .86396	16 16 17 16 16	10.43187.43249.43310.43372.43434	62 61 62 61 62	9.87320 .87337 .87353 .87370 .87386	16 16 16 16 16	10.46975.47040.47104.47169.47234	65 64 65 64 65 65	20 21 22 23 24	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
25 26 27 28 29	9.86413 .86430 .86446 .86463 .86479	$17 \\ 16 \\ 16 \\ 16 \\ 16 \\ 17 \\ 17 \\ 17 \\ $	10.43496.43558.43620.43682.43744	62 62 62 62 62 62 62	9.87402 .87419 .87435 .87451 .87468	16 16 16 16 16	10.47299.47364.47429.47494.47559	65 65 65 65 65	25 26 27 28 29	$\begin{array}{c} 10 & 10 \cdot \overline{6} & 10 \cdot 6 & 10 \cdot 5 \\ 20 & 21 \cdot 3 & 21 \cdot 1 & 21 \cdot 0 \\ 30 & 32 \cdot 0 & 31 \cdot 7 & 31 \cdot 5 \\ 40 & 42 \cdot 6 & 42 \cdot 3 & 42 & 0 \\ 50 & 53 \cdot 3 & 52 \cdot 9 & 52 \cdot 5 \end{array}$
30 31 32 33 34	9.86496 .86513 .86529 .86546 .86562	16 16 16 16 16	$10.4380\underline{6}\\.43868\\.43931\\.4399\underline{3}\\.44055$	6212 622 622 622 622 622 622 622	9.87484 .87500 .87516 .87533 .87549	16 16 16 16 16	$10.47624 \\ .47689 \\ .47754 \\ .47820 \\ .47885$	65 65 65 65 65 65	30 31 32 33 34	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
35 36 37 38 39	9-86579 -86596 -86612 -86629 -86645	16 16 16 16 16	$10.44118 \\ .44180 \\ .44242 \\ .44305 \\ .44368 \\ \hline$	62212 62212 63 63 62	9.87565 .87582 .87598 .87614 .87631	16 16 16 16 16 16	10.47950.48016.48081.48147.48213	655 65 66 65 65	35 36 37 38 39	$\begin{array}{c} 9 \\ 9 \\ 9 \\ -3 \\ -4 \\ -4 \\ -3 \\ -3 \\ -3 \\ -3 \\ -3$
40 41 42 43 44	9.86662 .86678 .86695 .86712 .86728	$16 \\ 17 \\ 16 \\ 16 \\ 16 \\ 16 \\ 16 \\ 16 \\ $	$10.44430 \\ .44493 \\ .44556 \\ .44618 \\ .44681 \\ .44681 \\ \end{array}$	63 63 63 63 63 63 63 63 63	9.87647 .87653 .87679 .87696 .87712	$16 \\ 16 \\ 16 \\ 16 \\ 16 \\ 16 \\ 16 \\ 16 \\$	$   \begin{array}{r}     10.4827\overline{8} \\     .48344 \\     .48410 \\     .48476 \\     .48542 \\   \end{array} $	65 66 66 66 65	40 41 42 43 44	$\begin{array}{ccc} 61 6\overline{0} \\ 6 6 \cdot 1 6 \cdot \overline{0} \end{array}$
45 46 47 48 49	9.86745 .86761 .86778 .86794 .86811	16 16 16 16 16	$10.44744 \\ .44807 \\ .44870 \\ .44933 \\ .44996 \\ .4490 \\ .4400 \\$	63 63 63 63 63	9.8772 <u>8</u> .87744 .87761 .87777 <u>.87773</u>	$16 \\ 16 \\ 16 \\ 16 \\ 16 \\ 1\overline{6} $	10.48607 .48674 .48740 .48806 .48806 .48872	66 66 66 66 66	45 46 47 48 49	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
50 51 52 53 54	- 86844 - 86860 - 86877 - 86873	16 16 16 16 16	$ \begin{array}{r} 10.45059 \\ .45122 \\ .45185 \\ .45248 \\ .45312 \\ \hline .45312 \\ $	63 63 63 63 63	9.87809 .87825 .87842 .87858 .87858 .87874	$     \begin{array}{c}       16 \\        16 \\       16 $	$ \begin{array}{r} 10.4893\overline{8} \\ .49004 \\ .49071 \\ .49137 \\ .49204 \\ \end{array} $	66 66 66 66 66 66 66	50 51 52 53 54	$17 1\overline{6} 16$ 6) 1.7 1.6 1.6
55 56 57 58 59 60	9.86910 .86926 .86943 .86959 .86976 9.86992	1 <u>6</u> 1 <u>6</u> 1 <u>6</u>	$   \begin{array}{r}     10.45375 \\     .45439 \\     .45502 \\     .45565 \\     \underline{.45629} \\     10.45693   \end{array} $	63 63 63 63 63 63 63 64	9.87890 .87906 .87923 .87939 <u>.87955</u> 9.87971	$     \begin{array}{c}       16 \\        16 \\       16 $	$   \begin{array}{r}     10.4927\overline{0} \\     .49337 \\     .4940\overline{3} \\     .4947\overline{0} \\     .49537 \\     10.49537 \\   \end{array} $	66 67 67 67	55 56 57 58 59 60	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
7	Lg. Vers.		Log. Exs.	D	Lg. Vers.	D	10.49604 Log. Exs.	D	100	P. P.
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TABLE VIIILOGARITHMIC	VERSED SINES AND	EXTERNAL SECANTS
76°	77°	

	76°		77°		
' Lg. Vers. D	Log.Exs. D	Lg. Vers. D	Log.Exs. Z	<u>) /</u>	P. P.
$\begin{array}{c} 0 \\ 9 \cdot 8797\overline{1} \\ 1 \\ 2 \\ 88003 \\ 0 \\ 3 \\ 88020 \\ 16 \\ 4 \\ -88036 \\ 16 \\ -88036 \\ 16 \\ -88036 \\ 16 \\ -88036 \\ 16 \\ -88036 \\ 16 \\ -88036 \\ 16 \\ -8803$	.49670 67 .49737 67 .49804 67 .49871 67	$\begin{array}{c c}9.88933\\ .88949\\ .88964\\ .88980\\ .88980\\ .88996\\ .88996\\ .6\\ .88996\\ .6\\ .88996\\ .6\\ .6\\ .6\\ .6\\ .6\\ .6\\ .6\\ .6\\ .6\\ .$	$ \begin{array}{r} 10.53724\\ .53794\\ .53865\\ .53936\\ .54007\\ 10.54078\\ 7\end{array} $	$ \begin{array}{c c} 1 \\ 1 \\ 0 \\ 1 \\ 4 \end{array} $	$\begin{array}{cccccccccccccccccccccccccccccccccccc$
$\begin{array}{c} \hline 1 \\ \hline 5 \\ \hline 9 \\ \cdot 88052 \\ \hline 6 \\ \cdot 88063 \\ \hline 7 \\ \cdot 88084 \\ \cdot 88100 \\ \hline 6 \\ \hline 9 \\ \cdot 88110 \\ \hline 1 \\ 0 \\ \cdot 88110 \\ - 1 \\ 0 \\ - 1 \\$	$\begin{array}{c} 10.49939 & 67 \\ \cdot 50006 & 67 \\ \cdot 50073 & 67 \\ \cdot 50140 & 67 \\ \cdot 50208 & 67 \end{array}$	$\begin{array}{r} 1600001 \\ \hline 9.8901\overline{2} \\ 15 \\ .89028 \\ .89024 \\ 16 \\ .89060 \\ 15 \\ .89075 \\ 16 \\ .89075 \\ 16 \\ \end{array}$	$\begin{array}{c} 10.54078 \\ \cdot 54149 \\ 7 \\ \cdot 54220 \\ 7 \\ \cdot 54291 \\ \cdot 54367 \\ 7 \end{array}$	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	$8 10 \cdot 0 9 \cdot 8 9 \cdot 7$
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{r} 9.89091 \\ .89107 \\ 15 \\ .89123 \\ 16 \\ .89139 \\ 16 \\ .89155 \\ 15 \\ 15 \\ 15 \\ 15 \\ 15 \\ 15 \\ 15 $	$\begin{array}{c} 10.54433 \\ \hline 10.54433 \\ .54505 \\ .54576 \\ .54647 \\ .54719 \\ .54719 \\ 7 \end{array}$	$     \begin{array}{ccc}       1 & 12 \\       2 & 13 \\       1 & 14     \end{array} $	00102-0101-0160-8
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{array}{r} 9.89170 \\ .89186 \\ 15 \\ .89202 \\ 16 \\ .89218 \\ 16 \\ .89234 \\ 15 \\ \end{array}$	. 00070	$     \begin{array}{c}       2 \\       1 \\       2 \\       1 \\       2 \\       1 \\     $	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
$\begin{array}{c} 20 & 9 \cdot 88 294 \\ 21 & \cdot 88310 \\ 22 & \cdot 88326 \\ 23 & \cdot 88342 \\ 24 & \cdot 88358 \end{array}$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{array}{r} 9.89249 \\ .89265 \\ .89281 \\ .89297 \\ .89217 \\ 15 \\ .89217 \\ 15 \end{array}$	$\begin{array}{c} 10.55150\\ \cdot 55222\\ \cdot 55294\\ \cdot 55366\\ 7\\ \cdot 55438\\ 7\\ \cdot 55438\\ 7\end{array}$	$     \begin{array}{c}       2 \\     $	$\begin{array}{c} 10 & 12 \cdot 0 & 13 \cdot 0 & 11 \cdot 0 \\ 20 & 24 \cdot 0 & 123 \cdot 0 & 13 \cdot 3 \\ 30 & 36 \cdot 0 & 35 \cdot 5 & 35 \cdot 2 \\ 40 & 48 \cdot 0 & 47 \cdot 3 & 47 \cdot 0 \\ 50 & 60 \cdot 0 & 59 \cdot 1 & 58 \cdot 7 \end{array}$
25 9.88374 10 26 .88390 10 27 .88406 10 28 .88422 10 29 .88438 10	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	9.89328 .89344 .89360 .89376 .89376 15 .89397 15	$ \begin{array}{c} 10.55511 \\ .55583 \\ 7.55655 \\ .55728 \\ .55801 \\ 7 \end{array} $	2 26 2 26 2 27 2 28 29 29	$\begin{array}{cccccccccccccccccccccccccccccccccccc$
SU         3.88434         10           31         .88470         10           32         .88486         10           33         .88502         10           34         .88518         10	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$     \begin{array}{r}       9.89407 \\             89423 \\             15 \\             89438 \\             89454 \\             15 \\             89470 \\             15         \end{array} $	$     \begin{array}{c}       10.55873 \\       \cdot 55946 \\       7 \\       \cdot 56019 \\       \cdot 56092 \\       \cdot 56165 \\       7     \end{array} $	$     \begin{array}{c}       3 \\       3 \\       2 \\       3 \\     $	$\begin{array}{c} 9 & 10 \cdot \overline{3} & 10 \cdot 2 & 10 \cdot \overline{0} \\ 10 & 11 \cdot 5 & 11 \cdot \overline{3} & 11 \cdot \overline{1} \\ 20 & 23 \cdot 0 & 22 \cdot \overline{6} & 22 \cdot \overline{3} \\ 30 & 34 \cdot 5 & 34 \cdot 0 & 33 \cdot 5 \\ 40 & 46 \cdot 0 & 45 \cdot \overline{3} & 44 \cdot \overline{6} \\ 50 & 57 \cdot 5 & 56 \cdot \overline{6} & 55 \cdot \overline{8} \end{array}$
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$     \begin{array}{ccccccccccccccccccccccccccccccccc$	.89501 16 .89517 15 .89533 15	$\begin{array}{c} 10.56238 \\ .56311 \\ .56384 \\ .56457 \\ .56531 \\ .56531 \\ 7 \end{array}$	335 35 36 37 38 39	66 0 6 6.60.0 7 7.70.0 8 8.80.0
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	.89580 16 .89596 15 .89611 15	· 56825 7 · 56899 7	$39 \\ 40 \\ 41 \\ 42 \\ 43 \\ 43 \\ 44 \\ 45 \\ 44 \\ 45 \\ 45 \\ 45$	$\begin{array}{c} 9 & 9 \cdot 9 & 0 \cdot 1 \\ 10 & 11 \cdot 0 & 0 \cdot 1 \\ 20 & 22 \cdot 0 & 0 \cdot 1 \\ 30 & 33 \cdot 0 & 0 \cdot 2 \end{array}$
45 9.88694 1 46 .88710 1 47 .88726 1 48 .88742 1 49 .88758 1	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$     \begin{array}{c}       10.56973 \\       \cdot 57047 \\       \cdot 57120 \\       \cdot 57195 \\       \cdot 57269 \\       7     \end{array} $	$43 \\ 46 \\ 47 \\ 48 \\ 49 $	50155.010.4
$\begin{array}{c} 50 & 9.88774 \\ 51 & 88790 \\ 52 & 88805 \\ 53 & 88821 \\ 54 & 88837 \\ \end{array}$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	·57491 7 ·57491 7 ·57566 7		$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
$\begin{array}{c} 55 & 9 \cdot 88853 \\ 56 & \cdot 88869 \\ 57 & \cdot 88885 \\ 58 & \cdot 88901 \\ 59 & \cdot 88917 \\ \end{array}$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	9.89799 15 .89815 15 .89830 15 .89846 16 .89862 15	·57939 7 ·58014 7	59	$\begin{array}{cccccccccccccccccccccccccccccccccccc$
$\frac{609.88933}{Lg. Vers.}$ $\frac{1}{7}$	10 53724	9.89877	10.58089 / Log.Exs. 1	_00	P. P.
	1-08.5401	1-9, 10,01	1-08.2001	<u> </u>	

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	Lg. Vers.	D	Log.Exs.	D	Lg. Vers.	D	Log. Exs.	D	·	P. P.
0 1 2 3 4	9.89877 .89893 .89908 .89924 .89939	1 <u>5</u> 1 <u>5</u> 1 <u>5</u> 1 <u>5</u>	$10.58089 \\ .58164 \\ .58239 \\ .58315 \\ .58390 \\$	75 75 75 75	9.90805 .90820 .90835 .90851 .90866	$1\overline{5}$ 15 $1\overline{5}$ $1\overline{5}$ $1\overline{5}$	$\begin{array}{r} 10\cdot 62745\\ \cdot 62825\\ \cdot 62906\\ \cdot 62986\\ \cdot 63067\end{array}$	80 80 80 81	0 1 2 3 4	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
5 6 7 8 9	9.89955 .89971 .89986 .90002 .90017	16 15 15 15 15	10.58465 .5854 <u>1</u> .5861 <u>6</u> .58692 .58768	75 75 75 76 75 76	9.90881 .90897 .90912 .90927 .90943	$15 \\ 15 \\ 15 \\ 15 \\ 15 \\ 15 \\ 15 \\ 15 \\$	$10.63148 \\ .63229 \\ .63310 \\ .63391 \\ .63472$	80 81 81 81 81 81	5 6 7 8 9	$ \begin{array}{c} 9 & 12 \cdot 9 & 12 \cdot 7 & 12 \cdot 6 \\ 10 & 14 \cdot 3 & 14 \cdot 1 & 14 \cdot 0 \\ 20 & 28 \cdot 6 & 28 \cdot 3 & 28 \cdot 0 \\ 30 & 43 \cdot 0 & 142 \cdot 5 & 42 \cdot 0 \\ 40 & 57 \cdot 3 & 56 \cdot 6 & 56 \cdot 0 \\ 50 & 71 \cdot 6 & 70 \cdot 8 & 70 \cdot 0 \end{array} $
10 11 12 13 14	9.90033 .90048 .90064 .90080 .90095	15 15 15 16 15	10.58844 .58920 .58995 .59072 .59148	76 76 75 75 76 76	9.90958 .9097 <u>3</u> .90988 .91004 .91019	15 15 15 15 15	10.6355 <u>3</u> .63634 .63716 .63797 .63879	81 81 81 81 81	10 11 12 13 14	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
15 16 17 18 19	9.90111 .90126 .90142 .90157 .90173	15 15 15 15 15 15	10.5922 <u>4</u> .59300 .5937 <u>7</u> .59453 .59530	76 76 76 76 76 76 76	$9.9103\overline{4}$ .9104 $\overline{9}$ .91065 .91080 .91095	15 15 15 15 15	10.63961 .64043 .64125 .64207 .64289	82 82 82 82 82 82 82	15 16 17 18 19	$\begin{array}{c} 9 & 12 \cdot \frac{1}{4} & 12 \cdot \frac{3}{5} & 12 \cdot 1 \\ 10 & 13 \cdot \frac{8}{5} & 13 \cdot 6 & 13 \cdot 5 \\ 20 & 27 \cdot 6 & 27 \cdot 3 & 27 \cdot 0 \\ 30 & 41 \cdot 5 & 41 \cdot 0 & 40 \cdot 5 \\ 40 & 55 \cdot \frac{3}{5} & 54 \cdot 6 & 54 \cdot 0 \\ 50 & 69 \cdot 1 & 68 \cdot 3 & 67 \cdot 5 \end{array}$
20 21 22 23 24	9.90188 .90204 .90219 .90235 .90250	15 15 15 15 15 15 15 15	$10.5960\overline{6} \\ .59683 \\ .59760 \\ .59837 \\ .59914$	70 7 <u>7</u> 76 77 77 77	$9.9111\overline{0}$ .91126 .91141 .9115 <u>6</u> .91171	15 15 15 15 15 15	$10.6437\overline{1} \\ .64453 \\ .64536 \\ .64618 \\ .64701$	82 82 82 82 82 83 82 82	20 21 22 23 24	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
25 26 27 28 29	9.9026 <u>6</u> .90281 .90297 .90312 .90328	$15 \\ 15 \\ 15 \\ 15 \\ 15 \\ 15 \\ 15 \\ 15 \\$	10.59991 .60068 .60145 .60223 .60300	77 77 77 77 77	9.91187 .91202 .91217 .91232 .91247	15 15 15 15 15 15	$10.64784 \\ .64867 \\ .64950 \\ .65033 \\ .65116$	83 83 83 83	25 26 27 28 29	$\begin{array}{c} 6 & 8 & 0 & 7 & 9 & 7 & 8 \\ 7 & 9 & 3 & 9 & 2 & 9 & 1 \\ 8 & 10 & 6 & 10 & 5 & 10 & 4 \\ 9 & 12 & 0 & 11 & 8 & 11 & 7 \\ 10 & 13 & 3 & 13 & 1 & 13 & 0 \\ 20 & 26 & 6 & 26 & 3 & 26 & 0 \\ 30 & 40 & 0 & 39 & 5 & 39 & 0 \\ 40 & 53 & 35 & 52 & 6 & 52 & 0 \\ 50 & 66 & 6 & 65 & 8 & 65 & 0 \end{array}$
30 31 32 33 34	9.90343 .90359 .90374 .90389 .90405	15 15 15 15 15 15	$10.60378 \\ .60455 \\ .60533 \\ .60611 \\ .60688$	777 777 777 778 777 78	$9.91263 \\ .91278 \\ .91293 \\ .91308 \\ .91323$	15 1 <u>5</u> 15 15	$10.6519\overline{9} \\ .65283 \\ .65366 \\ .65450 \\ .65534$	833 833 833 833 83 83 83 83 83	30 31 32 33 34	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
35 36 37 38 39	9.90420 .90436 .90451 .90467 .90482	15 15 15 15 15 15 15	$10.6076\overline{6} \\ .60844 \\ .60923 \\ .61001 \\ .61079$	78 78 78 78 78	$9.9133\overline{8}$ .91354 .91369 .91384 .91389 .91399	15 15 15 15 15	$10.6561\overline{7} \\ .6570\overline{1} \\ .6578\overline{5} \\ .65870 \\ .65954$	84 84 84 84	35 36 37 38 39	9 11 $\cdot \frac{5}{5}$ 11 $\cdot \frac{4}{5}$ 11 $\cdot \frac{2}{5}$ 12 $\cdot \frac{5}{5}$ 12 $\cdot \frac{5}{5}$ 20 25 $\cdot \frac{5}{6}$ 25 $\cdot \frac{3}{5}$ 25 $\cdot \frac{3}{5}$ 25 $\cdot \frac{3}{5}$ 25 $\cdot \frac{3}{5}$ 38 $\cdot \frac{3}{5}$ 38 $\cdot \frac{3}{5}$ 38 $\cdot \frac{3}{5}$ 37 $\cdot \frac{5}{5}$ 40 51 $\cdot \frac{3}{5}$ 50 $\cdot \frac{6}{5}$ 50 $\cdot 0$ 50 $\cdot 64 \cdot 1$ $\cdot 63 \cdot 3$ $\cdot 62 \cdot 5$
40 41 42 43 44	9.90497 .90513 .90528 .90544 .90559	15 15 15 15 15	$10.61158 \\ .61236 \\ .61315 \\ .61393 \\ .61472$	78878787878787878787878787878787878787	$\begin{array}{r} 9.9141\overline{4} \\ .91429 \\ .91445 \\ .91460 \\ .91475 \end{array}$	15 15 15 15 15	$10.6603\overline{8} \\ .66123 \\ .66207 \\ .66292 \\ .66377$	8444 888 885 85	$40 \\ 41 \\ 42 \\ 43 \\ 44$	0,04.1103.3102.5 0 6[0.0 7[0.0 8]0.0
45 46 47 48 49	9.90574 .90590 .90605 .90621 .90636	15 15 15 15 15	$\begin{array}{r} 10.61551 \\ .61630 \\ .61709 \\ .61788 \\ .61867 \end{array}$	78 79 79 79 79 79	$\begin{array}{r} 9.91490 \\ .91505 \\ .91520 \\ .91535 \\ .91535 \\ .91550 \end{array}$	15 15 15 15 15	10.66462 .66547 .66632 .66717 .66803	85 85 85 55 55 55 55 55 55 55 55 55 55 5	45 46 47 48 49	$ \begin{array}{c} 9 \\ 10 \\ 0 \\ 20 \\ 0 \\ 1 \\ 30 \\ 0 \\ 2 \\ 40 \\ 0 \\ 3 \\ 3 \\ 40 \\ 0 \\ 3 \\ 3 \\ 3 \\ 3 \\ 3 \\ 3 \\ 3 \\ 3 \\ 3 \\ 3$
50 51 52 53 54	9.90651 .90667 .90682 .90697 .90713	15 15 15 15 15	10.61947 .62026 .62105 .62185 .62265	79 79 79 80 79	9.91565 .91581 .91596 .91611 .91626	$15 \\ 15 \\ 15 \\ 15 \\ 15 \\ 15 \\ 15 \\ 15 \\$	$10.6688\overline{8} \\ .66974 \\ .67059 \\ .67145 \\ .67231$	8 <u>5</u> 8 <u>5</u> 85 86 86	50 51 52 53 54	5010-4
55 56 57 18 59	9.90728 .90744 .90759 .90774 .90774 .90790	$1\overline{5}$ $1\overline{5}$ $1\overline{5}$ $1\overline{5}$ $1\overline{5}$ $1\overline{5}$	$\begin{array}{r} 10.62345\\ .62424\\ .62504\\ .62585\\ .62585\\ .62665\end{array}$	80 79 80 80 80	9.91641 .91656 .91671 .91686 .91701	$     \begin{array}{r}       15 \\$	10.67317 .67403 .67490 .67576 .67663	86 86 86 86 86 86 86 86	55 56 57 58 59	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
<u>60</u> /	<u>9.90805</u> Lg. Vers.	$\frac{15}{D}$	10.62745 Log.Exs.	80 D	9.91716 Lg. Vers.	15 D	10.67749 Log.Exs.	8 <u>6</u> D	<u>60</u> ′	40 10.6 10.3 10.0 50 13.3 12.9 12.5 P. P.

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'	Lg. Vers.	D	Log.Exs.	D	Lg. Vers.	D	Log. Exs.	D	<u>  ·</u>	P. P.
0 1 2 3 4	9.91716 .91731 .91746 .91746 .91761 .91776	15 15 15 15	10.67749.67836.67923.68010.68097	86 87 87 87 87	9.92612 .92626 .92641 .92656 .92671	$14 \\ 15 \\ 14 \\ 15 \\ 15 \\ 15 \\ 15 \\ 15 \\ $	$10.7317\overline{8} \\.73273 \\.73368 \\.73463 \\.73558$	95 94 95 95	3	$\begin{array}{c cccc} 90 & 80 \\ 6 & 9 \cdot 0 & 8 \cdot 0 \\ 7 & 10 \cdot 5 & 9 \cdot 3 \\ 8 & 12 \cdot 0 & 10 \cdot 6 \\ 9 & 13 \cdot 5 & 12 \cdot 0 \end{array}$
5 6 7 8 9	9.91791 .91807 .91822 .91837 .91852	15 15 15 15 15	10.68184 .68272 .68359 .68447 .68534	87 87 87 87 87 87	9.92686 .92700 .92715 .92730 .92745	$15 \\ 14 \\ 15 \\ 14 \\ 15 \\ 15 \\ 15 \\ 15 \\ $	10.73653.73748.73844.73940.74035	95 95 95 95 95	5 6 7 8 9	$ \begin{array}{c} 10 & 15 \cdot 0 & 13 \cdot \overline{3} \\ 20 & 30 \cdot 0 & 26 \cdot \overline{6} \\ 30 & 45 \cdot 0 & 40 \cdot 0 \\ 40 & 60 \cdot 0 & 53 \cdot \overline{3} \\ 50 & 75 \cdot 0 & 66 \cdot \overline{6} \end{array} $
10 11 12 13 14	9.91867 .91882 .91897 .91912 .91927	15 15 15 15 15	10.68622 .68710 .68798 .68886 .68886 .68975	88 88 88 88 88 88	9.92759 .92774 .92789 .92804 .92818	$1\overline{4} \\ 15 \\ 14 \\ 15 \\ 14 \\ 15 \\ 14 \\ 14 \\ 14$	$10.7413\overline{1} \\ .74227 \\ .74324 \\ .74420 \\ .74517$	96 96 96 96 96	10 11 12 13 14	$\begin{array}{c c} 9 & 8 \\ 6 & 0.9 & 0.8 \\ 7 & 1.0 & 0.9 \\ 8 & 1.2 & 1.0 \\ 9 & 1.3 & 1.2 \\ 10 & 1.5 & 1.2 \\ 10 & 1.5 & 1.2 \\ \end{array}$
15 16 17 18 19	9.91942 .91957 .91972 .91987 .92002	15 15 15 15 15	$     \begin{array}{r}       10.6906\overline{3} \\       .69152 \\       .69240 \\       .69329 \\       .69418     \end{array} $	88 88 88 89 89	9.92833 .92848 .92862 .92877 .92892	$15 \\ 14 \\ 14 \\ 15 \\ 14 \\ 14 \\ 14 \\ 14 \\ $	$     \begin{array}{r} 10.7461\overline{3} \\ .74710 \\ .74807 \\ .74807 \\ .74905 \\ .75002 \end{array} $	96 97 97 97 97	15 16 17 18 19	$\begin{array}{c} 1 & 1 & 2 & 1 & 0 \\ 9 & 1 & 3 & 1 & 2 \\ 1 & 0 & 1 & 5 & 1 & 3 \\ 2 & 0 & 3 & 0 & 2 & 6 \\ 3 & 0 & 4 & 5 & 4 & 0 \\ 4 & 0 & 6 & 0 & 5 & 3 \\ 5 & 0 & 7 & 5 & 6 & 6 \end{array}$
20 21 22 23 24	$\begin{array}{r} 9 \cdot 9201\overline{6} \\ \cdot 9203\overline{1} \\ \cdot 9204\overline{6} \\ \cdot 9206\overline{1} \\ \cdot 9207\overline{6} \end{array}$	$1\overline{4} \\ 15 \\ 15 \\ 15 \\ 15 \\ 15 \\ 15 \\ 15 \\ 1$	10.69507 .69596 .69686 .69775 .69865	89 89 89 89 89 89 89	9.92907 .92921 .92936 .92951 .92965	$15 \\ 14 \\ 14 \\ 15 \\ 14 \\ 15 \\ 14 \\ 14 \\ $	10.75099 .75197 .75295 .75393 .75491	97 98 97 98 98	20 21 22 23 24	76 60.70.6 70.80.7 80.00.8
25 26 27 28 29	$\begin{array}{r} 9 \cdot 9209\overline{1} \\ \cdot 9210\overline{6} \\ \cdot 9212\overline{1} \\ \cdot 9213\overline{6} \\ \cdot 92151 \end{array}$	$15 \\ 15 \\ 15 \\ 15 \\ 15 \\ 14 \\ 14$	10.6995 <u>5</u> .7004 <u>4</u> .7013 <u>4</u> .70224 .70315	90 90 90 90	9 · 92980 • 92995 • 93009 • 93024 • 93039	$15 \\ 14 \\ 14 \\ 15 \\ 14 \\ 15 \\ 14 \\ 14 \\ $	10.75589 .75688 .75786 .75786 .75885 .75984	98 98 98 99 99 99	25 26 27 28 29	9 1 . 0 0 . 9 10 1 . 1 1 . 0 20 2 . 3 2 . 0 30 3 . 5 3 . 0 40 4 . 6 4 . 0 50 5 . 8 5 . 0
30 31 32 33 34	9.92166 .92181 .92196 .92211 .92226	15 15 15 15 15	10.70405 .70495 .70586 .70677 .70768	90 91 90 91	9.9305 <u>3</u> .93068 .93083 .93097 .93112	$1\overline{4} \\ 15 \\ 14 \\ 14 \\ 15 \\ 15 \\ 17 \\ 15 \\ 17 \\ 17 \\ 17 \\ 17$	.76382	99 9 <u>9</u> 99 100 99	30 31 32 33 34	54 6]0.5]0.4
35 36 37 38 39	9.92240 .92255 .92270 .92285 .92285 .92300	$1\overline{4}$ 15 15 15 15	10.70859 .70950 .71041 .71133 .71224	91 91 91 91 91	9.93127 .93141 .93150 .93171 .93185	$1\frac{1}{4}$ $1\frac{1}{4}$ $1\frac{5}{14}$ $1\frac{7}{4}$	10.76381 .76681 .76782 .76882 .76983	100 100 100 100 100	35 36 37 38 39	$\begin{array}{c} 8 & 0 & .6 \\ 0 & .6 \\ 0 & .6 \\ 0 & .7 \\ 0 & .6 \\ 0 & .6 \\ 1 & .3 \\ 30 & 2 & .5 \\ 40 & 3 & .3 \\ 50 & 4 & .1 \\ 3 & .3 \\ \end{array}$
40 41 42 43 44	9.92315 .92330 .92345 .92360 .92374	$1\frac{4}{15}$ 15 $1\frac{5}{14}$	10.71316 .71408 .71500 .71592 .71684	91 92 92 92 92 92	9.93200 .93214 .93229 .93244 .93258	$1\overline{4}$ $1\overline{4}$ 15 $1\overline{4}$ $1\overline{4}$ $1\overline{4}$	10.7708 <u>3</u> •77184	100 101 101 101 101	40 41 42 43 44	$\begin{array}{cccccccccccccccccccccccccccccccccccc$
45 46 47 48 49	$9.9238\overline{9}$ .92404 .92419 .92434 .92434 .92449	$15 \\ 15 \\ 14 \\ 15 \\ 15 \\ 15 \\ 15 \\ -$	10.71776 .71869 .71961 .72054 .72147	92 92 93 93 93 93 93 93 93 93 93	9.93273 .93287 .93302 .93317 .93317 .93331	$1\overline{4}$ $1\overline{4}$ $1\overline{5}$ $1\overline{4}$ $1\overline{4}$ $1\overline{4}$	10.77590 .77692 .77794 .77896 .77998	101 102 102 102 102	45 46 47 48 49	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
50 51 52 53 54	9.9246 <u>3</u> .9247 <u>8</u> .92493 .92508 .92523	$1\overline{4} \\ 15 \\ 15 \\ 1\overline{4} \\ 15 \\ 15 \\ 15 \\ 15 \\ 15 \\ 15 \\ 15 \\ 1$	10.72240 .72333 .72427 .72520 .72614	93 93 93 93 93 93 93 93 93 93 93 93 93 9	9.93346 .93360 .93375 .93389 .93404	$1\overline{4} \\ 1\overline{4} \\ 1\overline{4} \\ 1\overline{4} \\ 1\overline{4} \\ 1\overline{5} \\ 15$	•78203 •78306 •78409 •78513	102 102 103 103 103	50 51 52 53 54	1 <b>4</b> 61 1.4
55 56 57 58 59	9.92538 .92552 .92567 .92582 .92582 .92597	$15 \\ 14 \\ 15 \\ 15 \\ 14 \\ 14 \\ 14 \\ 14 \\ $	10.72707 .72801 .72895 .72990 .73084	93 94 94 94 94 94	9.93419.93433.93448.93462.93477	$1\overline{4}$ 14	·78720 •78823 •78927	103 104 103 104 104	55 56 57 58 59	7 1.7 8 1.9 9 2.2 10 2.4 20 4.88 30 7.2 40 9.6
<u>60</u> /	9.92612 Lg. Vers.	15 D	10.73178 Log.Exs.	54 7	<u>9 · 93491</u> Lg. Vers.	$\frac{1\overline{4}}{D}$	<u>10.79136</u> Log. Exs.	104 D	<u>60</u> '	50 12 · 1 P. P.
_	-3.10.01				-8					

TABLE VIIILOG	ARITHMIC VERSED	SINES AND	EXTERNAL SECANTS	•
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TABLE VIII	-LOGARITHMIC	VERSED	SINES AND	EXTERNAL	SECANTS.

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' [Lg. Ve	ers, D	Log.Exs.	D	Lg. Vers.	D	Log.Exs.	D	1	P. P.
0 9.952 1 .952 2 .952 3 .952 4 .952	$\begin{array}{c c c c c c c c c c c c c c c c c c c $	.93821	$13\overline{4} \\ 135 \\ 1$	9.9603 <u>9</u> .96053 .96067 .96081 .96095	14 13 14 14	$\begin{array}{r} 11.02010 \\ .02168 \\ .02327 \\ .02487 \\ .02646 \end{array}$	$   \begin{array}{r} 15\overline{8} \\     159 \\     159 \\     159 \\     159 \\     159 \\     159 \\   \end{array} $	0 1 2 3 4	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
5 9.952 6 .952 7 .953 8 .953 9 .953	$28\overline{9}   14$ $30\overline{3}   14$ $31\overline{7}   14$ $31\overline{7}   14$ $33\overline{1}   14$	94093 94229 94229 94366 94503	$13\overline{5}$ 136 $13\overline{6}$ 137 137 137	$9.9610\overline{8} \\ .96122 \\ .96136 \\ .96150 \\ .96163 \\ .96164$	$1\overline{3} \\ 14 \\ 1\overline{3} \\ 14 \\ 1\overline{3} \\ 1\overline$	11.02807 .02968 .03129 .03291 .03453	$16\overline{0}$ 161 $16\overline{1}$ $16\overline{1}$ $16\overline{2}$ $16\overline{2}$	5 6 7 8 9	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
$ \begin{array}{c} 10 & 9 \cdot 953 \\ 11 & \cdot 953 \\ 12 & \cdot 953 \\ 13 & \cdot 953 \\ 14 & \cdot 954 \\ 15 & 9 \cdot 954 \end{array} $	$     \begin{array}{c}       35\overline{9} \\       373 \\       387 \\       401 \\       415 \\       14     \end{array} $	10.94641 .94778 .94917 .95055 .95194 10.95333	$   \begin{array}{r} 13\overline{7} \\     13\overline{7} \\     13\overline{8} \\     13\overline{8} \\     13\overline{9} \\     13\overline{9} \\     13\overline{9} \\     13\overline{9} \\     13\overline{9} \\   \end{array} $	$9.96177 \\ .96191 \\ .96205 \\ .96218 \\ .96232 \\ 9.96232 \\ 9.96246 \\ 9.9624 \\ 9.96246 \\ 9.9624 \\ 9$	14 13 14 13 14 13 14 13 13	$11.0361\overline{6} \\ .03780 \\ .03944 \\ .04108 \\ .04273 \\ 11.0443\overline{8}$	$     \begin{array}{r}       163 \\       164 \\       164 \\       165 \\       165 \\       165 \\       166 \\       \end{array} $	$     \begin{array}{r}       10 \\       11 \\       12 \\       13 \\       14 \\       15 \\       15     \end{array} $	$\begin{array}{cccccccccccccccccccccccccccccccccccc$
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	$     \begin{array}{c}             129 \\             143 \\             14 \\             457 \\             14 \\             171 \\             14 \\             14 \\           $	.95473 .95613 .95753 .95894	$140 \\ 140 \\ 140 \\ 140 \\ 141 $	·96259 ·96273 ·96287 ·96301 9·96314	$     \begin{array}{r}       14 \\       13 \\       14 \\       1\overline{3}     \end{array}   $	·04604 ·04771 ·04938 ·05106 11·05274	167 167 167 168	$     \begin{array}{r}       16 \\       17 \\       18 \\       19 \\       20     \end{array} $	$\begin{array}{cccccccccccccccccccccccccccccccccccc$
21 .95 22 .95 23 .95 24 .95	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	·9617 <u>6</u> ·96318 ·9646 <u>1</u> ·96603	$141 \\ 142 \\ 142 \\ 142 \\ 142 \\ 143 \\ 143 \\ 143 \\ 143 \\ 143 \\ 143 \\ 141 \\ 143 $	·96328 ·96342 ·96355 ·96369	$     \begin{array}{r}       14 \\       13 \\       13 \\       14 \\       13 \\       14 \\       13 \\       13 \\       14 \\       13 \\       13 \\       14 \\       13 \\       13 \\       14 \\       13 \\       14 \\       13 \\       13 \\       14 \\       13 \\       14 \\       13 \\       13 \\       14 \\       13 \\       14 \\       13 \\       14 \\       13 \\       14 \\       13 \\       14 \\       13 \\       14 \\       13 \\       14 \\       13 \\       14 \\       13 \\       14 \\       13 \\       13 \\       14 \\       14 \\       13 \\       14 \\       14 \\       13 \\       14 \\       15 \\       14 \\       15 \\       14 \\       15 \\       14 \\       15 \\       14 \\       15 \\       14 \\       15 \\       14 \\       15 \\       14 \\       15 \\       14 \\       14 \\       15 \\$	·05443 ·05612 ·05782 ·05952	16 <u>9</u> 16 <u>9</u> 169 170 171	21 22 23 24	$\begin{array}{ccccccc} 150 & 140 \\ 6 & 15 \cdot 0 & 14 \cdot 0 \\ 7 & 17 \cdot 5 & 16 \cdot 3 \\ 8 & 20 \cdot 0 & 18 \cdot 6 \\ 9 & 22 \cdot 5 & 21 \cdot 0 \end{array}$
25 9.95 26 .95 27 .95 28 .95 29 .95	$     \begin{array}{c}       504 \\       568 \\       582 \\       14 \\       596 \\       50 \\       14 \\       50 \\       50 \\       14 \\       50 \\$	·96889 ·97033 ·97177 ·97322	$143 \\ 144 \\ 144 \\ 144 \\ 144 \\ 145 $	9.96383.96397.96410.96424.96438	$     \begin{array}{r}       14 \\       13 \\       13 \\       14     \end{array}   $	$11.0612\overline{3} \\ .06295 \\ .06467 \\ .06640 \\ .06813$	171 172 173 173 173	25 26 27 28 29	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
<b>30</b> 9 . 95 31 . 95 32 . 95 33 . 95 34 . 95		•97467 •97612 •97758 •97904 •98050	$145 \\ 145 \\ 146 $	.96506	$   \begin{array}{r} 1\overline{3} \\    1\overline{3} \\    14 \\    1\overline{3} \\   \end{array} $	11.06987 .07161 .07336 .07512 .07688	$17\overline{4} \\ 175 \\ 176 \\ 176 \\ 176 \\ 176 \\ 176 \\ 176 \\ 176 \\ 176 \\ 176 \\ 176 \\ 176 \\ 176 \\ 100 \\ 1$	$30 \\ 31 \\ 32 \\ 33 \\ 34 $	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
35 9.95 36 .95 37 .95 38 .95 39 .95	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	10.98197 98345 983492 98492 98492 98492 98492 98789	147 147 148 149	·96547 ·96560 ·96574	14	11.07865 .08043 .08221 .08400 .08579	177 177 178 179 179	35 36 37 38 39	$\begin{array}{c} 130 & 9 & 8 \\ 6 & 13 & 0 & 0 & 9 & 9 \\ 7 & 15 & 1 & 1 & 0 & 0 & 0 \\ 8 & 17 & 3 & 1 & 2 & 1 & 0 \\ 9 & 19 & 5 & 1 & 3 & 1 & 2 \\ 10 & 21 & 6 & 1 & 5 & 1 & 3 \\ 20 & 43 & 33 & 0 & 2 & 6 \\ 30 & 65 & 0 & 4 & 54 & 0 \\ 40 & 86 & 66 & 0 & 5 & 3 \\ 50 & 108 & 3 & 7 & 56 & 6 \end{array}$
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$763 \\ 777 \\ 14 \\ 791 \\ 13 \\ 804 \\ 17 \\ 14 \\ 17 \\ 14 \\ 17 \\ 14 \\ 17 \\ 14 \\ 17 \\ 14 \\ 17 \\ 14 \\ 17 \\ 14 \\ 17 \\ 14 \\ 17 \\ 14 \\ 17 \\ 14 \\ 17 \\ 14 \\ 17 \\ 14 \\ 14$	99087 - 99087 - 99237 - 99387 - 99538	$149 \\ 150 \\ 150 \\ 151 \\ 151$	9.96588 .96601	$13 \\ 13 \\ 13 \\ 14 \\ 13 \\ 13 \\ 13 \\ 13 \\ $	11.08759 .08940 .09121 .09303 .09486	1102	40 41 42 43 44	$\begin{array}{cccccccccccccccccccccccccccccccccccc$
48 · 95 49 · 95	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	10.99689     .99841     .99993     10.99993     11.00145     .00298     .00298	151 152 152	·96683 ·96683 ·96697 ·96710	$     \begin{array}{c}       13 \\       13 \\       14 \\       13 \\       13     \end{array} $	$11.09669 \\ .09853 \\ .10038 \\ .10223 \\ .10409$	$184 \\ 185 \\ 185 \\ 186 \\ 186 \\$	45 46 47 48 49	$\begin{array}{c} 9 1 \cdot \overrightarrow{0} 0 \cdot 9 0 \cdot \overrightarrow{7} \\ 10 1 \cdot 1 1 \cdot 0 0 \cdot \overrightarrow{8} \\ 20 2 \cdot \overrightarrow{3} 2 \cdot 0 1 \cdot \overrightarrow{6} \\ 30 3 \cdot 5 3 \cdot 0 2 \cdot 5 \\ 40 4 \cdot \overrightarrow{6} 4 \cdot 0 3 \cdot \overrightarrow{3} \\ 50 5 \cdot \overrightarrow{8} 5 \cdot 0 4 \cdot \overrightarrow{1} \end{array}$
52 ·95 53 ·95	$\begin{array}{c} 901 \\ 915 \\ 1 \\ 929 \\ 1 \\ 943 \\ 1 \\ 957 \\ 1 \end{array}$	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$		9.96724 ·96737 ·96751 ·96764 ·96778	$13 \\ 13 \\ 13 \\ 14$	11.10595 .10783 .10971 .11160 .11349	$189 \\ 189 \\ 189$	$50 \\ 51 \\ 52 \\ 53 \\ 54$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
57 ·95 58 ·96		$\begin{array}{c ccccccccccccccccccccccccccccccccccc$		9.96792 96805 96819 96832 96846	$13 \\ 13 \\ 13 \\ 13 \\ 13 \\ 13 \\ 13 \\ 13 \\$	11.11539.11730.11922.12114.12307	192 193	55 56 57 58 59	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$
<u>60 9.96</u> Lg.	$303\bar{9}^{1}$	11.02010		9 . 96859 Lg. Vers		11.12501 Log.Exs.	$\frac{19\overline{3}}{D}$	<u>60</u> ′	<u>50</u> 12.111.611.2 P. P.

TABLE VIIILOGARITHMIC	VERSED SINES AND	EXTERNAL SECANTS.
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. •	Lg. Vers.	D	Log. Exs.	D	Lg. Vers.	D	Log. Exs.	D	1	P, P,
0 1 2 3 4	9.96859 .96837 .96887 .96900 .96914	$1\overline{3}$ 14 $1\overline{3}$ $1\overline{3}$ $1\overline{3}$	11.12501 .12696 .12891 .13087 .13284	195 195 196 196 196	·97705 ·97718	$1\overline{3} \\ 13 \\ 13 \\ 13 \\ 13 \\ 13 \\ 1\overline{3}$	$\begin{array}{r} 11.25785 \\ \cdot 26040 \\ \cdot 26297 \\ \cdot 26554 \\ \cdot 26814 \end{array}$	255 256 257 259	0 1 2 3 4	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
5 6 7 8 9	9.96927 .9694 <u>1</u> .96954 .96968 .96981	13313131313131313131313131313131313131	$11.13482 \\ .13680 \\ .13879 \\ .14079 \\ .14280$	$198 \\ 199 \\ 200 \\ 201$		$13 \\ 13 \\ 13 \\ 13 \\ 13 \\ 13 \\ 13 \\ 13 \\$	$11.2707\overline{4} \\ .2733\overline{6} \\ .2759\overline{9} \\ .27864 \\ .28131$	260 262 263 265 265	5 6 7 8 9	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
10 11 12 13 14	9.96995 .97008 .97022 .97035 .97049		$11.14432 \\ .14684 \\ .14887 \\ .15092 \\ .15297$	201 202 203 204 205	9.9779 <u>8</u> .97811 .97825 .97838 .97838	$     \begin{array}{c}       13 \\       13 \\       13 \\       13 \\       13     \end{array}   $	$11.2839\overline{8} \\ .28668 \\ .28938 \\ .29211 \\ .29485$	267 269 270 272 274	$10 \\ 11 \\ 12 \\ 13 \\ 14$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
15 16 17 18 19	9.97062 .97076 .97089 .97103 .97116	$13 \\ 13 \\ 13 \\ 13 \\ 13 \\ 13 \\ 13 \\ 13 \\$	.10334	205 206 208 208 209	9.97864 .97878 .97891 .97904 .97917	$     \begin{array}{c}       13 \\$	11.29760 .30037 .30316 .30596 .30878	275 277 278 280 282	15 16 17 18 19	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
20 21 22 23 24	9.97130 .97143 .97157 .97170 .97183	13 13 13 13 13	·16755 ·16967 ·17180 ·17394	210 211 212 213 214	9.97931 .97944 .97957 .97970 .97984	$     \begin{array}{c}       13 \\       13 \\       13 \\       13 \\       13     \end{array}   $	$11.31162 \\ .31447 \\ .31734 \\ .32023 \\ .32313$	283 285 287 288 290	20 21 22 23 24	$\begin{array}{c ccccc} 210 & 200 \\ 6 & 21.0 & 20.0 \\ 7 & 24.5 & 23.3 \\ 8 & 28.0 & 26.6 \\ 9 & 31.5 & 30.0 \end{array}$
25 26 27 28 29	9.97197 .97210 .97224 .97237 .97251	13 13 13 13 13 13 13 13	·18041 ·18259	214 215 216 218 218	9.97997 .98010 .98023 .98036 .98050	$13 \\ 13 \\ 13 \\ 13 \\ 13 \\ 13 \\ 13 \\ 13 \\$	11-32606 -32900 -33196 -33494 -33793	292 294 296 298 299	25 26 27 28 29	$\begin{array}{c ccccc} 9 & 31.5 & 30.0 \\ 10 & 35.0 & 33.3 \\ 20 & 70.0 & 66.6 \\ 30 & 105.0 & 100.0 \\ 40 & 140.0 & 133.3 \\ 50 & 175.0 & 166.6 \end{array}$
30 31 32 33 34	9.97264 .97277 .97291 .97304 .97318	13 13 13 13 13 13 13	·19138 ·19361 ·19584	219 220 221 222 223	9.9806 <u>3</u> .9807 <u>6</u> .9808 <u>9</u> .98102 .98116	$     \begin{array}{c}       13 \\$	11 34095 34398 34704 35011 35321	301 303 305 307 309	30 31 32 33 34	$\begin{array}{cccccccccccccccccccccccccccccccccccc$
35 36 37 38 39	9.97331 .97345 .97358 .97371 .97385		·20034 ·20261 ·20489 ·20717	224 225 227 227 228	9.98129 .98142 .9815 <u>5</u> .9816 <u>8</u> .98181	$     \begin{array}{c}       13 \\$	36899	$31\overline{1} \\ 31\overline{3} \\ 31\overline{5} \\ 31\overline{5} \\ 318 \\ 320 $	35 36 37 38 39	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
40 41 42 43 44	9.97398 .97412 .97425 .97438 .97452	$1\overline{3}$ $1\overline{3}$ $1\overline{3}$ $1\overline{3}$ $1\overline{3}$ $1\overline{3}$	·21178 ·21178 ·21410 ·21643 ·21877	230 230 232 23 <u>3</u> 23 <u>3</u> 23 <u>4</u>	9.98195.98208.98221.98234.98247	$1\overline{3}$ 13 13 13 13 13	11 · 37221 · 37546 · 37872 · 38201 · 38532	322 324 326 328 328 331	40 41 42 43 44	$21\overline{0}$
45 46 47 48 49	9.9746 <u>5</u> .97478 .97492 .97505 .97519	$1\overline{3}$ $1\overline{3}$ $1\overline{3}$ $1\overline{3}$ $1\overline{3}$ $1\overline{3}$	·22349 ·22586 ·22825 ·23065	230 237 239 239	9.98260 .98273 .98287 .98300 .98313	13 1 <u>3</u> 13 13 13	11.38866 .39201 .39540 .39880 .40224	3335 335 340 343	45 46 47 48 49	$\begin{array}{c} 6 0 \cdot 2 0 \cdot 1 \mid 0 \cdot 0 \\ 7 \left( 0 \cdot 2 0 \cdot 1 \mid 0 \cdot 0 \right) \\ 8 \left( 0 \cdot 2 0 \cdot 1 \mid 0 \cdot 1 \right) \\ 9 \left( 0 \cdot 3 0 \cdot 1 \mid 0 \cdot 1 \right) \\ 1 \left( 0 0 \cdot 3 0 \cdot 1 \mid 0 \cdot 1 \right) \\ 2 \left( 0 0 \cdot 6 0 \cdot 3 \mid 0 \cdot 5 \mid 0 \cdot 2 \right) \\ 3 \left( 0 \cdot 1 0 \cdot 5 \mid 0 \cdot 5 \mid 0 \cdot 2 \right) \\ 4 \left( 0 \mid 1 \cdot 6 \mid 0 \cdot 8 \mid 0 \cdot 4 \right) \\ \end{array}$
50 51 52 53 54	9.97532 .97545 .97559 .97572 .97585	$13 \\ 13 \\ 13 \\ 13 \\ 13 \\ 13 \\ 13 \\ 13 \\$	11.23306 23548 23792 24037 24283	241 242 243 245 246	9.98326 .98339 .98352 .98365 .98365 .98378	13 13 13 13 13 13	11.40569.40918.41269.41622.41622.41979	34 <u>5</u> 348 351 35 <u>3</u> 35 <u>5</u>	50 51 52 53 54	$14 \ 1\overline{3} \ 13$ 6 1.4 1.3 1.3
55 56 57 58 59	9.97599 .97612 .97625 .97639 .97652	$1\overline{3}$ 13 13 13 13 13 13	11.24530 .24778 .25028 .25279 .25531	247 248 250 251 252	9.98392 .98405 .98418 .98431 .98444	$1\overline{3} \\ 13 \\ 13 \\ 13 \\ 13 \\ 13 \\ 13 \\ 13 \\ $	$11.42338 \\ .42699 \\ .43064 \\ .43064$	359 361 364 367 370	55 56 57 58 59	$\begin{array}{c} 7 & 1 \cdot \hat{6} & 1 \cdot 6 \\ 8 & 1 \cdot 8 & 1 \cdot 8 \\ 9 & 2 \cdot 1 & 2 \cdot 0 & 1 \cdot 5 \\ 10 & 2 \cdot 3 & 2 \cdot 2 & 2 \cdot 1 \\ 20 & 4 \cdot 6 & 4 \cdot 5 & 4 \cdot 3 \\ 30 & 7 \cdot 0 & 6 \cdot 7 & 6 \cdot 5 \\ 40 & 9 \cdot 3 & 9 \cdot 0 & 8 \cdot 6 \end{array}$
<u>60</u> /	9.97665 Lg. Vers.	$1\overline{3}$ <b>D</b>	<u>11 · 25785</u> Log. Exs.	254 D	9.98457 Lg. Vers.	$\frac{1\overline{3}}{D}$	<u>11.44175</u> Log. Exs.	$\frac{37\overline{3}}{D}$	<u>60</u> ′	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$

# TABLE VIII.—LOGARITHMIC VERSED SINES AND EXTERNAL SECANTS. 88° 89°

'	Lg. Vers.	D	Log.Exs.	D	Lg. Vers.	D	Log.Exs.	D	'	P. P.
0	9.98457 .98470	13	11.44175 .44551	376		$1\overline{2}$	11.75050 .75792	742		
23	·98483	13 13	.44931	379	00261	113	.76547	755		
3	•98496	13	.44931 .45313	382 386	•99274	13	.77316	700		
_4	<u>.98509</u>	13	<u>.45699</u>	389	.99207	12	.78097	1 707		
5 6	9.98522 .98535	13	$11.4608\overline{8}$ .46480	392	9.99299	13	11.78892 .79702	0.07		
7	.98548	$13 \\ 13$	-46876	395	00305	$\frac{13}{12}$	.80527	820	7	
8	·98562	13	·47275	399 402	•99338	13	·81367	840		
9	<u>·98575</u>	13	47677	406	- 99201	12	.82223	077	·	
10	9.98588 .98601	13	$11.4808\overline{3}$ .48493	409	9.99363 .99376	13	11.83095 .83986	1 0.07	10 11	
$\frac{11}{12}$	.98614	13 13	·48906	413	.99389	$13 \\ 12$	·84894	908	12	
13	·98627	13	·49323	420	•99402	13	·85821	927 947	1 10	
$\frac{14}{15}$	$\frac{.98640}{9.98653}$	13		425	.99415	13	<u>·86768</u>	967	$\frac{14}{15}$	
$16^{15}$	•98666	13	$11.5016\overline{8}$ .50597	428	9.99428 .99440	112	11.87735	0.00	16	
17	·98679	13 13	·51029	432 436	·99453	$13 \\ 12$	·88724 ·89735	1009 1034	17	
18	·98692 ·98705	13	·51466	440	·99466	13	•90769	1059		
$\frac{19}{20}$	$\frac{.98705}{9.98718}$	13	<u>.51906</u> 11.52351	445	·99479 9·99491	12	.91829 11.92914	1085	$\frac{19}{20}$	-
21	.98731	13	.52801	$44\bar{9}$	·99504	13	.94026	$111\bar{2}$	21	
22	.98744	13 13	.53255	454 458	·99517	$13 \\ 12$	.95167	$  1140 \\ 1171$	22	
$\frac{23}{24}$	·98757 ·98770	13	.53713 .54176	463	·99530 ·99543	13	·96338 ·97541	1203	23 24	i i
<u>24</u> 25	9.98783	13	$11.5464\overline{3}$	$46\bar{7}$	9.99555	$1\overline{2}$	11.98777	1236	25	
26	.98796	13	·55116	472	•99568	$13 \\ 12$	12.00048	1271	26	
27	.98809	$13 \\ 13$	•55593	$47\overline{7} \\ 48\overline{2}$	·99581	$12 \\ 13$	.01358	$  130\overline{9} \\ 1349$	27	
28 29	·98822 ·98835	īš	• 5607 <u>6</u> • 56563	187	·99594 ·99606	$1\overline{2}$	·02707 ·04098	1391	28 29	
30	9.98848	13	$\frac{100000}{11.57056}$	$49\overline{2}$	9.99619	$13 \\ 12$	12.05535	1436	30	
31	·98861	$\frac{13}{13}$	.57554	498 504	.99632	12	.07020	1485 1537	31	
32	·98874	13	·58058	509	·99645	$\tilde{13}$ 12	·08557	1592	32 33	-
33 34	·98887 ·98900	13	·58567 ·59082	515	·99657 ·99670	13	·10149 ·11801	1652	34	
35	9.98913	$\frac{13}{12}$	$11.5960\overline{2}$	520	9.99683	$1\overline{2}$ $1\overline{2}$	12.13517	1716	35	
36	·98925	13	.60129	527 533	·99695	13	·15302	$178\overline{5}$ 1861	36	
37 38	·9893 <u>8</u> ·98951	13	$6066\overline{2}$ 61202	53 <u>9</u>	·99708 ·99721	$\frac{13}{12}$	.17163 .19106	1943	37 38	
<u>39</u>	.98964	13	.61747	545	.99734	13	21139	2033	39	
40	9.9897 <u>7</u>	$\frac{13}{13}$	11.62300	$55\overline{2}$ 559	$9.9974\overline{6}$	$1\bar{2} \\ 13$	12.23271	2131 2240	40	13 13
41 42	•9899 <u>0</u> •99003	13	62859 63425	566	·99759 ·99772	$1\overline{2}$ $1\overline{2}$	$.2551\overline{1}$ $.2787\overline{2}$	2361	41	6 1.3 1.3
43	.99016	$\frac{13}{12}$	.63998	573	.99784	$\frac{12}{13}$	-30367	2495	43	7 1.6 1.5 8 1.8 1.7
<u>44</u>	99029	12	.64579	581	<u>.99797</u>	$13 \\ 1\overline{2}$	.33013	2645 2815	.44	9 2.0 $1.9$
45	9.99042	13	${}^{11.65167}_{-65762}_{-66366}$	588 595	9.99810	$12 \\ 13$	$12.3582\overline{8}$	3009	45	10 2.2 2.1
46 47	·99055 ·99068	13	.66366	604	•9982 <u>3</u> •99835	$\frac{13}{12}$ 12	$+3883\overline{7}$ $+4206\overline{8}$	3231	46 47	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
48	.99081	$\frac{13}{12}$		$611 \\ 620$	.99848	$\frac{12}{13}$	·45557	$3489 \\ 3791$	48	40 9.0 8.6
<u>49</u>	<u>.99093</u>	13	.67598	628	.99861		.49349	4152	<u>49</u>	50 11.2 10 <b>.8</b>
50 51	$9.9910\overline{6}$ .99119	13	11.00221	638	$9.9987\overline{3}$	$1\overline{2}$ $1\overline{2}$	$12.53501 \\ .58089$	$458\overline{8}$	$\frac{50}{51}$	17_
52	·99132	13		646	•99886 •9989 <u>9</u>	$\frac{13}{12}$	.63217	5127	52	$6 1 \cdot \overline{2}$
53	$.9914\overline{5}$	$\frac{13}{12}$	•70168	656 666	·99911	$12 \\ 12$	·69029	5812 6707	53	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$
54	<u>·99158</u>	13	.70834	675	.99924		.75736	7931	54	9 1.9
55 56	$9.99171 \\ .99184$	13		68 <u>ē</u>	9.99937 .99949	$13 \\ 12 \\ 12 \\ 12 \\ 12 \\ 12 \\ 12 \\ 12 \\ $	12.83667 .9337 <u>1</u>	9704	55 56	$10 2 \cdot 1$
57	·99197	$\frac{13}{12}$	·72892	69 <u>6</u> 707	·99962	12	13.05877	$12506 \\ 17621$	57	$\begin{array}{cccc} 10 & 2 \cdot \underline{1} \\ 20 & 4 \cdot \underline{1} \\ 30 & 6 \cdot \overline{2} \end{array}$
58 59	·99209	13	·73600	719	·99974	13	.23499	30116	58 59	40 8.3
<u>60</u>	·99222 9·99235	13	<u>.74319</u> 11.75050	730	$\frac{.99987}{10.0000}$	$1\overline{2}$	•53615 Infinity		$\frac{59}{60}$	50 10 - 4
<del>~</del>	Lg. Vers.	$\overline{D}$	Log. Exs.	D	Lg. Vers.	D	Log. Exs.	D	~	P. P.
1	-6				-9. 10.01)	- 1				

#### TABLE IX.-NATURAL SINES, COSINES, TANGENTS, AND COTANGENTS.

0°

1°

			0°			1°				
	Sin.	Cos.	Tan.	Cot.	Sin.	Cos.	Tan.	Cot.		
0 1 2 3 4	.00000 .00029 .00058 .00087 .00116	One One One One One	.00000 .00029 .00058 .00087 .00116	Infinite 3437.75 1718.87 1145.92 859.436	.01745 .01774 .01803 .01832 .01862	.99985 .99984 .99984 .99983 .99983	.01746 .01775 .01804 .01833 .01862	$\begin{array}{r} 57.2900\\ 56.3506\\ 55.4415\\ 54.5613\\ 53.7086\end{array}$	60 59 58 57 56	
5 6 7 8 9	.00145 .00175 .00204 .00233 .00262	One One One One One	.00145 .00175 .00204 .00233 .00262	$\begin{array}{r} 687 \cdot 549 \\ 572 \cdot 957 \\ 491 \cdot 106 \\ 429 \cdot 718 \\ 381 \cdot 971 \end{array}$	.01891 .01920 .01949 .01978 .02007	.99982 .99982 .99981 .99980 .99980	.01891 .01920 .01949 .01978 .02007	52.882152.080751.303250.548549.8157	55 54 53 52 51	
10 11 12 13 14	.00291 .00320 .00349 .00378 .00407	One .99999 .99999 .99999 .99999	.00291 .00320 .00349 .00378 .00407	$\begin{array}{r} 343.774\\ 312.521\\ 286.478\\ 264.441\\ 245.552\end{array}$	.02036 .02065 .02094 .02123 .02152	.99979 .99979 .99978 .99977 .99977	.02036 .02066 .02095 .02124 .02153	$\begin{array}{r} 49.1039 \\ 48.4121 \\ 47.7395 \\ 47.0853 \\ 46.4489 \end{array}$	50 49 48 47 46	
15 16 17 18 19	•00436 •00465 •00495 •00524 •00553	.99999 .99999 .99999 .99999 .99999	$\begin{array}{r} .00436\\ .00465\\ .00495\\ .00524\\ .00553\end{array}$	$\begin{array}{r} 229.182\\ 214.858\\ 202.219\\ 190.984\\ 180.932 \end{array}$	.02181 .02211 .02240 .02269 .02298	-99976 -99976 -99975 -99974 -99974	.02182 .02211 .02240 .02269 .02298	$\begin{array}{r} 45.8294\\ 45.2261\\ 44.6386\\ 44.0661\\ 43.5081 \end{array}$	45 44 43 42 41	
20 21 22 23 24	.00582 .00611 .00640 .00669 .00698	.99998 .99998 .99998 .99998 .99998	.00582 .00611 .00640 .00669 .00698	171.885163.700156.259149.465143.237	02327 02356 02385 02414 02443	.99973 .99972 .99972 .99971 .99970	·02328 ·02357 ·02386 ·02415 ·02444	$\begin{array}{r} 42.9641 \\ 42.4335 \\ 41.9158 \\ 41.4106 \\ 40.9174 \end{array}$	40 39 38 37 36	
25 26 27 28 29	.00727 .00756 .00785 .00814 .00844	.999997 .999997 .999997 .90997 .90997	.00727 .00756 .00785 .00815 .00844	137.507132.219127.321122.774118.540	.02472 .02501 .02530 .02560 .02589	.99969 .99969 .99968 .99967 .99966	.02473 .02502 .02531 .02560 .02589	$\begin{array}{r} 40.4358\\ 39.9655\\ 39.5059\\ 39.0568\\ 38.6177\end{array}$	35 34 33 32 31	
30 31 32 33 34	.00873 .00902 .00931 .00960 .00989	.99996 .99996 .99996 .99996 .99995 .99995	.00873 .00902 .00931 .00960 .00989	114.589110.892107.426104.171101.107	.02618 .02647 .02676 .02705 .02734	.99966 .99965 .99964 .99963 .99963	.02619 .02648 .02677 .02706 .02735	$38 \cdot 1885$ $37 \cdot 7686$ $37 \cdot 3579$ $36 \cdot 9560$ $36 \cdot 5627$	30 29 28 27 26	
35 36 37 38 39	.01018 .01047 .01076 .01105 .01134	.99995 .99995 .99994 .99994 .99994	.01018 .01047 .01076 .01105 .01135	$\begin{array}{r} 98.2179 \\ 95.4895 \\ 92.9085 \\ 90.4633 \\ 88.1436 \end{array}$	.02763 .02792 .02821 .02850 .02879	.99962 .99961 .99960 .99959 .99959	·02764 ·02793 ·02822 ·02851 ·02881	36.1776 35.8006 35.4313 35.0695 34.7151	25 24 23 22 21	
40 41 42 43 44	.01164 .01193 .01222. .01251 .01280	.99993 .99993 .99993 .99992 .99992	.01164 .01193 .01222 .01251 .01280	85.9398 83.8435 81.8470 79.9434 78.1263	·02908 ·02938 ·02967 ·02996 ·03025	.99958 .99957 .99956 .99955 .99954	.02910 .02939 .02968 .02997 .03026	$\begin{array}{r} 34.3678\\ 34.0273\\ 33.6935\\ 33.3652\\ 33.0452\end{array}$	20 19 18 17 16	
45 46 47 48 49	.01309 .01338 .01367 .01396 .01425	.99991 .99991 .99991 .99990 .99990	·01309 ·01338 ·01367 ·01396 ·01425	76.3900 74.7292 73.1390 71.6151 70.1533	·03054 ·03083 ·03112 ·03141 ·03170	.99953 .99952 .99952 .99951 .99950	.03055 .03084 .03114 .03143 .03172	$\begin{array}{r} 32.7303\\ 32.4213\\ 32.1181\\ 31.8205\\ 81.5284 \end{array}$	15 14 13 12 11	
50 51 52 53 54	·01454 ·01483 ·01513 ·01542 ·01571	.99989 .99989 .99989 .99988 .99988 .99988	·01455 ·01484 ·01513 ·01542 ·01571	68.7501 67.4019 66.1055 64.8580 63.6567	.03199 .03228 .03257 .03286 .03316	.99949 .99948 .99947 .99946 .99945	·03201 ·03230 ·03259 ·03288 ·03317	31.2416 30.9599 30.6833 30.4116 30.1446	10 9 8 7 6	
55 56 57 58 59	•01600 •01629 •01658 •01687 •01716	.99987 .99987 .99986 .99986 .99986 .99985	.01600 .01629 .01658 .01687 .01716	62.4992 61.3829 60.3058 59.2659 58.2612	.03345 .03374 .03403 .03432 .03461	.99944 .99943 .99942 .99941 .99940	$\begin{array}{r} .03346 \\ .03376 \\ .03405 \\ .03434 \\ .03463 \end{array}$	29.8823 29.6245 29.3711 29.1220 28.8771	5 4 3 2 1	
<u>60</u>	<u>.01745</u> Cos.	<u>.99985</u> Sin.	<u>.01746</u> Cot.	57.2900 Tan.	<u>•03490</u> Cos.	<u>.99939</u> Sin.	<u>.03492</u> Cot.	<u>28.6363</u> Tan.	<del>~</del>	
			200	01	15		0.0			

89°

695

88°

**FABLE IX.—NATURAL SINES, COSINES, TANGENTS, AND COTANGENTS.** 

2° 3°									
-	Sin.	Cos.	Tan.	Cot.	Sin.	Cos.	Tan.	Cot.	1
01234	·03490 ·03519 ·03548 ·03577 ·03606	.99939 .99938 .99937 .99936 .99935	·03492 ·03521 ·03550 ·03579 ·03609	$\begin{array}{r} 28.6363\\ 28.3994\\ 28.1664\\ 27.9372\\ 27.7117\end{array}$	·05234 ·05263 ·05292 ·05321 ·05350	·99863 ·99861 ·99860 ·99858 ·99857	·05241 ·05270 ·05299 ·05328 ·05357	$     \begin{array}{r}       19.0811 \\       18.9755 \\       18.8711 \\       18.7678 \\       18.6656     \end{array} $	60 59 58 57 56
5 6 7 8 9	·03635 ·03664 ·03693 ·03723 ·03752	.99934 .99933 .99932 .99931 .99930	·03638 ·03667 ·03696 ·03725 ·03754	$\begin{array}{r} 27.4899\\ 27.2715\\ 27.0566\\ 26.8450\\ 26.6367\end{array}$	·05379 ·05408 ·05437 ·05466 ·05495	.99855 .99854 .99852 .99851 .99849	·05387 ·05416 ·05445 ·05474 ·05503	$   \begin{array}{r}     18.5645 \\     18.4645 \\     18.3655 \\     18.2677 \\     18.1708   \end{array} $	55 54 53 52 51
10 11 12 13 14	.03781 .03810 .03839 .03868 .03897	.99929 .99927 .99926 .99925 .99924	·03783 ·03812 ·03842 ·03871 ·03900	$\begin{array}{r} 26.4316\\ 26.2296\\ 26.0307\\ 25.8348\\ 25.6418\end{array}$	$\begin{array}{r} .05524 \\ .05553 \\ .05582 \\ .05611 \\ .05640 \end{array}$	.99847 .99846 .99844 .99842 .99841	.05533 .05562 .05591 .05620 .05649	$\begin{array}{r} 18.0750\\ 17.9802\\ 17.8863\\ 17.7934\\ 17.7015\end{array}$	50 49 48 47 46
15 16 17 18 19	.03926 .03955 .03984 .04013 .04042	.99923 .99922 .99921 .99919 .99918	.03929 .03958 .03987 .04016 .04046	$\begin{array}{r} 25.4517\\ 25.2644\\ 25.0798\\ 24.8978\\ 24.7185 \end{array}$	.05669 .05698 .05727 .05756 .05785	.99839 .99838 .99836 .99834 .99833	.05678 .05708 .05737 .05766 .05795	$\begin{array}{r} 17.6106 \\ 17.5205 \\ 17.4314 \\ 17.3432 \\ 17.2558 \end{array}$	45 44 43 42 41
20 21 22 23 24	.04071 .04100 .04129 .04159 .04188	.99917 .99916 .99915 .99913 .99912	.04075 .04104 .04133 .04162 .04191	$\begin{array}{r} 24.5418\\ 24.3675\\ 24.1957\\ 24.0263\\ 23.8593 \end{array}$	.05814 .05844 .05873 .05902 .05931	.99831 .99829 .99827 .99826 .99824	·05824 ·05854 ·05883 ·05912 ·05941	$\begin{array}{r} 17.1693 \\ 17.0837 \\ 16.9990 \\ 16.9150 \\ 16.8319 \end{array}$	40 39 38 37 36
25 26 27 28 29	.04217 .04246 .04275 .04304 .04333	.99911 .99910 .99909 .99907 .99906	.04220 .04250 .04279 .04308 .04337	$\begin{array}{r} 23.6945\\ 23.5321\\ 23.3718\\ 23.2137\\ 23.0577\end{array}$	.05960 .05989 .06018 .06047 .06076	.99822 .99821 .99819 .99817 .99815	·05970 ·05999 ·06029 ·06058 ·06087	16.749616.668116.587416.507516.4283	35 34 33 32 31
30 31 32 33 34	04362 04391 04420 04449 04478	.99905 .99904 .99902 .99901 .99900	$04366 \\ 04395 \\ 04424 \\ 04454 \\ 04483$	$\begin{array}{r} 22.9038\\ 22.7519\\ 22.6020\\ 22.4541\\ 22.3081 \end{array}$	$     \begin{array}{r}         & .06105 \\             .06134 \\             .06163 \\             .06192 \\             .06221         \end{array} $	.99813 .99812 .99810 .99808 .99806	$     \begin{array}{r}         \cdot 06116 \\         \cdot 06145 \\         \cdot 06175 \\         \cdot 06204 \\         \cdot 06233     \end{array} $	$\begin{array}{r} 16.3499 \\ 16.2722 \\ 16.1952 \\ 16.1190 \\ 16.0435 \end{array}$	30 29 28 27 26
35 36 37 38 39	04507 04536 04565 04594 04623	.99898 .99897 .99896 .99894 .99893	.04512 .04541 .04570 .04599 .04628	$\begin{array}{r} 22.1640\\ 22.0217\\ 21.8813\\ 21.7426\\ 21.6056\end{array}$	·06250 ·06279 ·06308 ·06337 ·06366	.99804 .99803 .99801 .99799 .99797	$     \begin{array}{r}         \cdot 06262 \\         \cdot 06291 \\         \cdot 06321 \\         \cdot 06350 \\         \cdot 06379 \\         \cdot 06379     \end{array} $	$\begin{array}{r} 15.9687\\ 15.8945\\ 15.8211\\ 15.7483\\ 15.6762\end{array}$	25 24 23 22 21
40 41 42 43 44	·04653 ·04682 ·04711 ·04740 ·04769	.99892 .99890 .99889 .99888 .99888	·04658 ·04687 ·04716 ·04745 ·04774	21.470421.336921.204921.074720.9460	06395 06424 06453 06482 06511	.99795 .99793 .99792 .99790 .99788	06408 06437 06467 06496 06525	$\begin{array}{r} 15.6048\\ 15.5340\\ 15.4638\\ 15.3943\\ 15.3254\end{array}$	20 19 18 17 16
45 46 47 48 49	·04798 ·04827 ·04856 ·04885 ·04914	·99885 ·99883 ·99882 ·99881 ·99879	·04803 ·04833 ·04862 ·04891 ·04920	$\begin{array}{r} 20.8188\\ 20.6932\\ 20.5691\\ 20.4465\\ 20.3253\end{array}$	·06540 ·06569 ·06598 ·06627 ·06656	.99786 .99784 .99782 .99780 .99778	$     \begin{array}{r}         \cdot 06554 \\         \cdot 06584 \\         \cdot 06613 \\         \cdot 06642 \\         \cdot 06671 \\         \cdot 06671     \end{array} $	$\begin{array}{r} 15.2571 \\ 15.1893 \\ 15.1222 \\ 15.0557 \\ 14.9898 \end{array}$	15 14 13 12 11
50 51 52 53 54	.04943 .04972 .05001 .05030 .05059	.99878 .99876 .99875 .99873 .99872	·04949 ·04978 ·05007 ·05037 ·05066	$\begin{array}{c} 20 \cdot 2056 \\ 20 \cdot 0872 \\ 19 \cdot 9702 \\ 19 \cdot 8546 \\ 19 \cdot 7403 \end{array}$	·06685 ·06714 ·06743 ·06773 ·06802	.99776 .99774 .99772 .99770 .99768	.06700 .06730 .06759 .06788 .06817	$14.9244 \\ 14.8596 \\ 14.7954 \\ 14.7317 \\ 14.6685 $	10 9 8 7 6
55	05000	00070	05005	10 6072	06001	00766	06947	14 8050	5

87°

.99870

.99869

.99867

.99866

.99864

.99863

Sin.

.05095

.05124

.05153

.05182

.05212

05241

Cot.

69

60

.05088

.05117

·05146 ·05175

.05205

.05234

Cos.

696

.06831

.06860

.06889

.06918

.06947

.06976

Cos.

19.6273

19.5156

19.4051

19.2959

19.1879

19.0811

Tan.

86°

.06847

.06876

.06905

.06934

.06963

.06993

Cot.

14.6059

14.5438

14.4823

14.4212

14.3607

14.3007

Tan.

54321

0

.99766

.99764

.99762

.99760

.99758

.99756

Sin.

TABLE IX.-NATURAL SINES, COSINES, TANGENTS, AND COTANGENTS. 40 ·

<u>e</u>0

			<b>4°</b> °						
	Sin.	Cos.	Tap.	Cot.	Sin.	Cos.	Tan.	Cot.	,
01234	.06976 .07005 .07034 .07063 .07092	.99756 .99754 .99752 .99750 .99748	.06993 .07022 .07051 .07080 .07110	$\begin{array}{r} 14.3007 \\ 14.2411 \\ 14.1821 \\ 14.1235 \\ 14.0655 \end{array}$	·08716 ·08745 ·08774 ·08803 ·08831	.99619 .99617 .99614 .99612 .99609	·08749 ·08778 ·08807 ·08837 ·08837 ·08866	11.4301 11.3919 11.3540 11.3163 11.2789	60 59 58 57 56
5 6 7 8 9	.07121 .07150 .07179 .07208 .07237	.99746 .99744 .99742 .99740 .99738	.07139 .07168 .07197 .07227 .07256	14.0079 13.9507 13.8940 13.8378 13.7821	·08860 ·08889 ·08918 ·08947 ·08976	.99607 .99604 .99602 .99599 .99596	·08895 ·08925 ·08954 ·08983 ·09013	11.2417 11.2048 11.1681 11.1316 11.0954	55 54 53 52 51
10 11 12 13 14	.07266 .07295 .07324 .07353 .07382	.99736 .99734 .99731 .99729 .99727	.07285 .07314 .07344 .07373 .07402	$13.7267 \\ 13.6719 \\ 13.6174 \\ 13.5634 \\ 13.5098$	.09005 .09034 .09063 .09092 .09121	.99594 .99591 .99588 .99586 .99586	·09042 ·09071 ·09101 ·09130 ·09159	$11.0594 \\ 11.0237 \\ 10.9882 \\ 10.9529 \\ 10.9178$	50 49 48 47 46
15 16 17 18 19	.07411 .07440 .07469 .07498 .07527	.99725 .99723 .99721 .99719 .99716	.07431 .07461 .07490 .07519 .07548	$\begin{array}{r} 13.4566 \\ 13.4039 \\ 13.3515 \\ 13.2996 \\ 13.2480 \end{array}$	.09150 .09179 .09208 .09237 .09266	.99580 .99578 .99575 .99572 .99570	.09189 .09218 .09247 .09277 .09306	10.8829 10.8483 10.8139 10.7797 10.7457	45 44 43 42 41
20 21 22 23 24	.07556 .07585 .07614 .07643 .07672	.99714 .99712 .99710 .99708 .99705	.07578 .07607 .07636 .07665 .07695	13.196913.146113.095813.045812.9962	.09295 .09324 .09353 .09382 .09411	.99567 .99564 .99562 .99559 .99556	.09335 .09365 .09394 .09423 .09453	$\begin{array}{r} 10.7119 \\ 10.6783 \\ 10.6450 \\ 10.6118 \\ 10.5789 \end{array}$	40 39 38 37 36
25 26 27 28 29	.07701 .07730 .07759 .07788 .07817	.99703 .99701 .99699 .99696 .99694	.07724 .07753 .07782 .07812 .07841	12.9469 12.8981 12.8496 12.8014 12.7536	·09440 ·09469 ·09498 ·09527 ·09556	.99553 .99551 .99548 .99545 .99545	.09482 .09511 .09541 .09570 .09600	$10.5462 \\ 10.5136 \\ 10.4813 \\ 10.4491 \\ 10.4172$	35 34 33 32 31
30 31 32 33 34	.07846 .07875 .07904 .07933 .07962	.99692 .99689 .99687 .99685 .99683	.07870 .07899 .07929 .07958 .07987	$12.7062 \\ 12.6591 \\ 12.6124 \\ 12.5660 \\ 12.5199$	.09585 .09614 .09642 .09671 .09700	.99540 .99537 .99534 .99531 .99528	.09629 .09658 .09688 .09717 .09746	$\begin{array}{r} 10.3854 \\ 10.3538 \\ 10.3224 \\ 10.2913 \\ 10.2602 \end{array}$	30 29 28 27 26
35 36 37 38 <u>39</u>	.07991 .08020 .08049 .08078 .08107	.99680 .99678 .99676 .99673 .99673	.08017 .08046 .08075 .08104 .08134	$12.4742 \\ 12.4288 \\ 12.3838 \\ 12.3390 \\ 12.2946$	.09729 .09758 .09787 .09816 .09845	.99526 .99523 .99520 .99517 .99514	.09776 .09805 .09834 .09864 .09893	$\begin{array}{c} 10.2294 \\ 10.1988 \\ 10.1683 \\ 20.1381 \\ 10.1080 \end{array}$	25 24 23 22 21
40 41 42 43 44	.08136 .08165 .08194 .08223 .08252	.99668 .99666 .99664 .99661 .99659	·08163 ·08192 ·08221 ·08251 ·08280	12.250512.206712.163212.120112.0772	·09874 ·09903 ·09932 ·09961 ·09990	.99511 .99508 .99506 .99503 .99500	.09923 .09952 .09981 .10011 .10040	10.0780 10.0483 10.0187 9.98931 9.96007	20 19 18 17 16
45 46 47 48 49	.08281 .08310 .08339 .08368 .08397	.99657 .99654 .99652 .99649 .99647	.08309 .08339 .08368 .08397 .08427	12.0346 11.9923 11.9504 11.9087 11.8673	.10019 .10048 .10077 .10106 .10135	.99497 .99494 .99491 .99488 .99485	.10069 .10099 .10128 .10158 .10187	9.93101 9.90211 9.87338 9.84482 9.81641	15 14 13 12 11
50 51 52 53 54	.08426 .08455 .08484 .08513 .08542	.99644 .99642 .99639 .99637 .99635	·08456 ·08485 ·08514 ·08544 ·08573	11.8262 11.7853 11.7448 11.7045 11.6645	.10164 .10192 .10221 .10250 .10279	.99482 .99479 .99476 .99473 .99470	.10216 .10246 .10275 .10305 .10334	9.78817 9.76009 9.73217 9.70441 9.67680	10 9 8 7 6
55 56 57 58 59	.08571 .08600 .08629 .08658 .08687	.99632 .99630 .99627 .99625 .99622	.08602 .08632 .08661 .08690 .08720	11.6248 11.5853 11.5461 11.5072 11.4685	·10308 ·10337 ·10366 ·10395 ·10424	.99467 .99464 .99461 .99458 .99455	.10363 .10393 .10422 .10452 .10481	$\begin{array}{r} 9.64935\\ 9.62205\\ 9.59490\\ 9.56791\\ 9.54106\end{array}$	5 4 3 2 1
<u>60</u>	<u>.08716</u> Cos.	<u>.99619</u> Sin.	<u>.08749</u> Cot.	<u>11.4301</u> Tan.	<u>.10453</u> Cos.	<u>.99452</u> Sin.	<u>.10510</u> Cot.	<u>9.51436</u> Tan.	<del>_0</del>
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TABLE IXNATURAL SINES,	COSINES.	TANGENTS. A	ND	COTANGENTS.

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	6° 7°									
1	Sin.	Cos.	Tan.	Cot.	Sin.	Cos.	Tan.	Cot.	,	
0	·10453	•99452	·10510	9.51436	.12187	.99255	·12278	8.14435	60	
1	·10482	•99449	·10540	9.48781	.12216	.99251	·12308	8.12481	59	
2	·10511	•99446	·10569	9.46141	.12245	.99248	·12338	8.10536	58	
3	·10540	•99443	·10599	9.43515	.12274	.99244	·12367	8.08600	57	
4	·10569	•99440	·10628	9.40904	.12302	.99244	·12397	8.06674	56	
5	.10597	.99437	·10657	9.38307	·12331	•99237	·12426	8.04756	55	
6	.10626	.99434	·10687	9.35724	·12360	•99233	·12456	8.02848	54	
7	.10655	.99431	·10716	9.33155	·12389	•99230	·12485	8.00948	53	
8	.10684	.99428	·10746	9.30599	·12418	•99226	·12515	7.99058	52	
9	.10713	.99424	·10775	9.28058	·12447	•99222	·12544	7.97176	51	
$10\\11\\12\\13\\14$	.10742 .10771 .10800 .10829 .10858	.99421 .99418 .99415 .99412 .99409	.10805 .10834 .10863 .10893 .10922	9.25530 9.23016 9.20516 9.18028 9.15554	.12476 .12504 .12533 .12562 .12591	.99219 .99215 .99211 .99208 .99204	<pre>.12574 .12603 .12633 .12662 .12692</pre>	7.95302 7.93438 7.91582 7.89734 7.87895	50 49 48 47 46	
15	•10887	.99406	.10952	9.13093	.12620	.99200	.12722	7.86064	45	
16	•10916	.99402	.10981	9.10646	.12649	.99197	.12751	7.84242	44	
17	•10945	.99399	.11011	9.08211	.12678	.99193	.12781	7.82428	43	
18	•10973	.99396	.11040	9.05789	.12706	.99189	.12810	7.80622	42	
19	•11002	.99393	.11070	9.03379	.12735	.99186	.12840	7.78825	41	
20	·11031	.99390	.11099	9.00983	.12764	.99182	.12869	7.77035	40	
21	·11060	.99386	.11128	8.98598	.12793	.99178	.12899	7.75254	39	
22	·11089	.99383	.11158	8.96227	.12822	.99175	.12929	7.73480	38	
23	·11118	.99380	.11187	8.93867	.12851	.99171	.12958	7.71715	37	
24	·11147	.99377	.11217	8.91520	.12880	.99167	.12988	7.69957	36	
25	·11176	.99374	.11246	8.89185	.12908	.99163	.13017	7.68208	35	
26	·11205	.99370	.11276	8.86862	.12937	.99160	.13047	7.66466	34	
27	·11234	.99367	.11305	8.84551	.12966	.99156	.13076	7.64732	33	
28	·11263	.99364	.11335	8.82252	.12995	.99152	.13106	7.63005	32	
29	·11291	.99360	.11364	8.79964	.13024	.99148	.13136	7.61287	31	
30 31 32 33 34	·11320 ·11349 ·11378 ·11407 ·11436	.99357 .99354 .99351 .99347 .99344	$\begin{array}{r} .11394\\ .11423\\ .11452\\ .11452\\ .11482\\ .11511\end{array}$	8.77689 8.75425 8.73172 8.70931 8.68701	.13053 .13081 .13110 .13139 .13168	.99144 .99141 .99137 .99133 .99129	$     \begin{array}{r}         & \cdot 13165 \\         & \cdot 13195 \\         & \cdot 13224 \\         & \cdot 13254 \\         & \cdot 13284 \\         & \cdot 13284     \end{array} $	7.59575 7.57872 7.56176 7.54487 7.52806	30 29 28 27 26	
35	·11465	·99341	.11541	8.66482	.13197	.99125	$     \begin{array}{r}         & \cdot 13313 \\         & \cdot 13343 \\         & \cdot 13372 \\         & \cdot 13402 \\         & \cdot 13432     \end{array}   $	7.51132	25	
36	·11494	·99337	.11570	8.64275	.13226	.99122		7.49465	24	
37	·11523	·99334	.11600	8.62078	.13254	.99118		7.47806	23	
38	·11552	·99331	.11629	8.59893	.13283	.99114		7.46154	22	
39	·11580	·99327	.11659	8.57718	.13312	.99110		7.44509	21	
40	·11609	.99324	·11688	8.55555	.13341     .13370     .13399     .13427     .13456	.99106	.13461	7.42871	20	
41	·11638	.99320	·11718	8.53402		.99102	.13491	7.41240	19	
42	·11667	.99317	·11747	8.51259		.99098	.13521	7.39616	18	
43	·11696	.99314	·11777	8.49128		.99094	.13550	7.37999	17	
44	·11725	.99310	·11777	8.47007		.99091	.13580	7.36389	16	
45	.11754	.99307	.11836	8.44896	$     \begin{array}{r}             .13485 \\             .13514 \\             .13543 \\             .13572 \\             .13600 \\         \end{array}     $	.99087	.13609	7.34786	15	
46	.11783	.99303	.11865	8.42795		.99083	.13639	7.33190	14	
47	.11812	.99300	.11895	8.40705		.99079	.13669	7.31600	13	
48	.11840	.99297	.11924	8.38625		.99075	.13698	7.30018	12	
49	.11869	.99293	.11954	8.36555		.99071	.13728	7.28442	11	
50 51 52 53 54	·11898 ·11927 ·11956 ·11985 ·12014	.99290 .99286 .99283 .99279 .99276	·11983 ·12013 ·12042 ·12072 ·12101	8.34496 8.32446 8.30406 8.28376 8.26355	$     \begin{array}{r}             .13629 \\             .13658 \\             .13687 \\             .13716 \\             .13744 \\         \end{array}     $	.99067 .99063 .99059 .99055 .99051	.13758 .13787 .13817 .13846 .13876	$\begin{array}{r} 7.26873 \\ 7.25310 \\ 7.23754 \\ 7.22204 \\ 7.20661 \end{array}$	10 9 8 7 6	
55 56 57 58 59	.12043 .12071 .12100 .12129 .12158	.99272 .99269 .99265 .99262 .99258	$ \begin{array}{r} \cdot 12131 \\ \cdot 12160 \\ \cdot 12190 \\ \cdot 12219 \\ \cdot 12249 \\ \hline \end{array} $		.13773 .13802 .13831 .13860 .13889	.99047 .99043 .99039 .99035 .99031	.13906 .13935 .13965 .13995 .14024	$\begin{array}{r} 7.19125 \\ 7.17594 \\ 7.16071 \\ 7.14553 \\ 7.13042 \end{array}$	54321	
<u>60</u>	<u>. 12187</u> Cos.	<u>.99255</u> Sin.	<u>-12278</u> Cot.	8.14435 Tan.	<u>·13917</u> Cos.	<u>.99027</u> Sin.	<u>.14054</u> Cot.	7.11537 Tan.	~	
				0.0						

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TABLE IXNATURAL SINES,	, COSINES, TANGENTS, AND COTANGENTS.
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	•	8	8°				9°		
	Sin.	Cos.	Tan.	Cot.	Sin.	Cos.	Tan.	Cot.	,
0 1 2 3 4	·13917 ·13946 ·13975 ·14004 ·14033	.99027 .99023 .99019 .99015 .99011	$     \begin{array}{r}             .14054 \\             .14084 \\             .14113 \\             .14143 \\             .14173         \end{array}     $	7.11537 7.10038 7.08546 7.07059 7.05579	.15643 .15672 .15701 .15730 .15758	.98769 .98764 .98760 .98755 .98751	.15838 .15868 .15898 .15928 .15958	$\begin{array}{r} 6\cdot 31375\\ 6\cdot 30189\\ 6\cdot 29007\\ 6\cdot 27829\\ 6\cdot 26655\end{array}$	60 59 58 57 56
5 6 7 8 9	·14061 ·14090 ·14119 ·14148 ·14177	.99006 .99002 .98998 .98994 .98990	.14202 .14232 .14262 .14291 .14321	$\begin{array}{r} 7.04105 \\ 7.02637 \\ 7.01174 \\ 6.99718 \\ 6.98268 \end{array}$	•15787 •15816 •15845 •15873 •15902	.98746 .98741 .98737 .98732 .98728	•15988 •16017 •16047 •16077 •16107	6.25488 6.24321 6.23160 6.22003 6.20851	55 54 53 52 51
10 11 12 13 14	.14205 .14234 .14263 .14292 .14320	•98986 •98982 •98978 •98973 •98969	.14351 .14381 .14410 .14440 .14470	$\begin{array}{c} 6.96823\\ 6.95385\\ 6.93952\\ 6.92525\\ 6.91104 \end{array}$	.15931 .15959 .15988 .16017 .16046	·98723 ·98718 ·98714 ·98709 ·98704	.16137     .16167     .16196     .16226     .16256     .16256	6.19703 6.18559 6.17419 6.16283 6.15151	50 49 48 47 46
15 16 17 18 19	.14349     .14378     .14407     .14436     .14464	.98965 .98961 .98957 .98953 .98948	$     \begin{array}{r}         & \cdot 14499 \\         & \cdot 14529 \\         & \cdot 14559 \\         & \cdot 14588 \\         & \cdot 14618 \\     \end{array} $	6 · 89688 6 · 88278 6 · 86874 6 · 85475 6 · 84082	$     .16074 \\     .16103 \\     .16132 \\     .16160 \\     .16189 $	.98700 .98695 .98690 .98686 .98681	.16286 .16316 .16346 .16376 .16405	6.14023 6.12899 6.11779 6.10664 6.09552	45 44 43 42 41
20 21 22 23 24	·14493 ·14522 ·14551 ·14580 ·14608	.98944 .98940 .98936 .98931 .98927	.14648 .14678 .14707 .14737 .14767	6.82694 6.81312 6.79936 6.78564 6.77199	.16218 .16246 .16275 .16304 .16333	.98676 .98671 .98667 .98662 .98657	.16435   .16465   .16495   .16525   .16555	$\begin{array}{r} 6.08444\\ 6.07340\\ 6.06240\\ 6.05143\\ 6.04051 \end{array}$	40 39 38 37 36
25 26 27 28 29	.14637     .14666     .14695     .14723     .14752	·98923 ·98919 ·98914 ·98910 ·98906	.14796 .14826 .14856 .14886 .14915	6.75838 6.74483 6.73133 6.71789 6.70450	.16361 .16390 .16419 .16447 .16476	.98652 .98648 .98643 .98638 .98633	.16585     .16615     .16645     .16674     .16704	6.02962 6.01878 6.00797 5.99720 5.98646	35 34 33 32 31
30 31 32 33 34	.14781 .14810 .14838 .14867 .14896	.98902 .98897 .98893 .98889 .98889 .98884	.14945 .14975 .15005 .15034 .15064	6.69116 6.67787 6.66463 6.65144 6.63831	.16505 .16533 .16562 .16591 .16620	.98629 .98624 .98619 .98614 .98609	$     \begin{array}{r}         & \cdot 16734 \\         & \cdot 16764 \\         & \cdot 16794 \\         & \cdot 16824 \\         & \cdot 16854 \\     \end{array} $	5.97576 5.96510 5.95448 5.94390 5.93335	30 29 28 27 26
35 36 37 38 39	.14925 .14954 .14982 .15011 .15040	·98880 ·98876 ·98871 ·98867 ·98863	.15094 .15124 .15153 .15183 .15213	6.62523 6.61219 6.59921 6.58627 6.57339	.16648     .16677     .16706     .16734     .16763	•98604 •98600 •98595 •98590 •98585	.16884     .16914     .16944     .16974     .16974     .17004	5.92283 5.91236 5.90191 5.89151 5.88114	25 24 23 22 21
40 41 42 43 44	.15069 .15097 .15126 .15155 .15184	·98858 ·98854 ·98849 ·98845 ·98841	·15243 ·15272 ·15302 ·15332 ·15362	6.56055 6.54777 6.53503 6.52234 6.50970	.16792 .16820 .16849 .16878 .16906	•98580 •98575 •98570 •98565 •98561	.17033 .17063 .17093 .17123 .17153	5.87080 5.86051 5.85024 5.84001 5.82982	20 19 18 17 16
45 46 47 48 49	.15212 .15241 .15270 .15299 .15327	·98836 ·98832 ·98827 ·98823 ·98818	.15391 .15421 .15451 .15481 .15511	6.49710 6.48456 6.47206 6.45961 6.44720	·16935 ·16964 ·16992 ·17021 ·17050	.98556 .98551 .98540 .98541 .98536	.17183 .17213 .17243 .17273 .17203	5.81966 5.80953 5.79944 5.78938 5.77936	15 14 13 12 11
50 51 52 53 54	.15356 .15385 .15414 .15442 .15471	.98814 .98809 .98805 .98800 .98796	.15540 .15570 .15600 .15630 .15660	$\begin{array}{r} 6.43484 \\ 6.42253 \\ 6.41026 \\ 6.39804 \\ 6.38587 \end{array}$	·17078 ·17107 ·17136 ·17164 ·17193	.98531 .98526 .98521 .98516 .98511	.17333 .17363 .17393 .17423 .17453	$\begin{array}{r} 5.76937\\ 5.75941\\ 5.74949\\ 5.73960\\ 5.72974\end{array}$	10 9 8 7 6
55 56 57 58 59	.15500     .15529     .15557     .15586     .15615	.98791 .98787 .98782 .98778 .98778	.15689     .15719     .15749     .15779     .15779     .15809	$     \begin{array}{r}       6 \cdot 37374 \\       6 \cdot 36165 \\       6 \cdot 34961 \\       6 \cdot 33761 \\       6 \cdot 32566 \\     \end{array} $	.17222 .17250 .17279 .17308 .17336	.98506 .98501 .98496 .98491 .98486	.17483 .17513 .17543 .17573 .17603	$\begin{array}{c} 5.71992\\ 5.71013\\ 5.70037\\ 5.69064\\ 5.68094 \end{array}$	5 4 3 2 1
<u>60</u>	<u>·15643</u> Cos.	<u>.98769</u> Sin.	.15838 Cot.	6.31375 Tan.	• 17365 Cos.	<u>.98481</u> Sin.	<u>. 17633</u> Cot.	<u>5.67128</u> Tan.	<del>,0</del>
<u> </u>			1°	69		<u> </u>	09		

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TABLE IX.—NATURAL SINES	. COSINES.	TANGENTS.	AND	COTANGENTS.

1       1.77898       .98476       1.77663       5.66165       .19138       .98152       .19498       5.12862         3       1.7451       .98466       .17723       5.66236       .19138       .98152       .19595       .512069         4       .17479       .98446       .17783       5.662364       .19254       .98140       .19559       5.11279         5       .17563       .98455       .17783       5.662364       .19224       .98135       .19589       5.08704         7       .17564       .98445       .17873       5.56713       .19328       .98112       .19710       5.07360         9       .17621       .984450       .17873       5.56773       .19328       .98101       .19770       5.06809         12       .17766       .98449       .18053       5.56777       .19423       .98094       .18813       5.04267         14       .17764       .98449       .18053       5.56777       .19423       .98074       .19821       5.01371         13       .17774       .98444       .18063       5.56777       .19423       .98074       .19821       5.01201         14       .17764       .98449       .18053       <		LE 1A	-NAI01 1	.0°	115,00511			.1°	OTANGE	
1       1.77898       .98476       1.77663       5.66165       .19138       .98152       .19498       5.12862         3       1.7451       .98466       .17723       5.66236       .19136       .98152       .19595       .512069         4       .17479       .98446       .17783       5.662365       .19155       .98140       .19559       5.11279         5       .17568       .98445       .17813       5.61397       .19252       .98122       .19648       5.08704         7       .17565       .98445       .17873       5.56731       .19338       .9122       .19649       5.08736         9       .17624       .98440       .17873       5.567838       .19366       .98101       .19770       5.06809         10       .17661       .98420       .17993       5.56777       .19423       .98096       .19831       5.06376         13       .17774       .98444       .18063       5.56307       .19431       .98074       .19831       5.04267         14       .17764       .98499       .18055       5.55277       .19423       .98076       .19821       5.01201         13       .17774       .98494       .18055 <td< th=""><th>1</th><th>Sin.</th><th>Cos.</th><th>Tan.</th><th>Cot.</th><th>Sin.</th><th>Cos.</th><th>Tan.</th><th>Cot.</th><th></th></td<>	1	Sin.	Cos.	Tan.	Cot.	Sin.	Cos.	Tan.	Cot.	
6         .17537         .98450         .17813         5.61397         .19252         .98129         .19619         5.09704           7         .17564         .88446         .17873         5.59511         .19839         .98118         .19640         5.08921           9         .17651         .98436         .17933         5.58573         .19338         .98112         .19710         5.06584           10         .17660         .98420         .17933         5.56706         .19335         .98101         .19770         5.06584           12         .17708         .98420         .17933         5.56777         .19432         .98090         .19801         5.06507           13         .17737         .98404         .18083         5.5007         .19481         .98034         .19861         5.02734           16         .17782         .98389         .18113         5.50264         .19650         .98077         .19825         5.01210           18         .17860         .98378         .18233         5.44851         .19652         .98050         .20012         4.98940           21         .17905         .98376         .18233         5.44851         .19652         .98050 <t< td=""><td></td><td>.17393 .17422 .17451</td><td>.98476 .98471 .98466</td><td>17663</td><td>5.66165 5.65205 5.64248</td><td>·19109 ·19138 ·19167</td><td>.98157 .98152 .98146</td><td>·19468 ·19498 ·19529</td><td><math>5.13658 \\ 5.12862 \\ 5.12069</math></td><td>60 59 58 57 56</td></t<>		.17393 .17422 .17451	.98476 .98471 .98466	17663	5.66165 5.65205 5.64248	·19109 ·19138 ·19167	.98157 .98152 .98146	·19468 ·19498 ·19529	$5.13658 \\ 5.12862 \\ 5.12069$	60 59 58 57 56
11       .17680       .98425       .17963       5       .56706       .19353       .98101       .19770       5       .56087         12       .17787       .98414       .18023       5       .53927       .19431       .98094       .18811       5       .05087         14       .17766       .98404       .18063       5       .53927       .19431       .98084       .19861       5       .03499         15       .17794       .98404       .18063       5       .53027       .19431       .98073       .19861       5       .03499         16       .17823       .98399       .18113       5       .52007       .19858       .98073       .19921       5       .01710         17       .17852       .98389       .18173       5       .50264       .1955       .98061       .20012       4.98945       .01411         20       .17987       .98378       .18233       5.44841       .19652       .89016       .20013       4.97438         23       .18023       .98347       .18335       5.44857       .19767       .98033       .20134       4.96694         24       .18052       .98357       .18345       .43077	5 6 7 8 9	.17537 .17565 .17594	•98450 •98445 •98440	.17813 .17843 .17873	5.61397 5.60452 5.59511	·19252 ·19281 ·19309	·98129 ·98124 ·98118	.19619 .19649 .19680	5.09704 5.08921 5.08139	55 54 53 52 51
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$11 \\ 12 \\ 13$	.17680 .17708 .17737	.98425 .98420 .98414	.17963 .17993 .18023	$5.56706 \\ 5.65777 \\ 5.54851$	.19395 .19423 .19452	·98101 ·98096 ·98090	.19770 .19801 .19831	$5.05809 \\ 5.05037 \\ 5.04267$	50 49 48 47 46
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	16 17 18	·17823 ·17852 ·17880	.98399 .98394 .98389	.18113 .18143 .18173	$5.52090 \\ 5.51176 \\ 5.50264$	·19538 ·19566 ·19595	·98073 ·98067 ·98061	.19921 .19952 .19982	5.01971 5.01210 5.00451	45 44 43 42 41
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	20 21 22 23	.17966 .17995 .18023	.98373 .98368 .98362	·18263 ·18293 ·18323	5.48451 5.47548 5.46648 5.45751	·19680 ·19709 ·19737	.98044 .98039 .98033	·20073 ·20103 ·20133	4.98188 4.97438 4.96690	40 39 38 37 36
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	) 25 26 27 28	.18109 .18138 .18166	.98347 .98341 .98336	.18414 .18444 .18474	5.43077 5.42192 5.41309	·19823 ·19851 ·19880	.98016 .98010 .98004	·20224 ·20254 ·20285	$4.94460 \\ 4.93721 \\ 4.92984$	35 34 33 32 31
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	81 32 33	.18252 .18281 .18309	.98320 .98315 .98310	.18564 .18594 .18624	5.38677 5.37805 5.36936	·19965 ·19994 ·20022	.97987 .97981 .97975	·20376 ·20406 ·20436	$4.90785 \\ 4.90056 \\ 4.89330$	30 29 28 27 26
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	36 37 38	·18395 ·18424 ·18452	·98294 ·98288 ·98283	.18714 .18745 .18775	5.34345 5.33487 5.32631	·20108 ·20136 ·20165	·97958 ·97952 ·97946	·20527 ·20557 ·20588	4.86444 4.85727	25 24 23 22 21
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	41 42 43	·18538 ·18567 ·18595	·98267 ·98261 ·98256	.18865 .18895 .18925	5.30080 5.29235 5.28393	·20250 ·20279 ·20307	.97928 .97922 .97916	·20679 ·20709 ·20739	$4.83590 \\ 4.82882 \\ 4.82175$	20 19 18 17 16
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	46 47 48	.18681 .18710 .18738	·98240 ·98234 ·98229	.19016 .19046 .19076	5.25880 5.25048 5.24218	20393 20421 20450	·97899 ·97893 ·97887	·20830 ·20861 ·20891 ·20921	$\begin{array}{r} 4.80068\\ 4.79370.\\ 4.78673\\ 4.77978\end{array}$	15 14 13 12 11
EF 10000 100100 10007 F 10400 100040 107045 01104 14 72951	51 52 53 54	·18824 ·18852 ·18881	·98212 ·98207 ·98201	·19166 ·19197 ·19227	$\begin{array}{r} 5\cdot 21744\\ 5\cdot 20925\\ 5\cdot 20107\\ 5\cdot 19293\end{array}$	·20535 ·20563 ·20592 ·20620	·97869 ·97863 ·97857 ·97851	·20982 ·21013 ·21043 ·21073	$\begin{array}{r} 4.76595 \\ 4.75906 \\ 4.75219 \\ 4.74534 \end{array}$	10 9 8 7 6
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	57 58 59	·18995 ·19024 ·19052	.98179 .98174 .98168	·19347 ·19378 ·19408	5.16863 5.16058 5.15256	·20706 ·20734 ·20763	·97833 ·97827 ·97821	21164 21195 21225	4.71137	876 54321
$\underbrace{\begin{array}{c} 60 \\ \hline \\ $	<u>60</u>			distant strength and the strength of the stren	Tan.	Cos.	Sin.	Cot.		-0

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ė	Sin.	Cos.	Tan.	Cot.	Sin	Cos.	Tan.	Cot.	'
01234	·20791 ·20820 ·20848 ·20877 ·20905	.97815 .97809 .97803 .97797 .97791	·21256 ·21286 ·21316 ·21347 ·21377	$\begin{array}{r} 4.70463 \\ 4.69791 \\ 4.69121 \\ 4.68452 \\ 4.67786 \end{array}$	·22495 ·22523 ·22552 ·22552 ·22580 ·22608	·97437 ·97430 ·97424 ·97417 ·97411	·23087 ·23117 ·23148 ·23179 ·23209	$\begin{array}{r} 4 \cdot 33148 \\ 4 \cdot 32573 \\ 4 \cdot 32001 \\ 4 \cdot 31430 \\ 4 \cdot 30860 \end{array}$	60 59 58 57 56
56789	·20933 ·20962 ·20990 ·21019 ·21047	.97784 .97778 .97772 .97766 .97760	21408 21438 21469 21499 21529	$\begin{array}{r} 4.67121 \\ 4.66458 \\ 4.65797 \\ 4.65138 \\ 4.64480 \end{array}$	·22637 ·22665 ·22693 ·22722 ·22750	·97404 ·97398 ·97391 ·97384 ·97378	·23240 ·23271 ·23301 ·23332 ·23363	$\begin{array}{r} 4\cdot 30291 \\ 4\cdot 29724 \\ 4\cdot 29159 \\ 4\cdot 28595 \\ 4\cdot 28032 \end{array}$	55 54 53 52 51
10 11 12 13 14	·21076 ·21104 ·21132 ·21161 ·21189	.97754 .97748 .97742 .97735 .97729	.21560 .21590 .21621 .21651 .21682	$\begin{array}{r} 4\cdot 63825\\ 4\cdot 63171\\ 4\cdot 62518\\ 4\cdot 61868\\ 4\cdot 61219\end{array}$	·22778 ·22807 ·22835 ·22863 ·22892	.97371 .97365 .97358 .97351 .97345	·23393 ·23424 ·23455 ·23485 ·23516	$\begin{array}{r} 4 \cdot 27471 \\ 4 \cdot 26911 \\ 4 \cdot 26352 \\ 4 \cdot 25795 \\ 4 \cdot 25239 \end{array}$	50 49 48 47 46
15 16 17 18 19	·21218 ·21246 ·21275 ·21303 ·21331	.97723 .97717 .97711 .97705 .97698	.21712 .21743 .21773 .21804 .21834	$\begin{array}{r} 4 \cdot 60572 \\ 4 \cdot 59927 \\ 4 \cdot 59283 \\ 4 \cdot 58641 \\ 4 \cdot 58001 \end{array}$	·22920 ·22948 ·22977 ·23005 ·23033	·97338 ·97331 ·97325 ·97318 ·97311	·23547 ·23578 ·23608 ·23639 ·23670	$\begin{array}{r} 4 \cdot 24685 \\ 4 \cdot 24132 \\ 4 \cdot 23580 \\ 4 \cdot 23030 \\ 4 \cdot 22481 \end{array}$	45 44 43 42 41
20 21 22 23 24	21360 21388 21417 21445 21474	.97692 .97686 .97680 .97673 .97667	·21864 ·21895 ·21925 ·21956 ·21986	$\begin{array}{r} 4 \cdot 57363 \\ 4 \cdot 56726 \\ 4 \cdot 56091 \\ 4 \cdot 55458 \\ 4 \cdot 54826 \end{array}$	$ \begin{array}{r} \cdot 23062 \\ \cdot 23090 \\ \cdot 23118 \\ \cdot 23146 \\ \cdot 23175 \\ \end{array} $	·97304 ·97298 ·97291 ·97284 ·97278	·23700 ·23731 ·23762 ·23793 ·23823	$\begin{array}{r} 4 \cdot 21933 \\ 4 \cdot 21387 \\ 4 \cdot 20842 \\ 4 \cdot 20298 \\ 4 \cdot 19756 \end{array}$	40 39 38 37 36
25 26 27 28 29	.21502 .21530 .21559 .21587 .21616	.97661 .97655 .97648 .97642 .97636	·22017 ·22047 ·22078 ·22108 ·22139	$\begin{array}{r} 4.54196\\ 4.53568\\ 4.52941\\ 4.52316\\ 4.51693\end{array}$	·23203 ·23231 ·23260 ·23288 ·23316	.97271 .97264 .97257 .97251 .97244	·23854 ·23885 ·23916 ·23946 ·23977	$\begin{array}{r} 4.19215\\ 4.18675\\ 4.18137\\ 4.17600\\ 4.17064\end{array}$	35 34 33 32 31
30 31 32 33 34	·21644 ·21672 ·21701 ·21729 ·21758	.97630 .97623 .97617 .97611 .97604	·22169 ·22200 ·22231 ·22261 ·22292	$\begin{array}{r} 4.51071 \\ 4.50451 \\ 4.49832 \\ 4.49215 \\ 4.48600 \end{array}$	·23345 ·23373 ·23401 ·23429 ·23458	·97237 ·97230 ·97223 ·97217 ·97210	24008 24039 24069 24100 24131	$\begin{array}{r} 4 \cdot 16530 \\ 4 \cdot 15997 \\ 4 \cdot 15465 \\ 4 \cdot 14934 \\ 4 \cdot 14405 \end{array}$	30 29 28 27 26
35 36 37 38 39	·21786 ·21814 ·21843 ·21871 ·21899	.97598 .97592 .97585 .97579 .97573	22322 22353 22383 22414 22444	$\begin{array}{r} 4.47986\\ 4.47374\\ 4.46764\\ 4.46155\\ 4.45548\end{array}$	$23486 \\ \cdot 23514 \\ \cdot 23542 \\ \cdot 23571 \\ \cdot 23599$	.97203 .97196 .97189 .97182 .97176	$ \begin{array}{r} \cdot 24162 \\ \cdot 24193 \\ \cdot 24223 \\ \cdot 24254 \\ \cdot 24285 \\ \end{array} $	$\begin{array}{r} 4\cdot13877\\ 4\cdot13350\\ 4\cdot12825\\ 4\cdot12301\\ 4\cdot11778\end{array}$	25 24 23 22 21
40 41 42 43 44	·21928 ·21956 ·21985 ·22013 ·22041	.97566 .97560 .97553 .97547 .97541	·22475 ·22505 ·22536 ·22567 ·22597	$\begin{array}{r} 4 \cdot 44942 \\ 4 \cdot 44338 \\ 4 \cdot 43735 \\ 4 \cdot 43134 \\ 4 \cdot 42534 \end{array}$	·23627 ·23656 ·23684 ·23712 ·23740	.97169 .97162 .97155 .97148 .97141	$ \begin{array}{r} \cdot 24316 \\ \cdot 24347 \\ \cdot 24377 \\ \cdot 24408 \\ \cdot 24439 \\ \end{array} $	$\begin{array}{r} 4\cdot 11256\\ 4\cdot 10736\\ 4\cdot 10216\\ 4\cdot 09699\\ 4\cdot 09182\end{array}$	20 19 18 17 16
45 46 47 48 49	·22070 ·22098 ·22126 ·22155 ·22183	.97534 .97528 .97521 .97515 .97508	·22628 ·22658 ·22689 ·22719 ·22750	$\begin{array}{r} 4 \cdot 41936 \\ 4 \cdot 41340 \\ 4 \cdot 40745 \\ 4 \cdot 40152 \\ 4 \cdot 39560 \end{array}$	·23769 ·23797 ·23825 ·23853 ·23882	.97134 .97127 .97120 .97113 .97106	24470 24501 24532 24562 24593	$\begin{array}{r} 4.08666\\ -4.08152\\ 4.07639\\ 4.07127\\ -4.06616\end{array}$	$15 \\ 14 \\ 13 \\ 12 \\ 11$
50 51 52 53 54	·22212 ·22240 ·22268 ·22297 ·22325	.97502 .97496 .97489 .97483 .97476	· 22781 · 22811 · 22842 · 22872 · 22908	$\begin{array}{r} 4\cdot 38969\\ 4\cdot 38381\\ 4\cdot 37793\\ 4\cdot 37207\\ 4\cdot 36623\end{array}$	·23910 ·23938 ·23968 ·23995 ·24023	.97100 .97093 .97086 .97079 .97072	·24624 ·24655 ·24686 ·24717 ·24747	$\begin{array}{r} 4.06107\\ 4.05599\\ 4.05092\\ 4.04586\\ 4.04081 \end{array}$	10 9 8 7 6
55 56 57 58 59	·22353 ·22382 ·22410 ·22438 ·22467	•97470 •97463 •97457 •97450 •97444	·22934 ·22964 ·22995 ·23026 ·23056	$\begin{array}{r} 4.36040 \\ 4.35459 \\ 4.34879 \\ 4.34300 \\ 4.33723 \end{array}$	$\begin{array}{r} \cdot 24051 \\ \cdot 24079 \\ \cdot 24108 \\ \cdot 24136 \\ \cdot 24164 \end{array}$	.97065 .97058 .97051 .97044 .97037	·24778 ·24809 ·24840 ·24871 ·24902	$\begin{array}{r} 4\cdot03578\\ 4\cdot03076\\ 4\cdot02574\\ 4\cdot02074\\ 4\cdot01576\end{array}$	5 4 3 2 1
<u>60</u>	· 22495 Cos.	<u>.97437</u> Sin.	<u>· 23087</u> Cot.	<u>4.33148</u> Tan.	<u>· 24192</u> Cos.	<u>.97030</u> Sin.	<u>·24933</u> Cot.	<u>4.01078</u> Tan.	$\frac{-0}{-}$
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TABLE IX.-NATURAL SINES, COSINES, TANGENTS, AND COTANGENTS, T

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'	Sin.	Cos.	Tan.	Cot.	Sin.	Cos.	Tan.	Cot.	1
0	·24192	·97030	·24933	$\begin{array}{r} 4\cdot01078\\ 4\cdot00582\\ 4\cdot00086\\ 3\cdot99592\\ 3\cdot99099\end{array}$	·25882	·96593	·26795	3.73205	60
1	·24220	·97023	·24964		·25910	·96585	·26826	3.72771	59
2	·24249	·97015	·24995		·25938	·96578	·26857	3.72338	58
3	·24277	·97008	·25026		·25966	·96570	·26888	3.71907	57
4	·24305	·97001	·25056		·25994	·96562	·26920	3.71476	56
5	·24333	.96994	·25087	3.98607	·26022	·96555	·26951	3.71046	55
6	·24362	.96987	·25118	3.98117	·26050	·96547	·26982	3.70616	54
7	·24390	.96980	·25149	3.97627	·26079	·96540	·27013	3.70188	53
8	·24418	.96973	·25180	3.97139	·26107	·96532	·27044	3.69761	52
9	·24446	.96966	·25211	3.96651	·26135	·96524	·27076	3.69335	51
10	24474	.96959	·25242	3.96165	$ \begin{array}{r} \cdot 26163 \\ \cdot 26191 \\ \cdot 26219 \\ \cdot 26247 \\ \cdot 26275 \\ \end{array} $	.96517	·27107	3.68909	50
11	24503	.96952	·25273	3.95680		.96509	·27138	3.68485	49
12	24531	.96945	·25304	3.95196		.96502	·27169	3.68061	48
13	24559	.96937	·25335	3.94713		.96494	·27201	3.67638	47
14	24587	.96930	·25366	3.94232		.96486	·27232	3.67217	46
15	·24615	·96923	·25397	3.93751	·26303	·96479	·27263	3.66796	45
16	·24644	·96916	·25428	3.93271	·26331	·96471	·27294	3.66376	44
17	·24672	·96909	·25459	3.92793	·26359	·96463	·27326	3.65957	43
18	·24700	·96902	·25490	3.92316	·26387	·96456	·27357	3.65538	42
19	·24728	·96894	·25521	3.91839	·26415	·96448	·27388	3.65121	41
20	·24756	·96887	$     \begin{array}{r}             25552 \\             25583 \\             25614 \\             25645 \\             25676 \\         \end{array}     $	3.91364	·26443	.96440	·27419	$3 \cdot 64705$	40
21	·24784	·96880		3.90890	·26471	.96433	·27451	$3 \cdot 64289$	39
22	·24813	·96873		3.90417	·26500	.96425	·27482	$3 \cdot 63874$	38
23	·24841	·96866		3.89945	·26528	.96417	·27513	$3 \cdot 63461$	37
24	·24869	·96858		3.89474	·26556	.96410	·27545	$3 \cdot 63048$	36
25	·24897	·96851	·25707	3.89004	·26584	·96402	·27576	3.62636	35
26	·24925	·96844	·25738	3.88536	·26612	·96394	·27607	3.62224	34
27	·24954	·96837	·25769	3.88068	·26640	·96386	·27638	3.61814	33
28	·24982	·96829	·25800	3.87601	·26668	·96379	·27670	3.61405	32
29	·25010	·96822	·25831	3.87136	·26696	·96371	·27701	3.60996	31
30	·25038	·96815	·25862	$3 \cdot 86671$	· 26724	·96363	·27732	3.60588	30
31	·25066	·96807	·25893	$3 \cdot 86208$	· 26752	·96355	·27764	3.60181	29
32	·25094	·96800	·25924	$3 \cdot 85745$	· 26780	·96347	·27795	3.59775	28
33	·25122	·96793	·25955	$3 \cdot 85284$	· 26808	·96340	·27826	3.59370	27
34	·25151	·96786	·25986	$3 \cdot 84824$	· 26836	·96332	·27858	3.58966	26
35	·25179	·96778	·26017	3 · 84364	·26864	·96324	·27889	$3 \cdot 58562$	25
36	·25207	·96771	·26048	3 · 83906	·26892	·96316	·27921	$3 \cdot 58160$	24
37	·25235	·96764	·26079	3 · 83449	·26920	·96308	·27952	$3 \cdot 57758$	23
38	·25263	·96756	·26110	3 · 82992	·26948	·96301	·27983	$3 \cdot 57357$	22
39	·25291	·96749	·26141	3 · 82537	·26976	·96293	·28015	$3 \cdot 56957$	21
40	·25320	·96742	·26172	3.82083	·27004	·96285	·28046	$3 \cdot 56557$	20
41	·25348	·96734	·26203	3.81630	·27032	·96277	·28077	$3 \cdot 56159$	19
42	·25376	·96727	·26235	3.81177	·27060	·96269	·28109	$3 \cdot 55761$	18
43	·25404	·96719	·26266	3.80726	·27088	·96261	·28140	$3 \cdot 55364$	17
44	·25432	·96712	·26297	3.80276	·27116	·96253	·28172	$3 \cdot 54968$	16
45	·25460	·96705	·26328	3.79827	·27144	96246	· 28203	3.54573	15
46	·25488	·96697	·26359	3.79378	·27172	96238	· 28234	3.54179	14
47	·25516	·96690	·26390	3.78931	·27200	96230	· 28266	3.53785	13
48	·25545	·96682	·26421	3.78485	·27228	96222	· 28297	3.53393	12
49	·25573	·96675	·26452	3.78040	·27256	96214	· 28329	3.53001	11
50 51 52 53 54	25601 25629 25657 25685 25685	·96687 ·96660 ·96653 ·96645 ·96638	·26483 ·26515 ·26546 ·26577 ·26608	3.77595 3.77152 3.76709 3.76268 3.75828	·27284 ·27312 ·27340 ·27368 ·27396	·96206 ·96198 ·96190 ·96182 ·96174	·28360 ·28391 ·28423 ·28454 ·28454 ·28486	3.52609 3.52219 3.51829 3.51441 3.51053	10 9 8 7 6
55	·25741	·96630	·26639	3.75388	·27424	.96166	·28517	3.50666	54321
56	·25769	·96623	·26670	3.74950	·27452	.96158	·28549	3.50279	
57	·25798	·96615	·26701	3.74512	·27480	.96150	·28580	3.49894	
58	·25826	·96608	·26733	3.74075	·27508	.96142	·28612	3.49509	
59	·25854	·96600	·26764	3.73640	·27536	.96134	·28643	3.49125	
<u>60</u>	<u>· 25882</u>	<u>.96593</u>	<u>· 26795</u>	<u>3.73205</u>	<u>· 27564</u>	<u>•96126</u>	<u>· 28675</u>	<u>3.48741</u>	
/	Cos.	Sin.	Cot.	Tan.	Cos.	Sin.	Cot.	Tan.	
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1	Sin.	Cos.	Tan.	Cot.	Sin.	Cos.	Tan.	Cot.	<u></u>
01234	·27564	.96126	·28675	3.48741	·29237	.95630	· 30573	$3 \cdot 27085$	60
	·27592	.96118	·28706	3.48359	·29265	.95622	· 30605	$3 \cdot 26745$	59
	·27620	.96110	·28738	3.47977	·29293	.95613	· 30637	$3 \cdot 26406$	58
	·27648	.96102	·28769	3.47596	·29321	.95605	· 30669	$3 \cdot 26067$	57
	·27676	.96094	·28800	3.47216	·29348	.95596	· 30700	$3 \cdot 25729$	56
56789	·27704	.96086	·28832	3.46837	·29376	.95588	·30732	$3 \cdot 25392$	55
	·27731	.96078	·28864	3.46458	·29404	.95579	·30764	$3 \cdot 25055$	54
	·27759	.96070	·28895	3.46080	·29432	.95571	·30796	$3 \cdot 24719$	53
	·27787	.96062	·28927	3.45703	·29460	.95562	·30828	$3 \cdot 24383$	52
	·27815	.96054	·28958	3.45327	·29487	.95554	·30860	$3 \cdot 24049$	51
10	·27843	.96046	·28990	3.44951	·29515	.95545	.30891	$3 \cdot 23714$	$50 \\ 49 \\ 48 \\ 47 \\ 46$
11	·27871	.96037	·29021	3.44576	·29543	.95536	.30923	$3 \cdot 23381$	
12	·27899	.96029	·29053	3.44202	·29571	.95528	.30955	$3 \cdot 23048$	
13	·27927	.96021	·29084	3.43829	·29599	.95519	.30987	$3 \cdot 22715$	
14	·27955	.96013	·29116	3.43456	·29626	.95511	.31019	$3 \cdot 22384$	
15	·27983	.96005	.29147	3.43084	·29654	.95502	.31051	$\begin{array}{r} 3 \cdot 22053 \\ 3 \cdot 21722 \\ 3 \cdot 21392 \\ 3 \cdot 21063 \\ 3 \cdot 20734 \end{array}$	45
16	·28011	.95997	.29179	3.42713	·29682	.95493	.31083		44
17	·28039	.95989	.29210	3.42343	·29710	.95485	.31115		43
18	·28067	.95981	.29242	3.41973	·29737	.95476	.31147		42
19	·28095	.95972	.29274	3.41604	·29765	.95467	.31178		41
20	·28123	.95964	·29305	3.41236	·29793	.95459	.31210	$3 \cdot 20406$	40
21	·28150	.95956	·29337	3.40869	·29821	.95450	.31242	$3 \cdot 20079$	39
22	·28178	.95948	·29368	3.40502	·29849	.95441	.31274	$3 \cdot 19752$	38
23	·28206	.95940	·29400	3.40136	·29876	.95433	.31306	$3 \cdot 19426$	37
24	·28234	.95931	·29432	3.39771	·29904	.95424	.31338	$3 \cdot 19100$	36
25	·28262	.95923	·29463	3.39406	·29932	.95415	.31370	3.18775	35
26	·28290	.95915	·29495	3.39042	·29960	.95407	.31402	3.18451	34
27	·28318	.95907	·29526	3.38679	·29987	.95398	.31434	3.18127	33
28	·28346	.95898	·29558	3.38317	·30015	.95389	.31466	3.17804	32
29	·28374	.95890	·29590	3.37955	·30043	.95380	.31498	3.17481	31
30	·28402	.95882	.29621	3.37594	.30071	.95372	.31530	3.17159	30
31	·28429	.95874	.29653	3.37234	.30098	.95363	.31562	3.16838	29
32	·28457	.95865	.29685	3.36875	.30126	.95354	.31594	3.16517	28
33	·28485	.95857	.29716	3.36516	.30154	.95345	.31626	3.16197	27
34	·28513	.95849	.29748	3.36158	.30182	.95337	.31658	3.15877	26
35	28541	.95841	.29780	3.35800	.30209	.95328	.31690	3.15558	25
36	28569	.95832	.29811	3.35443	.30237	.95319	.31722	3.15240	24
37	28597	.95824	.29843	3.35087	.30265	.95310	.31754	3.14922	23
38	28625	.95816	.29875	3.34732	.30292	.95301	.31786	3.14605	22
39	28652	.95807	.29906	3.34377	.30320	.95293	.31818	3.14288	21
40	·28680	.95799	29938	3.34023	·30348	.95284	.31850	$3 \cdot 13972$	20
41	·28708	.95791	29970	3.33670	·30376	.95275	.31882	$3 \cdot 13656$	19
42	·28736	.95782	30001	3.33317	·30403	.95266	.31914	$3 \cdot 13341$	18
43	·28764	.95774	30033	3.32965	·30431	.95257	.31946	$3 \cdot 13027$	17
44	·28792	.95766	30065	3.32614	·30459	.95248	.31978	$3 \cdot 12713$	16
45	·28820	.95757	·30097	3.32264	·30486	·95240	.32010	3.12400	15
46	·28847	.95749	·30128	3.31914	·30514	·95231	.32042	3.12087	14
47	·28875	.95740	·30160	3.31565	·30542	·95222	.32074	3.11775	13
48	·28903	.95732	·30192	3.31216	·30570	·95213	.32106	3.11464	12
49	·28931	.95724	·30224	3.30868	·30597	·95204	.32139	3.11153	11
50	·28959	.95715	·30255	3.30521	·30625	.95195	.32171	3.10842	10
51	·28987	.95707	·30287	3.30174	·30653	.95186	.32203	3.10532	9
52	·29015	.95698	·30319	3.29829	·30680	.95177	.32235	3.10223	8
53	·29042	.95690	·30351	3.29483	·30708	.95168	.32267	3.09914	7
54	·29070	.95681	·30382	3.29139	·30736	.95159	.32299	3.09606	6
55	·29098	·95673	·30414	$3 \cdot 28795$	·30763	.95150	.32331	3.09298	5
56	·29126	·95664	·30446	$3 \cdot 28452$	·30791	.95142	.32363	3.08991	4
57	·29154	·95656	·30478	$3 \cdot 28109$	·30819	.95133	.32396	3.08685	3
58	·29182	·95647	·30509	$3 \cdot 27767$	·30846	.95124	.32428	3.08379	2
59	·29209	·95639	·30541	$3 \cdot 27426$	·30874	.95115	.32460	3.08073	1
<u>60</u>	.29237 Cos.	<u>.95630</u> Sin.	<u>·30573</u> Cot.	<u>3.27085</u> Tan.	<u>· 30902</u> Cos.	<u>.95106</u> Sin.	<u>· 32492</u> Cot.	<u>3.07768</u> Tan.	<del>_0</del>
-	- 5150		3°	7(		7			
5.				1	<i>.</i>	17	v		

73°

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19°

	18°				19°				
	Sin.	Cos.	Tan.	Cot.	Sin.	Cos.	Tan.	Cot.	,
0	.30902	.95106	·32492	3.07768	·32557	.94552	$     \begin{array}{r}         & \cdot 34433 \\         & \cdot 34465 \\         & \cdot 34498 \\         & \cdot 34530 \\         & \cdot 34563 \\     \end{array} $	2.90421	60
1	.30929	.95097	·32524	3.07464	·32584	.94542		2.90147	59
2	.30957	.95088	·32556	3.07160	·32612	.94533		2.89873	58
3	.30985	.95079	·32588	3.06857	·32639	.94523		2.89600	57
4	.31012	.95070	·32621	3.06554	·32667	.94514		2.89327	56
5 6 7 8 9	.31040 .31068 .31095 .31123 .31151	.95061 .95052 .95043 .95033 .95024	· 32653 · 32685 · 32717 · 32749 · 32782	3.06252 3.05950 3.05649 3.05349 3.05049 3.05049	· 32694 · 32722 · 32749 · 32777 · 32804	·94504 ·94495 ·94485 ·94476 ·94466	.34596 .34628 .34661 .34693 .34726	2.89055 2.88783 2.88511 2.88240 2.87970	55 54 53 52 51
$10 \\ 11 \\ 12 \\ 13 \\ 14$	.31178	.95015	· 32814	3.04749	· 32832	.94457	.34758	$2 \cdot 87700$	50
	.31206	.95006	· 32846	3.04450	· 32859	.94447	.34791	$2 \cdot 87430$	49
	.31233	.94997	· 32878	3.04152	· 32887	.94438	.34824	$2 \cdot 87161$	48
	.31261	.94988	· 32911	3.03854	· 32914	.94428	.34856	$2 \cdot 86892$	47
	.31289	.94979	· 32943	3.03556	· 32942	.94418	.34889	$2 \cdot 86624$	46
15 16 17 18 19	.31316 .31344 .31372 .31399 .31427	.94970 .94961 .94952 .94943 .94933	.32975 .33007 .33040 .33072 .33104	$3 \cdot 03260$ $3 \cdot 02963$ $3 \cdot 02667$ $3 \cdot 02372$ $3 \cdot 02077$	.32969 .32997 .33024 .33051 .33079	.94409 .94399 .94390 .94380 .94380 .94370	.34922 .34954 .34987 .35020 .35052	2.86356 2.86089 2.85822 2.85555 2.85289	45 44 43 42 41
20	.31454	.94924	·33136	3.01783	.33106	.94361	.35085	$\begin{array}{r} 2 \cdot 85023 \\ 2 \cdot 84758 \\ 2 \cdot 84494 \\ 2 \cdot 84229 \\ 2 \cdot 83965 \end{array}$	40
21	.31482	.94915	·33169	3.01489	.33134	.94351	.35118		39
22	.31510	.94906	·33201	3.01196	.33161	.94342	.35150		38
23	.31537	.94897	·33233	3.00903	.33189	.94332	.35183		37
24	.31565	.94888	·33266	3.00611	.33216	.94322	.35216		36
25	·31593	.94878	·33298	3.00319	.33244	.94313	.35248	$\begin{array}{r} 2 \cdot 83702 \\ 2 \cdot 83439 \\ 2 \cdot 83176 \\ 2 \cdot 82914 \\ 2 \cdot 82653 \end{array}$	35
26	·31620	.94869	·33330	3.00028	.33271	.94303	.35281		34
27	·31648	.94860	·33363	2.99738	.33298	.94293	.35314		33
28	·31675	.94851	·33395	2.99447	.33326	.94284	.35346		32
29	·31703	.94842	·33427	2.99158	.33353	.94274	.35379		31
30	·31730	.94832	.33460	2.98868	·33381	.94264	.35412	2.82391	30
31	·31758	.94823	.33492	2.98580	·33408	.94254	.35445	2.82130	29
32	·31786	.94814	.33524	2.98292	·33436	.94245	.35477	2.81870	28
33	·31813	.94805	.33557	2.98004	·33463	.94235	.35510	2.81610	27
34	·31841	.94795	.33589	2.97717	·33490	.94225	.35543	2.81350	36
35	·31868	•94786	.33621	$2 \cdot 97430$	·33518	.94215	·35576	2.81091	25
36	·31896	•94777	.33654	$2 \cdot 97144$	·33545	.94206	·35608	2.80833	24
37	·31923	•94768	.33686	$2 \cdot 96858$	·33573	.94196	·35641	2.80574	23
38	·31951	•94758	.33718	$2 \cdot 96573$	·33600	.94186	·35674	2.80316	22
39	·31979	•94749	.33751	$2 \cdot 96288$	·33627	.94176	·35707	2.80059	21
40	·32006	.94740	·33783	2.96004	·33655	·94167	.35740	2.79802	20
41	·32034	.94730	·33816	2.95721	·33682	·94157	.35772	2.79545	19
42	·32061	.94721	·33848	2.95437	·33710	·94147	.35805	2.79289	18
43	·32089	.94712	·33881	2.95155	·33737	·94137	.35838	2.79033	17
44	·32116	.94702	·33913	2.94872	·33764	·94127	.35871	2.78778	16
45	.32144	·94693	·33945	2.94591	-33792	·94118	.35904	2.78528	15
46	.32171	·94684	·33978	2.94309	-33819	·94108	.35937	2.78269	14
47	.32199	·94674	·34010	2.94028	-33846	·94098	.35969	2.78014	13
48	.32227	·94665	·34043	2.93748	-33874	·94088	.36002	2.77761	12
49	.32254	·94656	·34075	2.93468	-33901	·94078	.36035	2.77507	11
50	· 32282	·94646	· 34108	2.93189	·33929	·94068	·36068	2.77254	10
51	· 32309	·94637	· 34140	2.92910	·33956	·94058	·36101	2.77002	9
52	· 32337	·94627	· 34173	2.92632	·33983	·94049	·36134	2.76750	8
53	· 32364	·94618	· 34205	2.92354	·34011	·94039	·36167	2.76498	7
54	· 32392	·94609	· 34238	2.92076	·34038	·94029	·36199	2.76247	6
55	.32419	.94599	· 34270	$\begin{array}{r} 2.91799\\ 2.91523\\ 2.91246\\ 2.90971\\ 2.90696\end{array}$	·34065	.94019	-36232	2.75996	5
56	.32447	.94590	· 34303		·34093	.94009	-36265	2.75746	4
57	.32474	.94580	· 34335		·34120	.93999	-36298	2.75496	3
58	.32502	.94571	· 34368		·34147	.93989	-36331	2.75246	2
59	.32529	.94561	· 34400		·34175	.93979	-36364	2.74997	1
<u>60</u>	<u>. 32557</u>	<u>.94552</u>	<u>· 34433</u>	<u>2.90421</u>	<u>.34202</u>	<u>.93969</u>	<u>.36397</u>	<u>2.74748</u>	<u>,</u>
′	Cos.	Sin.	Cot.	Tan.	Cos.	Sin.	Cot.	Tan.	

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			\$U				\$1°		
· _	Sin.	Cos.	Tan.	Cot.	Sin.	Cos.	Tan.	Cot.	1
0 1 2 3 4	·34202 ·34229 ·34257 ·34284 ·34311	.93969 .93959 .93949 .93939 .93929	$     \begin{array}{r}         & \cdot 36397 \\         & \cdot 36430 \\         & \cdot 36463 \\         & \cdot 36496 \\         & \cdot 36529     \end{array} $	$\begin{array}{r} 2.74748\\ 2.74499\\ 2.74251\\ 2.74004\\ 2.73756\end{array}$	·35837 ·35864 ·35891 ·35918 ·35945	·93358 ·93348 ·93337 ·93327 ·93316	-38386 -38420 -38453 -38487 -38520	$\begin{array}{r} 2.60509\\ 2.60283\\ 2.60057\\ 2.59831\\ 2.59606\end{array}$	60 59 58 57 56
5 6 7 8 9	$     \begin{array}{r}         .34339 \\         .34366 \\         .34393 \\         .34421 \\         .34448 \\         .34448     \end{array} $	.93919 .93909 .93899 .93889 .93889 .93879	.36562 .36595 .36628 .36661 .36694	$\begin{array}{r} 2.73509\\ 2.73263\\ 2.73017\\ 2.72771\\ 2.72526\end{array}$	-35973 -36000 -36027 -36054 -36081	.93306 .93295 .93285 .93274 .93264	·38553 ·38587 ·38620 ·38654 ·38687	2.59381 2.59156 2.58932 2.58708 2.58484	55 54 53 52 51
10 11 12 13 14	.34475 .34503 .34530 .34557 .34584	.93869 .93859 .93849 .93839 .93839 .93829	·36727 ·36760 ·36793 ·36826 ·36859	$\begin{array}{r} 2.72281\\ 2.72036\\ 2.71792\\ 2.71548\\ 2.71305 \end{array}$	·36108 ·36135 ·36162 ·36190 ·36217	·93253 ·93243 ·93232 ·93222 ·93211	·38721 ·38754 ·38787 ·38821 ·38854	$\begin{array}{r} 2.58261 \\ 2.58038 \\ 2.57815 \\ 2.57593 \\ 2.57371 \end{array}$	50 49 48 47 46
15 16 17 18 19	.34612 .34639 .34666 .34694 .34721	.93819 .93809 .93799 .93789 .93779	·36892 ·36925 ·36958 ·36991 ·37024	2.71062 2.70819 2.70577 2.70335 2.70094	·36244 ·36271 ·36298 ·36325 ·36352	.93201 .93190 .93180 .93169 .93159	-38888 -38921 -38955 -38988 -39022	$\begin{array}{r} 2.57150\\ 2.56928\\ 2.56707\\ 2.56487\\ 2.56266\end{array}$	45 44 43 42 41
20 21 22 23 24	.34748 .34775 .34803 .34830 .34857	·93769 ·93759 ·93748 ·93738 ·93728	.37057 .37090 .37123 .37157 .37190	$\begin{array}{r} 2.69853\\ 2.69612\\ 2.69371\\ 2.69131\\ 2.68892 \end{array}$	·36379 ·36406 ·36434 ·36461 ·36488	.93148 .93137 .93127 .93116 .93106	.39055 .39089 .39122 .39156 .39190	$\begin{array}{r} 2.56046\\ 2.55827\\ 2.55608\\ 2.55389\\ 2.55170\end{array}$	40 39 38 37 36
25 26 27 28 29	·34884 ·34912 ·34939 ·34966 ·34993	·93718 ·93708 ·93698 ·93688 ·93677	·37223 ·37256 ·37289 ·37322 ·37355	2.68653 2.68414 2.68175 2.67937 2.67700	·36515 ·36542 ·36569 ·36596 ·36623	·93095 ·93084 ·93074 ·93063 ·93052	·39223 39257 ·39290 ·39324 ·39357	$\begin{array}{r} 2.54952 \\ 2.54734 \\ 2.54516 \\ 2.54299 \\ 2.54082 \end{array}$	35 34 33 32 31
30 31 32 33 34	.35021 .35048 .35075 .35102 .35130	•93667 •93657 •93647 •93637 •93626	·37388 ·37422 ·37455 ·37488 ·37521	2.67462 2.67225 2.66989 2.66752 2.66516	·36650 ·36677 ·36704 ·36731 ·36758	•93042 •93031 •93020 •93010 •92999	·39391 ·39425 ·39458 ·39492 ·39526	$\begin{array}{r} 2.53865\\ 2.53648\\ 2.53432\\ 2.53217\\ 2.53001 \end{array}$	30 29 28 27 26
35 36 37 38 39	·35157 ·35184 ·35211 ·35239 ·35266	.93616 .93606 .93596 .93585 .93575	·37554 ·37588 ·37621 ·37654 ·37687	$\begin{array}{r} 2.66281 \\ 2.66046 \\ 2.65811 \\ 2.65576 \\ 2.65342 \end{array}$	·36785 ·36812 ·36839 ·36867 ·36894	·92988 ·92978 ·92967 ·92956 ·92945	·39559 ·39593 ·39626 ·39660 ·39694	$\begin{array}{r} 2.52786\\ 2.52571\\ 2.52357\\ 2.52142\\ 2.51929\end{array}$	25 24 23 22 21
40 41 42 43 44	·35293 ·35320 ·35347 ·35375 ·35402	·93565 ·93555 ·93544 ·93534 ·93524	·37720 ·37754 ·37787 ·37820 ·37853	$\begin{array}{r} 2.65109\\ 2.64875\\ 2.64642\\ 2.64410\\ 2.64177\end{array}$	·36921 ·36948 ·36975 ·37002 ·37029	·92935 ·92924 ·92913 ·92902 ·92892	·39727 ·39761 ·39795 ·39829 ·39862	$\begin{array}{r} 2 \cdot 51715 \\ 2 \cdot 51502 \\ 2 \cdot 51289 \\ 2 \cdot 51076 \\ 2 \cdot 50864 \end{array}$	20 19 18 17 16
45 46 47 48 49	·35429 ·35456 ·35484 ·35511 ·35538	.93514 .93503 .93493 .93483 .93472	·37887 ·37920 ·37953 ·37986 ·38020	2.63945 2.63714 2.63483 2.63252 2.63021	·37056 ·37083 ·37110 ·37137 ·37164	.92881 .92870 .92859 .92849 .92838	·39896 ·39930 ·39963 ·39997 ·40031	$\begin{array}{r} 2 \cdot 50652 \\ 2 \cdot 50440 \\ 2 \cdot 50229 \\ 2 \cdot 50018 \\ 2 \cdot 49807 \end{array}$	$15 \\ 14 \\ 13 \\ 12 \\ 11$
50 51 52 53 54	.35565 .35592 .35619 .35647 .35674	.93462 .93452 .93441 .93431 .93420	-38053 -38086 -38120 -38153 -38186	2.62791 2.62561 2.62332 2.62103 2.61874	·37191 ·37218 ·37245 ·37272 ·37299	·92827 ·92816 ·92805 ·92794 ·92784	·40065 ·40098 ·40132 ·40166 ·40200	2.49597 2.49386 2.49177 2.48967 2.48758	10 9 8 7 6
55 56 57 58 59	-35701 -35728 -35755 -35782 -35810	·93410 ·93400 ·93389 ·93379 ·93368	· 38220 · 38253 · 38286 · 38320 · 38353	2.61646 2.61418 2.61190 2.60963 2.60736	-37326 -37353 -37380 -37407 -37434	.92773 .92762 .92751 .92740 .92729	·40234 ·40267 ·40301 ·40335 ·40369	$\begin{array}{r} 2.48549\\ 2.48340\\ 2.48132\\ 2.47924\\ 2.47716\end{array}$	54321
<u>60</u>	.35837 Cos.	<u>.93358</u> Sin.	<u>.38386</u> Cot.	2.60509 Tan.	.37461 Cos.	<u>.92718</u> Sin.	<u>.40403</u> Cot.	2.47509 Tan.	-0
	000.							1 411.	
		6	9°	70	5	6	89		

705

23°

-	<u>22°</u>				23°					
•	Sin.	Cos.	Tan.	Cot.	Sin.	Cos.	Tan.	Cot.		
0 1 2 3 4	.37461 .37488 .37515 .37542 .37569	.92718 .92707 .92697 .92686 .92675	.40403 .40436 .40470 .40504 .40538	$\begin{array}{r} 2.47509 \\ 2.47302 \\ 2.47095 \\ 2.46888 \\ 2.46682 \end{array}$	·39073 ·39100 ·39127 ·39153 ·39180	•92050 •92039 •92028 •92016 •92005	•42447 •42482 •42516 •42551 •42585	$\begin{array}{r} 2.35585\\ 2.35395\\ 2.35205\\ 2.35015\\ 2.34825\end{array}$	60 59 58 57 56	
5 6 7 8 9	·37595 ·37622 ·37649 ·37676 ·37703	.92664 .92653 .92642 .92631 92620	.40572 .40606 .40640 .40674 .40707	2.46476 2.46270 2.46065 2.45860 2.45655	.39207 .39234 .39260 .39287 .39314	.91994 .91982 .91971 .91959 .91948	·42619 ·42654 ·42688 ·42722 ·42757	$\begin{array}{r} 2 \cdot 34636 \\ 2 \cdot 34447 \\ 2 \cdot 34258 \\ 2 \cdot 34069 \\ 2 \cdot 33881 \end{array}$	55 54 53 52 51	
10 11 12 13 14	·37730 ·37757 ·37784 ·37811 ·37838	.92609 .92598 .92587 .92576 .92565	.40741 .40775 .40809 .40843 .40877	$\begin{array}{r} 2.45451 \\ 2.45246 \\ 2.45043 \\ 2.44839 \\ 2.44636 \end{array}$	.39341 .39367 .39394 .39421 .39448	.91936 .91925 .91914 .91902 .91891	.42791 .42826 .42860 .42894 .42929	$\begin{array}{r} 2 \cdot 33693 \\ 2 \cdot 33505 \\ 2 \cdot 33317 \\ 2 \cdot 33130 \\ 2 \cdot 32943 \end{array}$	50 49 48 47 46	
15 16 17 18 19	·37865 ·37892 ·37919 ·37946 ·37973	.92554 .92543 .92532 .92521 .92510	.40911 .40945 .40979 .41013 .41047	$\begin{array}{r} 2.44433 \\ 2.44230 \\ 2.44027 \\ 2.43825 \\ 2.43623 \end{array}$	.39474 .39501 .39528 .39555 .39581	.91879 .91868 .91856 .91845 .91833	·42963 ·42998 ·43032 ·43067 ·43101	$\begin{array}{r} 2 \cdot 32756 \\ 2 \cdot 32570 \\ 2 \cdot 32383 \\ 2 \cdot 32197 \\ 2 \cdot 32012 \end{array}$	45 44 43 42 41	
20 21 22 23 24	.37999 .38026 .38053 .38080 .38107	.92499 .92488 .92477 .92466 .92455	.41081 .41115 .41149 .41183 .41217	$\begin{array}{r} 2 \cdot 43422 \\ 2 \cdot 43220 \\ 2 \cdot 43019 \\ 2 \cdot 42819 \\ 2 \cdot 42618 \end{array}$	· 39608 · 39635 · 39661 · 39688 · 39715	.91822 .91810 .91799 .91787 .91775	$ \begin{array}{r}     .43136 \\     .43170 \\     .43205 \\     .43239 \\     .43274 \\   \end{array} $	$\begin{array}{r} 2\cdot 31826\\ 2\cdot 31641\\ 2\cdot 31456\\ 2\cdot 31271\\ 2\cdot 31086\end{array}$	40 39 38 37 36	
25 26 27 28 29	.38134 .38161 .38188 .38215 .38241	.92444 .92432 .92421 .92410 .92399	.41251 .41285 .41319 .41353 .41387	$\begin{array}{r} 2 \cdot 42418 \\ 2 \cdot 42218 \\ 2 \cdot 42019 \\ 2 \cdot 41819 \\ 2 \cdot 41620 \end{array}$	·39741 ·39768 ·39795 ·39822 ·39848	.91764 .91752 .91741 .91729 .91718	·43308 ·43343 ·43378 ·43412 ·43447	$\begin{array}{r} 2 \cdot 30902 \\ 2 \cdot 30718 \\ 2 \cdot 30534 \\ 2 \cdot 30351 \\ 2 \cdot 30167 \end{array}$	35 34 33 32 31	
30 31 32 33 34	.38268 .38295 .38322 .33349 .38376	.92388 .92377 .92366 .92355 .92343	.41421 .41455 .41490 .41524 .41558	$\begin{array}{r} 2 \cdot 41421 \\ 2 \cdot 41223 \\ 2 \cdot 41025 \\ 2 \cdot 40827 \\ 2 \cdot 40629 \end{array}$	·39875 ·39902 ·39928 ·39955 ·39982	.91706 .91694 .91683 .91671 .91660	.43481 .43516 .43550 .43585 .43620	$2 \cdot 29984$ $2 \cdot 29801$ $2 \cdot 29619$ $2 \cdot 29437$ $2 \cdot 29254$	<b>30</b> 29 28 27 26	
35 36 37 38 39	.38403 .38430 .38456 .38483 .38510	.92332 .92321 .92310 .92299 .92287	.41592 .41626 .41660 .41694 .41728	2.40432 2.40235 2.40038 2.39841 2.39645	·40008 ·40035 ·40062 ·40088 ·40115	.91648 .91636 .91625 .91613 .91601	·43654 ·43689 ·43724 ·43758 ·43793	2.29073 2.28891 2.28710 2.28528 2.28348	25 24 23 22 21	
$\begin{array}{c} 40 \\ 41 \\ 42 \\ 43 \\ \underline{44} \end{array}$	·38537 ·38564 ·38591 ·38617 ·38644	.92276 .92265 .92254 .92243 .92231	.41763 .41797 .41831 .41865 .41899	$2 \cdot 39449$ $2 \cdot 39253$ $2 \cdot 39058$ $2 \cdot 38863$ $2 \cdot 38668$	.40141 .40168 .40195 .40221 .40248	.91590 .91578 .91566 .91555 .91543	·43828 ·43862 ·43897 ·43932 ·43966	$2 \cdot 28167$ $2 \cdot 27987$ $2 \cdot 27806$ $2 \cdot 27626$ $2 \cdot 27447$	20 19 18 17 16	
45 46 47 48 49	.38671 .38698 .38725 .38752 .38778	.92220 .92209 .92198 .92186 .92175	.41933 .41968 .42002 .42036 .42070	2.38473 2.38279 2.38084 2.37891 2.37697	· 40275 40301 · 40328 · 40355 · 40381	.91531 .91519 .91508 .91496 .91484	.44001 .44036 .44071 .44105 .44140	2.27267 2.27088 2.26909 2.26730 2.26552	$     \begin{array}{r}       15 \\       14 \\       13 \\       12 \\       11     \end{array} $	
50 51 52 53 54	·38805 ·38832 ·38859 ·38886 ·38912	.92164 .92152 .92141 .92130 .92119	.42105 .42139 .42173 .42207 .42242	$\begin{array}{r} 2 \cdot 37504 \\ 2 \cdot 37311 \\ 2 \cdot 37118 \\ 2 \cdot 36925 \\ 2 \cdot 36733 \end{array}$	·40408 ·40434 ·40461 ·40488 ·40514	.91472 .91461 .91449 .91437 .91425	.44175 .44210 .44244 .44279 .44314	$\begin{array}{r} 2 \cdot 26374 \\ 2 \cdot 26196 \\ 2 \cdot 26018 \\ 2 \cdot 25840 \\ 2 \cdot 25663 \end{array}$	10 9 8 7 6	
55 56 57 58 59	·38939 ·38966 ·38993 ·39020 ·39046	•92107 •92096 •92085 •92073 •92062	·42276 ·42310 ·42345 ·42379 ·42413	2.36541 2.36349 2.36158 2.35967 2.35776	.40541 .40567 .40594 .40621 .40647	.91414 .91402 .91390 .91378 .91366	.44349 .44384 .44418 .44453 .44488	$\begin{array}{r} 2 \cdot 25486 \\ 2 \cdot 25309 \\ 2 \cdot 25132 \\ 2 \cdot 24956 \\ 2 \cdot 24780 \end{array}$	5 4 3 2 1	
<u>60</u>	<u>· 39073</u> Cos.	<u>·92050</u> Sin.	<u>·42447</u> Cot.	2.35585 Tan.	<u>.40674</u> Cos.	<u>.91355</u> Sin.	<u>.44523</u> Cot.	2.24604 Tan.	<del>,</del>	
			~ 0	70			a9			

67°

66°

24°

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-	Sin.	Cos.	Tan.	Cot.	Sin.	Cos.	Tan.	Cot.	<u></u>
0 1 2 3 4	.40674 .40700 .40727 .40753 .40780	.91355 .91343 .91331 .91319 .91307	·44523 ·44558 ·44593 ·44627 ·44662	$\begin{array}{r} 2 \cdot 24604 \\ 2 \cdot 24428 \\ 2 \cdot 24252 \\ 2 \cdot 24077 \\ 2 \cdot 23902 \end{array}$	·42262 ·42288 ·42315 ·42341 ·42367	·90631 ·90618 ·90606 ·90594 ·90582	-46631 -46666 -46702 -46737 -46772	2.14451 2.14288 2.14125 2.13963 2.13801	60 59 58 57 56
5 6 7 8 9	.40806 .40833 .40860 .40886 .40913	.91295 .91283 .91272 .91260 .91248	·44697 ·44732 ·44767 ·44802 ·44837	$2 \cdot 23727$ $2 \cdot 23553$ $2 \cdot 23378$ $2 \cdot 23204$ $2 \cdot 23030$	·42394 ·42420 ·42446 ·42473 ·42499	·90569 ·90557 ·90545 ·90532 ·90520	.46808     .46843     .46879     .46914     .46950	$2 \cdot 13639$ $2 \cdot 13477$ $2 \cdot 13316$ $2 \cdot 13154$ $2 \cdot 12993$	55 54 53 52 51
10 11 12 13 14	.40939 .40966 .40992 .41019 .41045	.91236 .91224 .91212 .91200 .91188	·44872 ·44907 ·44942 ·44977 ·45012	$2 \cdot 22857$ $2 \cdot 22683$ $2 \cdot 22510$ $2 \cdot 22337$ $2 \cdot 22164$	·42525 ·42552 ·42578 ·42604 ·42631	.90507 .90495 .90483 .90470 .90458	.46985 .47021 .47056 .47092 .47128	2.12832 2.12671 2.12511 2.12350 2.12190	50 49 48 47 46
15 16 17 18 19	·41072 ·41098 ·41125 ·41151 ·41178	.91176 .91164 .91152 .91140 .91128	·45047 ·45082 ·45117 ·45152 ·45187	$2 \cdot 21992$ $2 \cdot 21819$ $2 \cdot 21647$ $2 \cdot 21475$ $2 \cdot 21304$	·42657 ·42683 ·42709 ·42736 ·42762	·90446 ·90433 ·90421 ·90408 ·90396	.47163 .47199 .47234 .47270 .47305	$\begin{array}{r} 2 \cdot 12030 \\ 2 \cdot 11871 \\ 2 \cdot 11711 \\ 2 \cdot 11552 \\ 2 \cdot 11392 \end{array}$	45 44 43 42 41
20 21 22 23 24	.41204 .41231 .41257 .41284 .41310	.91116 .91104 .91092 .91080 .91068	·45222 ·45257 ·45292 ·45327 ·45362	$2 \cdot 21132$ $2 \cdot 20961$ $2 \cdot 20790$ $2 \cdot 20619$ $2 \cdot 20449$	.42788 .42815 .42841 .42867 .42894	·90383 ·90371 ·90358 ·90346 ·90334	.47341 .47377 .47412 .47448 .47483	$\begin{array}{r} 2 \cdot 11233 \\ 2 \cdot 11075 \\ 2 \cdot 10916 \\ 2 \cdot 10758 \\ 2 \cdot 10600 \end{array}$	40 39 38 37 36
25 26 27 28 29	$ \begin{array}{r}     .41337 \\     .41363 \\     .41390 \\     .41416 \\     .41443 \\   \end{array} $	.91056 .91044 .91032 .91020 .91008	.45397 .45432 .45467 .45502 .45538	2.20278 2.20108 2.19938 2.19769 2.19599	.42920 .42946 .42972 .42999 .43025	.90321 .90309 .90296 .90284 .90271	.47519 .47555 .47590 .47626 .47662	$2 \cdot 10442$ $2 \cdot 10284$ $2 \cdot 10126$ $2 \cdot 09969$ $2 \cdot 09811$	35 34 33 32 31
30 31 32 33 34	.41469 .41496 .41522 .41549 .41575	.90996 .90984 .90972 .90960 .90948	·45573 ·45608 ·45643 ·45678 ·45713	2.19430 2.19261 2.19092 2.18923 2.18755	.43051 .43077 .43104 .43130 .43156	.90259 .90246 .90233 .90221 .90208	.47698 .47733 .47769 .47805 .47840	2.09654 2.09498 2.09341 2.09184 2.09028	30 29 28 27 26
35 36 37 38 39	.41602 .41628 .41655 .41681 .41707	.90936 .90924 .90911 .90899 .90887	·45748 ·45784 ·45819 ·45854 ·45889	2.18587 2.18419 2.18251 2.18084 2.17916	$     \begin{array}{r}         & \cdot 43182 \\         & \cdot 43209 \\         & \cdot 43235 \\         & \cdot 43261 \\         & \cdot 43287 \\     \end{array} $	.90196 .90183 .90171 .90158 .90146	·47876 ·47912 ·47948 ·47984 ·48019	$\begin{array}{r} 2.08872\\ 2.08716\\ 2.08560\\ 2.08405\\ 2.08250\end{array}$	25 24 23 22 21
40 41 42 43 44	·41734 ·41760 ·41787 ·41813 ·41840	·90875 ·90863 ·90851 ·90839 ·90826	$     \begin{array}{r}                                     $	$\begin{array}{r} 2 \cdot 17749 \\ 2 \cdot 17582 \\ 2 \cdot 17416 \\ 2 \cdot 17249 \\ 2 \cdot 17083 \end{array}$	·43313 ·43340 ·43366 ·43392 ·43418	.90133 .90120 .90108 .90095 .90082	·48055 ·48091 ·48127 ·48163 ·48198	2.08094 2.07939 2.07785 2.07630 2.07476	20 19 18 17 16
45 46 47 48 49	·41866 ·41892 ·41919 ·41945 ·41972	·90814 ·90802 ·90790 ·90778 ·90766	$ \begin{array}{r}     .46101 \\     .46136 \\     .46171 \\     .46206 \\     .46242 \\   \end{array} $	2.16917 2.16751 2.16585 2.16420 2.16255	$     \begin{array}{r}         & \cdot 43445 \\         & \cdot 43471 \\         & \cdot 43497 \\         & \cdot 43523 \\         & \cdot 43549 \\     \end{array} $	.90070 .90057 .90045 .90032 .90019	·48234 ·48270 ·48306 ·48342 ·48378	2.07321 2.07167 2.07014 2.06860 2.06706	15 14 13 12 11
50 51 52 53 54	·41998 ·42024 ·42051 ·42077 ·42104	.90753 .90741 .90729 .90717 .90704	·46277 ·46312 ·46348 ·46383 ·46418	$\begin{array}{r} 2 \cdot 16090 \\ 2 \cdot 15925 \\ 2 \cdot 15760 \\ 2 \cdot 15596 \\ 2 \cdot 15432 \end{array}$	·43575 ·43602 ·43628 ·43654 ·43680	·90007 ·89994 ·89981 ·89968 ·89956	·48414 ·48450 ·48486 ·48521 ·48557	$\begin{array}{r} 2 \cdot 06553 \\ 2 \cdot 06400 \\ 2 \cdot 06247 \\ 2 \cdot 06094 \\ 2 \cdot 05942 \end{array}$	10 9 8 7 6
55 56 57 58 59	$ \begin{array}{r}     .42130 \\     .42156 \\     .42183 \\     .42209 \\     .42235 \\ \end{array} $	.90692 .90680 .90668 .90655 .90643	.46454     .46489     .46525     .46560     .46595	$\begin{array}{r} 2.15268\\ 2.15104\\ 2.14940\\ 2.14777\\ 2.14614\end{array}$	·43706 ·43733 ·43759 ·43785 ·43811	·89943 ·89930 ·89918 ·89905 ·89892	·48593 ·48629 ·48665 ·48701 ·48737	2.05790 2.05637 2.05485 2.05333 2.05182	5 4 2 1
<u>60</u>	<u>•42262</u> Cos.	<u>.90631</u> Sin.	<u>.46631</u> Cot.	<u>2.14451</u> Tan.	<u>·43837</u> Cos.	<u>·89879</u> Sin.	<u>.48773</u> Cot.	2.05030 Tan.	<u>_0</u>
	-	·		70					

65°

**64°** 

BLE IX.--NATURAL SINES, COSINES, TANGENTS, AND COTANGENTS.

26°

27°

-	20		0				21	-	-
	Sin.	Cos.	Tan.	Cot.	Sin.	Cos.	Tan.	Cot.	1
	$     \begin{array}{r}         & \cdot 43837 \\         & \cdot 43863 \\         & \cdot 43889 \\         & \cdot 43916 \\         & \cdot 43942     \end{array} $	·89879 ·89867 ·89854 ·89841 ·89828	.48773 .48809 .48845 .48881 .48917	$\begin{array}{r} 2.05030\\ 2.04879\\ 2.04728\\ 2.04577\\ 2.04426\end{array}$	.45399 .45425 .45451 .45477 .45503	·89101 ·89087 ·89074 ·89061 ·89048	.50953     .50989     .51026     .51063     .51099	$\begin{array}{r} 1.96261 \\ 1.96120 \\ 1.95979 \\ 1.95838 \\ 1.95698 \end{array}$	60 59 58 57 56
	.43968     .43994     .44020     .44046     .44072	·89816 ·89803 ·89790 ·89777 ·89764	.48953 .48989 .49026 .49062 .49098	$\begin{array}{r} 2.04276\\ 2.04125\\ 2.03975\\ 2.03825\\ 2.03675\end{array}$	.45529 .45554 .45580 .45606 .45632	.89035 .89021 .89008 .88995 .88981	·51136 ·51173 ·51209 ·51246 ·51283	1.955571.954171.952771.951371.94997	55 54 53 52 51
	·44098 ·44124 ·44151 ·44177 ·44203	·89752 ·89739 ·89726 ·89713 ·89700	.49134 .49170 .49206 .49242 .49278	$\begin{array}{r} 2.03526\\ 2.03376\\ 2.03227\\ 2.03078\\ 2.02929\end{array}$	·45658 ·45684 ·45710 ·45736 ·45762	·88968 ·88955 ·88942 ·88928 ·88915	.51319     .51356     .51393     .51430     .51467	$ \begin{array}{r} 1.94858\\1.94718\\1.94579\\1.94579\\1.94440\\1.94301\end{array} $	50 49 48 47 46
	$     \begin{array}{r}                                     $	·89687 ·89674 ·89662 ·89649 ·89636	$ \begin{array}{r}         & \cdot 49315 \\         & \cdot 49351 \\         & \cdot 49387 \\         & \cdot 49423 \\         & \cdot 49459 \\     \end{array} $	$\begin{array}{r} 2.02780\\ 2.02631\\ 2.02483\\ 2.02335\\ 2.02187\end{array}$	$     .45787 \\     .45813 \\     .45839 \\     .45865 \\     .45891   $	·88902 ·88888 ·88875 ·88862 ·88848	·51503 ·51540 ·51577 ·51614 ·51651	$\begin{array}{r} 1.94162 \\ 1.94023 \\ 1.93885 \\ 1.93746 \\ 1.93608 \end{array}$	45 44 43 42 41
	$     \begin{array}{r}         & \cdot 44359 \\         & \cdot 44385 \\         & \cdot 44411 \\         & \cdot 44437 \\         & \cdot 44464 \\     \end{array} $	·89623 ·89610 ·89597 ·89584 ·89571	.49495     .49532     .49568     .49604     .49640	2.02039 2.01891 2.01743 2.01596 2.01449	.45917 .45942 .45968 .45994 .46020	·88835 ·88822 ·88808 ·88795 ·88782	·51688 ·51724 ·51761 ·51798 ·51835	$\begin{array}{r} 1.93470 \\ 1.93332 \\ 1.93195 \\ 1.93057 \\ 1.92920 \end{array}$	40 39 38 37 36
	.44490 .44516 .44542 .44568 .44594	.89558 .89545 .89532 .89519 .89506	·49677 ·49713 ·49749 ·49786 ·49822	$\begin{array}{r} 2.01302 \\ 2.01155 \\ 2.01008 \\ 2.00862 \\ 2.00715 \end{array}$	.46046 .46072 .46097 .46123 .46149	·88768 ·88755 ·88741 ·88728 ·88715	.51872 .51909 .51946 .51983 .52020	1.927821.926451.925081.923711.92235	35 34 33 32 31
	.44620 .44646 .44672 .44698 .44724	·89493 ·89480 ·89467 ·89454 ·89441	.49858 .49894 .49931 .49967 .50004	2.00569 2.00423 2.00277 2.00131 1.99986	$     \begin{array}{r}             .46175 \\             .46201 \\             .46226 \\             .46252 \\             .46278 \\         \end{array} $	·88701 ·88688 ·88674 ·88661 ·88647	.52057 .52094 .52131 .52168 .52205	1.92098 1.91962 1.91826 1.91690 1.91554	<b>30</b> 29 28 27 26
	.44750 .44776 .44802 .44828 .44854	.89428 .89415 .89402 .89389 .89376	.50040 .50076 .50113 .50149 .50185	$\begin{array}{r} 1.99841 \\ 1.99695 \\ 1.99550 \\ 1.99406 \\ 1.99261 \end{array}$	$     \begin{array}{r}                                     $	·88634 ·88620 ·88607 ·88593 ·88580	·52242 ·52279 ·52316 ·52353 ·52390	1.91418 1.91282 1.91147 1.91012 1.90876	25 24 23 22 21
	.44880 .44906 .44932 .44958 .44984	·89363 ·89350 ·89337 ·89324 ·89311	.50222 .50258 .50295 .50331 .50368	$\begin{array}{r} 1.99116 \\ 1.98972 \\ 1.98828 \\ 1.98684 \\ 1.98540 \end{array}$	$     \begin{array}{r}                                     $	·88566 ·88553 ·88539 ·88526 ·88512	·52427 ·52464 ·52501 ·52538 ·52575	1.90741 1.90607 1.90472 1.90837 1.90203	20 19 18 17 16
	.45010 .45036 .45062 .45088 .45114	·89298 ·89285 ·89272 ·89259 ·89245	·50404 ·50441 ·50477 ·50514 ·50550	1.98396 1.98253 1.98110 1.97966 1.97823	$     .46561 \\     .46587 \\     .46613 \\     .46639 \\     .46664 $	.88499 .88485 .88472 .88458 .88445	.52613 .52650 .52687 .52724 .52761	1.90069 1.89935 1.89801 1.89667 1.89533	15 14 13 12 11
	.45140 .45166 .45192 .45218 .45243	.89232 .89219 .89206 .89193 .89180	.50587 .50623 .50660 .50696 .50733	1.97681 1.97538 1.97395 1.97253 1.97111	.46690 .46716 .46742 .46767 .46793	.88431 .88417 .88404 .88390 .88377	.52798 .52836 .52873 .52910 .52947	1.89400 1.89266 1.89133 1.89000 1.88867	10 9 8 7 6
	$ \begin{array}{r}     .45269 \\     .45295 \\     .45321 \\     .45347 \\     .45373 \\   \end{array} $	.89167 .89153 .89140 .89127 .89114	.50769 .50806 .50843 .50879 .50916	1.96969 1.96827 1.96685 1.96544 1.96402	.46819 .46844 .46870 .46896 .46921	.88363 .88349 .88336 .88322 .88308	.52985 .53022 .53059 .53096 .53134	1.88734 1.88602 1.88469 1.88337 1.88205	5 4 3 2 1
-	. 45399 Cos.	<u>. 89101</u> Sin.	.50953 Cot.	<u>1.96261</u> Tan.	<u>46947</u> Cos.	<u>.88295</u> Sin.	<u>.53171</u> Cot.	<u>1.88073</u> Tan.	<u>, 0</u>
_			3°	708		6			-

TABLE IX.—NATURAL SINES, COSINES, TANGEN IS, AND COTANGEN         28°       29°									
,	Sin.	Cos.	Tan.	Cot.	Sin.	Cos.	Tan.	Cot.	1,
01234	.46947 .46973 .46999 .47024 .47050	-88295 -88281 -88267 -88254 -88240	$ \begin{array}{r} \cdot 53171 \\ \cdot 53208 \\ 53246 \\ \cdot 53283 \\ \cdot 53320 \\ \end{array} $	1.88073 1.87941 1.87809 1.87677 1.87546	·48481 ·48506 ·48532 ·48557 ·48583	87462 ·87448 ·87434 87420 ·87406	.55431 .55469 .55507 .55545 .55583	1 80405 1.80281 1.80158 1.80034 1.79911	60 59 58 57 56
5 6 7 8 9	.47076 .47101 .47127 .47153 .47178	-88226 88213 -88199 -88185 -88172	.53358 .53395 .53432 53470 .53507	1.87415 1.87283 1.87152 1.87021 1.86891	.48608 .48634 .48659 .48684 .48710	.87391 .87377 .87363 .87349 .87335	.55621 .55659 .55697 .55736 .55774	1 79788 1 79665 1.79542 1.79419 1.79296	55 54 53 52 51
10 11 12 13 14	.47204 .47229 .47255 .47281 .47306	.88158 .88144 .88130 .88117 .88103	.53545 .53582 .53620 .53657 .53694	$\begin{array}{r} 1.86760 \\ 1.86630 \\ 1.86499 \\ 1.86369 \\ 1.86239 \end{array}$	·48735 ·48761 ·48786 ·48811 ·48837	-87321 -87306 -87292 -87278 -87264	-55812 -55850 -55888 -55926 -55964	1.79174 1.79051 1.78929 1.78807 1.78685	50 49 48 47 46
15 16 17 18 <u>19</u>	.47332 .47358 .47383 .47409 .47434	.88089 .88075 .88062 .88048 .88034	.53732 .53769 .53807 .53844 .53882	$\begin{array}{r} 1.86109 \\ 1.85979 \\ 1.85850 \\ 1.85720 \\ 1.85591 \end{array}$	.48862 .48888 .48913 .48938 .48964	.87250 .87235 .87221 .87207 .87193	56003 56041 56079 56117 56156	1.78563 1.78441 1.78319 1.78198 1.78077	$     \begin{array}{r}       45 \\       44 \\       43 \\       42 \\       41 \\     \end{array} $
20 21 22 23 24	.47460 .47486 .47511 .47537 .47562	-88020 -88006 -87993 -87979 -87965	.53920 .53957 .53995 .54032 .54070	$\begin{array}{r} 1 \cdot 85462 \\ 1 \cdot 85333 \\ 1 \cdot 85204 \\ 1 \cdot 85075 \\ 1 \cdot 84946 \end{array}$	-48989 -49014 -49040 -49065 -49090	.87178 .87164 .87150 .87136 .87121	.56194 .56232 .56270 .56309 .56347	$\begin{array}{r} 1.77955\\ 1.77834\\ 1.77713\\ 1.77592\\ 1.77471\end{array}$	40 39 38 37 36
25 26 27 28 29	.47588 .47614 .47639 .47665 .47690	.87951 .87937 .87923 .87909 .87896	.54107 .54145 .54183 .54220 .54258	$\begin{array}{r} 1.84818 \\ 1.84689 \\ 1.84561 \\ 1.84433 \\ 1.84305 \end{array}$	.49116 .49141 .49166 .49192 .49217	-87107 87093 -87079 -87064 -87050	.56385 .56424 .56462 .56501 .56539	$ \begin{array}{r} 1.77351 \\ 1.77230 \\ 1.77110 \\ 1.76990 \\ 1.76869 \\ \end{array} $	35 34 33 32 31
30 31 32 33 34	.47716 .47741 .47767 .47793 .47818	.87882 .87868 .87854 .87840 .87826	·54296 ·54333 ·54371 ·54409 ·54446	1.84177 1.84049 1.83922 1.83794 1.83667	.49242 .49268 .49293 .49318 .49344	.87036 .87021 .87007 .86993 .86978	56577 56616 56654 56693 56731	$\begin{array}{r} 1.76749 \\ 1.76629 \\ 1.76510 \\ 1.76390 \\ 1.76271 \end{array}$	30 29 28 27 26
35 36 37 38 39	.47844 .47869 .47895 .47920 .47946	.87812 .87798 .87784 .87770 .87756	.54484 .54522 .54560 .54597 .54635	$\begin{array}{r} 1.83540 \\ 1.83413 \\ 1.83286 \\ 1.83159 \\ 1.83033 \end{array}$	.49369 .49394 .49419 .49445 .49470	·26964 ·86949 ·86935 ·86921 ·86906	.56769 .56808 .56846 .56885 .56923	$\begin{array}{r} 1.76151 \\ 1.76032 \\ 1.75913 \\ 1.75794 \\ 1.75675 \end{array}$	25 24 23 22 21
40 41 42 43 44	.47971 .47997 .48022 .48048 .48073	·87743 ·87729 ·87715 ·87701 ·87687	·54673 ·54711 ·54748 ·54786 ·54824	1.829061.827801.826541.825281.82402	.49495 .49521 .49546 .49571 .49596	-86892 -86878 -86863 -86849 -86834	.56962 .57000 .57039 .57078 .57116	1.755561.754371.753191.752001.75082	20 19 18 17 16
45 46 47 48 49	.48099 .48124 .48150 .48175 .48201	.87673 .87659 .87645 .87631 .87617	.54862 .54900 .54938 .54975 .55013	1.82276 1.82150 1.82025 1.81899 1.81774	.49622 .49647 .49672 .49697 .49723	.86820 .86805 .86791 .86777 .86762	.57155 .57193 .57232 .57271 .57309	1.74964 1.74846 1.74728 1.74610 1.74492	$     \begin{array}{r}       15 \\       14 \\       13 \\       12 \\       11 \\       11     \end{array} $
50 51 52 53 54	.48226 .48252 .48277 .48303 .48328	.87603 .87589 .87575 .87561 .87546	.55051 .55089 .55127 .55165 .55203	$1.81649 \\ 1.81524 \\ 1.81399 \\ 1.81274 \\ 1.81150 $	.49748 .49773 .49798 .49824 .49849	-86748 -86733 -86719 -86704 -86690	.57348 .57386 .57425 .57464 .57503	$1.74375 \\ 1.74257 \\ 1.74140 \\ 1.74022 \\ 1.73905$	10 9 8 7 6
55 56 57 58 59	$ \begin{array}{r} .48354\\ .48379\\ .48405\\ .48430\\ .48456 \end{array} $	.87532 .87518 .87504 .87490 .87476	.55241 .55279 .55317 .55355 .55393	$1.81025 \\ 1.80901 \\ 1.80777 \\ 1.80653 \\ 1.80529$	.49874 .49899 .49924 .49950 .49975	-86675 -86661 -86646 -86632 -86617	.57541 .57580 .57619 .57657 .57696	1.73788 1.73671 1.73555 1.73438 1.73321	5 4 3 2 1
<u>60</u> '	<u>.48481</u> Cos.	<u>. 87462</u> Sin.	<u>. 55431</u> Cot.	<u>1.80405</u> Tan.	.50000 Cos.	<u>- 86603</u> Sin.	<u>.57735</u> Cot.	<u>1.73205</u> Tan.	<u>_0</u>

30°

31°

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	30-				31					
	Sin.	Cos.	Tan.	Cot.	Sin.	Cos.	Tan.	Cot.	•	
0	.50000	·86603	.57735	1.73205	.51504	·85717	-60086	1.66428	60	
1	.50025	·86588	.57774	1.73089	.51529	·85702	-60126	1.66318	59	
2	.50050	·86573	.57813	1.72973	.51554	·85687	-60165	1.66209	58	
3	.50076	·86559	.57851	1.72857	.51579	·85672	-60205	1.66099	57	
4	.50101	·86544	.57890	1.72741	.51604	·85657	-60245	1.65990	56	
5 6 7 8 9	.50126 .50151 .50176 .50201 .50227	·86530 ·86515 ·86501 ·86486 ·86471	.57929 .57968 .58007 .58046 .58085	$\begin{array}{r} 1.72625\\ 1.72509\\ 1.72393\\ 1.72278\\ 1.72163\end{array}$	·51628 ·51653 ·51678 ·51703 ·51728	·85642 ·85627 ·85612 ·85597 ·85582	·60284 ·60324 ·60364 ·60403 ·60443	1.658811.657721.656631.655541.65445	55 54 53 52 51	
10	.50252	·86457	.58124	1.72047	·51753	.85567	· 60483	1.653371.652281.651201.650111.64903	50	
11	.50277	·86442	.58162	1.71932	·51778	.85551	· 60522		49	
12	.50302	·86427	.58201	1.71817	·51803	.85536	· 60562		48	
13	.50327	·86413	.58240	1.71702	·51828	.85521	· 60602		47	
14	.50327	·86398	.58279	1.71588	·51852	.85506	· 60642		46	
15	· 50377	.86384	.58318	1.71473	.51877	.85491	·60681	$\begin{array}{r} 1 \cdot 64795 \\ 1 \cdot 64687 \\ 1 \cdot 64579 \\ 1 \cdot 64471 \\ 1 \cdot 64363 \end{array}$	45	
16	· 50403	.86369	.58357	1.71358	.51902	.85476	·60721		44	
17	· 50428	.86354	.58396	1.71244	.51927	.85461	·60761		43	
18	· 50453	.86340	.58435	1.71129	.51952	.85446	·60801		42	
19	· 50478	.86325	.58474	1.71015	.51977	.85431	·60841		41	
20 21 22 23 24	· 50503 · 50528 · 50553 · 50578 · 50603	-86310 -86295 -86281 -86266 -86251	.58513 .58552 .58591 .58631 .58670	$\begin{array}{r} 1.70901 \\ 1.70787 \\ 1.70673 \\ 1.70560 \\ 1.70446 \end{array}$	·52002 ·52026 ·52051 ·52076 ·52101	.85416 .85401 .85385 .85370 .85355	.60881 .60921 .60960 .61000 .61040	1.642561.641481.640411.639341.63826	40 39 38 37 36	
25	· 50628	·86237	58709	1.70332	.52126	.85340	.61080	$\begin{array}{r} 1.63719 \\ 1.63612 \\ 1.63505 \\ 1.63398 \\ 1.63292 \end{array}$	35	
26	· 50654	·86222	58748	1.70219	.52151	.85325	.61120		34	
27	· 50679	·86207	58787	1.70106	.52175	.85310	.61160		33	
28	· 50704	·86192	58826	1.69992	.52200	.85294	.61200		32	
29	· 50729	·86178	58865	1.69879	.52225	.85279	.61240		31	
30	· 50754	·86163	.58905	1.69766	.52250	·85264	.61280	1.631851.630791.629721.628661.62760	30	
31	· 50779	·86148	.58944	1.69653	.52275	·85249	.61320		29	
32	· 50804	·86133	.58983	1.69541	.52299	·85234	.61360		28	
33	· 50829	·86119	.59022	1.69428	.52324	·85218	.61400		27	
34	· 50854	·86104	.59061	1.69316	.52349	·85203	.61440		26	
35 36 37 38 39	·50879 ·50904 ·50929 ·50954 ·50979	-86089 -86074 -86059 -86045 -86030	.59101 .59140 .59179 59218 .59258	1.692031.690911.689791.688661.68754	. 52374 . 52399 . 52423 . 52448 . 52473	·85188 ·85173 ·85157 ·85142 ·85127	.61480 .61520 .61561 .61601 .61641	1.626541.625481.624421.623361.62230	25 24 23 22 21	
40	.51004	·86015	.59297	1.68643	·52498	·85112	.61681	1.62125	20	
41	.51029	·86000	.59336	1.68531	·52522	·85096	.61721	1.62019	19	
42	.51054	·85985	.59376	1.68419	·52547	·85081	.61761	1.61914	18	
43	.51079	·85970	.59415	1.68308	·52572	·85066	.61801	1.61808	17	
44	.51104	·85956	.59454	1.68196	·52597	·85051	.61842	1.61703	16	
45	.51129	.85941	.59494	1.68085	·52621	·85035	•61882	1.61598	15	
46	.51154	.85926	.59533	1.67974	·52646	·85020	•61922	1.61493	14	
47	.51179	.85911	.59573	1.67863	·52671	·85005	•61962	1.61388	13	
48	.51204	.85896	.59612	1.67752	·52696	·84989	•62003	1.61283	12	
49	.51229	.85881	.59651	1.67641	·52720	·84974	•62043	1.61179	11	
50	.51254	.85866	·59691	1.67530	·52745	·84959	·62083	1.61074	10	
51	.51279	.85851	·59730	1.67419	·52770	·84943	·62124	1.60970	9	
52	.51304	.85836	·59770	1.67309	·52794	·84928	·62164	1.60865	8	
53	.51329	.85821	·59809	1.67198	·52319	·84913	·62204	1.60761	7	
54	.51354	.85806	·59849	1.67088	·52844	·84897	·62245	1.60657	6	
55 56 57 58 59	·51379 ·51404 ·51429 ·51454 ·51479	-85792 -85777 -85762 -85747 -85732	·59888 ·59928 ·59967 ·60007 ·60046	$1.66978 \\ 1.66867 \\ 1.66757 \\ 1.66647 \\ 1.66538$	-52869 -52893 -52918 -52943 -52967	·84882 ·84866 ·84851 ·84836 ·84820	•62285 •62325 •62366 •62406 •62446	1.605531.604491.603451.602411.60137	5 4 3 2 1	
<u>60</u>	• 51504 Cos.	<u>. 85717</u> Sin.	<u>. 60086</u> Cot.	<u>1.66428</u> Tan.	<u>. 52992</u> Cos.	• 84805 Sin.	<u>· 62487</u> Cot.	<u>1.60033</u> Tan.	<del>~</del>	
			- 0						-	

**59°** 

710

ES .	CABLE IXNATURAL SINES,	COSINES, TANGENTS, AND COTANGENTS
3	32°	33°

IAI	5LE 1A	-NAIO	32°	(ES, COSI)	33°					
	Sin.	Cos	Tan.	Cot	Sin.	Cos.	Tan.	Cot.	•	
01234 5	.52992 .53017 .53041 .53066 .53091	·84805 ·84789 ·84774 ·84759 ·84743	·62487 ·62527 ·62568 ·62608 ·62649	$\begin{array}{r} 1.60033 \\ 1.59930 \\ 1.59826 \\ 1.59723 \\ 1.59620 \end{array}$	•54464 •54488 •54513 •54537 •54561	·83867 ·83851 ·83835 ·83819 ·83804	$     \begin{array}{r}                                     $	1.53986 1.53888 1.53791 1.53693 1.53595	60 59 58 57 56	
5 6 7 8 9	.53115 .53140 .53164 .53189 .53214	.84728 .84712 .84697 .84681 .84666	·62689 ·62730 ·62770 ·62811 ·62852	$\begin{array}{r} 1.59517\\ 1.59414\\ 1.59311\\ 1.59208\\ 1.59105\end{array}$	•54585 •54610 •54635 •54659 •54683	·83788 ·83772 ·83756 ·83740 ·83724	$     \begin{array}{r}         \cdot 65148 \\         \cdot 65189 \\         \cdot 65231 \\         \cdot 65272 \\         \cdot 65314 \\     \end{array} $	1.534971.534001.533021.532051.53107	55 54 53 52 51	
10 11 12 13 14	.53238 .53263 .53288 .53312 .53337	.84650 .84635 .84619 .84604 .84588	.62892 .62933 .62973 .63014 .63055	1.59002 1.58900 1.58797 1.58695 1.58593	·54708 ·54732 ·54756 ·54781 ·54805	.83708 .83692 .83676 .83660 .83645	$ \begin{array}{r} \cdot 65355 \\ \cdot 65397 \\ \cdot 65438 \\ \cdot 65480 \\ \cdot 65521 \\ \end{array} $	$\begin{array}{r} 1.53010 \\ 1.52913 \\ 1.52816 \\ 1.52719 \\ 1.52622 \end{array}$	50 49 48 47 46	
15 16 17 18 <u>19</u>	53361 53386 53411 53435 53460	.84573 .84557 .84542 .84526 .84511	.63095 .63136 .63177 .63217 .63258	1.58490 1.58388 1.58286 1.58184 1.58083	.54829 .54854 .54878 .54902 .54927	.83629 .83613 .83597 .83581 .83565	.65563 .65604 .65646 .65688 .65729	$\begin{array}{r} 1.52525\\ 1.52429\\ 1.52332\\ 1.52235\\ 1.52139\\ \end{array}$	45 44 43 42 41	
20 21 22 23 24	.53484 .53509 .53534 .52558 .53583	.84495 .84480 .84464 .84448 .84433	.63299 .63340 .63380 .63421 .63462	1.57981 1.57879 1.57778 1.57676 1.57575	54951 54975 54999 55024 55048	.83549 .83533 .83517 .83501 .83485	.65771 .65813 .65854 .65896 .65938	$\begin{array}{r} 1.52043 \\ 1.51946 \\ 1.51850 \\ 1.51754 \\ 1.51658 \end{array}$	40 39 38 37 36	
25 26 27 28 29	.53607 .53632 .53656 .53681 .53705	.84417 .84402 .84386 .84370 .84355	.63503 .63544 .63584 .63625 .63666	1.57474 1.57372 1.57271 1.57170 1.57069	.55072 .55097 .55121 .55145 .55169	.83469 .83453 .83437 .83421 .83405	65980 66021 66063 66105 66147	$\begin{array}{r} 1.51562 \\ 1.51466 \\ 1.51370 \\ 1.51275 \\ 1.51179 \end{array}$	35 34 33 32 31	
30 31 32 33 34	.53730 .53754 .53779 .53804 .53828	.84339 .84324 .84308 .84292 .84277	.63707 .63748 .63789 .63830 .63871	$\begin{array}{r} 1.56969 \\ 1.56868 \\ 1.56767 \\ 1.56667 \\ 1.56566 \end{array}$	.55194 .55218 .55242 .55266 .55291	-83389 -83373 -83356 -83340 -83324	$     \begin{array}{r}             .66189 \\             .66230 \\             .66272 \\             .66314 \\             .66356 \\         \end{array} $	1.51084 1.50988 1.50893 1.50797 1.50702	30 29 28 27 26	
35 36 37 38 39	.53853 .53877 .53902 .53926 .53951	.84261 .84245 .84230 .84214 .84198	$     \begin{array}{r}             .63912 \\             .63953 \\             .63994 \\             .64035 \\             .64076 \\         \end{array}     $	1.56466 1.56366 1.56265 1.56165 1.56065	.55315 .55339 .55363 .55388 .55412	-83308 -83292 -83276 -83260 -83244	-66398 -66440 -66482 -66524 -66566	$\begin{array}{r} 1.50607 \\ 1.50512 \\ 1.50417 \\ 1.50322 \\ 1.50228 \end{array}$	25 24 23 22 21	
40 41 42 43 44	.53975 .54000 .54024 .54049 .54073	.84182 .84167 .84151 .84135 .84120	.64117 .64158 .64199 .64240 .64281	1.55966 1.55866 1.55766 1.55666 1.55567	.55436 .55460 .55484 .55509 .55533	·83228 ·83212 ·83195 ·83179 ·83163	.66608 .66650 .66692 .66734 .66776	$\begin{array}{r} 1.50133 \\ 1.50038 \\ 1.49944 \\ 1.49849 \\ 1.49755 \end{array}$	20 19 18 17 16	
45 46 47 48 49	.54097 .54122 .54146 .54171 .54195	.84104 .84088 .84072 .84057 .84041	64322 64363 64404 64446 64487	1.55467 1.55368 1.55269 1.55170 1.55071	55557 55581 55605 55630 55654	.83147 .83131 .83115 .83098 .83082	$     \begin{array}{r}             .66818 \\             .66860 \\             .66902 \\             .66944 \\             .66986 \\         \end{array}     $	$1.49661 \\ 1.49566 \\ 1.49472 \\ 1.49378 \\ 1.49284$	$     \begin{array}{r}       15 \\       14 \\       13 \\       12 \\       11 \\     \end{array} $	
50 51 52 53 54	.54220 .54244 .54269 .54293 .54317	-84025 -84009 -83994 -83978 -83962	64528 64569 64610 64652 64693	$1.54972 \\ 1.54873 \\ 1.54774 \\ 1.54675 \\ 1.54576 \\ \hline 1.5576 \\ \hline$	·55678 ·55702 ·55726 ·55750 ·55775	-83066 -83050 -83034 -83017 -83001	·67028 ·67071 ·67113 ·67155 ·67197	$1.49190 \\ 1.49097 \\ 1.49003 \\ 1.48909 \\ 1.48816$	10 9 8 7 6	
55 56 57 58 59	54342 54366 54391 54415 54440	-83946 -83930 -83915 -83899 -83883	64734 64775 64817 64858 64899	$1.54478 \\ 1.54379 \\ 1.54281 \\ 1.54183 \\ 1.54085 $	.55799 .55823 .55847 .55871 .55895	- 82985 - 82969 - 82953 - 82936 - 82920	·67239 ·67282 ·67324 ·67366 ·67409	$1.48722 \\ 1.48629 \\ 1.48536 \\ 1.48442 \\ 1.48349 $	54 32 	
<u>60</u> /	<u>.54464</u> Cos.	<u>·83867</u> Sin.	<u>· 64941</u> Cot.	<u>1.53986</u> Tan.	<u>· 55919</u> Cos.	<u>.82904</u> Sin.	<u>.67451</u> Cot.	<u>1.48256</u> Tan.	<del></del>	

711

56°

34°

35°

-	34°			35						
	Sin.	Cos.	Tan.	Cot.	Sin.	Cos.	Tan.	Cot.	,	
0 1 2 3 4	.55919 .55943 .55968 .55992 .56016	·82904 ·82887 ·82871 ·82855 82839	·67451 ·67493 ·67536 ·67578 ·67620	1.48256 1.48163 1.48070 1.47977 1.47885	·57358 ·57381 ·57405 ·57429 ·57453	.81915 .81899 .81882 .81865 .81848	.70021 .70064 .70107 .70151 .70194	1.428151.427261.426381.425501.42462	60 59 58 57 56	
5 6 7 8 9	.56040 .56064 .56088 .56112 .56136	·82822 ·82806 ·82790 ·82773 ·82757	·67663 ·67705 ·67748 ·67790 ·67832	1.47792 1.47699 1.47607 1.47514 1.47422	·57477 ·57501 ·57524 ·57548 ·57572	·81832 ·81815 ·81798 ·81782 ·81765	·70238 ·70281 ·70325 ·70368 ·70412	$\begin{array}{r} 1.42374 \\ 1.42286 \\ 1.42198 \\ 1.42110 \\ 1.42022 \end{array}$	55 54 53 52 51	
10 11 12 13 14	.56160 .56184 .56208 .56232 .56256	-82741 -82724 -82708 -82692 -82675	·67875 ·67917 ·67960 ·68002 ·68045	$1.47330 \\ 1.47238 \\ 1.47146 \\ 1.47053 \\ 1.46962$	-57596 -57619 -57643 -57667 -57691	.81748 .81731 .81714 .81698 .81681	.70455 .70499 .70542 .70586 .70629	$\begin{array}{r} 1.41934 \\ 1.41847 \\ 1.41759 \\ 1.41672 \\ 1.41584 \end{array}$	50 49 48 47 46	
15 16 17 18 <u>19</u>	·56280 ·56305 ·56329 ·56353 ·56377	.82659 .82643 .82626 .82610 .82593	·68088 ·68130 ·68173 ·68215 ·68258	$1.46870 \\ 1.46778 \\ 1.46686 \\ 1.46595 \\ 1.46503 \\ 1.46$	.57715 .57738 .57762 .57786 .57810	·81664 ·81647 ·81631 ·81614 ·81597	·70673 ·70717 ·70760 ·70804 ·70848	$\begin{array}{r} 1.41497 \\ 1.41409 \\ 1.41322 \\ 1.41235 \\ 1.41148 \end{array}$	45 44 43 42 41	
20 21 22 23 24	·56401 ·56425 ·56449 ·56478 ·56497	.82577 .82561 .82544 .82528 .82511	·68301 ·68343 ·68386 ·68429 ·68471	1.46411 1.46320 1.46229 1.46137 1.46046	·57833 ·57857 ·57881 ·57904 ·57928	.81580 .81563 .81546 .81530 .81513	.70891 .70935 .70979 .71023 .71066	1.410611.409741.408871.408001.40714	40 39 38 37 36	
25 26 27 28 29	·56521 ·56545 ·56569 ·56593 ·56617	.82495 .82478 .82462 .82446 .82429	.68514 .68557 .68600 .68642 .68685	1.459551.458641.457731.456821.45592	.57952 .57976 .57999 .58023 .58047	.81496 .81479 .81462 .81445 .81428	.71110 .71154 .71198 .71242 .71285	1.406271.405401.404541.403671.40281	35 34 33 32 31	
30 31 32 33 34	.56641 .56665 .56689 .56713 .56736	.82413 .82396 .82380 .82363 .82347	-68728 -68771 -68814 -68857 -68900	$\begin{array}{r} 1.45501 \\ 1.45410 \\ 1.45320 \\ 1.45229 \\ 1.45139 \end{array}$	.58070 .58094 .58118 .58141 .58165	.81412 .81395 .81378 .81361 .81344	.71329 .71373 .71417 .71461 .71505	$\begin{array}{r} 1.40195 \\ 1.40109 \\ 1.40022 \\ 1.39936 \\ 1.39850 \end{array}$	30 29 28 27 26	
35 36 37 38 39	·56760 ·56784 ·56803 ·56832 ·56856	.82330 .82314 .82297 .82281 .82264	.68942 .68985 .69028 .69071 .69114	1.45049 1.44958 1.44868 1.44778 1.44688	·58189 ·58212 ·58236 ·58260 ·58283	.81327 .81310 .81293 .81276 .81259	.71549 .71593 .71637 .71681 .71725	1.39764 1.39679 1.39503 1.39507 1.39421	25 24 23 22 21	
40 41 42 43 44	.56880 .56904 .56928 .56952 .56976	.82248 .82231 .82214 .82198 .82181	·69157 ·69200 ·69243 ·69286 ·69329	1.445981.445081.444181.443291.44239	.58307 .58330 .58354 .58378 .58401	-81242 -81225 -81208 -81191 -81174	.71769 .71813 .71857 .71901 .71946	$\begin{array}{r} 1 \cdot 39336 \\ 1 \cdot 39250 \\ 1 \cdot 39165 \\ 1 \cdot 39079 \\ 1 \cdot 38994 \end{array}$	20 19 18 17 16	
45 46 47 48 49	.57000 .57024 .57047 .57071 .57095	-82165 -82148 -82132 -82115 -82098	-69372 -69416 -69459 -69502 -69545	1.441491.440601.439701.438811.43792	.58425 .58449 .58472 .58496 .58519	.81157 .81140 .81123 .81106 .81089	·71990 ·72034 ·72078 ·72122 ·72167	1.38909 1.38824 1.38738 1.38653 1.38568	$     \begin{array}{r}       15 \\       14 \\       13 \\       12 \\       11 \\       10 \\       11     \end{array} $	
50 51 52 53 54	.57119 .57143 .57167 .57191 .57215	-82082 -82065 -82048 -82032 -82015	-69588 -69631 -69675 -69718 -69761	$1.43703 \\ 1.43614 \\ 1.43525 \\ 1.43436 \\ 1.43347$	.58543 .58567 .58590 .58614 .58637	-81072 -81055 -81038 -81021 -81004	·72211 ·72255 ·72299 ·72344 ·72388	$ \begin{array}{r} 1.38484 \\ 1.38399 \\ 1.38314 \\ 1.38229 \\ 1.38145 \\ \hline 1.88229 \\ \hline 1.38145 \\ \hline 1.88229 \\ \hline 1.88145 \\ \hline 1.88229 \\ \hline 1.8829$	10 9 8 7 6	
55 56 57 58 59	· 57238 · 57262 · 57286 · 57310 · 57334	.81999 .81982 .81965 .81949 .81932	$     \begin{array}{r}             .69804 \\             .69847 \\             .69891 \\             .69934 \\             .69977 \\         \end{array}     $	1.432581.431691.430801.429921.42903	· 58661 · 58684 · 58708 · 58731 · 58755	.80987 .80970 .80953 .80936 .80919	·72432 ·72477 ·72521 ·72565 ·72610	$ \begin{array}{r} 1.38060 \\ 1.37976 \\ 1.37891 \\ 1.37807 \\ 1.37722 \\ \hline 1.37722 \end{array} $	5 4 3 2 1	
<u>60</u>	<u>· 57358</u> Cos.	<u>.81915</u> Sin.	.70021 Cot.	<u>1.42815</u> Tan.	<u>. 58779</u> Cos.	<u>-80902</u> Sin.	.72654 Cot.	<u>1.37638</u> Tan.	<u>, 0</u>	

712

36°

37°

-	36°			37					
·	Sin.	Cos.	Tan.	Cot.	Sin.	Cos.	Tan.	Cot.	,
0 1 2 3 4	-58802 -58826 -58849	• 80902 • 80885 • 80867 • 80850 • 80833	•72654 •72699 •72743 •72788 •72882	1.37386 1.37302	· 60182 60205 · 60228 · 60251 · 60274	·79864 ·79846 ·79829 ·79811 ·79793	·75355 ·75401 ·75447 ·75492 ·75538	1.327041.326241.325441.324641.32384	60 59 58 57 56
5 6 7 8 9	·58920 ·58943	· 80816 · 80799 · 80782 · 80765 · 80748	.72877 .72921 .72966 .73010 .73055	1.37134	· 60298 · 60321 · 60344 · 60367 · 60390	·79776 ·79758 ·79741 ·79723 ·79706	.75584 .75629 .75675 .75721 .75767	$\begin{array}{c} 1\cdot 32304 \\ 1\cdot 32224 \\ 1\cdot 32144 \\ 1\cdot 32064 \\ 1\cdot 31984 \end{array}$	55 54 53 52 51
10 11 12 13 14	.59014 .59037 .59061 .59084 .59108	.80730 .80713 .80696 .80679 .80662	.73100 .73144 .73189 .73234 .73278	$\begin{array}{r} 1.36800 \\ 1.36716 \\ 1.36633 \\ 1.36549 \\ 1.36466 \end{array}$	·60414 ·60437 ·60460 ·60483 ·60506	.79688 .79671 .79653 .79635 .79618	.75812 .75858 .75904 .75950 .75996	1.31904 1.31825 1.31745 1.31666 1.31586	50 49 48 47 46
15 16 17 18 19	.59131 .59154 .59178 .59201 .59225	-80644 -80627 -80610 -80593 -80576	·73323 ·73368 ·73413 ·73457 ·73502	$\begin{array}{r} 1.36383\\ 1.36300\\ 1.36217\\ 1.36134\\ 1.36051 \end{array}$	·60529 ·60553 ·60576 ·60599 ·60622	·79600 ·79583 ·79565 ·79547 ·79530	.76042 .76088 .76134 .76180 .76226	1.31507 1.31427 1.31348 1.31269 1.31190	45 44 43 42 41
20 21 22 23 24	·59248 ·59272 ·59295 ·59318 ·59342	·80558 ·80541 ·80524 ·80507 ·80489	·73547 ·73592 ·73637 ·73681 ·73726	$\begin{array}{r} 1.35968 \\ 1.35885 \\ 1.35802 \\ 1.35719 \\ 1.35637 \end{array}$	.60645 .60668 .60691 .60714 .60738	·79512 ·79494 ·79477 ·79459 ·79441	·76272 ·76318 ·76364 ·76410 ·76456	1.31110 1.31031 1.30952 1.30873 1.30795	40 39 38 37 36
25 26 27 28 29	.59365 .59389 .59412 .59436 .59459	.80472 .80455 .80438 .80420 .80403	·73771 ·73816 ·73861 ·73906 ·73951	1.35554 1.35472 1.35389 1.35307 1.35224	·60761 ·60784 ·60807 ·60830 ·60853	.79424 .79406 .79388 .79371 .79353	·76502 ·76548 ·76594 ·76640 ·76686	$ \begin{array}{r} 1 \cdot 30716 \\ 1 \cdot 30637 \\ 1 \cdot 30558 \\ 1 \cdot 30480 \\ 1 \cdot 30401 \end{array} $	35 34 33 32 31
30 31 32 33 34	.59482 .59506 .59529 .59552 .59576	.80386 .80368 .80351 .80334 .80316	.73996 .74041 .74086 .74131 .74176	1.35142 1.35060 1.34978 1.34896 1.34814	·60876 ·60899 ·60922 ·60945 ·60968	.79335 .79318 .79300 .79282 .79264	•76733 •76779 •76825 •76871 •76918	$1 \cdot 30323$ $1 \cdot 30244$ $1 \cdot 30166$ $1 \cdot 30087$ $1 \cdot 30009$	30 29 28 27 26
35 36 37 38 39	.59599 .59622 .59646 .59669 .59693	.80299 .80282 .80264 .80247 .80230	·74221 ·74267 ·74312 ·74357 ·74402	$\begin{array}{r} 1.34732 \\ 1.34650 \\ 1.34568 \\ 1.34487 \\ 1.34405 \end{array}$	.60991 .61015 .61038 .61061 .61084	79247 .79229 .79211 .79193 .79176	·76964 ·77010 ·77057 ·77103 ·77149	1.299311.298531.297751.296961.29618	25 24 23 22 21
40 41 42 43 44	.59716 .59739 .59763 .59786 .59809	.80212 .80195 .80178 .80160 .80143	.74447 .74492 .74538 .74583 .74628	$\begin{array}{r} 1.34323 \\ 1.34242 \\ 1.34160 \\ 1.34079 \\ 1.33998 \end{array}$	·61107 ·61130 ·61153 ·31176 ·61199	.79158 .79140 .79122 .79105 .79087	.77196 .77242 .77289 .77335 .77382	$\begin{array}{r} 1 \cdot 29541 \\ 1 \cdot 29463 \\ 1 \cdot 29385 \\ 1 \cdot 29307 \\ 1 \cdot 29229 \end{array}$	20 19 18 17 16
45 46 47 48 40	59832 59856 59879 59902 59926	.80125 .80108 .80091 .80073 .80056	•74674 •74719 •74764 •74810 •74855	$\begin{array}{r} 1.33916 \\ 1.33835 \\ 1.33754 \\ 1.33673 \\ 1.33592 \end{array}$	·61222 ·61245 ·61268 ·61291 ·61314	.79069 .79051 .79033 .79016 .78998	.77428 .77475 .77521 .77568 .77615	$1 \cdot 29152 \\ 1 \cdot 29074 \\ 1 \cdot 28997 \\ 1 \cdot 28919 \\ 1 \cdot 28842$	$15 \\ 14 \\ 13 \\ 12 \\ 11$
50 51 52 53 54	.59949 .59972 .59995 .60019 .60042	.80038 .80021 .80003 .79986 .79968	.74900 .74946 .74991 .75037 .75082	$\begin{array}{r} 1.33511 \\ 1.33430 \\ 1.33349 \\ 1.33268 \\ 1.33187 \end{array}$	·61337 ·61360 ·61383 ·61406 ·61429	·78980 ·78962 ·78944 ·78926 ·78908	·77661 ·77708 ·77754 ·77801 ·77848	$\begin{array}{r} 1\cdot 28764 \\ 1\cdot 28687 \\ 1\cdot 28610 \\ 1\cdot 28533 \\ 1\cdot 28456 \end{array}$	10 9 8 7 6
55 56 57 58 59	.60065 .60089 .60112 .60135 .60158	.79951 .79934 .79916 .79899 .79881	.75128 .75173 .75219 .75264 .75310	1.33107 1.33026 1.32946 1.32865 1.32785	.61451     .61474     .61497     .61520     .61543     .61543	·78891 ·78873 ·78855 ·78837 ·78837 78819	.77895 .77941 .77988 .78035 .78082	$\begin{array}{r} 1\cdot28379\\ 1\cdot28302\\ 1\cdot28225\\ 1\cdot28148\\ 1\cdot28071 \end{array}$	5 4 3 2 1
<u>60</u>	.60182 Cos.	.79864 Sin.	.75355 Cot.	<u>1.32704</u> Tan.	<u>.61566</u> Cos.	.78801 Sin.	. 78129 Cot.	<u>1.27994</u> Tan.	.  <u>_</u> 0
-		1				1	1		<u> </u>

52°

38°

**39°** 

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	Sin.	Cos.	Tan.	Cot.	Sin.	Cos.	Tan.	Cot.	1
0 1 2 3 4	.61566 .61589 .61612 .61635 .61658	·78801 ·78783 ·78765 ·78747 ·78729	.78129 .78175 .78222 .78269 .78316	1.27994 1.27917 1.27841 1.27764 1.27688	·62932 ·62955 ·62977 ·63000 ·63022	.77715 .77696 .77678 .77660 .77641	.80978 .81027 .81075 .81123 .81123	$1 \cdot 23490$ $1 \cdot 23416$ $1 \cdot 23343$ $1 \cdot 23270$ $1 \cdot 23196$	60 59 58 57 56
5 6 7 8 9	·61681 ·61704 ·61726 ·61749 ·61772	·78711 ·78694 ·78676 ·78658 ·78640	·78363 ·78410 ·78457 ·78504 ·78551	1.276111.275351.274581.273821.27306	$     \begin{array}{r}                                     $	·77623 ·77605 77586 ·77568 ·77550	·81220 ·81268 ·81316 ·81364 ·81413	1.231231.230501.229771.229041.22831	55 54 53 52 51
10 11 12 13 14	·61795 ·61818 ·61841 ·61864 ·61887	·78622 ·78604 ·78586 ·78568 ·78550	·78598 ·78645 ·78692 ·78739 ·78786	$ \begin{array}{r} 1 \cdot 27230 \\ 1 \cdot 27153 \\ 1 \cdot 27077 \\ 1 \cdot 27001 \\ 1 \cdot 26925 \end{array} $	-63158 -63180 -63203 -63225 -63248	·77531 ·77513 ·77494 ·77476 ·77458	·81461 ·81510 ·81558 ·81606 ·81655	$\begin{array}{r} 1 \cdot 22758 \\ 1 \cdot 22685 \\ 1 \cdot 22612 \\ 1 \cdot 22539 \\ 1 \cdot 22467 \end{array}$	50 49 48 47 46
15 16 17 18 19	·61909 ·61932 ·61955 ·61978 ·62001	·78532 ·78514 ·78496 ·78478 ·78460	·78834 ·78881 ·78928 ·78975 ·79022	1.268491.267741.266981.266221.26546	· 63271 · 63293 · 63316 · 63338 · 63361	·77439 ·77421 ·77402 ·77384 ·77366	.81703 .81752 .81800 .81849 .81898	$\begin{array}{r} 1 \cdot 22394 \\ 1 \cdot 22321 \\ 1 \cdot 22249 \\ 1 \cdot 22176 \\ 1 \cdot 22104 \end{array}$	45 44 43 42 41
20 21 22 23 24	·62024 ·62046 ·62069 ·62092 ·62115	·78442 ·78424 ·78405 ·78387 ·78369	.79070 .79117 .79164 .79212 .79259	1.26471 1.26395 1.26319 1.26244 1.26169	·63383 ·63406 ·63428 ·63451 ·63473	•77347 •77329 •77310 •77292 •77273	·81946 ·81995 ·82044 ·82092 ·82141	$\begin{array}{r} 1\cdot 22031 \\ 1\cdot 21959 \\ 1\cdot 21886 \\ 1\cdot 21814 \\ 1\cdot 21742 \end{array}$	40 39 38 37 36
25 26 27 28 29	·62138 ·62160 ·62183 ·62206 ·62229	·78351 ·78333 ·78315 ·78297 ·78279	·79306 ·79354 ·79401 ·79449 ·79496	1.26093 1.26018 1.25943 1.25867 1.25792	-63496 -63518 -63540 -63563 -63585	.77255 .77236 .77218 .77199 .77181	.82190 .82238 .82287 .82336 .82385	$\begin{array}{r} 1\cdot 21670 \\ 1\cdot 21598 \\ 1\cdot 21526 \\ 1\cdot 21454 \\ 1\cdot 21382 \end{array}$	35 34 33 32 31
30 31 32 33 34	·62251 ·62274 ·62297 ·62320 ·62342	·78261 ·78243 ·78225 ·78206 ·78188	.79544 .79591 .79639 .79686 .79734	1.25717 1.25642 1.25567 1.25492 1.25417	.63608 .63630 .63653 .63675 .63698	.77162 .77144 .77125 .77107 .77088	.82434 .82483 .82531 .82580 .82629	1.21310 1.21238 1.21166 1.21094 1.21023	30 29 28 27 26
35 36 37 38 39	·62365 ·62388 ·62411 ·62433 ·62456	·78170 ·78152 ·78134 ·78116 ·78098	.79781 .79829 .79877 .79924 .79972	$\begin{array}{r} 1 \cdot 25343 \\ 1 \cdot 25268 \\ 1 \cdot 25193 \\ 1 \cdot 25118 \\ 1 \cdot 25044 \end{array}$	-63720 -63742 -63765 -63787 -63810	·77070 ·77051 ·77033 ·77014 ·76996	·82678 ·82727 ·82776 ·82825 ·82874	$1 \cdot 20951$ $1 \cdot 20879$ $1 \cdot 20808$ $1 \cdot 20736$ $1 \cdot 20665$	25 24 23 22 21
40 41 42 43 44	·62479 ·62502 ·62524 ·62547 ·62570	.78079 .78061 .78043 .78025 .78007	·80020 ·80067 ·80115 ·80163 ·80211	$1 \cdot 24969$ $1 \cdot 24895$ $1 \cdot 24820$ $1 \cdot 24746$ $1 \cdot 24672$	·63832 ·63854 ·63877 ·63899 ·63922	·76977 ·76959 ·76940 ·76921 ·76903	·82923 ·82972 ·83022 ·83071 ·83120	$1 \cdot 20593 \\ 1 \cdot 20522 \\ 1 \cdot 20451 \\ 1 \cdot 20379 \\ 1 \cdot 20308$	20 19 18 17 16
45 46 47 48 49	.62592 .62615 .62638 .62660 .62683	.77988 .77970 .77952 .77934 .77916	·80258 ·80306 ·80354 ·80402 ·80450	$1 \cdot 24597 \\ 1 \cdot 24523 \\ 1 \cdot 24449 \\ 1 \cdot 24375 \\ 1 \cdot 24301$	·63944 ·63966 ·63989 ·64011 ·64033	·76884 ·76866 ·76847 ·76828 ·76810	·83169 ·83218 ·83268 ·83317 ·83366	$1 \cdot 20237 \\ 1 \cdot 20166 \\ 1 \cdot 20095 \\ 1 \cdot 20024 \\ 1 \cdot 19953$	15 14 13 12 11
50 51 52 53 54	·62706 ·62728 ·62751 ·62774 ·62796	·77897 ·77879 ·77861 ·77843 ·77824	.80498 .80546 .80594 .80642 .80690	$1 \cdot 24227 \\ 1 \cdot 24153 \\ 1 \cdot 24079 \\ 1 \cdot 24005 \\ 1 \cdot 23931$	· 64056 · 64078 · 64100 · 64123 · 64145	·76791 ·76772 ·76754 ·76735 ·76717	·83415 ·83465 ·83514 ·83564 ·83613	$\begin{array}{r} 1 \cdot 19882 \\ 1 \cdot 19811 \\ 1 \cdot 19740 \\ 1 \cdot 19669 \\ 1 \cdot 19599 \end{array}$	10 9 8 7 6
55 56 57 58 59	·62819 ·62842 ·62864 ·62887 ·62909	·77806 ·77788 ·77769 ·77751 ·77733	·80738 ·80786 ·80834 ·80882 ·80930	$1 \cdot 23858 \\ 1 \cdot 23784 \\ 1 \cdot 23710 \\ 1 \cdot 23637 \\ 1 \cdot 23563$	$     \begin{array}{r}                                     $	·76698 ·76679 ·76661 ·76642 ·76623	-83662 -83712 -83761 -83811 -83860	$\begin{array}{r} 1.19528 \\ 1.19457 \\ 1.19387 \\ 1.19316 \\ 1.19246 \end{array}$	5 4 3 2 1
<u>60</u>	<u>· 62932</u> Cos.	<u>.77715</u> Sin.	80978 Cot.	<u>1.23490</u> Tan.	<u>. 64279</u> Cos.	<u>· 76604</u> Sin.	<u>. 83910</u> Cot.	<u>1.19175</u> Tan.	-0
-		F	10	71	A	E	09		

51°

50°

**40°** 

**41°** 

		4	0°			4	1°		
1	Sin.	Cos.	Tan.	Cot.	Sin.	Cos.	Tan.	Cot.	1
01234	·64279 ·64301 ·64323 ·64346 ·64368	·76604 ·76586 ·76567 ·76548 ·76530	-83910 -83960 -84009 -84059 -84108	$1 \cdot 19175$ $1 \cdot 19105$ $1 \cdot 19035$ $1 \cdot 18964$ $1 \cdot 18894$	·65606 ·65628 ·65650 ·65672 ·65694	·75471 ·75452 ·75433 ·75414 ·75395	·86929 ·86980 ·87031 ·87082 ·87133	1.15037 1.14969 1.14902 1.14834 1.14767	60 59 58 57 56
5 6 7 8 9	·64390 ·64412 ·64435 ·64457 ·64479	·76511 ·76492 ·76473 ·76455 ·76436	.84158 .84208 .84258 .84307 .84357	1.18824 1.18754 1.18684 1.18614 1.18544	·65716 ·65738 ·65759 ·65781 ·65803	·75375 ·75356 ·75337 ·75318 ·75299	·87184 ·87236 ·87287 ·87338 ·87389	1.14699 1.14632 1.14565 1.14498 1.14430	55 54 53 52 51
10 11 12 13 14	· 64501 · 64524 · 64546 · 64568 · 64590	·76417 ·76398 ·76380 ·76361 ·76342	- 84407 - 84457 - 84507 - 84556 - 84606	1.18474 1.18404 1.18334 1.18264 1.18194	·65825 ·65847 ·65869 ·65891 ·65913	·75280 ·75261 ·75241 ·75222 ·75203	·87441 ·87492 ·87543 ·87595 ·87646	$1.14363 \\ 1.14296 \\ 1.14229 \\ 1.14162 \\ 1.14095$	50 49 48 47 46
15 16 17 18 19	.64612     .64635     .64657     .64679     .64701	•76323 •76304 •76286 •76267 •76248	.84656 .84706 .84756 .84806 .84856	$1.18125 \\ 1.18055 \\ 1.17986 \\ 1.17916 \\ 1.17846 \\ 1.17846 \\ 1.17846 \\ 1.17846 \\ 1.17846 \\ 1.17846 \\ 1.17846 \\ 1.1846 \\$	·65935 ·65956 ·65978 ·66000 ·66022	·75184 ·75165 ·75146 ·75126 ·75107	·87698 ·87749 ·87801 ·87852 ·87904	1.14028 1.13961 1.13894 1.13828 1.13761	45 44 43 42 41
20 21 22 23 24	·64723 ·64746 ·64768 ·64790 ·64812	·76229 ·76210 ·76192 ·76173 ·76154	·84906 ·34956 ·85006 ·85057 ·85107	$1.17777 \\ 1.17708 \\ 1.17638 \\ 1.17569 \\ 1.17500 \\ 1.17$	·66044 ·66066 ·66088 ·66109 ·66131	·75088 ·75069 ·75050 ·75030 ·75011	.87955 .88007 .88059 .88110 .88162	$\begin{array}{r} 1 \cdot 13694 \\ 1 \cdot 13627 \\ 1 \cdot 13561 \\ 1 \cdot 13494 \\ 1 \cdot 13428 \end{array}$	40 39 38 37 36
25 26 27 28 29	·64834 ·64856 ·64878 ·64901 ·64923	·76135 ·76116 ·76097 ·76078 ·76059	·85157 ·85207 ·85257 ·85308 ·85358	$\begin{array}{r} 1 \cdot 17430 \\ 1 \cdot 17361 \\ 1 \cdot 17292 \\ 1 \cdot 17223 \\ 1 \cdot 17154 \end{array}$	·66053 ·66175 ·66197 ·66218 ·66240	·74992 ·74973 ·74953 ·74934 ·74915	-88204 -88265 -88317 -88369 -88421	1.133611.132951.132281.131621.13096	35 34 33 32 31
30 31 32 33 34	·64945 ·64967 ·64989 ·65011 ·65033	·76041 ·76022 ·76003 ·75984 ·75965	·85408 ·85458 ·85509 ·85559 ·85609	1.170851.170161.169471.168781.16809	·66262 ·66284 ·66306 ·66327 ·66349	·74896 ·74876 ·74857 ·74838 ·74818	-88473 -88524 -88576 -88628 -88680	$\begin{array}{r} 1 \cdot 13029 \\ 1 \cdot 12963 \\ 1 \cdot 12897 \\ 1 \cdot 12831 \\ 1 \cdot 12765 \end{array}$	30 29 28 27 26
35 36 37 38 39	·65055 ·65077 ·65100 ·65122 ·65144	·75946 ·75927 ·75908 ·75889 ·75870	·85660 ·85710 ·85761 ·85811 ·85862	$\begin{array}{r} 1 \cdot 16741 \\ 1 \cdot 16672 \\ 1 \cdot 16603 \\ 1 \cdot 16535 \\ 1 \cdot 16466 \end{array}$	$     \begin{array}{r}                                     $	·74799 ·74780 ·74760 ·74741 <u>·74722</u>	-88732 -88784 -88836 -88888 -88888 -88940	$\begin{array}{r} 1 \cdot 12699 \\ 1 \cdot 12633 \\ 1 \cdot 12567 \\ 1 \cdot 12501 \\ 1 \cdot 12435 \end{array}$	25 24 23 22 21
40 41 42 43 44	-65166 -65188 -65210 -65232 -65254	·75851 ·75832 ·75813 ·75794 ·75775	-85912 -85963 -86014 -86064 -86115	$\begin{array}{r} 1 \cdot 16398 \\ 1 \cdot 16329 \\ 1 \cdot 16261 \\ 1 \cdot 16192 \\ 1 \cdot 16124 \end{array}$	-66480 -66501 -66523 -66545 -66566	·74703 ·74683 ·74664 ·74644 ·74525	-88992 -89045 -89097 -89149 -89201	$\begin{array}{c} 1\cdot 12369\\ 1\cdot 12303\\ 1\cdot 12238\\ 1\cdot 12172\\ 1\cdot 12106\end{array}$	20 19 18 17 16
45 46 47 48 49	-65276 -65298 -65320 -65342 -65364	·75756 ·75738 ·75719 ·75700 ·75680	·86166 86216 ·86267 ·86318 ·86368	$\begin{array}{r} 1.16056 \\ 1.15987 \\ 1.15919 \\ 1.15851 \\ 1.15783 \end{array}$	- 66588 - 66610 - 66632 - 66653 - 66675	·74606 ·74586 ·74567 ·74548 ·74528	-89253 -89306 -89358 -89410 -89463	$\begin{array}{r} 1.12041 \\ 1.11975 \\ 1.11909 \\ 1.11844 \\ 1.11778 \end{array}$	$     \begin{array}{r}       15 \\       14 \\       13 \\       12 \\       11     \end{array} $
50 51 52 53 54	-65386 -65408 -65430 -65452 -65474	·75661 ·75642 ·75623 ·75604 ·75585	-86419 -86470 -86521 -86572 -86623	$\begin{array}{r} 1.15715 \\ 1.15647 \\ 1.15579 \\ 1.15511 \\ 1.15443 \end{array}$	-66697 -66718 -66740 -66762 -66783	·74509 ·74489 ·74470 ·74451 ·74431	- 89515 - 89567 - 89620 - 89672 - 89725	$\begin{array}{r} 1 \cdot 11713 \\ 1 \cdot 11648 \\ 1 \cdot 11582 \\ 1 \cdot 11517 \\ 1 \cdot 11452 \end{array}$	10 9 8 7 6
55 56 57 58 59	-65496 -65518 -65540 -65562 -65584	·75566 ·75547 ·75528 ·75509 ·75490	-86674 -86725 -86776 -86827 -86878	1.153751.153081.152401.151721.15104	·66805 ·66827 ·66848 ·66870 ·66891	·74412 ·74392 ·74373 ·74353 ·74334	.89777 .89830 .89883 .89935 .89988	$\begin{array}{r} 1.11387 \\ 1.11321 \\ 1.11256 \\ 1.11191 \\ 1.11126 \end{array}$	5 4 3 2 1
<u>60</u>	<u>•65606</u> Cos.	.75471 Sin.	<u>·86929</u> Cot.	<u>1.15037</u> Tan.	<u>· 66913</u> Cos.	<u>.74314</u> Sin.	<u>.90040</u> Cot.	<u>1.11061</u> Tan.	-
1	·	,	100	7	15		129		

49°

**48°** 

IUI	SLE 1A	NATU. 4	2°	125, 0051	43°					
	Sin.	Cos.	Tan.	Cot.	Sin.	Cos.	Tan.	Cot.	,	
01234	•66913 •66935 •66956 •66978 •66999	·74314 ·74295 ·74276 ·74256 ·74237	.90040 .90093 .90146 .90199 .90251	1.11061 1 10996 1.10931 1.10867 1.10802	·68200 ·68221 ·68242 ·68264 ·68285	·73135 ·73116 ·73096 ·73076 ·73056	·93252 ·93306 ·93360 ·93415 ·93469	1.072371.071741.071121.070491.06987	60 59 58 57 56	
5	.67021	.74217	.90304	1.107371.106721.106071.105431.10478	68306	·73036	·93524	1.06925	55	
6	67043	.74198	.90357		68327	·73016	·93578	1.06862	54	
7	.67064	.74178	.90410		68349	·72996	·93633	1.06800	53	
8	.67086	.74159	.90463		68370	·72976	·93688	1.06738	52	
9	.67107	.74139	.90516		68391	·72957	·93742	1.06676	51	
10 11 12 13 14	.67129 .67151 .67172 .67194 .67215	.74120 .74100 .74080 .74061 .74041	·90569 ·90621 ·90674 90727 ·90781	1.10414 1.10349 1.10285 1.10220 1.10156	·68412 ·68434 ·68455 ·68476 ·68497	.72937 .72917 .72897 .72877 .72877 .72857	·93797 ·93852 ·93906 ·93961 ·94016	1.06613 1.06551 1.06489 1.06427 ,1.06365	50 49 48 47 46	
15	·67237	.74022	·90834	1.10091	-68518	.72837	.94071	1.06303	45	
16	·67258	.74002	·90887	1.10027	-68539	.72817	.94125	1.06241	44	
17	·67280	.73983	·90940	1.09963	-68561	.72797	.94180	1.06179	43	
18	·67301	.73963	·90993	1.09899	-68582	.72777	.94235	1.06117	42	
19	·67323	.73944	·91046	1.09834	-68603	.72757	.94290	1.06056	41	
20	·67344	.73924	.91099	1.09770	· 68624	.72737	.94345	1.059941.059321.058701.058091.05747	40	
21	·67366	.73904	.91153	1.09706	· 68645	.72717	.94400		39	
22	·67387	.73885	.91206	1.09642	· 68666	.72697	.94455		38	
23	·67409	.73865	.91259	1.09578	· 68688	.72677	.94510		37	
24	·67430	.73846	.91313	1.09514	· 68709	.72657	.94565		36	
25	67452	·73826	.91365	$\begin{array}{c} 1.09450 \\ 1.09386 \\ 1.09322 \\ 1.09258 \\ 1.09195 \end{array}$	.68730	·72637	.94620	1.05685	35	
26	.67473	·73806	.91419		.68751	·72617	.94676	1.05624	34	
27	.67495	·73787	.91473		.68772	·72597	.94731	1.05562	33	
28	.67516	·73767	.91526		.68793	·72577	.94786	1.05501	32	
29	.67538	·73747	.91580		.68814	·72557	.94841	1.05439	31	
30	.67559	·73728	·91633	1.09131	· 68835	·72537	·94896	1.05378	30	
31	.67580	·73708	·91687	1.09067	· 68857	·72517	·94952	1.05317	29	
32	.67602	·73688	·91740	1.09003	· 68878	·72497	·95007	1.05255	28	
33	.67623	·73669	·91794	1.08940	· 68899	·72477	·95062	1.05194	27	
34	.67645	·73649	·91847	1.08876	· 68920	·72457	·95118	1.05133	26	
35	·67668	.73629	.91901	1.08813	·68941	.72437	·95173	1.05072	25	
36	·67688	.73610	.91955	1.08749	·68962	.72417	·95229	1.05010	24	
37	·67709	.73590	.92008	1.08686	·68983	.72397	·95284	1.04949	23	
38	·67730	.73570	.92062	1.08622	·69004	.72377	·95340	1.04888	22	
39	·67752	.73551	.92116	1.08559	·69025	.72357	·95395	1.04827	21	
40	·67773	.73531	·92170	1.08496	·69046	.72337	.95451	$1.04766 \\ 1.04705 \\ 1.04644 \\ 1.04583 \\ 1.04522$	20	
41	·67795	.73511	·92224	1.08432	·69067	.72317	.95506		19	
42	·67816	.73491	·92277	1.08369	·69088	.72297	.95562		18	
43	·67837	.73472	·92331	1.08306	·69109	.72277	.95618		17	
44	·67859	.73452	·92385	1.08243	·69130	.72257	.95673		16	
45 46 47 48 49	·67880 ·67901 ·67923 ·67944 ·67965	·73432 ·73413 ·73393 ·73373 ·73353	·92439 ·92493 ·92547 ·92601 ·92655	1.081791.081161.080531.079901.07927	.69151 .69172 .69193 .69214 .69235	·72236 ·72216 ·72196 ·72176 ·72156	.95729 .95785 .95841 .95897 .95952	$\begin{array}{r} 1.04461 \\ 1.04401 \\ 1.04340 \\ 1.04279 \\ 1.04218 \end{array}$	15 14 13 12 11	
50 51 52 53 54	·67987 ·68008 ·68029 ·68051 ·68072	·73333 ·73314 ·73294 ·73274 ·73254	.92709 .92763 .92817 .92872 .92926	1.078641.078011.077381.076781.07613	·69256 ·69277 ·69298 ·69319 ·69340	.72136 .72116 .72095 .72075 .72055	·96008 ·96064 ·96120 ·96176 ·96232	$\begin{array}{r} 1.04158 \\ 1.04097 \\ 1.04036 \\ 1.03976 \\ 1.03915 \end{array}$	10 9 8 7 6	
55 56 57 58 59	·68093 ·68115 ·68136 ·68157 ·68179	·73234 ·73215 ·73195 ·73175 ·73155	.92980 .93034 .93088 .93143 .93197	$\begin{array}{r} 1.07550\\ 1.07487\\ 1.07425\\ 1.07362\\ 1.07299 \end{array}$	·69361 ·69382 ·69403 ·69424 ·69445	·72035 ·72015 ·71995 ·71974 ·71954	·96288 ·96344 ·96400 96457 ·96513	$\begin{array}{r} 1.03855\\ 1.03794\\ 1.03734\\ 1.03674\\ 1.03613\end{array}$	54321	
<u>60</u>	<u>· 68200</u>	<u>• 73135</u>	<u>. 93252</u>	<u>1.07237</u>	<u>· 69466</u>	71934	<u>· 96569</u>	1.03553	-9	
/	Cos.	Sin.	Cot.	Tan.	Cos.	Sin.	Cot.	Tan.		

TABLE IX.—NATURAL SINES, COSINES, TANGENTS, AND COTANGENTS 44° 44°

		-	•								
	Sin.	Cos.	Tan.	Cot.	'	1	Sin.	Cos.	Tan.	Cot.	1
0-1934	.69529	·71934 ·71914 ·71894 ·71873 ·71853	·96625 ·96681 ·96738	1.03553 1.03493 1.03433 1.03372 1.03312	60 59 58 57 56	30 31 32 33 34	.70091 .70112 .70132 .70153 .70174	•71325 •71305 •71284 •71264 •71243	·98327 ·98384 ·98441	1.01761 1.01702 1.01642 1.01583 1.01524	30 29 28 27 26
56789	·69570 ·69591 ·69612 ·69633 ·69654	·71833 ·71813 ·71792 ·71772 ·71752	·96907 ·96963 ·97020	1.03132	55 54 53 52 51	35 36 37 38 39	·70195 ·70215 ·70236 ·70257 ·70277	·71223 ·71203 ·71182 ·71162 ·71141	·98613 ·98671 ·98728	1.01465 1.01406 1.01347 1.01288 1.01229	25 24 23 22 21
10 411 412 13 114	·69675 ·69696 ·69717 ·69737 ·69758	.71732 .71711 .71691 .71671 .71650	·97189 ·97246 ·97302	1 02952 1.02892 1.02832 1.02772 1.02773	50 49 48 47 46	40 41 42 43 44	·70298 ·70319 ·70339 ·70360 ·70381	·71100 ·71080 ·71059	.98901 .98958 .99016	1.011701.011121.010531.009941.00935	20 19 18 17 16
15 16 17 18	·69779 ·69800 ·69821 ·69842 ·69862	.71630 .71610 .71590 .71569 .71549	·97472 ·97529	1.02653 1.02593 1.02533 1.02474 1.02414	45 44 43 42 41	45 46 47 48 49	·70401 ·70422 70443 ·70463 ·70484	· 70998 · 70978 · 70957	·99189 ·99247	1.00876 1.00818 1.00759 1.00701 1.00642	15 14 13 12 11
20 21 22 23 24	.69946	·71529 ·71508 ·71488 ·71468 ·71447	·97756 ·97813 ·97870	1.023551.022951.022361.021761.02117	40 39 38 37 36	50 51 52 53 54		· 70896 · 70875 · 70855	·99478 ·99536 ·99594	$1.00583 \\ 1.00525 \\ 1.00467 \\ 1.00408 \\ 1.00350$	10 9 8 7 6
25 26 27 28 29	· 69987 · 70008 · 70029 · 70049 · 70070	·71386 ·71366	98041 98098 98155	1.02057 1.01998 1.01939 1.01879 1.01820	35 34 33 32 31	55 56 57 58 59	· 70608 · 70628 · 70649 · 70670 · 70690	·70793 ·70772 ·70752	·99768 ·99826 ·99884	1.00291 1.00233 1.00175 1.00116 1.00058	6 5 4 3 2 1
30	• 70091 Cos.	<u>.71325</u> Sin.	<u>. 98270</u> Cot.	<u>1.01761</u> Tan.	30	<u>60</u> ′	<u>. 70711</u> Cos.	<u>.70711</u> Sin.	$\frac{1.00000}{\text{Cot.}}$	<u>1.00000</u> Tan.	<b></b> 0

**45°** 

717

TABLE X.—NATURAL VERSED SINES AND EXTERNAL SECANTS.0°1°2°3°									
,	Vers.	Ex. sec.	Vers.	Ex. sec.	Vers.	Ex. sec.	Vers.	Ex. sec.	•
0	.00000	.00000	.00015	.00015	·00061	.00061	·00137	.00137	01234
1	.00000	.00000	.00016	.00016	·00062	.00062	·00139	.00139	
2	.00000	.00000	.00016	.00016	·00063	.00063	·00140	.00140	
3	.00000	.00000	.00017	.00017	·00064	.00064	·00142	.00142	
4	.00000	.00000	.00017	.00017	·00065	.00065	·00143	.00143	
5	· 00000	.00000	·00018	·00018	·00066	·00066	·00145	.00145	5
6	· 00000	.00000	·00018	·00018	·00067	·00067	·00146	.00147	6
7	· 00000	.00000	·00019	·00019	·00068	·00068	·00148	.00148	7
8	· 00000	.00000	·00020	·00020	·00069	·00069	·00150	.00150	8
9	· 00000	.00000	·00020	·00020	·00070	·00070	·00151	.00151	9
10 11 12 13 14	.00000 .00001 .00001 .00001 .00001	.00000 .00001 .00001 .00001 .00001	.00021 .00021 .00022 .00023 .00023	00021 00021 00022 00023 00023	-00071 -00073 -00074 -00075 -00076	.00072 .00073 .00074 .00075 .00076	00153 00154 00156 00158 00158 00159	00153 00155 00156 00158 00158 00159	10 11 12 13 14
15	.00001	.00001	·00024	$\begin{array}{r} .00024\\ .00024\\ .00025\\ .00026\\ .00026\\ .00026\end{array}$	·00077	.00077	.00161	.00161	15
16	.00001	.00001	·00024		·00078	.00078	.00162	.00163	16
17	.00001	.00001	·00025		·00079	.00079	.00164	.00164	17
18	.00001	.00001	·00026		·00081	.00081	.00166	.00166	18
19	.00001	.00002	·00026		·00082	.00082	.00168	.00168	19
20 21 22 23 24	·00002 ·00002 ·00002 ·00002 ·00002 ·00002	.00002 .00002 .00002 .00002 .00002	·00027 ·00028 ·00028 ·00029 ·00030	$\begin{array}{r} \cdot \ 00027 \\ \cdot \ 00028 \\ \cdot \ 00028 \\ \cdot \ 00029 \\ \cdot \ 00030 \end{array}$	· 00083 · 00084 · 00085 · 00087 · 00088	·00083 ·00084 ·00085 ·00087 ·00088	.00169 .00171 .00173 .00174 .00176	·00169 ·00171 ·00173 ·00175 ·00176	20 21 22 23 24
25	.00003	$\begin{array}{r} \cdot 00003 \\ \cdot 00003 \\ \cdot 00003 \\ \cdot 00003 \\ \cdot 00004 \end{array}$	·00031	.00031	00089	·00089	.00173	·00178	25
26	.00003		·00031	.00031	00090	·00090	.00179	·00180	26
27	.00003		·00032	.00032	00091	·00091	.00181	·00182	27
28	.00003		·00033	.00033	00093	·00093	.00183	·00183	28
29	.00004		·00034	.00034	00093	·00094	.00185	·00185	29
30	.00004	00004	·00034	.00034	00095	.00095	00187	.00187	30
31	.00004	00004	·00035	.00035	00096	.00097	00188	.00189	31
32	.00004	00004	·00036	.00036	00098	.00098	00190	.00190	32
33	.00005	00005	·00037	.00037	00099	.00099	00192	.00192	33
34	.00005	00005	·00037	.00037	00099	.00100	00192	.00194	34
35	.00005	.00005	·00038	$00038 \\ 00039 \\ 00040 \\ 00041 \\ 00041$	·00102	00102	·00196	.00196	35
36	.00005	.00005	·00039		·00103	00103	·00197	.00198	36
37	.00006	.00006	·00040		·00104	00104	·00199	.00200	37
38	.00006	.00006	·00041		·00106	00106	·00201	.00201	38
39	.00006	.00006	·00041		·00107	00107	·00203	.00203	39
40	· 00007	·00007	· 00042	00042	·00108	·00108	·00205	·00205	40
41	· 00007	·00007	· 00043	00043	·00110	·00110	·00207	·00207	41
42	· 00007	·00007	· 00044	00044	·00111	·00111	·00208	·00209	42
43	· 00008	·00008	· 00045	00045	·00112	·00113	·00210	·00211	43
44	· 00008	·00008	· 00046	00046	·00114	·00114	·00212	·00213	44
45	·00009	·00009	·00047	00047	·00115	·00115	·00214	00215	45
46	·00009	·00009	00048	00048	·00'17	·00117	·00216	. ' 0216	46
47	·00009	·00009	·00048	00048	·00118	·00118	·00218	. 00218	47
47	·00010	·00010	·00049	00049	·00119	·00120	·00220	. 00220	48
49	·00010	·00010	·00050	00050	·00121	·00121	·00222	. 00222	49
50	·00011	·00011	·00051	$ \begin{array}{r} \cdot \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \$	·00122	·00122	· 00224	·00224	50
51	·00011	·00011	·00052		·00124	·00124	· 00226	·00226	51
52	·00011	·00011	·00053		·00125	·00125	· 00228	·00228	52
53	·00012	·00012	·00054		·00127	·00127	· 00230	·00230	53
54	·00012	·00012	·00055		·00128	·00128	· 00232	·00232	54
55	·00013	·00013	00056	·00056	·00130	·00130	·00234	·00234	55
56	·00013	·00013	00057	·00057	·00131	·00131	·00236	·00236	56
57	·00014	·00014	00058	·00058	·00133	00133	·00238	·00238	57
58	·00014	·00014	00059	·00059	·00134	·00134	·00240	·00240	58
59	·00014	·00015	00060	00060	·00136	·00136	·00242	·00242	59
60	00015	.00015	.00061	·00061	· 00137	·00137	.00244	•00244	60

TABLE X .--- NATURAL VERSED SINES AND EXTERNAL SECANTS.

	4	1°	ł	5°		6°		7°	
1	Vers.	Ex. sec.	Vers.	Ex. sec.	Vers.	Ex. sec.	Vers.	Ex. sec.	,
0 1 2 3 4	·00244 ·00246 ·00248 ·00250 ·00250	·00244 ·00246 ·00248 ·00250 ·00252	·00381 ·00383 ·00386 ·00388 ·00388 ·00391	·00382 ·00385 ·00387 ·00390 ·00392	·00548 ·00551 ·00554 ·00557 ·00560	·00551 ·00554 ·00557 ·00560 ·00563	·00745 ·00749 ·00752 ·00756 ·00760	·00751 ·00755 ·00758 ·00762 ·00765	0 1 2 3 4
5 6 7 8 9	·00254 ·00256 ·00258 ·00260 ·00262	00254 00257 00259 00261 00263	·00393 ·00396 ·00398 ·00401 ·00404	00395 00397 00400 00403 00405	·00563 ·00566 ·00569 ·00572 ·00576	·00566 ·00569 ·00573 ·00576 ·00579	· 00763 · 00767 · 00770 · 00774 · 00778	.00769 .00773 .00776 .00780 .00784	5 6 7 8 9
10 11 12 13 14	00264 00266 00269 00271 00273	.00265 .00267 .00269 .00271 .00274	.00406 .00409 .00412 .00114 .00417	00408 00411 00413 00416 00419	00579 00582 00585 00588 00588	.00582 .00585 .00588 .00588 .00592 .00595	·00781 ·00785 ·00789 00792 ·00796	.00787 .00791 .00795 .00799 .00802	10 11 12 13 14
15 16 17 17 18 18 19	.00275 .00277 .00279 .00281 .00284	.00276 .00278 .00280 .00282 .00284	·00420 ·00422 ·00425 ·00428 ·00430	00421 00424 00427 00429 00432	00594 .00598 .00601 .00604 .00607	.00598 .00601 .00604 .00608 .00611	·00800 ·00803 ·00807 ·00811 ·00814	.00806 .00810 .00813 .00817 .00821	15 16 17 18 19
20 21 22 23 23 24	·00286 ·00288 ·00290 ·00293 ·00295	·00287 ·00289 ·00291 ·00293 ·00296	·00433 ·00436 ·00438 ·00441 ·00444	$\begin{array}{r} \cdot 00435 \\ \cdot 00438 \\ \cdot 00440 \\ \cdot 00443 \\ \cdot 00446 \end{array}$	·00610 ·00614 ·00617 ·00620 ·00623	$\begin{array}{r} 00614 \\ \cdot 00617 \\ \cdot 00621 \\ \cdot 00624 \\ \cdot 00627 \end{array}$	•00818 •00822 •00825 •00829 •00833	00825 00828 00832 00836 00840	20 21 22 23 24
25 26 27 28 29	·00297 ·00299 ·00301 ·00304 ·00306	.00298 .00300 .00302 .00305 .00307	·00447 ·00449 ·00452 ·00455 ·00458	$\begin{array}{r} .00449\\ .00451\\ .00454\\ .00457\\ .00457\\ .00460\end{array}$	·00626 ·00630 ·00633 ·00636 ·00640	00630 00634 00637 00640 00644	·00837 ·00840 ·00844 ·00848 ·00852	.00844 .00848 .00851 .00855 .00859	25 26 27 28 29
30 131 32 33 34	.00308 .00311 .00313 .00315 .00317	.00309 .00312 .00314 .00316 .00318	·00460 ·00463 ·00466 ·00469 ·00472	·00463 ·00465 ·00468 ·00471 ·00474	· 00643 · 00646 · 00649 · 00653 · 00656	00647 00650 00654 00657 00660	00856 00859 00863 00867 00867	.00863 .00867 .00871 .00875 .00878	30 31 32 33 34
35 36 37 38 39	-00320 -00322 -00324 -00327 -00329	.00321 .00323 .00326 .00328 .00330	·00474 ·00477 ·00480 ·00483 ·00486	00477 00480 00482 00485 00485	·00659 ·00663 ·00666 ·00669 ·00673	·00664 ·00667 ·00671 ·00674 ·00677	·00875 ·00878 ·00882 ·00886 ·00890	.00882 .00886 .00890 .00894 .00898	35 36 37 38 39
40 41 42 43 44	.00332 .00334 .00336 .00339 .00341	$\begin{array}{r} .00333 \\ .00335 \\ .00337 \\ .00340 \\ .00342 \end{array}$	·00489 ·00492 ·00494 ·00497 ·00500	·00491 ·00494 ·00497 ·00500 ·00503	·00676 ·00680 ·00683 ·00686 ·00690	00681 00684 00688 00691 00695	·00894 ·00898 ·00902 ·00906 ·00909	.00902 .00906 .00910 .00914 .00918	$\begin{array}{r} 40 \\ 41 \\ 42 \\ 43 \\ 44 \end{array}$
45 46 47 48 49	.00343 .00346 .00348 .00351 .00353	00345 00347 00350 00352 00354	.00503 .00506 .00509 .00512 .00515	.00506 .00509 .00512 .00515 .00518	- 00693 - 00607 - 00700 - 00703 - 00707	.00698 .00701 .00705 .00708 .00712	·00913 ·00917 00921 00925 ·00929	.00922 .00926 .00930 .00934 .00938	45 46 47 48 49
50 51 52 53 54	00356 00358 00361 00363 00365	.00357 .00359 .00362 .00364 .00367	$\begin{array}{r} .00518\\ .00521\\ .00524\\ .00527\\ .00530\end{array}$	00521 00524 00527 00530 00533	.00710 .00714 .00717 .00721 .00724	00715 00719 00722 00726 00730	·00933 00937 ·00941 ·00945 ·00949	00942 00946 00950 00954 00958	50 51 52 53 54
55 56 57 58 59	-00368 -00370 -00373 -00375 -00378	·00369 ·00372 ·00374 ·00377 ·00377 ·00379	·00533 ·00536 ·00539 ·00542 ·00545	00536 00539 00542 00545 00548	·00728 ·00731 ·00735 ·00738 ·00742	00733 00737 00740 00744 00744 00747	·00953 ·00957 ·00961 ·00965 ·00969	.00962 .00966 .00970 .00975 .00979	55 56 57 58 59
60	.00381	•00382	00548	·00551	·00745	.00751	.00973	.00983	60

TABLE X .- NATURAL VERSED SINES AND EXTERNAL SECANTS.

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	8	8°	9	9°	1	.0°	1	1°	
,	Vers.	Ex. sec.	Vers.	Ex. sec.	Vers.	Ex. sec.	Vers.	Ex. sec.	
0 1 2 3 4	.00973 .00977 .00981 .00985 .00989	00983 00987 00991 00995 00999	·01231 ·01236 ·01240 ·01245 ·01249	01247 01251 01256 01261 01265	$\begin{array}{r} \cdot 01519 \\ \cdot 01524 \\ \cdot 01529 \\ \cdot 01534 \\ \cdot 01540 \end{array}$	01543 01548 01553 01558 01564	·01837 ·01843 ·01848 ·01854 ·01854 ·01860	01872 01877 01883 01889 01895	0 1 2 3 4
5 6 7 8 9	00994 00998 01002 01006 01010	0.01004 0.01008 0.01012 0.01016 0.01020	·01254 ·01259 ·01263 ·01268 ·01272	0.01270 0.01275 0.01279 0.01284 0.01289	01545 01550 01555 01560 01565	01569 01574 01579 01585 01590	·01865 ·01871 ·01876 ·01882 ·01888	·01901 ·01906 ·01912 ·01918 ·01924	56789 1
$     \begin{array}{c}       10 \\       11 \\       12 \\       13 \\       14     \end{array}   $	.01014 .01018 .01022 .01027 .01031	0.01024 0.01029 0.0033 0.0037 0.0041	·01277 ·01282 ·01286 ·01291 ·01296	01294 01298 01303 01308 01313	.01570 .01575 .01580 .01586 .01591	0.01595 0.01601 0.01606 0.01611 0.01616	·01893 ·01899 ·01904 ·01910 ·01916	·01930 ·01936 ·01941 ·01947 ·01953	10 11 12 13 14
$15 \\ 16 \\ 17 \\ 18 \\ 19 \\ 28 \\ 19 \\ 28 \\ 19 \\ 29 \\ 15 \\ 15 \\ 15 \\ 15 \\ 15 \\ 15 \\ 15 \\ 1$	·01035 ·01039 ·01043 ·01047 ·01052	01046 01050 01054 01059 01063	·01300 ·01305 ·01310 ·01314 ·01319	0.01318 0.01322 0.01327 0.01332 0.01337	·01596 ·01601 ·01606 ·01612 ·01617	01622 01627 01633 01638 01643	0.01921 0.01927 0.01933 0.01939 0.01944	.01959 .01965 .01971 .01977 .01983	15 16 17 18 19
20 21 22 23 24	01056 01060 01064 01069 01073	0.01067 0.01071 0.01076 0.01080 0.01084	·01324 ·01329 ·01333 ·01338 ·01343	$\begin{array}{r} .01342 \\ .01346 \\ .01351 \\ .01356 \\ .01361 \end{array}$	·01622 ·01627 ·01632 ·01638 ·01643	01649 01654 01659 01665 01670	·01950 ·01956 ·01961 ·01967 ·01973	$\begin{array}{r} .01989\\ .01995\\ .02001\\ .02007\\ .02013\\ \end{array}$	20 21 22 23 24
25 26 27 28 29	.01077 .01081 .01086 .01090 .01094	0.01089 0.01093 0.01097 0.01102 0.01106	·01348 ·01352 ·01357 ·01362 ·01367	.01366 .01371 .01376 .01381 .01386	·01648 ·01653 ·01659 ·01664 ·01669	01676 01681 01687 01692 01698	·01979 ·01984 ·01990 ·01996 ·02002	02019 02025 02031 02037 02043	25 26 27 28 29
30 31 32 33 34	·01098 ·01103 ·01107 ·01111 ·01116	$\begin{array}{r} .01111\\ .01115\\ .01119\\ .01124\\ .01128\end{array}$	·01371 ·01376 ·01381 ·01386 ·01391	0.01391 0.01395 0.01400 0.01405 0.01410	·01675 ·01680 ·01685 ·01690 ·01696	0.01703 0.01709 0.01714 0.01720 0.01725	·02008 ·02013 ·02019 ·02025 ·02031	.02049 .02055 .02061 .02067 .02073	30 31 32 33 34
35 36 37 38 39	·01120 ·01124 ·01129 ·01133 ·01137	$\begin{array}{r} .01133\\ .01137\\ .01142\\ .01146\\ .01151\end{array}$	·01396 ·01400 ·01405 ·01410 ·01415	$\begin{array}{r} .01415 \\ .01420 \\ .01425 \\ .01430 \\ .01435 \end{array}$	.01701 .01706 .01712 .01717 .01723	.01731 .01736 .01742 .01747 .01753	·02037 ·02042 ·02048 ·02054 ·02054 ·02060	·02079 ·02085 ·02091 ·02097 ·02103	35 36 37 38 39
40 41 42 43 44	·01142 ·01146 ·01151 ·01155 ·01159	01155 01160 01164 01169 01173	·01420 ·01425 ·01430 ·01435 ·01439	01440 01445 01450 01455 01461	·01728 ·01733 ·01739 ·01744 ·01750	.01758 .01764 .01769 .01775 .01781	·02066 ·02072 ·02078 ·02084 ·02090	$\begin{array}{r} .02110\\ .02116\\ .02122\\ .02128\\ .02128\\ .02134\end{array}$	40 41 42 43 44
45 46 47 48 49	·01164 ·01168 ·01173 ·01177 ·01182	.01178 .01182 .01187 .01191 .01196	·01444 ·01449 ·01454 ·01459 ·01464	01466 01471 01476 01481 01486	.01755 .01760 .01766 .01771 .01777	01786 .01792 .01793 .01803 .01809	·02095 ·02101 ·02107 ·02113 ·02113	02140 02146 02153 02159 02165	45 46 47 48 49
50 51 52 53 54	·01186 ·01191 ·01195 ·01200 ·01204	.01200 .01205 .01209 .01214 .01219	·01469 ·01474 ·01479 ·01484 ·01489	·01491 ·01496 ·01501 ·01506 ·01512	·01782 ·01788 ·01793 ·01795 ·01804	.01815 .01820 .01826 .01832 .01837	·02125 ·02131 ·02137 ·02143 ·02143	.02171 .02178 .02184 .02190 .02196	50 51 52 53 54
55 56 57 58 59	.01209 .01213 .01218 .01222 .01227	.01223 .01228 .01233 .01237 .01242	·01494 ·01499 ·01504 ·01509 ·01514	0.01517 0.01522 0.01527 0.01532 0.01532	·01810 ·01815 ·01821 ·01826 ·01832	$\begin{array}{r} \cdot 01843 \\ \cdot 01849 \\ \cdot 01854 \\ \cdot 01860 \\ \underline{\cdot 01866} \\ \cdot 01866 \end{array}$	·02155 ·02161 ·02167 ·02173 ·02173 ·02179	02203 02209 02215 02221 02221 02228	55 56 57 58 59
60	01231	.01247	·01519	•01543	01837	·01872	·02185	·02234	60

TABI SECANTS.

$\mathbf{LE}$	XNATURAL	VERSED	SINES	AND	EXTERNAL
	12°	13°		14°	15°

	1	2°	1	3°	t	14°	1	5°	
	Vers.	Ex. sec.	Vers.	Ex. sec.	Vers.	Ex. sec.	Vers.	Ex. sec.	,
01234	·02185 ·02191 ·02197 ·02203 ·02210	·02234 ·02240 ·02247 ·02253 ·02259	·02563 ·02570 ·02576 ·02583 ·02589	·02630 ·02637 ·02644 ·02651 ·02658	·02970 ·02977 ·02985 ·02992 ·02999	·03061 ·03069 ·03076 ·03084 ·03091	·03407 ·03415 ·03422 ·03430 ·03438	·03528 ·03536 ·03544 ·03552 ·03560	01234
5	·02216	·02266	·02596	·02665	·03006	·03099	$\begin{array}{r} \cdot 03445 \\ \cdot 03453 \\ 03460 \\ \cdot 03468 \\ \cdot 03476 \end{array}$	·03568	5
6	·02222	·02272	·02602	·02672	·03013	·03106		·03576	6
7	·02228	·02279	·02609	·02679	·03020	·03114		·03584	7
8	·02234	·02285	·02616	·02686	·03027	·03121		·03592	8
9	·02240	·02291	·02622	·02693	·03034	·03129		·03601	9
$10 \\ 11 \\ 12 \\ 13 \\ 14$	·02246 ·02252 ·02258 ·02265 ·02271	·02298 ·02304 ·02311 ·02317 ·02323	·02629 ·02635 ·02642 ·02649 ·02655	02700 02707 02714 02721 02721 02728	•03041 •03048 •03055 •03063 •03070	03137 03144 03152 03159 03167	·03483 ·03491 ·03498 ·03506 ·03514	03609 03617 03625 03633 03642	10 11 12 13 14
15	·02277	02330	.02662	02735	.03077	03175	·03521	03650	15
16	·02283	02336	.02669	02742	.03084	03182	·03529	03658	16
17	·02289	02343	.02675	02749	.03091	03190	·03537	03666	17
18	·02295	02349	.02682	02756	.03098	03198	·03544	03674	18
19	·02302	02356	.02689	02763	.03106	03205	·03552	03683	19
20	·02308	·02362	·02696	02770	·03113	03213	·03560	03691	20
21	·02314	·02369	·02702	02777	·03120	03221	·03567	03699	21
22	·02320	·02375	·02709	02784	·03127	03228	·03575	03708	22
23	·02327	·02382	·02716	02791	·03134	03236	·03583	03716	23
24	·02333	·02388	·02722	02799	·03142	03244	·03590	03724	24
25	·02339	02395	·02729	.02806	.03149	03251	·03598	.03732	25
26	·02345	02402	·02736	.02813	.03156	03259	·03606	.03741	26
27	·02352	02408	·02743	.02820	.03163	03267	·03614	.03749	27
28	·02358	02415	·02749	.02827	.03171	03275	·03621	.03758	28
29	·02364	02421	·02756	.02834	.03178	03282	·03629	.03766	29
30	·02370	02428	·02763	.02842	·03185	.03290	·03637	.03774	30
31	·02377	02435	·02770	.02849	·03193	.03298	·03645	.03783	31
32	·02383	02441	·02777	.02856	·03200	.03306	·03653	.03791	32
33	·02389	02448	·02783	.02863	·03207	.03313	·03660	.03799	33
34	·02396	02454	·02790	.02870	·03214	.03321	·03668	.03808	34
36	·02402	.02461	·02797	-02878	·03222	$\begin{array}{r} .03329 \\ .03337 \\ .03345 \\ .03353 \\ .03360 \end{array}$	·03676	-03816	35
36	·02408	.02468	·0280 <u>4</u>	-02885	·03229		·03684	-03825	36
37	·02415	.02474	·02811	-02892	·03236		·03692	-03833	37
38	·02421	.02481	·02818	-02899	·03244		·03699	-03842	38
39	·02421	.02488	·02824	-02907	·03251		·03707	-03850	39
40	·02434	02494	·02831	02914	·03258	$03368 \\ 03376 \\ 03384 \\ 03392 \\ 03400$	-03715	·03858	40
41	·02440	02501	·02838	02921	·03266		-03723	·03867	41
42	·02447	02508	·02845	02928	·03273		-03731	·03875	42
43	·02453	02515	02852	02936	·03281		-03739	·03884	43
44	·02459	02521	·02859	02943	·03288		-03747	·03892	44
45 46 47 48 49	·02466 ·02472 ·02479 ·02485 ·02492	$02528 \\ 02535 \\ 02542 \\ 02548 \\ 02548 \\ 02555$	·02866 ·02873 ·02880 ·02887 ·02887 ·02894	.02950 .02958 .02965 .02972 .02980	·03295 ·03303 ·03310 ·03318 ·03325	03408 03416 03424 03432 03439	·03754 ·03762 ·03770 ·03778 ·03786	.03901 .03909 .03918 .03927 .03935	45 46 47 48 49
50	·02498	.02562	·02900	·02987	·03333	03447	·03794	.03944	50
51	·02504	.02569	·02907	·02994	·03340	03455	·03802	.03952	51
52	·02511	.02576	·02914	·03002	·03347	03463	·03810	.03961	52
53	·02517	.02582	·02921	·03009	·03355	03471	·03818	.03969	53
54	·02524	.02589	·02928	·03017	·03362	03479	·03826	.03978	54
55	·02530	02596	02935	•03024	·03370	03487	·03834	03987	55
56	·02537	02603	02942	•03032	·03377	03495	·03842	03995	56
57	·02543	02610	02949	•03039	·03385	03503	·03850	04004	57
58	·02550	02617	02956	•03046	·03392	03512	·03858	04013	58
59	·02556	02624	02963	•03054	·03400	03520	·03866	04021	59
60	.02563	-02630	.02970	•03061	03407	•03528	·03874	•04030	60

TABLE X.-NATURAL VERSED SINES AND EXTERNAL SECANTS.

16°

17°

18°

/ 19°

			~ •				10		
,	Vers.	Ex. sec.	Vers.	Ex. sec.	Vers.	Ex. sec.	Vers.	Ex. sec	,
0	·03874	04030	$\begin{array}{r} \cdot 04370 \\ \cdot 04378 \\ \cdot 04387 \\ \cdot 04395 \\ \cdot 04404 \end{array}$	04569	·04894	.05146	·05448	·05762	0
1	·03882	04039		04578	·04903	.05156	·05458	·05773	1
2	·03890	04047		04588	·04912	.05166	·05467	·05783	2
3	·03898	04056		04597	·04921	.05176	·05477	·05794	3
4	·03906	04065		04606	·04930	.05186	·05486	·05805	4
5	.03914	$\begin{array}{r} \cdot 04073 \\ \cdot 04082 \\ \cdot 04091 \\ \cdot 04100 \\ \cdot 04108 \end{array}$	.04412	04616	.04939	.05196	05496	.05815	5
6	.03922		.04421	04625	.04948	.05206	05505	.05826	6
7	.03930		.04429	04635	.04957	.05216	05515	.05836	7
8	.03938		.04438	04644	.04967	.05226	05524	.05847	8
9	.03946		.04446	04653	.04976	.05236	05534	.05858	9
10	.03954	$\begin{array}{r} .04117\\ .04126\\ .04135\\ .04144\\ .04152\end{array}$	.04455	04663	.04985	.05246	·05543	05869	10
11	.03963		.04464	04672	.04994	.05256	·05553	05879	11
12	.03971		.04472	04682	.05003	.05266	·05562	05890	12
13	.03979		.04481	04691	.05012	.05276	·05572	05901	13
14	.03987		.04489	04700	.05021	.05286	·05582	05911	14
15	.03995	$\begin{array}{r} .04161 \\ .04170 \\ .04179 \\ .04188 \\ .04197 \end{array}$	.04498	.04710	.05030	.05297	05591	05922	15
16	.04003		.04507	.04719	.05039	.05307	05601	05933	16
17	.04011		.04515	.04729	.05048	.05317	05610	05944	17
18	.04019		.04524	.04738	.05057	.05327	05620	05955	18
19	.04028		.04533	.04748	.05067	.05337	05630	05965	19
20	·04036	$\begin{array}{r} \cdot 04206 \\ \cdot 04214 \\ \cdot 04223 \\ \cdot 04232 \\ \cdot 04241 \end{array}$	.04541	.04757	.05076	.05347	·05639	.05976	20
21	·04044		.04550	.04767	.05085	.05357	·05649	.05987	21
22	·04052		.04559	.04776	.05094	.05367	·05658	.05998	22
23	04060		.04567	.04786	.05103	.05378	·05668	.06009	23
24	·04069		.04576	.04795	.05112	.05388	·05678	.06020	24
25	.04077	$\begin{array}{r} .04250 \\ .04259 \\ .04268 \\ .04277 \\ .04286 \end{array}$	.04585	04805	.05122	05398	.05687	06030	25
26	.04085		.04593	04815	.05131	05408	.05697	06041	26
27	.04093		.04602	04824	.05140	05418	.05707	06052	27
28	.04102		.04611	04834	.05149	05429	.05716	06063	28
29	.04110		.04620	04843	.05158	05439	.05726	06074	29
30 31 32 33 34	.04118 .04126 .04135 .04143 .04151	.04295 .04304 .04313 .04322 .04331	$04628 \\ 04637 \\ 04646 \\ 04655 \\ 04663$	04853 04863 04872 04882 04882 04891	.05168 .05177 .05186 .05195 .05205	05449 05460 05470 05480 05490	.05736 .05746 .05755 .05765 .05775	.06085 .06096 .06107 .06118 .06129	30 31 32 33 34
35 36 37 38 39	·04159 ·04168 ·04176 ·04184 ·04193	04340 04349 04358 04367 04376	04672 04681 04690 04699 04699 04707	04901 04911 04920 04930 04940	·05214 ·05223 ·05232 ·05242 ·05251	05501 05511 05521 05532 05532 05542	·05785 ·05794 ·05804 ·05814 ·05824	·06140 ·06151 ·06162 ·06173 ·06184	35 36 37 38 39
40	·04201	04385	·04716	04950	·05260	·05552	·05833	06195	40
41	·04209	04394	·04725	04959	·05270	·05563	·05843	06206	41
42	·04218	04403	·04734	04969	·05279	·05573	·05853	06217	42
43	·04226	04413	·04743	04979	·05288	·05584	·05863	06228	43
44	·04234	04422	·04752	04989	·05298	·05594	·05873	06239	44
45	·04243	04431	·04760	·04998	05307	05604	.05882	06250	45
46	·04251	04440	·04769	·05008	05316	05615	.05892	06261	46
47	04260	04449	·04778	·05018	05326	05625	.05902	06272	47
48	·04268	04458	·04787	·05028	05335	05636	.05912	06283	48
49	·04276	04468	·04787	·05038	05344	05646	.05922	06295	49
50 51 52 53 54	$\begin{array}{r} \cdot 04285 \\ \cdot 04293 \\ \cdot 04302 \\ \cdot 04310 \\ \cdot 04319 \end{array}$	04477 04486 04495 04504 04514	04805 04814 04323 04832 04832 04841	·05047 ·05057 ·05067 ·05077 ·05077	·05354 ·05363 ·05373 ·05382 ·05391	05657 05667 05678 05688 05699	·05932 ·05942 ·05951 ·05961 ·05971	06306 06317 06328 06339 06350	50 51 52 53 54
55	04327	$\begin{array}{r} \cdot 04523 \\ \cdot 04532 \\ \cdot 04531 \\ \cdot 04551 \\ \cdot 04560 \end{array}$	04850	·05097	05401	05709	·05981	06362	55
56	04336		04858	·05107	05410	05720	·05991	06373	56
57	04344		04867	·05116	05420	05730	·06001	06384	57
58	04353		04876	·05126	05429	05741	·06011	06395	58
59	04361		04885	·05136	05439	05751	·06021	06407	59
60	.04370	·04569	.04894	·05146	·05448	•05762	.06031	.06418	· 60

TABLE X .- NATURAL VERSED SINES AND EXTERNAL SECANTS.

20°			1°	00000	2°	n Enna 9	3°	10.	
-	2	1	~	1	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	<i></i>			
'	Vers.	Ex. sec.	Vers.	Ex. sec.	Vers.	Ex. sec.	Vers.	Ex. sec.	'
01234	·06031	06418	·06642	.07115	·07282	·07853	·07950	·08636	0
	·06041	06429	·06652	.07126	·07293	·07866	·07961	·08649	1
	·06051	06440	·06663	.07138	·07303	·07879	·07972	·08663	2
	·06061	06452	·06673	.07150	·07314	·07892	·07984	·08676	3
	·06071	06463	·06684	.07162	·07325	·07904	·07995	·08690	4
5	·06081	06474	·06694	.07174	·07336	•07917	·08006	·08703	5
6	·06091	06486	·06705	.07186	·07347	•07930	·08018	·08717	6
7	·06101	06497	·06715	.07199	·07358	•07943	·08029	·08730	7
8	·06111	06508	·06726	.07211	·07369	•07955	·08041	·08744	8
9	·06121	06520	·06736	.07223	·07380	•07968	·08052	·08757	9
10 11 12 13 14	·06131 ·06141 ·06151 ·06161 ·06171	06531 06542 06554 06565 06565 06577	.06747 .06757 .06768 .06778 .06789	·07235 ·07247 ·07259 ·07271 ·07283	·07391 ·07402 ·07413 ·07424 ·07435	·07981 ·07994 ·08006 ·08019 ·08032	·08064 ·08075 ·08086 ·08098 ·08109	·08771 ·08784 ·08798 ·08811 ·08825	10 11 12 13 14
15	·06181	·06588	.06799	.07295	·07446	.08045	·08121	·08839	15
16	·06191	·06600	.06810	.07307	·07457	.08058	·08132	·08852	16
17	·06201	·06611	.06820	.07320	·07468	.08071	·08144	·08866	17
18	·06211	·06622	.06831	.07332	·07479	.08084	·08155	·08880	18
19	·06221	·06634	.06841	.07344	·07490	.08097	·08167	·08893	19
20	·06231	06645	·06852	·07356	.07501	·08109	·08178	·08907	20
21	·06241	06657	·06863	·07368	.07512	·08122	·08190	·08921	21
22	·06252	06668	·06873	·07380	.07523	·08135	·08201	08934	22
23	·06262	06680	·06884	·07393	.07534	·08148	·08213	·08948	23
24	·06272	06691	·06884	·07405	.07545	·08161	·08225	·08962	24
25	·06282	·06703	·06905	07417	·07556	·08174	·08236	·08975	25
26	·06292	·06715	·06916	07429	·07568	·08087	08248	·08989	26
27	·06302	·06726	·06926	07442	·07579	·08200	·08259	·09003	27
28	·06312	·06738	·06937	07454	·07590	·08213	·08271	·09017	28
29	·06323	·06749	·06948	07454	·07601	·08226	08282	·09030	29
30	·06333	·06761	.06958	·07479	·07612	·08239	·08294	·09044	30
31	·06343	·06773	.06969	·07491	·07623	·08252	·08306	·09058	31
32	·06353	·06784	.06980	·07503	·07634	·08265	·08317	·09072	32
33	·06363	·06796	.06990	·07516	·07645	·08278	·08329	·09086	33
34	·06374	·06807	.07001	·07528	·07657	·08291	·08340	·09099	34
35 36 37 38 39	·06384 ·06394 ·06404 ·06415 ·06425	06819 06831 06843 06854 06854	.07012 .07022 .07033 .07044 .07055	·07540 ·07553 ·07565 ·07578 ·07590	·07668 ·07679 ·07690 ·07701 ·07713	·08305 ·08318 ·08331 ·08344 ·08357	·08352 ·08364 ·08375 ·08387 ·08387 ·08399	•09113 •09127 •09141 •09155 •09169	35 36 37 38 39
40	$     \begin{array}{r}         \cdot 06435 \\         \cdot 06445 \\         \cdot 06456 \\         \cdot 06466 \\         \cdot 06476 \\     \end{array} $	.06878	·07065	·07302	·07724	•08370	·08410	.09183	40
41		.06889	·07076	·07615	·07735	•08383	·08422	.09197	41
42		.06901	·07087	·07627	·07746	•08397	·08434	.09211	42
43		.06913	·07098	·07640	·07757	•08410	·08445	.09224	48
44		.06925	·07108	·07652	·07769	•08423	·08457	.09238	44
45	06486	.06936	·07119	.07665	·07780	·08436	08469	·09252	45
46	06497	.06948	·07130	.07677	·07791	·08449	08481	·09266	46
47	06507	.06960	·07141	.07690	·07802	·08463	08492	·09280	47
48	06517	.06972	·07151	.07702	·07814	·08476	08504	·09294	48
49	06528	.06984	·07162	.07715	·07825	·08489	08516	09308	49
50	06538	.06995	.07173	•07727	•07836	·08503	.08528	.09323	50
51	06548	.07007	.07184	•07740	07848	·08516	.08539	.09337	51
52	06559	.07019	.07195	•07752	07859	·08529	.08551	.09351	52
53	06569	.07031	.07206	•07765	•07870	·08542	.08563	.09365	53
54	06580	.07043	.07216	•07778	•07881	·08556	.08575	.09379	54
55	.06590	.07055	·07227	.07790	.07893	.08569	· 08586	09393	55
56	.06600	.07067	·07238	.07803	.07904	.08582	· 08598	09407	56
57	.06611	.07079	·07249	.07816	.07915	.08596	· 08610	09421	57
58	.06621	.07091	·07260	.07828	.07927	.08069	· 08622	09435	58
59	.06632	.07103	·07271	.07841	.07938	.08623	· 08634	09449	59
60	06642	07115	.07282	•07853	.07950	·08636	.08645	·09464	60
1					-			-	-

TABLE X .- NATURAL VERSED SINES AND EXTERNAL SECANTS.

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		<b>1</b> -	20	0	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	6*	2	7-	1
,	Vers.	Ex. sec.	Vers.	Ex. sec.	Vers.	Ex. sec.	Vers.	Ex. sec.	
01234	08645 •08657 •08669 •08681 •08693	•09464 •09478 •09492 •09506 •09520	·09369 ·09382 ·09394 ·09406 ·09418	•10338 •10353 •10368 •10383 •10398	·10121 ·10133 ·10146 ·10159 ·10172	$ \begin{array}{r} \cdot 11260 \\ \cdot 11276 \\ \cdot 11292 \\ \cdot 11308 \\ \cdot 11323 \\ \end{array} $	·10899 ·10913 ·10926 ·10939 ·10952	·12233 ·12245 ·12266 ·12283 ·12299	01234
5 6 7 8 9	.08705 .08717 .08728 .08740 .08752	.09535 .09549 .09563 .09577 .09592	·09431 ·09443 ·09455 09468 ·09480	·10413 ·10428 ·10443 ·10458 ·10473	·10184 ·10197 ·10210 ·10223 ·10236	$ \begin{array}{r} \cdot 11339 \\ 11355 \\ \cdot 11371 \\ \cdot 11387 \\ \cdot 11403 \\ \end{array} $	·10965 ·10979 ·10992 ·11005 ·11019	·12316 ·12333 ·12349 ·12366 ·12383	56789
10	.08764	09606	·09493	-10488	·10248	$ \begin{array}{r} \cdot 11419 \\ \cdot 11435 \\ \cdot 11451 \\ \cdot 11467 \\ \cdot 11483 \\ \end{array} $	·11032	.12400	10
11	.08776	09620	·09505	-10503	·10261		·11045	.12416	11
12	.08788	09635	·09517	-10518	·10274		·11058	.12433	12
13	.08800	09649	·09530	-10533	·10287		11072	.12450	13
14	.08812	09663	·09542	-10549	·10300		·11085	.12467	14
15	·08824	09678	09554	.10564	.10313	.11499	·11098	.12484	15
16	·08836	09092.	09567	.10579	.10326	11515	·11112	.12501	16
17	·08848	09707	09579	.10594	.10338	.11531	·11125	.12518	17
18	·08860	09721	09592	.10609	.10351	.11547	·11138	.12534	18
19	·08872	09735	09604	.10625	.10364	.11563	·11152	.12551	19
20 21 22 23 24	·08884 ·08896 ·08908 ·08920 ·08920 ·08932	.09750 .09764 .09779 .09793 .09808	·09617 ·09629 ·09642 ·09654 ·09666	·10640 ·10655 ·10670 ·10686 ·10701	·10377 ·10390 ·10403 ·10416 10429	.11579 .11595 .11611 .11627 .11643	.11165 .11178 .11192 .11205 .11218	.12568 .12585 .12602 .12619 12636	20 21 22 23 24
25 26 27 28 29	·08944 ·08956 ·08968 ·08980 ·08980 ·08992	.09822 .09837 .09851 .09866 .09880	·09679 ·09691 ·09704 ·09716 ·09729	.10716 .10731 .10747 .10762 .10777	·10442 ·10455 ·10468 ·10481 ·10494	.11659 .11675 .11691 .11708 .11724	.11232 .11245 .11259 .11272 .11285	-12653 -12670 -12687 -12704 -12721	25 26 27 28 29
30	.09004	09895	.09741	10793	.10507	.11740	$ \begin{array}{r} .11299\\ .11312\\ .11326\\ .11339\\ .11353 \end{array} $	.12738	30
31	.09016	09909	.09754	10808	.10520	.11756		.12755	31
32	.03028	09924	.09767	10824	.10533	.11772		.12772	32
33	.09040	09939	.09779	10839	.10546	.11789		.12789	33
34	.09052	09953	.09792	10854	.10559	.11805		.12807	34
35	.09064	.09968	·09804	.10870	.10572	.11821	.11366	.12824	35
36	.09076	.09982	09817	.10885	.10585	.11838	.11380	.12841	36
37	.09089	.09997	09829	.10901	.10598	.11854	.11393	.12858	37
38	.09101	.10012	·09842	.10916	.10611	.11870	.11407	.12875	38
39	.09113	.10026	·09854	.10932	.10624	.11886	.11420	.12892	39
40	·09125	.10041	·09867	.10947	·10637	.11903	·11434	·12910	40
41	·09137	.10055	·09880	.10963	·10650	.11919	·11447	·12927	41
42	·09149	.10071	·09892	.10978	·10663	.11936	·11461	·12944	42
43	·09161	.10085	·09905	.10994	·10676	.11952	·11474	·12961	43
44	·09174	.10100	·09918	.11009	·10689	.11968	·11488	·12979	44
45	·09186	.10115	·09930	·11025	·10702	.11985	.11501	12996	45
46	·09198	.10130	·09943	·11041	·10715	.12001	.11515	13013	46
47	·09210	.10144	·09955	·11056	·10728	.12018	.11528	13031	47
48	·09222	.10159	·09968	·11072	·10741	.12034	.11542	13048	48
49	·09234	.10174	·09981	·11087	·10755	.12051	.11555	13065	49
50	·09247	.10189	·09993	.11103	·10768	.12067	·11569	13083	50
51	·09259	.10204	·10006	.11119	·10781	.12084	·11583	13100	51
52	·09271	.10218	·10019	.11134	10794	.12100	·11596	13117	52
53	·09283	.10233	·10032	.11150	·10807	.12117	·11610	13135	53
54	·09296	.10248	·10044	.11166	10820	.12133	·11623	13152	54
55	·09308	.10263	.10057	.11181	· 10833	.12150	.11637	$\begin{array}{r} .13170 \\ .13187 \\ .13205 \\ .13222 \\ .13240 \end{array}$	55
56	·09320	.10278	.10070	.11197	· 10847	.12166	.11651		56
57	·09332	.10293	.10082	.11213	· 10860	.12183	.11664		57
58	·09345	.10308	.10095	.11229	· 10873	.12199	.11678		58
59	·09357	.10323	.10108	.112244	· 10886	.12216	.11692		59
60	·09369	.10338	.10121	.11260	.10899	.12233	.11705	•13257	60
				<b>H</b> C					

TABLE X.-NATURAL VERSED SINES AND EXTERNAL SECANTS. ) 980

)		8°		:9°	3	so°	3	s1°	
,	Vers.	Ex. sec.	Vers.	Ex. sec.	Vers.	Ex. sec.	Vers.	Ex. sec.	1
01234	·11705 ·11719 ·11733 ·11746 ·11760	·13257 ·13275 ·13292 ·13310 ·13327	·12538 ·12552 ·12566 ·12580 ·12595	.14335     .14354     .14372     .14391     .14409	·13397 ·13412 ·13427 ·13441 ·13456	.15470 .15489 .15509 .15528 .15548	$     \begin{array}{r}             \cdot 14283 \\             \cdot 14298 \\             \cdot 14313 \\             \cdot 14328 \\             \cdot 14343         \end{array} $		0 1 2 3 4
5 6 7 8 9	·11774 ·11787 ·11801 ·11815 ·11828	·13345 ·13362 ·13380 ·13398 ·13415	·12609 ·12623 ·12637 ·12651 ·12655	.14428 .14446 .14465 .14483 .14502	·13470 ·13485 ·13499 ·13514 ·13529	.15567     .15587     .15606     .15626     .15645	·14358 ·14373 ·14388 ·14403 ·14418	·16766 ·16786 ·16806 ·16827 ·16848	5 6 7 8 9
0 10 1 11 1 12 1 13 1 14	·11842 ·11856 ·11870 ·11883 ·11897	.13433 .13451 .13468 .13486 .13504	·12679 ·12694 ·12708 ·12722 ·12736	.14521 .14539 .14558 .14576 .14595	.13543     .13558     .13573     .13587     .13602	-15665 -15684 -15704 -15724 -15743	·14433 ·14449 ·14464 ·14479 ·14494	$     \begin{array}{r}         & \cdot 16868 \\         & \cdot 16889 \\         & \cdot 16909 \\         & \cdot 16930 \\         & \cdot 16950 \\     \end{array}   $	10 11 12 13 14
15 16 17 18 19	.11911 .11925 .11938 .11952 .11966	.13521 .13539 .13557 .13575 .13593	.12750 .12765 .12779 .12793 .12807	.14614 .14632 .14651 .14670 .14689	·13616 ·13631 ·13646 ·13660 ·13675	·15763 ·15782 ·15802 ·15822 ·15841	$     \begin{array}{r}         & \cdot 14509 \\         & \cdot 14524 \\         & \cdot 14539 \\         & \cdot 14554 \\         & \cdot 14569 \\     \end{array}   $	.16971 .16992 .17012 .17033 .17054	$     \begin{array}{r}       15 \\       16 \\       17 \\       18 \\       19 \\     \end{array} $
20 21 22 23 24	.11980 .11994 .12007 .12021 .12035	.13610     .13628     .13646     .13664     .13682	·12822 ·12836 ·12850 ·12864 ·12879	.14707 .14726 .14745 .14764 .14782	·13690 ·13705 ·13719 ·13734 ·13749	·15861 ·15881 ·15901 ·15920 ·15940	.14584     .14599     .14615     .14630     .14645	.17075 .17095 .17116 .17137 .17158	20 21 22 23 24
25 26 27 28 29	.12049 .12063 .12077 .12091 .12104	-13700 -13718 -13735 -13753 -13771	·12893 ·12907 ·12921 ·12936 ·12950	.14801 .14820 .14839 .14858 .14877	$     \begin{array}{r}         & \cdot 13763 \\         & \cdot 13778 \\         & \cdot 13793 \\         & \cdot 13808 \\         & \cdot 13822     \end{array} $	.15960 .15980 .16000 .16019 .16039	·14660 ·14675 ·14690 ·14706 ·14721	.17178 .17199 .17220 .17241 .17262	25 26 27 28 29
30 31 32 33 34	12118 12132 12146 12160 12174	.13789 .13807 .13825 .13843 .13861	.12964 .12979 .12993 .13007 .13022	•14896 •14914 •14933 •14952 •14971	·13837 ·13852 ·13867 ·13881 ·13896	.16059 .16079 .16099 .16119 .16139	.14736     .14751     .14766     .14782     .14797	.17283 .17304 .17325 .17346 .17367	30 31 32 33 34
25 36 37 38 39	.12188 .12202 .12216 .12230 .12244	.13879 .13897 .13916 .13934 13952	.13036 .13051 .13065 .13079 .13094	.14990 .15009 .15028 .15047 .15066	.13911 .13926 .13941 .13955 .18970	.16159 .16179 .16199 .16219 .16239	·14812 ·14827 ·14843 ·14858 ·14873	+17388 +17409 +17430 +17451 +17472	35 36 37 38 39
40 41 42 43 44	.12257 .12271 .12285 .12299 .12313	.13970 .13988 .14006 .14024 .14042	·13108 ·13122 ·13137 ·13151 ·13166	15085 15105 15124 15143 15162	13985 .14000 .14015 .14030 .14044	.16259 .16279 .16299 .16319 .16339	·14888 ·14904 ·14919 ·14934 ·14949	.17493 .17514 .17535 .17556 .17577	40 41 42 43 44
45 46 47 48 49	$ \begin{array}{r} \cdot 12327 \\ \cdot 12341 \\ \cdot 12355 \\ \cdot 12369 \\ 12383 \\ \end{array} $	.14061 .14079 .14097 .14115 .14134	.13180 .13195 .13209 .13223 .13238	.15181 .15200 .15219 .15239 .15258	14059 14074 14089 14104 14119	$\begin{array}{r} 16359 \\ \cdot 16380 \\ \cdot 16400 \\ \cdot 16420 \\ \cdot 16440 \end{array}$	·14965 ·14980 ·14995 ·15011 ·15026	.17598 .17620 .17641 .17662 .17683	45 46 47 48 49
50 51 52 53 54	·12397 ·12411 ·12425 ·12439 ·12454	•14152 •14170 •14188 •14207 •14225	.13252 .13267 .13281 .13296 .13310	.15277 .15296 .15315 .15335 .15354	·14134 ·14149 ·14164 ·14179 ·14194	.16460 16481 .16501 .16521 .16541	15041 .15057 .15072 .15087 .15103	.17704 .17726 .17747 .17768 .17790	50 51 52 53 54
55 56 57 58 59	$     \begin{array}{r}         \cdot 12468 \\         \cdot 12482 \\         \cdot 12496 \\         \cdot 12510 \\         \cdot 12524 \\     \end{array} $	.14243 .14262 .14280 .14299 .14317	·13325 ·13339 ·13354 ·13368 ·13383	.15373 .15393 .15412 .15431 .15451	·14208 ·14223 ·14238 ·14253 ·14253 ·14268	$     \begin{array}{r}         \cdot 16562 \\         \cdot 16582 \\         \cdot 16602 \\         \cdot 16623 \\         \cdot 16643 \\         \cdot 16643     \end{array} $	15118 15134 15149 15164 15180	.17811 .17832 .17854 .17875 .17896	55 56 57 58 59
60	.12538	·14335	•13397	.15470	.14283	.16663	.15195	.17918	60

TABLE X.-NATURAL VERSED SINES AND EXTERNAL SECANTS.

).	3	2°	3	3°	8	4°	ę	35° t	
,	Vers.	Ex. sec.	Vers.	Ex. sec.	Vers.	Ex. sec.	Vers.	Ex. sec.	
01234	·15195 ·15211 ·15226 ·15241 ·15257	·17918 ·17939 ·17961 ·17982 ·18004	$     \begin{array}{r}             \cdot 16133 \\             \cdot 16149 \\             \cdot 16165 \\             \cdot 16181 \\             \cdot 16196 \\         \end{array} $	·19236 ·19259 ·19281 ·19304 ·19327	·17096 ·17113 ·17129 ·17145 ·17161	·20622 ·20645 ·20669 ·20693 ·20717	·18085 ·18101 ·18118 ·18135 ·18152	$ \begin{array}{r} \cdot 22077 \\ \cdot 22102 \\ \cdot 22127 \\ \cdot 22152 \\ \cdot 22177 \\ \end{array} $	01234
5 6 7 8 9	$     .15272 \\     .15288 \\     .15303 \\     .15319 \\     .15334   $	·18025 ·18047 ·18068 ·18090 ·18111	$     \begin{array}{r}             .16212 \\             .16228 \\             .16244 \\             .16260 \\             .16276 \\         \end{array}     $	·19349 ·19372 ·19394 ·19417 ·19440	.17178 .17194 .17210 .17227 .17243	·20740 ·20764 ·20788 ·20812 ·20836	·18168 ·18185 ·18202 ·18218 ·18235	·22202 ·22227 ·22252 ·22277 ·22302	0123456789
10 11 12 13 14	.15350 .15365 .15381 .15396 .15412	.18133 .18155 .18176 .18198 .18220	$     \begin{array}{r}         & \cdot 16292 \\         & \cdot 16308 \\         & \cdot 16324 \\         & \cdot 16340 \\         & \cdot 16355 \\     \end{array} $	.19463 .19485 .19508 .19531 .19554	·17259 ·17276 ·17292 ·17308 ·17325	20859 20883 20907 20931 20955	·18252 ·18269 ·18286 ·18302 ·18319	·22327 ·22352 ·22377 ·22402 ·22428	10 11 12 13 14
15 16 17 18 19	.15427 .15443 .15458 .15474 .15489	.18241 .18263 .18285 .18307 .18328	.16371     .16387     .16403     .16419     .16435     .	·19576 ·19599 ·19622 ·19645 ·19668	.17341 .17357 .17374 .17390 .17407	·20979 ·21003 ·21027 ·21051 ·21075	.18336     .18353     .18369     .18386     .18403	22453 22478 22503 22528 22554	15 16 17 18 19
20 21 22 23 24	.15505     .15520     .15536     .15552     .15552     .15567	.18350 .18372 .18394 .18416 .18437	.16451     .16467     .16483     .16499     .16515	·19691 ·19713 ·19736 ·19759 ·19782	·17423 ·17439 ·17456 ·17472 ·17489	$\begin{array}{r} \cdot 21099 \\ \cdot 21123 \\ \cdot 21147 \\ \cdot 21171 \\ \cdot 21195 \end{array}$	·18420 ·18437 ·18454 ·18470 ·18487	22579 22604 22629 22655 22680	20 21 22 23 24
25 26 27 28 29	.15583 .15598 .15614 .15630 .15645	.18459 .18481 .18503 .18525 .18547	·16531 ·16547 ·16563 ·16579 ·16595	.19805 .19828 .19851 .19874 .19897	.17505 .17522 .17538 .17554 .17571	.21220 .21244 .21268 .21292 .21316	·18504 ·18521 ·18538 ·18555 ·18572	-22706 -22731 -22756 -22782 -22807	25 26 27 28 29
30 31 32 33 34	·15661 ·15676 ·15692 ·15708 ·15723	.18569     .18591     .18613     .18635     .18657	·16611 ·16627 ·16644 ·16660 ·16676	.19920 .19944 .19967 .19990 .20013	·17587 ·17604 ·17620 ·17637 ·17653	.21341 .21365 .21389 .21414 .21438	·18588 ·18605 ·18622 ·18639 ·18656	·22833 ·22858 ·22884 ·22909 ·22935	30 31 32 33 34
35 36 37 38 39	·15739 ·15755 ·15770 ·15786 ·15802	·18679 ·18701 ·18723 ·18745 ·18767	·16692 ·16708 ·16724 ·16740 ·16756	20036 20059 20083 20106 20129	·17670 ·17686 ·17703 ·17719 ·17736	.21462 .21487 .21511 .21535 .21560	·18673 ·18690 ·18707 ·18724 ·18741	·22960 ·22986 ·23012 ·23037 ·23063	35 36 37 38 39
40 41 42 43 44	.15818     .15833     .15849     .15865     .15880	.18790 .18812 .18834 .18856 .18878	·16772 ·16788 ·16805 ·16821 ·16837	20152 20176 20199 20222 20246	·17752 ·17769 ·17786 ·17802 ·17819	21584 21609 21633 21658 21682	·18758 ·18775 ·18792 ·18809 ·18826	$ \begin{array}{r} \cdot 23089 \\ \cdot 23114 \\ \cdot 23140 \\ \cdot 23166 \\ \cdot 23192 \\ \end{array} $	40 41 42 43 44
45 46 47 48 49	·15896 ·15912 ·15928 ·15943 ·15959	.18901 .18923 .18945 .18967 .18990	·16853 ·16869 ·16885 ·16902 ·16918	20269 20292 20316 20339 20363	·17835 ·17852 ·17868 ·17885 ·17902	21707 21731 21756 21781 21805	·18843 ·18860 ·18877 ·18894 ·18911	·23217 ·23243 ·23269 ·23295 ·23321	45 46 47 48 49
50 51 52 53 54	·15975 ·15991 ·16006 ·16022 ·18038	.19012 .19034 .19057 .19079 .19102	.16934     .16950     .16966     .16983     .16999	20386 20410 20433 20457 20480	·17918 ·17935 ·17952 ·17968 ·17985	· 21830 · 21855 · 21879 · 21904 · 21929	·18928 ·18945 ·18962 ·18979 ·18996	·23347 ·23373 ·23399 ·23424 ·23450	50 51 52 53 54
55 56 57 58 59	·16054 ·16070 ·16085 ·16101 ·16117	.19124 .19146 .19169 .19191 .19214	.17015 .17031 .17047 .17064 .17080	·20504 ·20527 ·20551 ·20575 ·20598	.18001 .18018 .18035 .18051 .18068	·21953 ·21978 ·22003 ·22028 ·22053	.19013 .19030 .19047 .19064 .19081	23476 23502 23529 23555 23581	55 56 57 58 59
60	.16133	.19236	.17096	.20622	·18085	.22077	.19098	-23607	60

TABLE X.-NATURAL VERSED SINES AND EXTERNAL SECANTS

IAI	ын а З	-NATUR 6°		RSED S	3	ND EA 8°	ILANA 3	9°	110
	Vers.	Ex. sec.	Vers.	Ex. sec.	Vers.	Ex. sec.	Vers.	Ex. sec.	,
01234	·19098 ·19115 ·19133 ·19150 ·19167	-23607 -23633 -23659 -23685 -23711	·20136 ·20154 ·20171 ·20189 ·20207	25214 25241 25269 25296 25324	·21199 ·21217 ·21235 ·21253 ·21271	·26902 ·26931 ·26960 ·26988 ·27017	· 22285 · 22304 · 22322 · 22340 · 22359	28676 28706 28737 28767 28767 28797	0 1 2 3 4
5 6 7 8 9	.19184 .19201 .19218 .19235 .19252	·23738 ·23764 ·23790 ·23816 ·23843	·20224 ·20242 ·20259 ·20277 ·20294	25351 25379 25406 25434 25462	·21289 ·21307 ·21324 ·21342 ·21360	·27046 ·27075 ·27104 ·27133 ·27162	·22377 ·22395 ·22414 ·22432 ·22450	·28828 ·28858 ·28889 ·28919 ·28950	5 6 7 8 9
10 11 12 13 14	·19270 ·19287 ·19304 ·19321 ·19338	$ \begin{array}{r} \cdot 23869 \\ \cdot 23895 \\ \cdot 23922 \\ \cdot 23948 \\ \cdot 23975 \\ \end{array} $	·20312 ·20329 ·20347 ·20365 ·20382	·25489 ·25517 ·25545 ·25572 ·25600	·21378 ·21396 ·21414 ·21432 ·21450	·27191 ·27221 ·27250 ·27279 ·27308	·22469 ·22487 ·22506 ·22524 ·22542	·28980 ·29011 ·29042 ·29072 ·29103	$10 \\ 11 \\ 12 \\ 13 \\ 14$
15 16 17 18 19	·19356 ·19373 ·19390 ·19407 ·19424	$     \begin{array}{r}         \cdot 24001 \\         \cdot 24028 \\         \cdot 24054 \\         \cdot 24081 \\         \cdot 24107 \\         \end{array}     $	·20400 ·20417 ·20435 ·20453 ·20453 ·20470	25628 25656 25683 25711 25739	·21468 ·21486 ·21504 ·21522 ·21540	$     \begin{array}{r}             27337 \\             27366 \\             27396 \\             27425 \\             27454 \\         \end{array}     $	·22561 ·22579 ·22598 ·22616 ·22634	·29133 ·29164 ·29195 ·29226 ·29256	15 16 17 18 19
20 21 22 23 24	·19442 ·19459 ·19476 ·19493 ·19511	24134 24160 24187 24213 24240	·20488 ·20506 ·20523 ·20541 ·20559	25767 25795 25823 25851 25879	·21558 ·21576 ·21595 ·21613 ·21631	·27483 ·27513 ·27542 ·27572 ·27601	·22653 ·22671 ·22690 ·22708 ·22727	·29287 ·29318 ·29349 ·29380 ·29411	20 21 22 23 24
25 26 27 28 29	-19528 -19545 -19562 -19580 -19597	24267 24293 24320 24347 24373	·20576 ·20594 ·20612 ·20629 ·20647	25907 25935 25963 25991 26019	·21649 ·21667 ·21685 ·21703 ·21721	·27630 ·27660 ·27689 ·27719 ·27748	·22745 ·22764 ·22782 ·22801 ·22819	·29442 ·29473 ·29504 ·29535 ·29566	25 26 27 28 29
30 31 32 33 34	·19614 ·19632 ·19649 ·19666 ·19684	.24400 .24427 .24454 .24481 .24508	·20665 ·20682 ·20700 ·20718 ·20736	26047 26075 26104 26132 26160	·21739 ·21757 ·21775 ·21794 ·21812	·27778 ·27807 ·27837 ·27867 ·27896	·22838 ·22856 ·22875 ·22893 ·22912	·29597 ·29628 ·29659 ·29690 ·29721	30 31 32 33 34
35 36 37 38 <u>39</u>	.19701 .19718 .19736 .19753 .19770	24534 24561 24588 24615 24642	·20753 ·20771 ·20789 ·20807 ·20824	$ \begin{array}{r} \cdot 26188 \\ \cdot 26216 \\ \cdot 26245 \\ \cdot 26273 \\ \cdot 26301 \\ \end{array} $	·21830 ·21848 ·21866 ·21884 ·21902	·27926 ·27956 ·27985 ·28015 ·28045	·22930 ·22949 ·22967 ·22986 ·23004	·29752 ·29784 ·29815 ·29846 ·29877	35 36 37 38 39
40 41 42 43 44	·19788 ·19805 ·19822 ·19840 ·19857	24669 24696 24723 24750 24777	·20842 ·20860 ·20878 ·20895 ·20913	$ \begin{array}{r} \cdot 26330 \\ \cdot 26358 \\ \cdot 26387 \\ \cdot 26415 \\ \cdot 26443 \\ \end{array} $	·21921 ·21939 ·21957 ·21975 ·21993	$ \begin{array}{r} \cdot 28075 \\ \cdot 28105 \\ \cdot 28134 \\ \cdot 28164 \\ \cdot 28194 \end{array} $	·23023 ·23041 ·23060 ·23079 ·23097	·29909 ·29940 ·29971 ·30003 ·30034	40 41 42 43 44
45 46 47 48 49	·19875 ·19892 ·19909 ·19927 ·19944	$\begin{array}{r} \cdot 24804 \\ \cdot 24832 \\ 24859 \\ \cdot 24886 \\ \cdot 24913 \end{array}$	·20931 ·20949 ·20967 ·20985 ·21002	-26472 -26500 -26529 -26557 -26586	·22012 ·22030 ·22048 ·22066 ·22084	·28224 ·28254 ·28284 ·28314 ·28344	$     \begin{array}{r}         \cdot 23116 \\         \cdot 23134 \\         \cdot 23153 \\         \cdot 23172 \\         \cdot 23190 \\         \cdot 23190 \\         \end{array} $	-30066 -30097 -30129 -30160 -30192	45 46 47 48 49
50 51 52 53 54	·19962 ·19979 ·19997 ·20014 ·20032	24940 24967 24995 25022 25049	·21020 ·21038 ·21056 ·21074 ·21092	26615 26643 26672 26701 26729	·22103 ·22121 ·22139 ·22157 ·22176	.28374     .28404     .28434     .28464     .28495	·23209 ·23228 ·23246 ·23265 ·23283	· 30223 · 30255 · 30287 · 30318 · 30350	50 51 52 53 54
55 56 57 58 59	·20049 ·20066 ·20084 ·20101 ·20119	·25077 ·25104 ·25131 ·25159 ·25186	·21109 ·21127 ·21145 ·21163 ·21181	·26758 ·26787 ·26815 ·26844 ·26873	·22194 ·22212 ·22231 ·22249 ·22267	·28525 ·28555 ·28585 ·28615 ·28646	·23302 ·23321 ·23339 ·23358 ·23377	· 30382 · 30413 · 30445 · 30477 · 30509	55 56 57 58 59
60	.20136	•25214	.21199	•26902	· 22285	•28676	.23396	· 80541	60

TABLE X .- NATURAL VERSED SINES AND EXTERNAL SECANTS. 4 4 0

40°			41°		A 621 MI25			L SECANIS. 13°	
$\neg$	 	0		<u>_</u>		1 1		1	
'	Vers.	Ex. sec.	Vers.	Ex. sec.	Vers.	Ex. sec.	Vers.	Ex. sec.	•
0	·23396	.30541	·24529	•32501	·25686	.34563	·26865	36733	01234
1	·23414	.30573	·24548	•32535	·25705	.34599	·26884	36770	
2	·23433	.30605	·24567	•32568	·25724	.34634	·26904	36807	
3	·23452	.30636	·24586	•32602	·25744	.34669	·26924	36844	
4	·23470	.30668	·24605	•32636	·25763	.34704	·26944	36881	
5	·23489	.30700	·24625	.32669	•25783	.34740	·26964	•36919	5
6	·23508	.30732	·24644	.32703	•25802	.34775	·26984	•36956	6
7	·23527	.30764	·24663	.32737	•25822	.34811	·27004	•36993	7
8	·23545	.30796	·24682	.32770	•25841	.34846	·27024	•37030	8
9	·23564	.30829	·24701	.32804	•25861	.34882	·27043	•37068	9
10	·23583	·30861	·24720	•32838	•25880	.34917	•27063	.37105	10
11	·23602	·30893	·24739	•32872	•25900	.34953	•27083	.37143	11
12	·23620	·30925	·24759	•32905	•25920	.34988	•27103	.37180	12
13	·23639	·30957	·24778	•32939	•25939	.35024	•27123	.37218	13
14	·23658	·30989	·24797	•32973	•25939	.35060	•27143	.37255	14
15	·23677	.31022	·24816	.33007	·25978	.35095	•27163	•37293	15
16	·23696	.31054	·24835	.33041	·25998	.35131	•27183	•37330	16
17	·23714	.31086	·24854	.33075	·26017	.35167	•27203	•37368	17
18	·23733	.31119	·24874	.33109	·26037	.35203	•27228	•37406	18
19	·23752	.31151	·24893	.33143	·26056	.35238	•27243	•37443	19
20 21 22 23 24	·23771 ·23790 ·23808 ·23827 ·23846	·31183 ·31216 ·31248 ·31281 ·31313	·24912 ·24931 ·24950 ·24970 ·24989	.33177 .33211 .33245 .33279 .33314	·26076 ·26096 ·26115 ·26135 ·26154	·35274 ·35310 ·35346 ·35382 ·35418	•27263 •27283 •27303 •27323 •27323 •27343	.37481 .37519 .37556 .37594 .37632	20 21 22 23 24
25	23865	.31346	·25008	•33348	·26174	.35454	·27363	-37670	25
26	23884	.31378	·25027	•33382	·26194	.35490	·27383	-37708	26
27	23903	.31411	·25047	•33416	·26213	.35526	·27403	-37746	27
28	23922	.31443	·25066	•33451	·26233	.35562	·27423	-37784	28
29	23921	.31476	·25085	•33485	·26253	.35598	·27443	-37822	29
30 31 32 33 34	·23959 ·23978 ·23997 ·24016 ·24035	.31509 .31541 .31574 .31607 .31640	·25104 ·25124 ·25143 ·25162 ·25182	.33519 .33554 .33588 .33622 .33657	•26272 •26292 •26312 •26331 •26331 •26351	·35634 ·35670 ·35707 ·35743 ·35779	·27463 ·27483 ·27503 ·27523 ·27543	•37860 •37898 •37936 •37974 •38012	30 31 32 33 34
35	·24054	•31672	·25201	.33691	·26371	.35815	·27563	.38051	35
36	·24073	•31705	·25220	.33726	·26390	.35852	·27583	.38089	36
37	·24092	•31738	·25240	.33760	·26410	.35888	·27603	.38127	37
38	·24111	•31771	·25259	.33795	·26430	.35924	·27623	.38165	38
39	·24130	•31804	·25278	.33830	·26449	.35961	·27643	.38204	39
40	·24149	.31837	·25297	·33864	·26469	.35997	·27663	•38242	40
41	·24168	.31870	·25317	·33899	·26489	.36034	·27683	•38280	41
42	·24187	.31903	·25336	·33934	·26509	.36070	·27703	•38319	42
43	·24206	.31936	·25356	·33968	·26528	.36107	·27723	•38357	43
44	·24225	.31969	·25375	·34003	·26548	.36143	·27743	•38396	44
45 46 47 48 49	·24244 ·24262 ·24281 ·24300 ·24320	.32002 .32035 .32068 .32101 .32134	·25394 ·25414 ·25433 ·25452 ·25472	·34038 ·34073 ·34108 ·34142 ·34177	·26568 ·26588 ·26607 ·26627 ·26647	.36180 .36217 .36253 .36290 .36327	·27764 ·27784 ·27804 ·27824 ·27824 ·27844	.38434 .38473 .38512 .38550 .38589	45 46 47 48 49
50	·24339	•32168	·25491	•34212	·26667	·36363	·27864	·38628	50
51	·24358	•32201	·25511	•34247	·26686	·36400	·27884	·38666	51
52	·24377	•32234	·25530	•34282	·26706	·36437	·27905	·38705	52
53	·24396	•32267	·25549	•34317	·26726	·36474	·27925	·38744	53
54	·24415	•32301	·25569	•34352	·26746	·36511	·27945	·38783	54
55	·24434	•32334	·25588	·34387	·26766	·36548	·27965	·38822	55
56	·24453	•32368	·25608	·34423	·26785	·36585	·27985	·38860	56
57	·24472	•32401	·25627	·34458	·26805	·36622	·28005	·38899	57
58	·24491	•32434	·25647	·34493	·26825	·36659	·28026	·38938	58
59	·24510	•32468	·25666	·34528	·26845	·36696	·28046	·38977	59
60	·24529	•32501	·256 <b>86</b>	•34563	•26865	•36733	•28066	•39016	60

TABLE X.—NATURAL VERSED SINES AND EXTERNAL SECANTS 44° 45° 46° 47°							NTS.		
1.	Vers.	Ex. sec.	Vers.	Ex. sec.	Vers.	Ex. sec.	Vers.	Ex. sec.	1.
0 1 2 3 4	28066 28086 28106 28127 28127 28147	.39016 .39055 .39095 .39134 .39173	·29289 ·29310 ·29330 ·29351 ·29372	.41421 .41463 .41504 .41545 .41586	· 30534 · 30555 · 30576 · 30597 · 30618	•43956 •43999 •44042 •44086 •44129	·31800 ·31821 ·31843 ·31864 ·31885	·46628 ·46674 ·46719 ·46765 ·46811	0 1 2 3 4
5 6 7 8 9	·28167 ·28187 ·28208 ·28228 ·28248	.39212 .39251 .39291 .39330 .39369	·29392 ·29413 ·29433 ·29454 ·29475	$\begin{array}{r} .41627\\ .41669\\ .41710\\ .41752\\ .41793\end{array}$	30639 30660 30681 30702 30723	$\begin{array}{r} \cdot 44173 \\ \cdot 44217 \\ \cdot 44260 \\ \cdot 44304 \\ \cdot 44347 \end{array}$	.31907 .31928 .31949 .31971 .31992	·46857 ·46903 ·46949 ·46995 ·47041	5 6 7 8 9
$     \begin{array}{c}       10 \\       11 \\       12 \\       13 \\       14     \end{array} $	·28268 ·28289 ·28309 ·28329 ·28350	·39409 ·39448 ·39487 ·39527 ·39566	·29495 ·29516 ·29537 ·29557 ·29578	.41835 .41876 .41918 .41959 .42001	.30744 .30765 .30786 .30807 .30828	$ \begin{array}{r}             .44391 \\             .44435 \\             .44479 \\             .44523 \\             .44567 \\         \end{array} $	-32013 -32035 -32056 -32077 -32099	·47087 ·47134 ·47180 ·47226 ·47272	10 11 12 13 14
15 16 17 18 <u>19</u>	·28370 ·28390 ·28410 ·28431 ·28451	·39606 ·39646 ·39685 ·39725 ·39764	.29599 .29619 .29640 .29661 .29681	$ \begin{array}{r}       42042 \\       42084 \\       42126 \\       42168 \\       42210 \\     \end{array} $	.30849 .30870 .30891 .30912 .30933	•44610 •44654 •44698 •44742 •44787	-32120 -32141 -32163 -32184 -32205	•47319 •47365 •47411 •47458 •47504	15 16 17 18 19
20 21 22 23 24	·28471 ·28492 ·28512 ·28532 ·28553	·39804 ·39844 ·39884 ·39924 ·39963	·29702 ·29723 ·29743 ·29764 ·29785	•42251 •42293 •42335 •42377 •42419	.30954 .30975 .30996 .31017 .31038	•44831 •44875 •44919 •44963 •45007	·32227 ·32248 ·32270 ·32291 ·32312	.47551     .47598     .47644     .47691     .47738	20 21 22 23 24
25 26 27 28 29	·28573 ·28593 ·28614 ·28634 ·28655	.40003 .40043 .40083 .40123 .40163	·29805 ·29826 ·29847 ·29868 ·29888	$\begin{array}{r} .42461 \\ .42503 \\ .42545 \\ .42587 \\ .42630 \end{array}$	-31059 -31080 -31101 -31122 -31143	•45052 •45096 •45141 •45185 •45229	·32334 ·32355 ·32377 ·32398 ·32420	.47784 .47831 .47878 .47925 .47972	25 26 27 28 29
30 31 32 33 34	·28675 ·28695 ·28716 ·28736 ·28757	•40203 •40243 •40283 •40324 •40364	·29909 ·29930 ·29951 ·29971 ·29992	$     .42672 \\     .42714 \\     .42756 \\     .42799 \\     .42841 $	·31165 ·31186 ·31207 ·31228 ·31249	.45274 .45319 .45363 .45408 .45452	· 32441 · 32462 · 32484 · 32505 · 32527	$ \begin{array}{r} .48019\\ .48066\\ .48113\\ .48160\\ .48207 \end{array} $	30 31 32 33 34
35 36 37 38 39	·28777 ·28797 ·28818 ·28838 ·28859	$ \begin{array}{r}     .40404 \\     .40444 \\     .40485 \\     .40525 \\     .40565 \\   \end{array} $	-30013 -30034 -30054 -30075 -30096	•42883 •42926 •42968 •43011 •43053	.`31270 .31291 .31312 .31334 .31355	$ \begin{array}{r}             .45497 \\             .45542 \\             .45587 \\             .45631 \\             .45676 \\         \end{array} $	·32548 ·32570 ·32591 ·32613 ·32634	.48254 .48301 .48349 .48396 .48443	35 36 37 38 39
40 41 42 43 44	·28879 ·28900 ·28920 ·28941 ·28961	•40606 •40646 •40687 •40727 •40768	·30117 ·30138 ·30158 ·30179 ·30200	•43096 •43139 •43181 •43224 •43267	·31376 ·31397 ·31418 ·31439 ·31461	.45721 .45766 .45811 .45856 .45901	· 32656 · 32677 · 32699 · 32720 · 32742	$ \begin{array}{r} .48491\\.48538\\.48586\\.48586\\.48633\\.48681\end{array} $	40 41 42 43 44
45 46 47 48 49	·28981 ·29002 ·29022 ·29043 ·29063		· 30221 · 30242 · 30263 · 30283 · 30304	.43310     .43352     .43395     .43438     .43481     .43481	·31482 ·31503 ·31524 ·31545 ·31567	•45946 •45992 •46037 •46082 •46127	· 32763 · 32785 · 32806 · 32828 · 32849	·48728 ·48776 ·48824 ·48871 ·48919	45 46 47 48 49
50 51 52 53 54	·29084 ·29104 ·29125 ·29145 ·29166	·41093 ·41134	· 30325 · 30346 · 30367 · 30388 · 30409	.43524 .43567 .43610 .43653 .43696	·31588 ·31609 ·31630 ·31651 ·31673	$     \begin{array}{r}         & \cdot 46173 \\         & \cdot 46218 \\         & \cdot 46263 \\         & \cdot 46309 \\         & \cdot 46354 \\     \end{array} $	-32871 -32893 -32914 -32936 -32957	·48967 ·49015 ·49063 ·49111 ·49159	50 51 52 53 54
55 56 57 58 59	·29187 ·29207 ·29228 ·29248 ·29269	.41339 .41380	·30430 ·30451 ·30471 ·30492 ·30513	•43739 •43783 •43826 •43869 •43912	·31694 ·31715 ·31736 ·31758 ·31758 ·31779	.46400 .46445 .46491 .46537 .46582	·32979 ·33001 ·33022 ·33044 ·33065	•49207 •49255 •49303 •49351 •49399	55 56 57 58 59
60	•29289	•41421	.30534	•43956	.31800	•46628	33087	.49448	60

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TABLE X .-- NATURAL VERSED SINES AND EXTERNAL SECANTS.

48°				49° 50°			51°		
	4	8°	4	9°	5	0°	31.		
,	Vers.	Ex. sec.	Vers.	Ex. sec.	Vers.	Ex. sec.	Vers.	Ex. sec.	1
0	·33087	•49448	·34394	•52425	·35721	•55572	·37068	.58902	0
1	·33109	•49496	·34416	•52476	·35744	•55626	·37091	.58959	1
2	·33130	•49544	·34438	•52527	·35766	•55680	·37113	.59016	2
3	·33152	•49593	·34460	•52579	·35788	•55734	·37136	.59073	3
4	·33173	•49641	·34482	•52630	·35810	•55789	·37158	.59130	4
5	.33195	•49690	·34504	·52681	·35833	• 55843	·37181	-59188	5
6	.33217	•49738	·34526	·52732	·35855	• 55897	·37204	-59245	6
7	.33238	•49787	·34548	·52784	·35877	• 55951	·37226	-59302	7
8	.33260	•49835	·34570	·52835	·35900	• 56005	·37249	-59360	8
9	.33282	•49884	·34592	·52886	·35922	• 56060	·37272	-59418	9
10	.33303	.49933	.34614	.52938	·35944	.56114	·37294	• 59475	10
11	.33325	.49981	.34636	.52989	·35967	.56169	·37317	• 59533	11
12	.33347	.50030	.34658	.53041	·35989	.56223	·37340	• 59590	12
13	.33368	.50079	.34680	.53092	·36011	.56278	·37362	• 59648	13
14	.33390	.50128	.34702	.53144	·36034	.56332	·37385	• 59706	14
15	•33412	•50177	.34724	53196	·36056	56387	·37408	• 59764	15
16	•33434	•50226	.34746	53247	·36078	56442	·37430	• 59822	16
17	•33455	•50275	.34768	53299	·36101	56497	·37453	• 59880	17
18	•33477	•50324	.34790	53351	·36123	56551	·37476	• 59938	18
19	•33499	•50373	.34812	53403	·36146	56606	·37498	• 59996	19
20	·33520	.50422	·34834	53455	·36168	56661	·37521	.60054	20
21	·33542	.50471	·34856	53507	·36190	56716	·37544	.60112	21
22	·33564	.50521	·34878	53559	·36213	56771	·37567	.60171	22
23	·33586	.50570	·34900	53611	·36235	56826	·37589	.60229	23
24	·33607	.50619	·34923	53663	·36258	56881	·37612	.60287	24
25	·33629	· 50669	.34945	.53715	·36280	•56937	·37635	.60346	25
26	·33651	· 50718	.34967	.53768	·36302	•56992	·37658	.60404	26
27	·33673	· 50767	.34989	.53820	·36325	•57047	·37680	.60463	27
28	·33694	· 50817	.35011	.53872	·36347	•57103	·37703	.60521	28
29	·33716	· 50866	.35033	.53924	·36370	•57158	·37726	.60580	29
30	·33738	50916	·35055	•53977	$     \begin{array}{r}         & \cdot 36392 \\         & \cdot 36415 \\         & \cdot 36437 \\         & \cdot 36460 \\         & \cdot 36482 \\     \end{array} $	•57213	·37749	60639	30
31	·33760	50966	·35077	•54029		•57269	·37771	60698	31
32	·33782	51015	·35099	•54082		•57324	·37794	60756	32
33	·33803	51065	·35122	•54134		•57380	·37817	60815	33
34	·33825	51115	·35144	•54187		•57436	·37840	60874	34
35 36 37 38 39	·33847 ·33869 ·33891 ·33912 ·33934	51165 51215 51265 51314 51364	$     \begin{array}{r}         & \cdot 35166 \\         & \cdot 35188 \\         & \cdot 35210 \\         & \cdot 35232 \\         & \cdot 35254 \\     \end{array} $	54240 54292 54345 54398 54451	$     \begin{array}{r}         & \cdot 36504 \\         & \cdot 36527 \\         & \cdot 36549 \\         & \cdot 36572 \\         & \cdot 36594 \\     \end{array} $	57491 57547 57603 57659 57715	·37862 ·37885 ·37908 ·37931 ·37954	.60933 .60992 .61051 .61111 .61170	35 36 37 38 39
40	·33956	51415	·35277	54504	·36617	•57771	-37976	·61229	$     \begin{array}{r}       40 \\       41 \\       42 \\       43 \\       44 \\     \end{array} $
41	·33978	51465	·35299	54557	·36639	•57827	-37999	·61288	
42	·34000	51515	·35321	54610	·36662	•57883	-38022	·61348	
43	·34022	51565	·35343	54663	·36684	•57939	-38045	·61407	
44	·34044	51615	·35365	54716	·36707	•57995	-38068	·61467	
45	·34065	.51665	·35388	.54769	-36729	.58051	.38091	.61526	45
46	·34087	.51716	·35410	.54822	-36752	.58108	.38113	.61586	46
47	·34109	.51766	·35432	.54876	-36775	.58164	.38136	.61646	47
48	·34131	.51817	·35454	.54929	-36797	.58221	.38159	.61705	48
49	·34153	.51867	·35476	.54982	-36820	.58277	.38182	.61765	49
50	·34175	.51918	.35499	55036	-36842	• 58333	- 38205	·61825	50
51	·34197	.51968	.35521	55089	-36865	• 58390	- 38228	·61885	51
52	·34219	.52019	.35543	55143	-36887	• 58447	- 38251	·61945	52
53	·34241	.52069	.35565	55196	-36910	• 58503	- 38274	·62005	53
54	·34262	.52120	.35588	55250	-36932	• 58560	- 38296	·62065	54
55	$     \begin{array}{r}         & \cdot 34284 \\         & \cdot 34306 \\         & \cdot 34328 \\         & \cdot 34350 \\         & \cdot 34372 \\     \end{array} $	.52171	35610	• 55303	·36955	• 58617	.38319	•62125	55
56		.52222	35632	• 55357	·36978	• 58674	.38342	•62185	56
57		.52273	35654	• 55411	·37000	• 58731	.38365	•62246	57
58		.52323	35677	• 55465	·37023	• 58788	.38388	•62306	58
59		.52374	35699	• 55518	·37045	• 58845	.38411	•62366	59
60 ~	·34394	• 52425	.35721	•55572	.37068	•58902	.38434	.62427	60

TABLE X .- NATURAL VERSED SINES AND EXTERNAL SECANTS.

	52°			53°	54°		55°		
•	Vers.	Ex. sec.	Vers.	Ex. sec.	Vers.	Ex. sec.	Vers.	Ex. sec.	,
01234	·38434 ·38457 ·38480 ·38503 ·38526	•62427 •62487 •62548 •62609 •62669	·39819 ·39842 ·39865 ·39888 ·39911	.66164 .66228 .66292 .66357 .66421	$     \begin{array}{r}         & \cdot 41221 \\         & \cdot 41245 \\         & \cdot 41269 \\         & \cdot 41292 \\         & \cdot 41316 \\     \end{array} $	•70130 •70198 •70267 •70335 •70403	$     \begin{array}{r}         & \cdot 42642 \\         & \cdot 42668 \\         & \cdot 42690 \\         & \cdot 42714 \\         & \cdot 42738 \\     \end{array} $	.74345 .74417 .74490 .74562 .74635	0 1 2 3 4
56789	·38549 ·38571 ·38594 ·38617 ·38640	·62730 ·62791 ·62852 ·62913 ·62974	·39935 ·39958 ·39981 ·40005 ·40028	$     \begin{array}{r}         \cdot 66486 \\         \cdot 66550 \\         \cdot 66615 \\         \cdot 66679 \\         \cdot 66744 \\         \end{array} $	·41339 ·41363 ·41386 ·41410 ·41433	.70472 .70540 .70609 .70677 .70746	·42762 ·42785 ·42809 ·42833 ·42857	·74708 ·74781 ·74854 ·74927 ·75000	5 6 7 8 9
10	·38663	·63035	.40051	•66809	.41457     .41481     .41504     .41528     .41551	·70815	·42881	·75073	10
11	·38686	·63096	.40074	•66873		·70884	·42905	·75146	11
12	·38709	·63157	.40098	•66938		·70953	·42929	·75219	12
13	·38732	·63218	.40121	•67003		·71022	·42953	·75293	13
14	·38755	·63279	.40144	•67068		·71091	·42976	·75366	14
15 16 17 18 19	.38778 .38801 .38824 .38847 .38847 .38870	$     \begin{array}{r}                                     $	.40168 .40191 .40214 .40237 .40261	.67133 .67199 .67264 .67329 .67394	$   .41575 \\   .41599 \\   .41622 \\   .41646 \\   .41670 $	•71160 •71229 •71298 •71368 •71437	•43000 •43024 •43048 •43072 •43096	.75440 .75513 .75587 .75661 .75734	15 16 17 18 19
20	.38893	•63648	•40284	$     \begin{array}{r}                                     $	·41693	·71506	·43120	.75808	20
21	.38916	•63710	•40307		·41717	·71576	·43144	.75882	21
22	.38939	•63772	•40331		·41740	·71646	·43168	.75956	22
23	.38962	•63834	•40354		·41764	·71715	·43192	.76031	23
24	.38985	•63895	•40378		·41788	·71785	·43216	.76105	24
25	.39009	·63957	.40401	·67788	.41811	·71855	· 43240	·76179	25
26	.39032	·64019	.40424	·67853	.41835	·71925	· 43264	·76253	26
27	.39055	·64081	.40448	·67919	.41859	·71995	· 43287	·76328	27
28	.39078	·64144	.40471	·67985	.41882	·72065	· 43311	·76402	28
29	.39101	·64206	.40494	·68051	.41906	·72135	· 43335	·76477	29
30	.39124	.64268	·40518	·68117	.41930	•72205	•43359	·76552	30
31	.39147	.64330	·40541	·68183	.41953	•72275	•43883	·76626	31
32	.39170	.64393	·40565	·68250	.41977	•72346	•43407	·76701	32
33	.39193	.64455	·40588	·68316	.42001	•72416	•43431	·76776	33
34	.39216	.64518	·40611	·68382	.42024	•72487	•43455	·76851	34
35	.39239	.64580	•40635	.68449     .68515     .68582     .68648     .68715     .	.42048	·72557	·43479	·76926	35
36	.39262	.64643	•40658		.42072	·72628	·43503	·77001	36
37	.39286	.64705	•40682		.42096	·72698	·43527	·77077	37
38	.39309	.64768	•40705		.42119	·72769	·43551	·77152	38
39	.39332	.64831	•40728		.42143	·72840	·43575	·77227	39
40	·39355	·64894	·40752	·68782	$     \begin{array}{r}         & \cdot 42167 \\         & \cdot 42191 \\         & \cdot 42214 \\         & \cdot 42238 \\         & \cdot 42262 \\     \end{array} $	·72911	·43599	•77303	40
41	·39378	·64957	·40775	·68848		·72982	·43623	•77378	41
42	·39401	·65020	·40799	·68915		·73053	·43647	•77454	42
43	·39424	·65083	·40822	·68982		·73124	·43671	•77530	43
44	·39447	·65146	·40846	·69049		·73195	·43695	•77606	44
45	.39471	·65209	.40869   .40893   .40916   .40939   .40963	.69116	·42285	·73267	.43720	.77681	45
46	.39494	·65272		.69183	·42309	·73338	.43744	.77757	46
47	.39517	·65336		.69250	·42333	·73409	.43768	.77833	47
48	.39540	·65399		.69318	·42357	·73481	.43792	.77910	48
49	.39563	·65462		.69385	·42381	·73552	.43816	.77986	49
50	·39586	·65526	·40986	.69452	•42404	•73624	.43840	·78062	50
51	·39610	·65589	·41010	.69520	•42428	•73696	.43864	·78138	51
52	·39633	·65653	·41033	.69587	•42452	•73768	.43888	·78215	52
53	·39656	·65717	·41057	.69655	•42476	•73840	.43912	·78291	53
54	·39679	·65780	·41080	.69723	•42499	•73911	.43936	·78368	54
55	·39702	·65844	.41104	.69790	•42523	.73983	·43960	.78445	55
56	·39726	·65908	.41127	.69858	•42547	.74056	·43984	.78521	56
57	·39749	·65972	.41151	.69926	•42571	.74128	·44008	.78598	57
58	·39772	·66036	.41174	.69994	•42595	.74200	·44032	.78675	58
59	·39795	·66100	.41198	.70062	•42619	.74272	·44057	.78752	59
60	.39819	·66164	.41221	•70130	•42642	•74345	•44081	•78829	60

56°

TABLE X.-NATURAL VERSED SINES AND EXTERNAL SECANTS.

58°

57°

	56°		57°		58°		59°		
,	Vers.	Ex. sec.							
0	·44081	·78829	·45536	- 83608	·47008	- 88708	·48496	·94160	0
1	·44105	·78906	·45560	- 83690	·47033	- 88796	·48521	·94254	1
2	·44129	·78984	·45585	- 83773	·47057	- 88884	·48546	·94349	2
3	·44153	·79061	·45609	- 83855	·47082	- 88972	·48571	·94443	3
4	·44177	·79138	·45634	- 83938	·47107	- 89060	·48596	·94537	4
5	.44201	.79216	·45658	-84020	.47131	.89148	.48621	·94632	5
6	.44225	.79293	·45683	-84103	.47156	.89237	.48646	·94726	6
7	.44250	.79371	·45707	-84186	.47181	.89325	.48671	·94821	7
8	.44274	.79449	·45731	-84269	.47206	.89414	.48696	·94916	8
9	.44298	.79527	·45756	-84352	.47230	.89503	.48721	·95011	9
10	.44322	.79604	.45780	.84435	.47255	.89591	·48746	·95106	10
11	.44346	.79682	.45805	.84518	.47280	.89680	·48771	·95201	11
12	.44370	.79761	.45829	.84601	.47304	.89769	·48796	·95296	12
13	.44395	.79839	.45854	.84685	.47329	.89858	·48821	·95392	13
14	.44419	.79917	.45878	.84768	.47354	.89948	·48846	·95487	14
15	·44443	.79995	.45903	.84852	·47379	.90037	.48871	.95583	15
16	·44467	.80074	.45927	.84935	·47403	.90126	.48896	.95678	16
17	·44491	.80152	.45951	.85019	·47428	.90216	.48921	.95774	17
18	·44516	.80231	.45976	.85103	·47453	.90305	.48946	.95870	18
19	·44540	.80309	.46000	.85187	·47478	.90395	.48971	.95966	19
20	·44564	- 80388	·46025	.85271	·47502	.90485	·48996	.96062	20
21	·44588	- 80467	·46049	.85355	·47527	.90575	·49021	.96158	21
22	·44612	- 80546	·46074	.85439	·47552	.90665	·49046	.96255	22
23	·44637	- 80625	·46098	.85523	·47577	.90755	·49071	.96351	23
24	·44661	- 80704	·46123	.85608	·47601	.90845	·49096	.96448	24
25	·44685	-80783	·46147	-85692	·47626	.90935	.49121	.96544	25
26	·44709	-80862	·46172	-85777	·47651	.91026	.49146	.96641	26
27	·44734	-80942	·46196	-85861	·47676	.91116	.49171	.96738	27
28	·44758	-81021	·46221	-85946	·47701	.91207	.49196	.96835	28
29	·44782	-81101	·46246	-86031	·47725	.91297	.49221	.96932	29
30	.44806	.81180	·46270	.86116	·47750	.91388	·49246	·97029	30
31	.44831	.81260	·46295	.86201	·47775	.91479	·49271	·97127	31
32	.44855	.81340	·46319	.86286	·47800	.91570	·49296	·97224	32
33	.44879	.81419	·46344	.86371	·47825	.91661	·49321	·97322	33
34	.44903	.81499	·46368	.86457	·47849	.91752	·49346	·97420	34
35	.44928	.81579	·46393	·86542	·47874	·91844	·49372	.97517	35
36	.44952	.81659	·46417	·86627	·47899	·91935	·49397	.97615	36
37	.44976	.81740	·46442	·86713	·47924	·92027	·49422	.97713	37
38	.45001	.81820	·46466	·86799	·47949	·92118	·49447	.97811	38
39	.45025	.81900	·46491	·86885	·47974	·92210	·49472	.97910	39
40	·45049	·81981	·46516	·86970	·47998	·92302	·49497	·98008	40
41	·45073	·82061	·46540	·87056	·48023	·92394	·49522	·98107	41
42	·45098	·82142	·46565	·87142	·48048	·92486	·49547	·98205	42
43	·45122	·82222	·46589	·87229	·48073	·92578	·49572	·98304	43
44	·45146	·82303	·46614	·87315	·48098	·92670	·49597	·98403	44
45	.45171	·82384	· 46639	·87401	.48123	.92762	·49623	.98502	45
46	.45195	·82465	· 46663	·87488	.48148	.92855	·49648	.98601	46
47	.45219	·82546	· 46688	·87574	.48172	.92947	·49673	.98700	47
48	.45244	·82627	· 46712	·87661	.48197	.93040	·49698	.98799	48
49	.45268	·82709	· 46737	·87748	.48222	.93133	·49723	.98899	49
50	· 45292	·82790	· 46762	·87834	· 48247	·93226	· 49748	.98998	50
51	· 45317	·82871	· 46786	·87921	· 48272	·93319	· 49773	.99098	51
52	· 45341	·82953	· 46811	·88008	· 48297	·93412	· 49799	.99198	52
53	· 45365	·83034	· 46836	·88095	· 48322	·93505	· 49824	.99298	53
54	· 45390	·83116	· 46860	·88183	· 48347	·93598	· 49849	.99398	54
55	· 45414	·83198	· 46885	·88270	.48372	·93692	.49874	·99498	55
56	· 45439	·83280	· 46909	·88357	.48396	·93785	.49899	·99598	56
57	· 45463	·83362	· 46934	·88445	.48421	·93879	.49924	·99698	57
58	· 45487	·83444	· 46959	·88532	.48446	·93973	.49950	·99799	58
59	· 45512	·83526	· 46983	·88620	.48471	·94066	.49975	·99899	59
60	. 45536	• 83608	·47008	·88708	·48496	•94160	.50000	1.00000	60
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TABLE X .- NATURAL VERSED SINES AND EXTERNAL SECANTS.

60°		61°		62°		63°			
-	Vers.	Ex. sec.	Vers.	Ex. sec.	Vers.	Ex. sec.	Vers.	Ex. sec.	1.
01234	· 50000 · 50025 · 50050 · 50076 · 50101	1.000001.001011.002021.003031.00404	.51519 .51544 .51570 .51595 .51621	1.062671.063751.064831.065921.06701	- 53053 - 53079 - 53104 - 53130 - 53156	1.130051.131221.132391.133561.13473	·54601 ·54627 ·54653 ·54679 ·54705	$1 \cdot 20269 \\ 1 \cdot 20395 \\ 1 \cdot 20521 \\ 1 \cdot 20647 \\ 1 \cdot 20773$	$     \begin{array}{c}             0 \\             1 \\           $
5 6 7 8 9	·50126 ·50151 ·50176 ·50202 ·50227	1.005051.006071.007081.008101.00912	·51646 ·51672 ·51697 ·51723 ·51748	1.068091.069181.070271.071371.07246	· 53181 · 53207 · 53233 · 53258 · 53284	$\begin{array}{r} 1.13590 \\ 1.13707 \\ 1.13825 \\ 1.13942 \\ 1.14060 \end{array}$	· 54731 · 54757 · 54782 · 54808 · 54834	1.209001.210261.211531.212801.21407	5 6 7 8 9
10 11 12 13 14	· 50252 · 50277 · 50303 · 50328 · 50353	$\begin{array}{c} 1 \cdot 01014 \\ 1 \cdot 01116 \\ 1 \cdot 01218 \\ 1 \cdot 01320 \\ 1 \cdot 01422 \end{array}$	·51774 ·51799 ·51825 ·51850 ·51876	1.073561.074651.075751.076851.07795	- 53310 - 53336 - 53361 - 53387 - 53413	$\begin{array}{r}1\cdot 14178\\1\cdot 14296\\1\cdot 14414\\1\cdot 14533\\1\cdot 14651\end{array}$	·54860 ·54886 ·54912 ·54938 ·54964	$\begin{array}{r} 1.21535 \\ 1.21662 \\ 1.21790 \\ 1.21918 \\ 1.22045 \end{array}$	$     \begin{array}{r}       10 \\       11 \\       12 \\       13 \\       14     \end{array} $
15 16 17 18 19	· 50378 · 50404 · 50429 · 50454 · 50479	1.01525 1.01628 1.01730 1.01833 1.01936	·51901 ·51927 ·51952 ·51978 ·52003	1.079051.080151.081261.082361.08347	·53439 ·53464 ·53490 ·53516 ·53542	1.14770 1.14889 1.15008 1.15127 1.15246	- 54990 - 55016 - 55042 - 55068 - 55094	1.221741.223021.224301.225591.22688	15 16 17 18 19
20 21 22 23 24	· 50505 · 50530 · 50555 · 50581 · 50606	1.020391.021431.022461.023491.02453	- 52029 - 52054 - 52080 - 52105 - 52131	1.084581.085691.086801.087911.08903	-53567 -53593 -53619 -53645 -53670	1.15366 1.15485 1.15605 1.15725 1.15845	- 55120 - 55146 - 55172 - 55198 - 55224	$\begin{array}{r} 1\cdot 22817\\ 1\cdot 22946\\ 1\cdot 23075\\ 1\cdot 23205\\ 1\cdot 23334 \end{array}$	20 21 22 23 24
25 26 27 28 29	- 50631 - 50656 - 50682 - 50707 - 50732	1.025571.026611.027651.028691.02973	· 52156 · 52182 · 52207 · 52233 · 52259	1.09014 1.09126 1.09238 1.09350 1.09462	·53696 ·53722 ·53748 ·53774 ·53799	1.15965 1.16085 1.16206 1.16326 1.16447	- 55250 - 55276 - 55302 - 55328 - 55354	1.234641.235941.237241.238551.23985	25 26 27 28 29
30 81 32 33 34	· 50758 · 50783 · 50808 · 50834 · 50859	$1.03077 \\ 1.03182 \\ 1.03286 \\ 1.03391 \\ 1.03496 \\ 1.03$	• 52284 • 52310 • 52335 • 52361 • 52386	1.09574 1.09686 1.09799 1.09911 1.10024	- 53825 - 53851 - 53877 - 53903 - 53928	1.16568 1.16689 1.16810 1.16932 1.17053	- 55380 - 55406 - 55432 - 55458 - 55484	1.241161.242471.243781.245091.24640	30 31 32 33 34
35 36 37 38 39	·50884 ·50910 ·50935 ·50960 ·50986	1.03601 1.03706 1.03811 1.03916 1.04022	- 52412 - 52438 - 52463 - 52489 - 52514	1.101371.102501.103631.104771.10590	- 53954 - 53980 - 54006 - 54032 - 54058	1.17175 1.17297 1.17419 1.17541 1.17663	.55510 .55536 .55563 .55589 .55615	1.247721.249031.250351.251671.25300	35 36 37 38 39
40 41 42 43 44	·51011 ·51036 ·51062 ·51087 ·51113	1.04128 1.04233 1.04339 1.04445 1.04551	- 52540 - 52566 - 52591 - 52617 - 52642	1.10704 1.10817 1.10931 1.11045 1.11159	·54083 ·54109 ·54135 ·54161 ·54187	1.17786 1.17909 1.18031 1.18154 1.18277	·55641 ·55667 ·55693 ·55719 ·55745	$1 \cdot 25432$ $1 \cdot 25565$ $1 \cdot 25697$ $1 \cdot 25830$ $1 \cdot 25963$	40 41 42 43 44
45 46 47 48 49	.51138 .51163 .51189 .51214 .51239	1.04658 1.04764 1.04870 1.04977 1.05084	·52668 ·52694 ·52719 ·52745 ·52771	1.11274 1.11388 1.11503 1.11617 1.11617 1.11732	·54213 ·54238 ·54264 ·54290 ·54316	1.18401 1.18524 1.18648 1.18772 1.18895	.55771 .55797 .55823 .55849 .55876	1.260971.262301.263641.264981.26632	45 46 47 48 49
50 51 52 53 54	.51265 .51290 .51316 .51341 .51366	$ \begin{array}{r} 1.05191\\ 1.05298\\ 1.05405\\ 1.05512\\ 1.05619 \end{array} $	·52796 ·52822 ·52848 ·52873 ·52899	1.11847 1.11963 1.12078 1.12193 1.12309	·54342 ·54368 ·54394 ·54420 ·54446	1.19019 1.19144 1.19268 1.19393 1.19517	·55902 ·55928 ·55954 ·55980 ·56006	1.26766 1.26900 1.27035 1.27169 1.27304	50 51 52 53 54
55 56 57 58 59	.51392 .51417 .51443 .51468 .51494	$ \begin{array}{r} 1.05727\\ 1.05835\\ 1.05942\\ 1.06050\\ 1.06158 \end{array} $	·52924 ·52950 ·52976 ·53001 ·53027	$ \begin{array}{r} 1.12425\\1.12540\\1.12657\\1.12773\\1.12773\\1.12889\end{array} $	·54471 ·54497 ·54523 ·54549 ·54575	1.196421.197671.198921.200181.20143	·56084 ·56111	1.27439 1.27574 1.27710 1.27845 1.27981	55 56 57 58 55
60	• 51519	1.06267	• 53053	1.13005	• 54601	1.20269	.56163	1.28117	60

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TABLE X.-NATURAL VERSED SINES AND EXTERNAL SECANTS.

TABLE X.—NATUR 64°			AL VERSED S. 65°		66°		TERNAL SECANI 67°		NTS.
,	Vers.	Ex. sec.	Vers.	Ex. sec.	Vers.	Ex. sec.	Vers.	Ex. sec.	
0 1 2 3 4	• 56163 • 56189 • 56215 • 56241 • 56267	1.281171.282531.283901.285261.28663	· 57738 · 57765 · 57791 · 57817 · 57844	$1.36620 \\ 1.36768 \\ 1.36916 \\ 1.37064 \\ 1.37212$	· 59326 · 59353 · 59379 · 59406 · 59433	1.458591.460201.461811.463421.46504	·60927 ·60954 ·60980 ·61007 ·61034	$\begin{array}{r} 1.55930\\ 1.56106\\ 1.56282\\ 1.56458\\ 1.56634\\ 1.56634 \end{array}$	01234
5 6 7 8 9	· 56294 · 56320 · 56346 · 56372 · 56398	1.28800 1.28937 1.29074 1.29211 1.29349	57870 57896 57923 57949 57976	$\begin{array}{r} 1\cdot 37361 \\ 1\cdot 37509 \\ 1\cdot 37658 \\ 1\cdot 37808 \\ 1\cdot 37957 \end{array}$	·59459 ·59486 ·59512 ·59539 ·59566	1.466651.468271.469891.471521.47314	·61061 ·61088 ·61114 ·61141 ·61168	1.568111.569881.571651.573421.57520	56789 9
10 11 12 13 14	- 56425 - 56451 - 56477 - 56503 - 56529	$1 \cdot 29487$ $1 \cdot 29625$ $1 \cdot 29763$ $1 \cdot 29901$ $1 \cdot 30040$	.58002 .58028 .58055 .58081 .58108	1.381071.382561.384061.385561.38707	.59592 .59619 .59645 .59672 .59699	1.47477 1.47640 1.47804 1.47967 1.48131	·61195 ·61222 ·61248 ·61275 ·61302	1.57698 1.57876 1.58054 1.58233 1.58412	10 11 12 13 14
15 16 17 18 19	·56555 ·56582 ·56608 ·56634 ·56660	1.301791.303181.304571.305961.30735	.58134 .58160 .58187 .58213 .58240	1.38857 1.39008 1.39159 1.39311 1.39462	- 59725 - 59752 - 59779 - 59805 - 59832	1.48295 1.48459 1.48624 1.48789 1.48954	·61329 ·61356 ·61383 ·61409 ·61436	1.58591 1.58771 1.58950 1.59130 1.59311	15 16 17 18 19
20 21 22 23 24	- 56687 - 56713 - 56739 - 56765 - 56791	$\begin{array}{r} 1\cdot 30875\\ 1\cdot 31015\\ 1\cdot 31155\\ 1\cdot 31295\\ 1\cdot 31436 \end{array}$	· 58266 · 58293 · 58319 · 58345 · 58372	1.396141.397661.399181.400701.40222	- 59859 - 59885 - 59912 - 59938 - 59965	1.491191.492841.494501.496161.49782	.61463 .61490 .61517 .61544 .61570	1.594911.596721.598531.600351.60217	20 21 22 23 24
25 26 27 28 29	- 56818 - 56844 - 56870 - 56896 - 56923	1.31576 1.31717 1.31858 1.31999 1.32140	- 58398 - 58425 - 58451 - 58478 - 58504	1.403751.405281.406811.408351.40988	- 59992 - 60018 - 60045 - 60072 - 60098	$\begin{array}{r} 1.49948 \\ 1.50115 \\ 1.50282 \\ 1.50449 \\ 1.50617 \end{array}$	·61597 ·61624 ·61651 ·61678 ·61705	1.603991.605811.607631.609461.61129	25 26 27 28 29
$30 \\ 31 \\ 32 \\ 33 \\ 34$	- 56949 - 56975 - 57001 - 57028 - 57054	$\begin{array}{r} 1\cdot 32282 \\ 1\cdot 32424 \\ 1\cdot 32566 \\ 1\cdot 32708 \\ 1\cdot 32850 \end{array}$	- 58531 - 58557 - 58584 - 58610 - 58637	1.41142 1.41296 1.41450 1.41605 1.41760	-60125 -60152 -60178 -60205 -60232	1.50784 1.50952 1.51120 1.51289 1.51457	·61732 ·61759 ·61785 ·61812 ·61839	1.61313 1.61496 1.61680 1.61864 1.62049	30 31 32 33 33 34
35 36 37 38 39	·57080 ·57106 ·57133 ·57159 ·57185	$\begin{array}{r} 1.32993 \\ 1.33135 \\ 1.33278 \\ 1.33422 \\ 1.33565 \end{array}$	- 58663 - 58690 - 58716 - 58743 - 58769	1.419141.420701.422251.423801.42536	· 60259 · 60285 · 60312 · 60339 · 60365	1.51626 1.51795 1.51965 1.52134 1.52304	·61866 ·61893 ·61920 ·61947 ·61974	1.622341.624191.626041.627901.62976	35 36 37 38 39
$40 \\ 41 \\ 42 \\ 43 \\ 44$	·57212 ·57238 ·57264 ·57291 ·57317	1.33708 1.33852 1.33996 1.34140 1.34284	- 58796 - 58822 - 58849 - 58875 - 58902	1.42692 1.42848 1.43005 1.43162 1.4318	· 60392 · 60419 · 60445 · 60472 · 60499	$1.52474 \\ 1.52645 \\ 1.52815 \\ 1.52986 \\ 1.53157$	· 62001 · 62027 · 62054 · 62081 · 62108	$1 \cdot 63162 \\ 1 \cdot 63348 \\ 1 \cdot 63535 \\ 1 \cdot 63722 \\ 1 \cdot 63909$	40 41 42 43 44
45 46 47 48 49	· 57343 · 57369 · 57396 · 57422 · 57448	$1.34429 \\ 1.34573 \\ 1.34718 \\ 1.34863 \\ 1.35009$	·58928 ·58955 ·58981 ·59008 ·59034	1.43476 1.43633 1.43790 1.43948 1.44106	·60526 ·60552 ·60579 ·60606 ·60633	1.533291.535001.536721.538451.54017	·62135 ·62162 ·62189 ·62216 ·62243	1.640971.642851.644731.646621.64851	45 46 47 48 49
50 51 52 53 54	·57475 ·57501 ·57527 ·57554 ·57580	$1.35154 \\ 1.35300 \\ 1.35446 \\ 1.35592 \\ 1.35738$	·59061 ·59087 ·59114 ·59140 ·59167	1.442641.444231.445821.447411.44900	·60659 ·60686 ·60713 ·60740 ·60766	$1.54190 \\ 1.54363 \\ 1.54536 \\ 1.54709 \\ 1.54883$	·62270 ·62297 ·62324 ·62351 ·62378	1.650401.652291.654191.656091.65799	50 51 52 53 54
55 56 57 58 59	·57606 ·57633 ·57659 ·57685 ·57712	1.358851.360311.361781.363251.36473	.59194 .59220 .59247 .59273 .59300	1.450591.452191.453781.455391.45699	·60793 ·60820 ·60847 ·60873 ·60900	$\begin{array}{r} 1.55057\\ 1.55231\\ 1.55405\\ 1.55580\\ 1.55755\\ \end{array}$	·62405 ·62431 ·62458 ·62485 ·62512	1.659891.661801.663711.665631.66755	55 56 57 58 59
60 	. 57738	1.36620	.59326	1.45859	· 60927	1.55930	· 62539	1.66947	60

TABLE X.—NATURA 68°

TABLE X .- NATURAL VERSED SINES AND EXTERNAL SECANTS.

70°

69°

71°

_	C	8		9		0		1	
,	Vers.	Ex. sec.	Vers.	Ex. sec.	Vers.	Ex. sec.	Vers.	Ex. sec.	•
0 1 2 3 4	·62539 ·62566 ·62593 ·62620 ·62647	1.669471.671391.673321.675251.67718	$     \begin{array}{r}         \cdot 64163 \\         \cdot 64190 \\         \cdot 64218 \\         \cdot 64245 \\         \cdot 64272 \\     \end{array} $	1.790431.792541.794661.796791.79891	·65798 ·65825 ·65853 ·65880 ·65907	$\begin{array}{r} 1.92380\\ 1.92614\\ 1.92849\\ 1.93083\\ 1.93318 \end{array}$	· 67443 · 67471 · 67498 · 67526 · 67553	$\begin{array}{r} 2.07155\\ 2.07415\\ 2.07675\\ 2.07936\\ 2.08197 \end{array}$	0. 1 2 3 4
5 6 7 8 9	·62674 ·62701 ·62728 ·62755 ·62782	1.679111.681051.682991.684941.68689	· 64299 · 64326 · 64353 · 64381 · 64408	1.80104 1.80318 1.80531 1.80746 1.80960	·65935 ·65962 ·65989 ·66017 ·66044	1.935541.937901.940261.942631.94500	·67581 ·67608 ·67636 ·67663 ·67691	2.08459 2.08721 2.08983 2.09246 2.09510	5 6 7 8 9
10 11 12 13 14	-62809 -62836 -62863 -62890 -62917	1.688841.690791.692751.694711.69667	· 64435 · 64462 · 64489 · 64517 · 64544	1.81175 1.81390 1.81605 1.81821 1.82037	·66071 ·66099 ·66126 ·66154 ·66181	$\begin{array}{r} 1.94737 \\ 1.94975 \\ 1.95213 \\ 1.95452 \\ 1.95691 \end{array}$	·67718 ·67746 ·67773 ·67801 ·67829	2.09774 2.10038 2.10303 2.10568 2.10834	$10 \\ 11 \\ 12 \\ 13 \\ 14$
15 16 17 18 19	·62944 ·62971 ·62998 ·63025 ·63052	1.698641.700611.702581.704551.70653	·64571 ·64598 ·64625 ·64653 ·64680	$1 \cdot 82254 \\ 1 \cdot 82471 \\ 1 \cdot 82688 \\ 1 \cdot 82906 \\ 1 \cdot 83124$	· 66208 · 66236 · 66263 · 66290 · 66318	1.95931 1.96171 1.96411 1.96652 1.96893	-67856 -67884 -67911 -67939 -67966	$2 \cdot 11101$ $2 \cdot 11367$ $2 \cdot 11635$ $2 \cdot 11903$ $2 \cdot 12171$	15 16 17 18 19
20 21 22 23 24	·63079 ·63106 ·63133 ·63161 ·63188	1.70851 1.71050 1.71249 1.71448 1.71647	· 64707 · 64734 · 64761 · 64789 · 64816	$1 \cdot 83342 \\1 \cdot 83561 \\1 \cdot 83780 \\1 \cdot 83999 \\1 \cdot 84219$	·66345 ·66373 ·66400 ·66427 ·66455	1.97135 1.97377 1.97619 1.97862 1.98106	·67994 ·68021 ·68049 ·68077 ·68104	$\begin{array}{r} 2 \cdot 12440 \\ 2 \cdot 12709 \\ 2 \cdot 12979 \\ 2 \cdot 13249 \\ 2 \cdot 13520 \end{array}$	20 21 22 23 24
25 26 27 28 29	-63215 -63242 -63269 -63296 -63323	1.71847 1.72047 1.72247 1.72448 1.72649	- 64843 - 64870 - 64898 - 64925 - 64952	1.84439 1.84659 1.84880 1.85102 1.85323	·66482 ·66510 ·66537 ·66564 ·66592	1.98349 1.98594 1.98838 1.99083 1.99329	-68132 -68159 -68187 -68214 -68242	$2 \cdot 13791$ $2 \cdot 14063$ $2 \cdot 14335$ $2 \cdot 14608$ $2 \cdot 14881$	25 26 27 28 29
30 31 32 33 34	-63350 -63377 -63404 -63431 -63458	1.728501.730521.732541.734561.73659	· 64979 · 65007 · 65034 · 65061 · 65088	1.85545 1.85767 1.85990 1.86213 1.86437	· 66619 · 66647 · 66674 · 66702 · 66729	1.995741.998212.000672.003152.00562	- 68270 - 68297 - 68325 - 68352 - 68380	$\begin{array}{r} 2 \cdot 15155 \\ 2 \cdot 15429 \\ 2 \cdot 15704 \\ 2 \cdot 15979 \\ 2 \cdot 16255 \end{array}$	30 31 32 33 34
35 36 37 38 39	· 63485 · 63512 · 63539 · 63566 · 63594	1.738621.740651.742691.744731.74677	·65116 ·65143 ·65170 ·65197 ·65225	1.86661 1.86885 1.87109 1.87334 1.87560	-66756 -66784 -66811 -66839 -66866	$\begin{array}{r} 2.00810\\ 2.01059\\ 2.01308\\ 2.01557\\ 2.01807 \end{array}$	- 68408 - 68435 - 68463 - 68490 - 68518	$2 \cdot 16531$ $2 \cdot 16808$ $2 \cdot 17085$ $2 \cdot 17363$ $2 \cdot 17641$	35 36 37 38 39
40 41 42 43 44	· 63621 · 63648 · 63675 · 63702 · 63729	1.74881 1.75086 1.75292 1.75497 1.75703	·65252 ·65279 ·65306 ·65334 ·65361	$1 \cdot 87785$ $1 \cdot 88011$ $1 \cdot 88238$ $1 \cdot 88465$ $1 \cdot 88692$	·66894 ·66921 ·66949 ·66976 ·67003	2.02057 2.02308 2.02559 2.02810 2.03062	- 68546 - 68573 - 68601 - 68628 - 68656	$2 \cdot 17920$ $2 \cdot 18199$ $2 \cdot 18479$ $2 \cdot 18759$ $2 \cdot 19040$	$40 \\ 41 \\ 42 \\ 43 \\ 44$
45 46 47 48 49	-63756 -63783 -63810 -63838 -63865	1.75909 1.76116 1.76323 1.76530 1.76737	·65388 ·65416 ·65443 ·65470 ·65497	1.88920 1.89148 1.89376 1.89605 1.89834	-67031 -67058 -67086 -67113 -67141	$\begin{array}{r} 2.03315\\ 2.03568\\ 2.03821\\ 2.04075\\ \underline{2.04329}\end{array}$	·68684 ·68711 ·68739 ·68767 ·68794	2.19322 2.19604 2.19886 2.20169 2.20453	45 46 47 48 49
50 51 52 53 54	·63892 ·63919 ·63946 ·63973 ·64000	1.76945 1.77154 1.77362 1.77571 1.77780	·65525 ·65552 ·65579 ·65607 ·65634	1.900631.902931.905241.907541.90986	·67168 ·67196 ·67223 ·67251 ·67278	$\begin{array}{r} 2.04584 \\ 2.04839 \\ 2.05094 \\ 2.05350 \\ 2.05607 \end{array}$	· 68822 · 68849 · 68877 · 68905 · 68932	$\begin{array}{r} 2 \cdot 20737 \\ 2 \cdot 21021 \\ 2 \cdot 21306 \\ 2 \cdot 21592 \\ 2 \cdot 21878 \end{array}$	$50 \\ 51 \\ 52 \\ 53 \\ 54$
55 56 57 58 59	·64027 ·64055 ·64082 ·64109 ·64136	1.77990 1.78200 1.78410 1.78621 1.78832	·65661 ·65689 ·65716 ·65743 ·65771	$\begin{array}{r} 1.91217 \\ 1.91449 \\ 1.91681 \\ 1.91914 \\ 1.92147 \end{array}$	·67306 ·67333 ·67361 ·67388 ·67416	$\begin{array}{r} 2.05864 \\ 2.06121 \\ 2.06379 \\ 2.06637 \\ 2.06896 \end{array}$	-68960 -68988 -69015 -69043 -69071	$\begin{array}{r} 2 \cdot 22165 \\ 2 \cdot 22452 \\ 2 \cdot 22740 \\ 2 \cdot 23028 \\ 2 \cdot 23317 \end{array}$	55 56 57 58 59
60	·64163	1.79043	·65798	1.92380	· 67443	2.07155	· 69098	2.23607	60
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TABLE X.-NATURAL VERSED SINES AND EXTERNAL SECANTS.

		72°	1	73°	3	4°	7	5°	
,	Vers.	Ex. sec.	Vers.	·Ex. sec.	Vers.	Ex. sec.	Vers.	Ex. sec.	•
0 1 2 3 4	·69098 ·69126 ·69154 ·69181 ·69209	$\begin{array}{r} 2\cdot23607\\ 2\cdot23897\\ 2\cdot24187\\ 2\cdot24478\\ 2\cdot24478\\ 2\cdot24770\end{array}$	·70763 ·70791 ·70818 ·70846 ·70874	$\begin{array}{r} 2 \cdot 42030 \\ 2 \cdot 42356 \\ 2 \cdot 42683 \\ 2 \cdot 43010 \\ 2 \cdot 43337 \end{array}$	·72436 ·72464 ·72492 ·72520 ·72548	$\begin{array}{r} 2 \cdot 62796 \\ 2 \cdot 63164 \\ 2 \cdot 63533 \\ 2 \cdot 63903 \\ 2 \cdot 64274 \end{array}$	·74118 ·74146 ·74174 ·74202 ·74231	2.86370 2.86790 2.87211 2.87633 2.88056	01234
5 6 7 8 9	- 69237 - 69264 - 69292 - 69320 - 69347	$2 \cdot 25062$ $2 \cdot 25355$ $2 \cdot 25648$ $2 \cdot 25942$ $2 \cdot 26237$	.70902 .70930 .70958 .70985 .71013	2.436662.439952.443242.446552.44986	·72576 ·72604 ·72632 ·72660 ·72688	$\begin{array}{r} 2.64645\\ 2.65018\\ 2.65391\\ 2.65765\\ 2.66140\end{array}$	·74259 ·74287 ·74315 ·74343 ·74371	2.88479 2.88904 2.89330 2.89756 2.90184	56789
10	· 69375	$\begin{array}{r} 2 \cdot 26531 \\ 2 \cdot 26827 \\ 2 \cdot 27123 \\ 2 \cdot 27420 \\ 2 \cdot 27717 \end{array}$	.71041	2.45317	·72716	2.66515	.74399	2.90613	10
11	· 69403		.71069	2.45650	·72744	2.66892	.74427	2.91042	11
12	· 69430		.71097	2.45983	·72772	2.67269	.74455	2.91473	12
13	· 69458		.71125	2.46316	·72800	2.67647	.74484	2.91904	13
14	· 69486		.71153	2.46651	·72828	2.68025	.74512	2.92337	14
15	-69514	$2 \cdot 28015$	.71180	2.46986	.72856	$2 \cdot 68405$	·74540	2.92770	15
16	-69541	$2 \cdot 28313$	.71208	2.47321	.72884	$2 \cdot 68785$	·74568	2.93204	16
17	-69569	$2 \cdot 28612$	.71236	2.47658	.72912	$2 \cdot 69167$	·74596	2.93640	17
18	-69597	$2 \cdot 28912$	.71264	2.47995	.72940	$2 \cdot 69549$	·74624	2.94076	18
19	-69624	$2 \cdot 29212$	.71292	2.48333	.72968	$2 \cdot 69931$	·74652	2.94514	19
20	· 69652	2.29512	.71320	2.48671	.72996	2.70315	·74680	2.94952	20
21	· 69680	2.29814	.71348	2.49010	.73024	2.70700	·74709	2.95392	21
22	· 69708	2.30115	.71375	2.49350	.73052	2.71085	·74737	2.95832	22
23	· 69735	2.30418	.71403	2.49691	.73080	2.71471	·74765	2.96274	23
24	· 69763	2.30721	.71431	2.50032	.73108	2.71858	·74793	2.96716	24
25	- 69791	2.31024	.71459	$\begin{array}{r} 2.50374 \\ 2.50716 \\ 2.51060 \\ 2.51404 \\ 2.51748 \end{array}$	·73136	2.72246	.74821	2.97160	25
26	- 69818	2.31328	.71487		·73164	2.72635	.74849	2.97604	26
27	- 69846	2.31633	.71515		·73192	2.73024	.74878	2.98050	27
28	- 69874	2.31939	.71543		·73220	2.73414	.74906	2.98497	28
29	- 69902	2.32244	.71571		·73248	2.73806	.74934	2.98944	29
30 31 32 33 34	· 69929 · 69957 · 69985 · 70013 · 70040	$2 \cdot 32551$ $2 \cdot 32858$ $2 \cdot 33166$ $2 \cdot 33474$ $2 \cdot 33783$	.71598 .71626 .71654 .71682 .71710	2.52094 2.52440 2.52787 2.53134 2.53482		2.74198 2.74591 2.74984 2.75379 2.75775	.74962 .74990 .75018 .75047 .75075	$\begin{array}{c} 2.99393\\ 2.99843\\ 3.00293\\ 3.00745\\ 3.01198 \end{array}$	30 31 32 33 34
35	.70068	$\begin{array}{r} 2\cdot 34092 \\ 2\cdot 34403 \\ 2\cdot 34713 \\ 2\cdot 35025 \\ 2\cdot 35336 \end{array}$	·71738	2.53831	.73416	2.76171	·75103	3.01652	35
36	.70096		·71766	2.54181	.73444	2.76568	·75131	3.02107	36
37	.70124		·71794	2.54531	.73472	2.76966	·75159	3.02563	37
38	.70151		·71822	2.54883	.73500	2.77365	·75187	3.03020	38
39	.70179		·71850	2.55235	.73529	2.77765	·75216	3.03479	39
40	.70207	$\begin{array}{r} 2.35649 \\ 2.35962 \\ 2.36276 \\ 2.36590 \\ 2.36905 \end{array}$	.71877	2.55587	·73557	2.78166	.75244	3.03938	40
41	.70235		.71905	2.55940	·73585	2.78568	.75272	3.04398	41
42	.70263		.71933	2.56294	·73613	2.78970	.75300	3.04860	42
43	.70290		.71961	2.56649	·73641	2.79374	.75328	3.05322	43
44	.70318		.71989	2.57005	·73669	2.79778	.75356	3.05786	44
45	· 70346	2.37221	·72017	2.57361	·73697	2.80183	.75385	3.06251	45
46	· 70374	2.37537	·72045	2.57718	·73725	2.80589	.75413	3.06717	46
47	· 70401	2.37854	·72073	2.58076	·73753	2.80996	.75441	3.07184	47
48	· 70429	2.38171	·72101	2.58434	·73781	2.81404	.75469	3.07652	48
49	· 70457	2.38489	·72129	2.58794	·73809	2.81813	.75497	3.08121	49
50	·70485	2.388082.391282.394482.397682.40089	.72157	2.59154	·73837	2 · 82223	·75526	3.08591	50
51	·70513		.72185	2.59514	·73865	2 · 82633	·75554	3.09063	51
52	·70540		.72213	2.59876	·73893	2 · 83045	·75582	3.09535	52
53	·70568		.72241	2.60238	·73921	2 · 83457	·75610	3.10009	53
54	·70596		.72269	2.60601	·73950	2 · 83871	·75639	3.10484	54
55 56 57 58 59	·70624 ·70652 ·70679 ·70707 ·70735	$\begin{array}{r} 2 \cdot 40411 \\ 2 \cdot 40734 \\ 2 \cdot 41057 \\ 2 \cdot 41381 \\ 2 \cdot 41705 \end{array}$	·72296 ·72324 ·72352 ·72380 ·72408	$\begin{array}{r} 2.60965\\ 2.61330\\ 2.61695\\ 2.62061\\ 2.62428\end{array}$	·73978 ·74006 ·74034 ·74062 ·74090	2.84285 2.84700 2.85116 2.85533 2.85951	·75667 ·75695 ·75723 ·75751 ·75780	$3 \cdot 10960$ $3 \cdot 11437$ $3 \cdot 11915$ $3 \cdot 12394$ $3 \cdot 12875$	55 56 57 58 59
60 	.70763	2.42030	.72436	2.62796	.74118	2.86370	•75808	3.13357	60

TABLE X .-- NATURAL VERSED SINES AND EXTERNAL SECANTS.

76°

77°

ED SINES AN 78°

79°

-		U				0		3	
•	Vers.	Ex. sec.	Vers.	Ex. sec.	Vers.	Ex. sec.	Vers.	Ex. sec.	
01234	·75808 ·75836 ·75864 ·75892 ·75921	$3 \cdot 13357$ $3 \cdot 13839$ $3 \cdot 14323$ $3 \cdot 14809$ $3 \cdot 15295$	·77505 ·77533 ·77562 ·77590 ·77618	3.44541 3.45102 3.45664 3.46228 3.46793	·79209 ·79237 ·79266 ·79294 ·79323	$3 \cdot 80973$ $3 \cdot 81633$ $3 \cdot 82294$ $3 \cdot 82956$ $3 \cdot 83621$	·80919 ·80948 ·80976 ·81005 ·81033	$\begin{array}{r} 4 \cdot 24084 \\ 4 \cdot 24870 \\ 4 \cdot 25658 \\ 4 \cdot 26448 \\ 4 \cdot 27241 \end{array}$	$     \begin{array}{c}       0 \\       1 \\       2 \\       3 \\       4     \end{array} $
56789	·75949 ·75977 ·76005 ·76034 ·76062	3.15782 3.16271 3.16761 3.17252 3.17744	·77647 ·77675 ·77703 ·77732 ·77760	3.47360 3.47928 3.48498 3.49069 3.49642	·79351 ·79380 ·79408 ·79437 ·79465	3 · 84288 3 · 84956 3 · 85627 3 · 86299 3 · 86973	-81062 -81090 -81119 -81148 -81176	$\begin{array}{r} 4 \cdot 28036 \\ 4 \cdot 28833 \\ 4 \cdot 29634 \\ 4 \cdot 30436 \\ 4 \cdot 31241 \end{array}$	5 6 7 8 9
10 11 12 13 14	·76090 ·76118 ·76147 ·76175 ·76203	$3 \cdot 18238$ $3 \cdot 18733$ $3 \cdot 19228$ $3 \cdot 19725$ $3 \cdot 20224$	·77788 ·77817 ·77845 ·77874 ·77902	$3 \cdot 50216$ $3 \cdot 50791$ $3 \cdot 51368$ $3 \cdot 51947$ $3 \cdot 52527$	·79493 ·79522 ·79550 ·79579 ·79607	3.87649 3.88327 3.89007 3.89689 3.90373	-81205 -81233 -81262 -81290 -81319	$\begin{array}{r} 4.32049 \\ 4.32859 \\ 4.33671 \\ 4.34486 \\ 4.35304 \end{array}$	10 11 12 13 14
15 16 17 18 19	·76231 ·76260 ·76288 ·76316 ·76344	$3 \cdot 20723$ $3 \cdot 21224$ $3 \cdot 21726$ $3 \cdot 22229$ $3 \cdot 22734$	.77930 .77959 .77987 .78015 .78044	3.53109 3.53692 3.54277 3.54863 3.55451	·79636 ·79664 ·79693 ·79721 ·79750	3.91058 3.91746 3.92436 3.93128 3.93821	-81348 -81376 -81405 -81433 -81462	$\begin{array}{r} 4.36124 \\ 4.36947 \\ 4.37772 \\ 4.38600 \\ 4.39430 \end{array}$	15 16 17 18 19
20 21 22 23 24	·76373 ·76401 ·76429 ·76458 ·76486	$3 \cdot 23239$ $3 \cdot 23746$ $3 \cdot 24255$ $3 \cdot 24764$ $3 \cdot 25275$	.78072 .78101 .78129 .78157 .78186	3.56041 3.56632 3.57224 3.57819 3.58414	·79778 ·79807 ·79835 ·79864 ·79892	$\begin{array}{r} 3.94517\\ 3.95215\\ 3.95914\\ 3.96616\\ 3.97320 \end{array}$	-81491 -81519 -81548 -81576 -81605	$\begin{array}{r} 4.40263\\ 4.41099\\ 4.41937\\ 4.42778\\ 4.43622 \end{array}$	20 2 22 23 24
25 26 27 28 29	.76514 .76542 .76571 .76599 .76627	$3 \cdot 25787$ $5 \cdot 26300$ $3 \cdot 26814$ $3 \cdot 27330$ $3 \cdot 27847$	• 78214 • 78242 • 78271 • 78299 • 78328	3.59012 3.59611 3.60211 3.60813 3.61417	·79921 ·79949 ·79978 ·80006 ·80035	$\begin{array}{r} 3.98025\\ 3.98733\\ 3.99443\\ 4.00155\\ 4.00869 \end{array}$	·81633 ·81662 ·81691 ·81719 ·81748	$\begin{array}{r} 4.44468\\ 4.45317\\ 4.46169\\ 4.47028\\ 4.47881\end{array}$	25 26 27 28 29
30 31 32 33 34	·76655 ·76684 ·76712 ·76740 ·76769	$3 \cdot 28366$ $3 \cdot 28885$ $3 \cdot 29406$ $3 \cdot 29929$ $3 \cdot 30452$	· 78356 · 78384 · 78413 · 78441 · 78440	3.62023 3.62630 3.63238 3.63849 3.64461	·80063 ·80092 ·80120 ·80149 ·80177	$\begin{array}{r} 4.01585\\ 4.02303\\ 4.03024\\ 4.03746\\ 4.04471 \end{array}$	-81776 -81805 -81834 -81862 -81891	$\begin{array}{r} 4.48740 \\ 4.49603 \\ 4.50468 \\ 4.51337 \\ 4.52208 \end{array}$	30 31 32 33 34
35 36 37 38 39	·76797 ·76825 ·76854 ·76882 ·76910	$3 \cdot 30977$ $3 \cdot 31503$ $3 \cdot 32031$ $3 \cdot 32560$ $3 \cdot 33090$	·78498 ·78526 ·78555 ·78583 ·78612	3.65074 3.65690 3.66307 3.66925 3.67545	- 80206 - 80234 - 80263 - 80291 - 80320	$\begin{array}{r} 4.05197 \\ 4.05926 \\ 4.06657 \\ 4.07390 \\ 4.08125 \end{array}$	·81919 ·81948 ·81977 ·82005 ·82034	$\begin{array}{r} 4.53081 \\ 4.53958 \\ 4.54837 \\ 4.55720 \\ 4.56605 \end{array}$	35 36 37 38 39
40 41 42 43 44	·76938 ·76967 ·76995 ·77023 ·77052	$3 \cdot 33622$ $3 \cdot 34154$ $3 \cdot 34689$ $3 \cdot 35224$ $3 \cdot 35761$	·78640 ·78669 ·78697 ·78725 ·78754	3.68167 3.68791 3.69417 3.70044 3.70673	·80348 ·80377 ·80405 ·80434 ·80462	$\begin{array}{r} 4.08863\\ 4.09602\\ 4.10344\\ 4.11088\\ 4.11835\end{array}$	·82063 ·82091 ·82120 ·82148 ·82177	$\begin{array}{r} 4.57493 \\ 4.58383 \\ 4.59277 \\ 4.60174 \\ 4.61073 \end{array}$	40 41 42 43 44
45 46 47 48 49	·77080 ·77108 ·77137 ·77165 ·77193	$3 \cdot 36299$ $3 \cdot 36839$ $3 \cdot 37380$ $3 \cdot 37923$ $3 \cdot 38466$	·78782 ·78811 ·78839 ·78868 ·78896	3.71303 3.71935 3.72569 3.73205 3.73843	·80491 ·80520 ·80548 ·80577 ·80605	$\begin{array}{r} 4.12583\\ 4.13334\\ 4.14087\\ 4.14842\\ 4.15599\end{array}$	•82206 •82234 •82263 •82292 •82292 •82320	$\begin{array}{r} 4.61976 \\ 4.62881 \\ 4.63790 \\ 4.64701 \\ 4.65616 \end{array}$	45 46 47 48 49
50 51 52 53 54	·77222 ·77250 ·77278 ·77307 ·77335	$3 \cdot 39012$ $3 \cdot 39558$ $3 \cdot 40106$ $3 \cdot 40656$ $3 \cdot 41206$	.78924 .78953 .78981 .79010 .79038	$3 \cdot 74482$ $3 \cdot 75123$ $3 \cdot 75766$ $3 \cdot 76411$ $3 \cdot 77057$	·80634 ·80662 ·80691 ·80719 ·80748	$\begin{array}{r} 4.16359\\ 4.17121\\ 4.17886\\ 4.18652\\ 4.18652\\ 4.19421 \end{array}$	- 82349 - 82377 - 82406 - 82435 - 82463	$\begin{array}{r} 4.66533\\ 4.67454\\ 4.68377\\ 4.69304\\ 4.70234\end{array}$	50 51 52 53 54
55 56 57 58 59	.77363 .77392 .77420 .77448 .77477	3.41759 3.42312 3.42867 3.43424 3.43982	.79067 .79095 .79123 .79152 .79180	3.77705 3.78355 3.79007 3.79661 3.80316	-80776 -80805 -80833 -80862 -80891	$\begin{array}{r} 4 \cdot 20193 \\ 4 \cdot 20966 \\ 4 \cdot 21742 \\ 4 \cdot 22521 \\ 4 \cdot 23301 \end{array}$	.82492 .82521 .82549 .82578 .82607	4.71166 4.72102 4.73041 4.73983 <u>4.74929</u>	55 56 57 58 59
60	•77505	3.44541	.79209	3.80973	·80919	4.24084	.82635	4.75877	60
				170	7				

TABLE X.--NATURAL VERSED SINES AND EXTERNAL SECANTS.

Q1<sup>0</sup> Q9<sup>0</sup>

80°			81°		8	32°	83°		
,	Vers.	Ex. sec.	Vers.	Ex. sec.	Vers.	Ex. sec.	Vers.	Ex. sec.	
0 1 2 3 4	·82635 ·82664 ·82692 ·82721 ·82750	4.75877 4.76829 4.77784 4.78742 4.79703	.84357 .84385 .84414 .84443 .84471	5.39245 5.40422 5.41602 5.42787 5.43977	·86083 ·86112 ·86140 ·86169 ·86198	$\begin{array}{c} 6.18530\\ 6.20020\\ 6.21517\\ 6.23019\\ 6.24529\end{array}$	.87818 .87842 .87871 .87900 .87929	7.205517.225007.244577.264257.28402	0 1 2 3 4
5 6 7 8 9	·82778 ·82807 ·82836 ·82864 ·82893	$\begin{array}{r} 4.80667 \\ 4.81635 \\ 4.82606 \\ 4.83581 \\ 4.84558 \end{array}$	-84500 -84529 -84558 -84586 -84615	5.45171 5.46369 5.47572 5.48779 5.49991	·86227 ·86256 ·86284 ·86313 ·86342	$\begin{array}{r} 6 \cdot 26044 \\ 6 \cdot 27566 \\ 6 \cdot 29095 \\ 6 \cdot 30630 \\ 6 \cdot 32171 \end{array}$	·87957 ·87986 ·88015 ·88044 ·88073	7.30388 7.32384 7.34390 7.36405 7.38431	5 6 7 8 9
10 11 12 13 14	·82922 ·82950 ·82979 ·83008 ·83036	4.85539 4.86524 4.87511 4.88502 4.89497	·84644 ·84673 ·84701 ·84730 ·84759	5.51208 5.52429 5.53655 5.54886 5.56121	·86371 ·86400 ·86428 ·86457 ·86486	$\begin{array}{r} 6\cdot 33719 \\ 6\cdot 35274 \\ 6\cdot 36835 \\ 6\cdot 38403 \\ 6\cdot 39978 \end{array}$	·88102 ·88131 ·88160 ·88188 ·88217	7.40466 7.42511 7.44566 7.46632 7.48707	10 11 12 13 14
15 16 17 18 19	·83065 ·83094 ·83122 ·83151 ·83180	$\begin{array}{r} 4.90495 \\ 4.91496 \\ 4.92501 \\ 4.93509 \\ 4.94521 \end{array}$	·84788 ·84816 ·84845 ·84874 ·84903	5.57361 5.58606 5.59855 5.61110 5.62369	·86515 ·86544 ·86573 ·86601 ·86630	$\begin{array}{r} 6.41560 \\ 6.43148 \\ 6.44743 \\ 6.46346 \\ 6.47955 \end{array}$	·88246 ·88275 ·88304 ·88333 ·88362	7.507937.528897.549967.571137.59241	15 16 17 18 19
20 21 22 23 24	·83208 ·83237 ·83266 ·83294 ·83323	$\begin{array}{r} 4.95536\\ 4.96555\\ 4.97577\\ 4.98603\\ 4.99633\end{array}$	.84931 .84960 .84989 .85018 .85046	$\begin{array}{c} 5\cdot 63633\\ 5\cdot 64902\\ 5\cdot 66176\\ 5\cdot 67454\\ 5\cdot 68738\end{array}$	·86659 ·86688 ·86717 ·86746 ·86774	6.49571 6.51194 6.52825 6.54462 6.56107	·88391 ·88420 ·88448 ·88477 ·88506	7.61379 7.63528 7.65688 7.67859 7.70041	20 21 22 23 24
25 26 27 28 29	·83352 ·83380 ·83409 ·83438 ·83467	5.00666 5.01703 5.02743 5.03787 5.04834	.85075 .85104 .85133 .85162 .85190	5.70027 5.71321 5.72620 5.73924 5.75233	·86803 ·86832 ·86861 ·86890 ·86919	$6.57759 \\ 6.59418 \\ 6.61085 \\ 6.62759 \\ 6.64441$	·88535 ·88564 ·88593 ·88622 ·88651	7.72234 7.74438 7.76653 7.78880 7.81118	25 26 27 28 29
30 31 32 33 34	·83495 ·83524 ·83553 ·83581 ·83610	$\begin{array}{c} 5.05886\\ 5.06941\\ 5.08000\\ 5.09062\\ 5.10129\end{array}$	<pre>.85219 .85248 .85277 .85305 .85334</pre>	5.76547 5.77866 5.79191 5.80521 5.81856	·86947 ·86976 ·87005 ·87034 ·87063	6.66130 6.67826 6.69530 6.71242 6.72962	- 88680 - 88709 - 88737 - 88766 - 88795	7.83367 7.85628 7.87901 7.90186 7.92482	30 31 32 33 34
35 36 37 38 39	·83639 ·83667 ·83696 ·83725 ·83754	5.11199 5.12273 5.13350 5.14432 5.15517	·85363 ·85392 ·85420 ·85449 ·85478	5.83196 5.84542 5.85893 5.87250 5.88612	·87092 ·87120 ·87149 ·87178 ·87207	$6.74689 \\ 6.76424 \\ 6.78167 \\ 6.79918 \\ 6.81677$	-88824 -88853 -88882 -88911 -88940	$\begin{array}{r} 7.94791 \\ 7.97111 \\ 7.99444 \\ 8.01788 \\ 8.04146 \end{array}$	35 36 37 38 39
40 41 42 43 44	·83782 ·83811 ·83840 ·83868 ·83897	5.16607 5.17700 5.18797 5.19898 5.21004	.85507 .85536 .85564 .85593 .85622	$\begin{array}{c} 5.89979 \\ 5.91352 \\ 5.92731 \\ 5.94115 \\ 5.9505 \end{array}$	·87236 ·87265 ·87294 ·87322 ·87351	6.83443 6.85218 6.87001 6.88792 6.90592	·88969 ·88998 ·89027 ·89055 ·89084	8.06515 8.08897 8.11292 8.13699 8.16120	40 41 42 43 44
$45 \\ 46 \\ 47 \\ 48 \\ 49$	·83926 ·83954 ·83983 ·84012 ·84041	$5.22113 \\ 5.23226 \\ 5.24343 \\ 5.25464 \\ 5.26590$	·85651 ·85680 ·85708 ·85737 ·85766	$5.96900 \\ 5.98301 \\ 5.99708 \\ 6.01120 \\ 6.02538$	·87380 ·87409 ·87438 ·87467 ·87496	$\begin{array}{c} 6.92400\\ 6.94216\\ 6.96040\\ 6.97873\\ 6.99714 \end{array}$	·89113 ·89142 ·89171 ·89200 ·89229		45 46 47 48 49
$50 \\ 51 \\ 52 \\ 53 \\ 54$	.84069 .84098 .84127 .84155 .84184	5.27719 5.28853 5.29991 5.31133 5.32279	.85795 .85823 .85852 .85881 .85910	$\begin{array}{c} 6.03962 \\ 6.05392 \\ 6.06828 \\ 6.08269 \\ 6.09717 \end{array}$	·87524 ·87553 ·87582 ·87611 ·87640	7.015657.034237.052917.071677.09052	.89258 .89287 .89316 .89345 .89374	8.30917 8.33430 8.35957 8.38497 8.41052	50 51 52 53 54
55 56 57 58 59	·84213 ·84242 ·84270 ·84299 ·84328	$\begin{array}{c} 5.33429\\ 5.34584\\ 5.35743\\ 5.36906\\ 5.38073 \end{array}$	.85939 .85967 .85996 .86025 .86054	$\begin{array}{c} 6\cdot 11171 \\ 6\cdot 12630 \\ 6\cdot 14096 \\ 6\cdot 15568 \\ 6\cdot 17046 \end{array}$	·87669 ·87698 ·87726 ·87755 ·87784	7.109467.128497.147607.166817.18612	.89403 .89431 .89460 .89489 .89518	8.43620 8.46203 8.48800 8.51411 8.54037	55 56 57 58 59
60 	·84357	5.39245	•86083	6.18530	.87813	7.20551	·89547	8.56677	60

CABLE X .- NATURAL VERSED SINES AND EXTERNAL SECANTS.

84°

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,	Vers.	Ex. sec.	Vers.	Ex. sec.	Vers.	Ex. sec.	•
0 1 2 3 4	-89547 -89576 -89605 -89634 -89663	8.56677 8.59332 8.62002 8.64687 8.67387	.91284 .91313 .91342 .91371 .91400	$\begin{array}{r} 10.47371 \\ 10.51199 \\ 10.55052 \\ 10.58932 \\ 10.62837 \end{array}$	.93024 .93053 .93082 .93111 .93140	$\begin{array}{r} 13 \cdot 33559 \\ 13 \cdot 39547 \\ 13 \cdot 45586 \\ 13 \cdot 51676 \\ 13 \cdot 57817 \end{array}$	0 1 2 3 4
5 6 7 8 9	-89692 -89721 -89750 -89779 -89808	8.70103 8.72833 8.75579 8.78341 8.81119	.91429 .91458 .91487 .91516 .91545	$\begin{array}{r} 10.66769 \\ 10.70728 \\ 10.74714 \\ 10.78727 \\ 10.82768 \end{array}$	.93169 .93198 .93227 .93257 .93286	$\begin{array}{r} 13.64011\\ 13.70258\\ 13.76558\\ 13.82913\\ 13.89323\end{array}$	5 6 7 8 9
10 11 12 13 14	-89836 -89865 -89894 -89923 -89952	8.83912 8.86722 8.89547 8.92389 8.95248	.91574 .91603 .91632 .91661 .91690	$\begin{array}{r} 10.86837 \\ 10.90934 \\ 10.95060 \\ 10.99214 \\ 11.03397 \end{array}$	-93315 -93344 -93373 -93402 -93431	$\begin{array}{r} 13.95788\\ 14.02310\\ 14.08890\\ 14.15527\\ 14.22223\end{array}$	$     \begin{array}{c}       10 \\       11 \\       12 \\       13 \\       14     \end{array} $
15 16 17 18 19	·89981 ·90010 ·90039 ·90068 ·90097	8.98123 9.01015 9.03923 9.06849 9.09792	.91719 .91748 .91777 .91806 .91835	11.07610 11.11852 11.16125 11.20427 11.24761	·93460 ·93489 ·93518 ·93547 ·93576	$\begin{array}{r} 14 \cdot 28979 \\ 14 \cdot 35795 \\ 14 \cdot 42672 \\ 14 \cdot 49611 \\ 14 \cdot 56614 \end{array}$	$     \begin{array}{r}       15 \\       16 \\       17 \\       18 \\       19 \\     \end{array} $
20 21 22 23 24	·90126 ·90155 ·90184 ·90213 ·90242	9.12752 9.15730 9.18725 9.21739 9.24770	·91864 ·91893 ·91922 ·91951 ·91980	$\begin{array}{c} 11.29125\\ 11.33521\\ 11.37948\\ 11.42408\\ 11.46900 \end{array}$	-93605 -9363 <u>4</u> -93663 -93692 -93721	$14.63679 \\ 14.70810 \\ 14.78005 \\ 14.85268 \\ 14.92597$	20 21 22 23 24
25 26 27 28 29	-90271 -90300 -90329 -90358 -90386	9.27819 9.30887 9.33973 9.37077 9.40201	•92009 •92038 •92067 •92096 •92125	11.51424 11.55982 11.60572 11.65197 11.69856	-93750 -93779 -93808 -93837 -93866	$\begin{array}{r} 14.99995\\ 15.07462\\ 15.14999\\ 15.22607\\ 15.30287\end{array}$	25 26 27 28 29
30 31 32 33 34	.90415 .90444 .90473 .90502 .90531	9.43343 9.46505 9.49685 9.52886 9.56106	.92154 .92183 .92212 .92241 .92270	11.74550 11.79278 11.84042 11.88841 11.93677	-93895 -93924 -93953 -93982 -94011	$\begin{array}{r} 15.38041 \\ 15.45869 \\ 15.53772 \\ 15.61751 \\ 15.69808 \end{array}$	$30 \\ 31 \\ 32 \\ 33 \\ 34$
85 36 37 38 39	•90560 •90589 •90618 •90647 •90676	9.59346 9.62605 9.65885 9.69186 9.72507	•92299 •92328 •92357 •92386 •92415	11.9854912.0345812.0804012.1338812.18411	·94040 ·94069 ·94098 ·94127 ·94156	$15.77944 \\ 15.86159 \\ 15.94456 \\ 16.02835 \\ 16.11297$	35 36 37 38 39
10 41 42 43 44	-90705 -90734 -90763 -90792 -90821	9.75849 9.79212 9.82596 9.86001 9.89428	.92444 .92473 .92502 .92531 .92560	$\begin{array}{r} 12\cdot23472\\ 12\cdot28572\\ 12\cdot33712\\ 12\cdot38891\\ 12\cdot44112\end{array}$	.94186 .94215 .94244 .94273 .94302	$16.19843 \\ 16.28476 \\ 16.37196 \\ 16.46005 \\ 16.54903$	$\begin{array}{r} 40 \\ 41 \\ 42 \\ 43 \\ 44 \end{array}$
45 46 47 48 49	.90850 .90879 .90908 .90937 .90966	9.92877 9.96348 9.99841 10.03356 10.06894	.92589 .92618 .92647 .92676 .92705	$12.49373 \\ 12.54676 \\ 12.60021 \\ 12.65408 \\ 12.70838$	94331 94360 94389 94418 94447	$\begin{array}{r} 16.63893\\ 16.72975\\ 16.82152\\ 16.91424\\ 17.00794 \end{array}$	45 46 47 48 49
50 51 52 53 54	.90995 .91024 .91053 .91082 .91111	$\begin{array}{c} 10.10455\\ 10.14039\\ 10.17646\\ 10.21277\\ 10.24932 \end{array}$	•92734 •92763 •92792 •92821 •92850	$\begin{array}{r} 12.76312 \\ 12.81829 \\ 12.87391 \\ 12.92999 \\ 12.98651 \end{array}$	94476 94505 94534 94563 94592	$\begin{array}{r} 17.10262 \\ 17.19830 \\ 17.29501 \\ 17.39274 \\ 17.49153 \end{array}$	$50 \\ 51 \\ 52 \\ 53 \\ 54$
55 56 57 58 59	.91140 .91169 .91197 .91226 .91255	$\begin{array}{c} 10.28610\\ 10.32313\\ 10.36040\\ 10.39792\\ 10.43569\end{array}$	.92879 .92908 .92937 .92966 .92995	$13.04350 \\ 13.10096 \\ 13.15889 \\ 13.21730 \\ 13.27620$	·94621 ·94650 ·94679 ·94708 ·94737	$\begin{array}{c} 17.59139 \\ 17.69233 \\ 17.79438 \\ 17.89755 \\ 18.00185 \end{array}$	55 56 57 58 59
60	·91284	10.47371	.93024	13.33559	.94766	18.10732	. 60

,	Vers.	Ex. sec.	Vers.	Ex. sec.	Vers.	Ex. sec.	1
01234	•94766 •94795 •94825 •94854 •94883	18.10732 18.21397 18.32182 18.43088 18.54119	•96510 •96539 •96568 •96597 •96626	$\begin{array}{r} 27.65371\\ 27.89440\\ 28.13917\\ 28.38812\\ 28.64137\end{array}$	•98255 •98284 •98313 •98342 •98371	$\begin{array}{r} 56\cdot 29869\\ 57\cdot 26976\\ 58\cdot 27431\\ 59\cdot 31411\\ 60\cdot 39105\end{array}$	0 1 2 3 4
5 6 7 8 9	.94912 .94941 .94970 .94999 .95028	18.65275 18.76560 18.87976 18.99524 19.11208	•96655 •96684 •96714 •96743 •96772	28.89903 29.16120 29.42802 29.69960 29.97607	·98400 ·98429 ·98458 ·98487 ·98517	61.50715 62.66460 63.86572 65.11304 66.40927	5 6 7 8 9
10 11 12 13 14	.95057 .95086 .95115 .95144 .95173	19.23028 19.34989 19.47093 19.59341 19.71737	•96801 •96830 •96859 •96888 •96917_	30.25758 30.54425 30.83623 31.13366 31.43671	·98546 ·98575 ·98604 ·98633 ·98662	67.75736 69.16047 70.62285 72.14583 73.73586	$10\\11\\12\\13\\14$
15 16 17 18 19	.95202 .95231 .95260 .95289 .95318	$\begin{array}{r} 19.84283\\ 19.96982\\ 20.09838\\ 20.22852\\ 20.36027 \end{array}$	.96946 .96975 .97004 .97033 .97062	31.74554 32.06030 32.38118 32.70835 33.04199	•98691 •98720 •98749 •98778 •98807	75.39655 77.13274 78.94968 80.85315 82.84947	15 16 17 18 19
20 21 22 23 24	•95347 •95377 •95406 •95435 •95464	$\begin{array}{r} 20.49368\\ 20.62876\\ 20.76555\\ 20.90409\\ 21.04440 \end{array}$	.97092 .97121 .97150 .97179 .97208	$\begin{array}{r} 33.38232\\ 33.72952\\ 34.08380\\ 34.44539\\ 34.81452\end{array}$	.98836 .98866 .98895 .98924 .98953	$\begin{array}{r} 84.94561\\ 87.14924\\ 89.46886\\ 91.91387\\ 94.49471\end{array}$	20 21 22 23 24
25 26 27 28 29	•95493 •95522 •95551 •95580 •95609	$\begin{array}{r} 21 \cdot 18653 \\ 21 \cdot 33050 \\ 21 \cdot 47635 \\ 21 \cdot 62413 \\ 21 \cdot 77386 \end{array}$	.97237 .97266 .97295 .97324 .97353	35.19141 35.57633 35.96953 36.37127 36.78185	•98982 •99011 •99040 •99069 •99098	97.22303 100.1119 103.1757 106.4311 109.8966	25 26 27 28 29
30 31 32 33 34	·95638 ·95667 ·95696 ·95725 ·95754	$\begin{array}{c} 21 \cdot 92559 \\ 22 \cdot 07935 \\ 22 \cdot 23520 \\ 22 \cdot 39316 \\ 22 \cdot 55328 \end{array}$	•97382 •97411 •97440 •97470 •97499	37.20155 37.63068 38.06957 38.51855 38.97797	.99127 .99156 .99186 .99215 .99244	$113.5930 \\ 117.5444 \\ 121.7780 \\ 126.3253 \\ 131.2223$	30 31 32 33 34
35 36 37 38 39	.95783 .95812 .95842 .95871 .95900	$\begin{array}{r} 22 \cdot 71563 \\ 22 \cdot 88022 \\ 23 \cdot 04712 \\ 23 \cdot 21637 \\ 23 \cdot 38802 \end{array}$	.97528 .97557 .97586 .97615 .97644	$\begin{array}{r} 39.44820\\ 39.92963\\ 40.42266\\ 40.92772\\ 41.44525\end{array}$	.99278 .99302 .99331 .99360 .99389	$136.5111\\142.2406\\148.4684\\155.2623\\162.7033$	35 36 37 38 39
40 41 42 43 44	.95929 .95958 .95987 .96016 .96045	$\begin{array}{c} 23 \cdot 56212 \\ 23 \cdot 73873 \\ 23 \cdot 91790 \\ 24 \cdot 09969 \\ 24 \cdot 28414 \end{array}$	.97673 .97702 .97731 .97760 .97789	$\begin{array}{r} 41.97571\\ 42.51961\\ 43.07746\\ 43.64980\\ 44.23720\end{array}$	.99418 .99447 .99476 .99505 .99535	$170.8883 \\ 179.9350 \\ 189.9868 \\ 201.2212 \\ 213.8600$	40 41 42 43 44
45 46 47 48 49	.96074 .96103 .96132 .96161 .96190	$\begin{array}{r} 24 \cdot 47134 \\ 24 \cdot 66132 \\ 24 \cdot 85417 \\ 25 \cdot 04994 \\ 25 \cdot 24869 \end{array}$	.97819 .97848 .97877 .97906 .97935	$\begin{array}{r} 44\cdot84026\\ 45\cdot45963\\ 46\cdot09596\\ 46\cdot74997\\ 47\cdot42241\end{array}$	.99564 .99593 .99622 .99651 .99680	$\begin{array}{r} 228 \cdot 1839 \\ 244 \cdot 5540 \\ 263 \cdot 4427 \\ 285 \cdot 4795 \\ 311 \cdot 5230 \end{array}$	45 46 47 48 49
50 51 52 53 54	•96219 •96248 •96277 •96307 •96336	$\begin{array}{r} 25.45051\\ 25.65546\\ 25.86360\\ 26.07503\\ 26.28981 \end{array}$	·97964 ·97993 ·98022 ·98051 ·98080	$\begin{array}{r} 48 \cdot 11406 \\ 48 \cdot 82576 \\ 49 \cdot 55840 \\ 50 \cdot 31290 \\ 51 \cdot 09027 \end{array}$	•99709 •99738 •99767 •99796 •99825	342.7752 380.9723 428.7187 490.1070 571.9581	50 51 52 53 54
55 56 57 58 59	•96365 •96394 •96423 •96452 •96481	$\begin{array}{r} 26.50804\\ 26.72978\\ 26.95513\\ 27.18417\\ 27.41700\\ \end{array}$	•98109 •98138 •98168 •98197 •98226	51.89156 52.71790 53.57046 54.45053 55.35946	.99855 .99884 .99913 .99942 .99971	$\begin{array}{r} 686.5496\\ 858.4369\\ 1144.916\\ 1717.874\\ 3436.747\end{array}$	55 56 57 58 59
60	•96510	27.65371	•98255	56.29869	1.00000	Infinite	60

## TABLE XI.-REDUCTION OF BAROMETER READING TO 32° F.

I

Temp.					:	Inches.					
O Fahr.	26.0	26.5	27.0	27.5	28.0	28.5	29.0	29.5	30.0	30.5	31.0
45	039	039	040	041	042	042	043	044	045	045	046
46	.041	.042	.043	.043	.044	045	.046	.046	.047	.048	.049
47	.043	.044	.045	.046	.047	.048	.048	.049	.050	.051	.052
48	.046	.047	.047	.048	.049	.050	.051	.052	.053	.053	.054
49	.048	.049	.050	.051	.052	.052	.054	.054	.055	.056	.057
50	.050	.051	.052	.053	.054	.055	·056	.057	.058	.059	.060
51	.053	.054	.055	.056	.057	.058	·059	.060	.061	.062	.063
52	.055	.056	.057	.058	.059	.060	·061	.062	.064	.065	.066
53	.057	.058	.060	.061	.062	.063	·064	.065	.066	.067	.068
54	.060	.061	.062	.063	.064	.065	·067	.068	.069	.070	.071
55	·062	-063	-064	-065	-066	-068	·069	.070	.071	.073	.074
56	·064	-065	-067	-068	-069	-070	·072	.073	.074	.075	.077
57	·067	-068	-069	-070	-072	-073	·075	.076	.077	.078	.080
58	·069	-070	-071	-073	-074	-076	·077	.078	.080	.081	.082
59	·072	-073	-074	-075	-077	-078	·080	.081	.083	.084	.085
60	.074	.076	.077	.078	.079	.081	.082	.084	.085	.086	.088
61	.076	.077	.079	.080	.082	.083	.085	.086	.088	.089	.091
62	.079	.080	.082	.083	.085	.086	.088	.089	.091	.092	.094
63	.081	.082	.084	.085	.087	.088	.090	.091	.093	.095	.096
64	.083	.085	.086	.088	.090	.091	.093	.094	.096	.097	.099
65	.086	.087	.089	.090	.092	.093	.095	.097	.099	.100	.102
66	.088	.089	.091	.093	.095	.096	.098	.099	.101	.103	.105
67	.090	.092	.094	.095	.097	.099	.101	.102	.104	.106	.108
68	.093	.094	.096	.098	.100	.101	.103	.105	.107	.108	.110
69	.095	.097	.099	.100	.102	.104	.106	.107	.110	.111	.113
70	.097	.099	.101	.103	.105	·106	.109	.110	.112	.114	.116
71	.100	.101	.103	.105	.107	·109	.111	.113	.115	.117	.119
72	.102	.104	.106	.108	.110	·112	.114	.116	.118	.120	.122
73	.104	.106	.108	.110	.112	·114	.116	.118	.120	.122	.124
74	.107	.109	.111	.113	.115	·117	.119	.121	.123	.125	.127
75	.109	.111	.113	.115	.117	.119	.122	.124	.126	.128	.130
76	.111	.113	.116	.118	.120	.122	.124	.126	.128	.130	.133
77	.114	.116	.118	.120	.122	.124	.127	.129	.131	.133	.136
78	.116	.118	.120	.122	.125	.127	.129	.131	.134	.136	.138
79	.118	.120	.123	.125	.127	.129	.132	.134	.137	.139	.141
80	.121	.123	.125	.127	-130	-132	·135	.137	.139	.141	.144
81	.123	.125	.128	.130	-132	-134	·137	.139	.142	.144	.147
82	.125	.128	.130	.132	-135	-137	·140	.142	.145	.147	.149
83	.128	.130	.133	.135	-138	-140	·142	.145	.147	.149	.152
84	.130	.132	.135	.138	-140	-142	·145	.147	.150	.152	.155
85 86 87 88 89	·132 ·135 ·137 ·139 ·142	.134 .137 .139 .142 .144	·137 ·140 ·142 ·145 ·147	·140 ·142 ·144 ·147 ·150	.143 .145 .148 .150 .153	•145 •148 •150 •152 •155	.148 .150 .153 .155 .158	.150 .153 .155 .158 .158 .161	·153 ·155 ·158 ·161 ·164	.155 .158 .161 .163 .166	-158 -161 -163 -166 -169
90	144	·147	150	153	155	158	161	164	166	169	172175
. 91	146	149	152	155	158	160	163	166	169	172	

#### TABLE XII.-BAROMETRIC ELEVATIONS.\*

( manual second s								
В	Å	Diff. for $\cdot 01$ .	В	A	Diff. for $\cdot 01.$	В	A	Diff. for .01.
Inches.	Feet.	Feet.	Inches.	Feet.	Feet.	Inches.	Feet.	Feet.
$\begin{array}{c} 20 \cdot 0 \\ 200 \cdot 1 \\ 200 \cdot 3 \\ 200 \cdot 4 \\ 200 \cdot 5 \\ 200 \cdot 7 \\ 200 \cdot 8 \\ 200 \cdot 1 \\ 211 \cdot 2 \\ 211 \cdot 5 \\ 611 \cdot 7 \\ 800 \cdot 1 \\ 222 \cdot 3 \\ 450 \cdot 6 \\ 222 \cdot 7 \\ 222 \cdot 3 \\ 222 \cdot 7 \\ 222 \cdot 7 \\ 222 \cdot 7 \\ 222 \cdot 7 \\ 222 \cdot 3 \\ 222 \cdot 7 \\ 222 \cdot 7 \\ 222 \cdot 3 \\ 222 \cdot 7 \\ 222 \cdot 7 \\ 222 \cdot 7 \\ 222 \cdot 3 \\ 223 \cdot 4 \\ 560 \cdot 6 \\ 7 \\ 200 \cdot 1 \\ 200 \cdot $	$\begin{array}{c} 11.047\\ 10.911\\ 10.776\\ 10.642\\ 10.508\\ 10.375\\ 10.242\\ 10.110\\ 9.979\\ 9.848\\ 9.718\\ 9.589\\ 9.460\\ 9.3204\\ 9.077\\ 8.9204\\ 9.0771\\ 8.925\\ 8.451\\ 8.3204\\ 8.082\\ 7.988\\ 7.717\\ 7.358\\ 7.997\\ 7.477\\ 7.358\\ 7.997\\ 7.477\\ 7.358\\ 7.997\\ 7.423\\ 7.997\\ 7.423\\ 7.904\\ 6.538\\ 6.423\\ \end{array}$	$\begin{array}{c} -13.6\\ 13.5\\ 13.4\\ 13.3\\ 13.3\\ 13.3\\ 13.2\\ 13.1\\ 13.1\\ 13.1\\ 13.1\\ 13.1\\ 12.9\\ 12.9\\ 12.8\\ 12.8\\ 12.8\\ 12.8\\ 12.6\\ 12.6\\ 12.6\\ 12.6\\ 12.6\\ 12.6\\ 12.6\\ 12.2\\ 12.2\\ 12.2\\ 12.2\\ 12.2\\ 12.2\\ 12.2\\ 12.2\\ 12.2\\ 12.2\\ 12.2\\ 12.2\\ 12.2\\ 12.2\\ 12.6\\ 11.7\\ 11.7\\ 11.7\\ 11.7\\ 11.6\\ -11.5\end{array}$	$\begin{array}{c} 23 & 7 \\ 233 & 8 \\ 24 & 0 \\ 24 & 1 \\ 24 & 3 \\ 24 & 4 \\ 24 & 3 \\ 24 & 4 \\ 24 & 3 \\ 24 & 4 \\ 24 & 3 \\ 24 & 4 \\ 24 & 3 \\ 24 & 4 \\ 24 & 3 \\ 24 & 4 \\ 24 & 3 \\ 24 & 4 \\ 24 & 3 \\ 24 & 4 \\ 24 & 3 \\ 24 & 4 \\ 24 & 3 \\ 24 & 4 \\ 24 & 3 \\ 24 & 4 \\ 24 & 3 \\ 24 & 4 \\ 24 & 3 \\ 24 & 4 \\ 24 & 3 \\ 24 & 4 \\ 24 & 3 \\ 24 & 4 \\ 24 & 3 \\ 24 & 4 \\ 24 & 3 \\ 24 & 4 \\ 24 & 4 \\ 24 & 3 \\ 24 & 4 \\ 24 & 4 \\ 25 & 1 \\ 25 & 3 \\ 25 & 4 \\ 25 &$	6.423 6.308 6.1940 5.967 5.8541 5.6298 5.5186 5.0777 4.9689 4.751 4.9689 4.751 4.45358 4.4221 4.2215 2.8771 2.5770 2.4770	$\begin{array}{c} -11.5\\ 11.4\\ 11.4\\ 11.3\\ 11.3\\ 11.3\\ 11.2\\ 11.1\\ 11.1\\ 11.1\\ 11.1\\ 11.0\\ 10.9\\ 10.9\\ 10.9\\ 10.9\\ 10.9\\ 10.8\\ 10.8\\ 10.8\\ 10.8\\ 10.8\\ 10.8\\ 10.8\\ 10.8\\ 10.8\\ 10.8\\ 10.6\\ 10.5\\ 10.6\\ 10.5\\ 10.4\\ 10.4\\ 10.4\\ 10.3\\ 10.2\\ 10.2\\ 10.2\\ 10.2\\ 10.1\\ 10.1\\ 10.1\\ 10.0\\ -10\ 0\end{array}$	$\begin{array}{c} 27.4\\ 27.5\\ 27.7\\ 27.7\\ 27.8\\ 28.0\\ 28.1\\ 28.3\\ 28.5\\ 28.6\\ 28.8\\ 28.5\\ 28.6\\ 28.8\\ 28.9\\ 29.1\\ 29.5\\ 29.4\\ 29.5\\ 29.4\\ 29.5\\ 29.4\\ 29.5\\ 29.9\\ 30.0\\ 1\\ 30.2\\ 30.3\\ 30.5\\ 30.6\\ 30.5\\ 30.6\\ 30.5\\ 30.6\\ 30.5\\ 30.6\\ 30$	$\begin{array}{c} 2.470\\ 2.371\\ 2.272\\ 2.173\\ 2.075\\ 1.977\\ 1.880\\ 1.589\\ 1.493\\ 1.397\\ 1.302\\ 1.302\\ 1.302\\ 1.202\\ 1.018\\ 830\\ 736\\ 643\\ 550\\ 458\\ 830\\ 550\\ 458\\ 830\\ 736\\ 830\\ 736\\ 830\\ 736\\ 830\\ 736\\ 830\\ 736\\ 830\\ 736\\ 830\\ 736\\ 830\\ 736\\ 830\\ 736\\ 830\\ 736\\ 830\\ 736\\ 736\\ 830\\ 736\\ 736\\ 736\\ 736\\ 736\\ 736\\ 736\\ 736$	$\begin{array}{c} -9.99\\ 9.98\\ 9.77\\ 9.76\\ 6555\\ 9.44\\ 4.4\\ 9.33\\ 2.22\\ 2.1\\ 1.00\\ 9.00\\ 9.00\\ 9.88\\ 8.8\\ 8.8\\ 8.8\\ 8.8\\ 8.8\\ 8.8\\ 8.$

\* Compiled from Report of U. S. C. & G. Survey for 1881, App. 10 Table XI.

TABLE XIII.—COEFFICIENTS F	OR CORRECTIONS	FOR	TEMPERATURE
AND	HUMIDITY.*		

t+t'	C	Diff. for 1°.	<i>t+t'</i>	<i>C</i>	Diff. for 1°.	<i>t+t'</i>	C	Diff. for 1°.
$ \begin{array}{r} 0^{\circ} \\ 10 \\ 20 \\ 30 \\ 40 \\ 50 \\ 60 \\ \end{array} $	$\begin{array}{c}1024\\.0915\\.0806\\.0698\\.0592\\.0486\\0380\end{array}$	$   \begin{array}{c}     10.9 \\     10.8 \\     10.6 \\     10.6 \\     10.6 \\     10.6 \\     10.6 \\   \end{array} $	60° 70 80 90 100 110 120	$\begin{array}{r}0380\\.0273\\.0166\\0058\\+.0049\\.0156\\+.0262\end{array}$		120° 130 140 150 160 170 180	$\begin{array}{r} + .0262 \\ .0368 \\ .0472 \\ .0575 \\ .0677 \\ .0779 \\ + .0879 \end{array}$	10.6 10.4 10.3 10.2 10.2

\* Compiled from Report of U. S. C. & G. Survey for 1881, App. 10, Tables I, IV. 742

#### TABLE XXX .--- USEFUL TRIGONOMETRICAL FORMULÆ.

13	$\sin 2a = 2\sin a \cos a = \frac{2\tan a}{1+\tan^2 a}.$
14	$\cos 2a = \cos^2 a - \sin^2 a = 1 - 2 \sin^2 a = 2 \cos^2 a - 1$
	$=\frac{1-\tan^2 a}{1+\tan^2 a}.$
15	$\tan 2a = \frac{2 \tan a}{1 - \tan^2 a}.$
16	$\cot 2a = \frac{1}{2} \cot a - \frac{1}{2} \tan a = \frac{\cot^2 a - 1}{2 \cot a} = \frac{1 - \tan^2 a}{2 \tan a}.$
17	vers $2a = 2\sin^2 a = 1 - \cos 2a = 2\sin a \cos a \tan a$ .
18	$\operatorname{exsec} 2a = \frac{\tan 2a}{\cot a} = \frac{2 \tan^2 a}{1 - \tan^2 a} = \frac{2 \sin^2 a}{1 - 2 \sin^2 a}.$
19	$\sin (a \pm b) = \sin a \cos b \pm \cos a \sin b.$
20	$\cos (a \pm b) = \cos a \cos b \mp \sin a \sin b.$
21	$\sin a + \sin b = 2 \sin \frac{1}{2}(a+b) \cos \frac{1}{2}(a-b).$
22	$\sin a - \sin b = 2 \sin \frac{1}{2}(a-b) \cos \frac{1}{2}(a+b).$
23	$\cos a + \cos b = 2 \cos \frac{1}{2}(a+b) \cos \frac{1}{2}(a-b).$
<b>24</b>	$\cos a - \cos b = -2 \sin \frac{1}{2}(a+b) \sin \frac{1}{2}(a-b).$
	2

Call the sides of any triangle A, B, C, and the opposite angles a, b, and c. Call  $s = \frac{1}{2}(A + B + C)$ .

$$\tan \frac{1}{2}(a-b) = \frac{A-B}{A+B} \tan \frac{1}{2}(a+b) = \frac{A-B}{A+B} \cot \frac{1}{2}c.$$

$$C = (A+B)\frac{\cos \frac{1}{2}(a+b)}{\cos \frac{1}{2}(a-b)} = (A-B)\frac{\sin \frac{1}{2}(a+b)}{\sin \frac{1}{2}(a-b)}.$$

$$\sin \frac{1}{2}a = \sqrt{\frac{(s-B)(s-C)}{BC}}.$$

$$28 \qquad \cos \frac{1}{2}a = \sqrt{\frac{\overline{s(s-A)}}{BC}}.$$

29 vers 
$$a = \frac{2(s-B)(s-C)}{BC}$$
.

30 Area = 
$$\sqrt{s(s-A)(s-B)(s-C)} = A^2 \frac{\sin b \sin c}{2 \sin a}$$
.

#### TABLE XXXI.-USEFUL FORMULÆ AND CONSTANTS.

Circumference of a circle (radius = $r$ ) = $2\pi r$ . Area of a circle = $\pi r^2$ . Area of sector (length of arc = $l$ ) = $\frac{1}{2}lr$ . " " (angle of arc = $\alpha^\circ$ ) = $\frac{a}{360}\pi r^2$ . Area of segment (chord = $c$ , mid. ord. = $m$ ) = $\frac{2}{3}cm$ (approx.). Area of a circle to radius 1 Circumference of a circle to diameter 1 Surface of a sphere to diameter 1 Volume of a sphere to radius 1 = $4\pi \div 3$ = 4.1887902 Arc equal to radius expressed in $\begin{cases} degrees = 57.2957795 \\ minutes = 3437.7467708 \\ seconds = 206264.8062471 \end{cases}$ Length of arc of 1°, radius unity0.01745329 Sine of one second = 0.0000048481 Cubic inches in United States standard gallon = 231 Weight of one cubic foot of water at maximum density (therm.	
Area of sector (length of arc = l) = $\frac{1}{2}lr$ . " " (angle of arc = $\alpha^{\circ}$ ) = $\frac{\alpha}{360}\pi r^2$ . Area of segment (chord = c, mid. ord. = m) = $\frac{2}{3}cm$ (approx.). Area of a circle to radius 1 Circumference of a circle to diameter 1 Circumference of a circle to diameter 1 Volume of a sphere to radius 1 = $4\pi \div 3$ = 4.1887902 Arc equal to radius expressed in $\begin{cases} degrees = 57.2957795 \\ minutes = 3437.7467708 \\ seconds = 206264.8062471 \end{cases}$ Length of are of 1°, radius unity	
" " " (angle of arc = $\alpha^{\circ}$ ) = $\frac{\alpha}{360}\pi r^2$ . Area of segment (chord = c, mid. ord. = m) = $\frac{2}{3}cm$ (approx.). Area of a circle to radius 1 Circumference of a circle to diameter 1 Surface of a sphere to diameter 1 Volume of a sphere to radius 1 = $4\pi \div 3$ = 4.1887902 Arc equal to radius expressed in $\begin{cases} degrees = 57.2957795 \\ minutes = 3437.7467708 \\ seconds = 206264.8062471 \end{cases}$ Length of arc of 1°, radius unity	
Area of segment (chord = c, mid. ord. = m) = $\frac{2}{3}cm$ (approx.).Area of a circle to radius 1Circumference of a circle to diameter 1Surface of a sphere to diameter 1Volume of a sphere to radius 1 = $4\pi + 3$ = 4.1887902Are equal to radius expressed in $\begin{cases} degrees = 57.2957795 \\ minutes = 3437.7467708 \\ seconds = 206264.8062471 \end{cases}$ Length of are of 1°, radius unity	
Area of a circle to radius 1Circumference of a circle to diameter 1Surface of a sphere to diameter 1Volume of a sphere to radius $1 = 4\pi \div 3 = 4.1887902$ Arc equal to radius expressed in $\begin{cases} degrees = 57.2957795 \\ minutes = 3437.7467708 \\ seconds = 206264.8062471 \end{cases}$ Length of arc of 1°, radius unity.*	
Circumference of a circle to diameter 1= $\pi =$ 3.1415927Surface of a sphere to diameter 1= $\pi =$ 3.1415927Volume of a sphere to radius $1 = 4\pi \div 3 =$ 4.1887902Arc equal to radius expressed in $\begin{cases} degrees = 57.2957795 \\ minutes = 3437.7467708 \\ seconds = 206264.8062471 \end{cases}$ Length of arc of 1°, radius unity.0.01745329Sine of one second = 0.0000048481.Cubic inches in United States standard gallon = 231.Weight of one cubic foot of water at maximum density (therm.	
Surface of a sphere to diameter 1 Volume of a sphere to radius $1 = 4\pi \div 3 = 4.1887902$ Arc equal to radius expressed in $\begin{cases} degrees = 57.2957795 \\ minutes = 3437.7467708 \\ seconds = 206264.8062471 \end{cases}$ Length of arc of 1°, radius unity	
Volume of a sphere to radius $1 = 4\pi \div 3 =$ 4.1887902Arc equal to radius expressed in $\begin{cases} degrees =$ 57.2957795minutes =3437.7467708seconds =206264.8062471Length of arc of 1°, radius unity	0.4971499
Arc equal to radius expressed in $\begin{cases} degrees = 57.2957795 \\ minutes = 3437.7467708 \\ seconds = 206264.8062471 \\ length of arc of 1°, radius unity0.01745329 \\ Sine of one second = 0.0000048481 \\ Cubic inches in United States standard gallon = 231 \\ Weight of one cubic foot of water at maximum density (therm.$	
Arc equal to radius expressed in {       minutes = 3437.7467708         seconds = 206264.8062471         Length of arc of 1°, radius unity	0.6220886
seconds =       206264.8062471         Length of arc of 1°, radius unity	1.7581226
Length of arc of 1°, radius unity	3.5362739
Sine of one second = 0.0000048481 Cubic inches in United States standard gallon = 231 Weight of one cubic foot of water at maximum density (therm.	5.3144251
Cubic inches in United States standard gallon = 231 Weight of one cubic foot of water at maximum density (therm.	8.2418774
Weight of one cubic foot of water at maximum density (therm.	4.6855749
	2.3636120
200 0 T 1 200//) 20 250	
39°.8 F., barom. 30")	1.7950384
Weight of one cubic foot of water at ordinary temperature (therm.	
62° F.)	1.7946349
Acceleration due to gravity at latitude of New York in feet per	
square second	1.507 3086
Feet in one metre	0.5159889
Metres in one foot 0.304797	9.4840111

No.	Squares.	Cubes.	Square Roots.	Cube Roots.	Reciprocals.
1 2 3 4 5	1 4 9 16 25	1 8 27 64 125	$\begin{array}{c} 1.0000000\\ 1.4142136\\ 1.7320508\\ 2.0000000\\ 2.2360680\end{array}$	1.0000000 1.2599210 1.4422496 1.5874011 1.7099759	1.000000000.50000000.33333333.250000000.20000000
6 7 8 9 10	36 49 64 81 100	216 343 512 729 1000	$\begin{array}{r} 2.4494897\\ 2.6457513\\ 2.8284271\\ 3.0000000\\ 3.1622777\end{array}$	$\begin{array}{r} 1 \cdot 8171206 \\ 1 \cdot 9129312 \\ 2 \cdot 0000000 \\ 2 \cdot 0800837 \\ 2 \cdot 1544347 \end{array}$	$\begin{array}{r} \cdot 166666667 \\ \cdot 142857143 \\ \cdot 125000000 \\ \cdot 111111111 \\ \cdot 100000000 \end{array}$
$11 \\ 12 \\ 13 \\ 14 \\ 15 $	121 144 169 196 225	1331 1728 2197 2744 3375	$3 \cdot 3166248$ $3 \cdot 4641016$ $3 \cdot 6055513$ $3 \cdot 7416574$ $3 \cdot 8729833$	$2 \cdot 2239801$ $2 \cdot 2894286$ $2 \cdot 3513347$ $2 \cdot 4101422$ $2 \cdot 4662121$	$\begin{array}{r} .090909091 \\ .083333333 \\ .076923077 \\ .071428571 \\ .066666667 \end{array}$
16 17 18 19 20	256 289 324 · 361 400	4096 4913 5832 6859 8000	$\begin{array}{r} 4.0000000\\ 4.1231056\\ 4.2426407\\ 4.3588989\\ 4.4721360\end{array}$	2.5198421 2.5712816 2.6207414 2.6684016 2.7144177	.062500000 .058823529 .055555556 .052631579 .050000000
21 22 23 24 25	441 484 529 576 625	9261 10648 12167 13824 15625	$\begin{array}{r} 4.5825757\\ 4.6904158\\ 4.7958315\\ 4.8989795\\ 5.0000000\\ \end{array}$	2.7589243 2.8020393 2.8438670 2.8844991 2.9240177	$\begin{array}{r} \cdot 047619048 \\ \cdot 04545454545 \\ \cdot 043478261 \\ \cdot 041666667 \\ \cdot 040000000 \end{array}$
26 27 28 29 <b>30</b>	676 729 784 841 900	17576 19683 21952 24389 27000	$\begin{array}{r} 5.0990195\\ 5.1961524\\ 5.2915026\\ 5.3851648\\ 5.4772256\\ \end{array}$	2.9624960 3.0000000 3.0365889 3.0723168 3.1072325	$\begin{array}{r} \cdot 038461538 \\ \cdot 037037037 \\ \cdot 035714286 \\ \cdot 034482759 \\ \cdot 033333333 \end{array}$
31 32 33 34 35	961 1024 1089 1156 1225	29791 82768 35937 39304 42875	5.5677644 5.6568542 5.7445626 5.8309519 5.9160798	3.1413806 3.1748021 3.2075343 3.2396118 3.2710663	$\begin{array}{r} \cdot 032258065 \\ \cdot 031250000 \\ \cdot 030303030 \\ \cdot 029411765 \\ \cdot 028571429 \end{array}$
36 37 38 39 40	1296 1369 1444 1521 1600	46656 50653 54872 59319 64000	$\begin{array}{c} 6\cdot 0000000\\ 6\cdot 0827625\\ 6\cdot 1644140\\ 6\cdot 2449980\\ 6\cdot 3245553\end{array}$	$3 \cdot 3019272$ $3 \cdot 3322218$ $3 \cdot 3619754$ $3 \cdot 3912114$ $3 \cdot 4199519$	02777778 027027027 026315789 025641026 025000000
41 42 43 44 45	1681 1764 1849 1936 2025	68921 74088 79507 85184 91125	$\begin{array}{c} 6.4031242\\ 6.4807407\\ 6.5574385\\ 6.6332496\\ 6.7082039\end{array}$	3.4482172 3.4760266 3.5033981 3.5303483 3.5568933	•024390244 •023809524 •023255814 •022727273 •0222222222
46 47 48 49 50	2116 2209 2304 2401 2500	97336 103823 110592 117649 125000	6.7823300 6.8556546 6.9282032 7.0000000 7.0710678	3.5830479 3.6088261 3.6342411 3.6593057 3.6840314	$\begin{array}{r} \bullet 021739130\\ \bullet 021276600\\ \bullet 020833333\\ \bullet 020408163\\ \bullet 020000000\end{array}$
51 52 53 54 55	2601 2704 2809 2916 3025	$132651 \\ 140608 \\ 148877 \\ 157464 \\ 166375$	$\begin{array}{c} \textbf{7.1414284} \\ \textbf{7.2111026} \\ \textbf{7.2801099} \\ \textbf{7.3484692} \\ \textbf{7.4161985} \end{array}$	3.7084298 3.7325111 3.7562858 3.7797631 3.8029525	.019607843 .019230769 .018867925 .018518519 .018181818
56 57 58 59 60	$3136 \\ 3249 \\ 3364 \\ 3481 \\ 3600$	175616 185193 195112 205379 216000	7.4833148 7.5498344 7.6157731 7.6811457 7.7459667	3.8258624 3.8485011 3.8708766 3.8929965 3.9148676	$\begin{array}{r} .017857143\\ .017543860\\ .017241379\\ .016949153\\ .016666667\end{array}$

No.	Squares.	Cubes.	Square Roots.	Cube Roots.	Reciprocals.
61 62 63 64 65	3721 3844 3969 4096 4225	226981 238328 250047 262144 274625	$\begin{array}{c} 7.8102497\\ 7.8740079\\ 7.9372539\\ 8.000000\\ 8.0622577\end{array}$	$3 \cdot 9364972$ $3 \cdot 9578915$ $3 \cdot 9790571$ $4 \cdot 0000000$ $4 \cdot 0207256$	.016393443 .016129032 .015873016 .015625000 .015384615
66 67 68 69 70	4356 4489 4624 4761 4900	287496 300763 314432 328509 343000	8.1240384 8.1853528 8.2462113 8.3066239 8.3666003	$\begin{array}{r} 4\cdot0412401\\ \cdot4\cdot0615480\\ 4\cdot0816551\\ 4\cdot1015661\\ 4\cdot1212853\end{array}$	0.015151515 0.014925873 0.014705882 0.014492754 0.014285714
71 72 73 74 75	5041 5184 5329 5476 5625	357911 373248 389017 405224 421875	$\begin{array}{r} 8.4261498\\ 8.4852814\\ 8.5440037\\ 8.6023253\\ 8.6602540\end{array}$	$\begin{array}{r} 4.1408178\\ 4.1601676\\ 4.1793390\\ 4.1983364\\ 4.2171633\end{array}$	$\begin{array}{r} \cdot 014084507\\ \cdot 013888889\\ \cdot 013698630\\ \cdot 013513514\\ \cdot 013333333\end{array}$
76 77 78 79 80	5776 5929 6084 6241 6400	438976 456533 474552 493039 512000	8.7177979 8.7749644 8.8317609 8.8881944 8.9442719	$\begin{array}{r} 4\cdot 2358236\\ 4\cdot 2543210\\ 4\cdot 2726586\\ 4\cdot 2908404\\ 4\cdot 3088695\end{array}$	$\begin{array}{r} .013157895\\ .012987013\\ .012820513\\ .012658228\\ .012500000\end{array}$
81 82 83 84 85	6561 6724 6889 7056 7225	531441 551368 571787 592704 614125	9.0000000 9.0553851 9.1104336 9.1651514 9.2195445	$\begin{array}{r} 4.3267487\\ 4.3444815\\ 4.3620707\\ 4.3795191\\ 4.3968296\end{array}$	012345679 012195122 012048193 011904762 011764706
86 87 88 89 90	7396 7569 7744 7921 8100	636056 658503 681472 704969 729000	9.2736185 9.3273791 9.3808315 9.4339811 9.4868330	$\begin{array}{r} 4.4140049\\ 4.4310476\\ 4.4479602\\ 4.4647451\\ 4.4814047\end{array}$	.011627907 .011494253 .011363636 .011235955 .01111111
91 92 93 94 95	8281 8464 8649 8836 9025	753571 778688 804357 830584 857375	$\begin{array}{r} 9.5393920\\ 9.5916630\\ 9.6436508\\ 9.6953597\\ 9.7467943\end{array}$	$\begin{array}{r} 4 \cdot 4979414 \\ 4 \cdot 5143574 \\ 4 \cdot 5306549 \\ 4 \cdot 5468359 \\ 4 \cdot 5629026 \end{array}$	.010989011 .010869565 .010752688 .010638298 .010526316
96 97 98 99 100	9216 9409 9604 9801 10000	884736 912673 941192 970299 1000000	$\begin{array}{r} 9.7979590\\ 9.8488578\\ 9.8994949\\ 9.9498744\\ 10.0000000\end{array}$	$\begin{array}{r} 4 \cdot 5788570 \\ 4 \cdot 5947009 \\ 4 \cdot 6104363 \\ 4 \cdot 6260650 \\ 4 \cdot 6415888 \end{array}$	•010416667 •010309278 •010204082 •010101010 •010000000
101 102 103 104 105	10201 10404 10609 10816 11025	$\begin{array}{r} 1030301 \\ 1061208 \\ 1092727 \\ 1124864 \\ 1157625 \end{array}$	$\begin{array}{r} 10.0498756\\ 10.0995049\\ 10.1488916\\ 10.1980390\\ 10.2469508 \end{array}$	$\begin{array}{r} 4.6570095\\ 4.6723287\\ 4.6875482\\ 4.7026694\\ 4.7176940\end{array}$	$\begin{array}{r} .009900990\\ .009803922\\ .009708738\\ .009615385\\ .009523810 \end{array}$
106 107 108 109 <b>110</b>	11236 11449 11664 11881 12100	1191016 1225043 1259712 1295029 1331000	$\begin{array}{r} 10.2956301\\ 10.3440804\\ 10.3923048\\ 10.4403065\\ 10.4880885\end{array}$	$\begin{array}{r} 4.7326235\\ 4.7474594\\ 4.7622032\\ 4.768562\\ 4.7914199\end{array}$	.009433962 .009345794 .009259259 .009174312 .009090909
$     \begin{array}{r}       111 \\       112 \\       113 \\       114 \\       115     \end{array} $	12321 12544 12769 12996 13225	$1367631 \\ 1404928 \\ 1442897 \\ 1481544 \\ 1520875$	$\begin{array}{r} 10.5356538\\ 10.5830052\\ 10.6301458\\ 10.6770783\\ 10.7238053\end{array}$	$\begin{array}{r} 4\cdot 8058955\\ 4\cdot 8202845\\ 4\cdot 8345881\\ 4\cdot 8488076\\ 4\cdot 8629442\end{array}$	$\begin{array}{r} .009009009\\ .008928571\\ .008849558\\ .008771930\\ .008695652\end{array}$
116 117 118 119 <b>120</b>	13456 13689 13924 14161 14400	1560896 1601613 1643032 1685159 1728000	$\begin{array}{c} 10.7703296\\ 10.8166538\\ 10.8627805\\ 10.9087121\\ 10.9544512 \end{array}$	$\begin{array}{r} 4.8769990\\ 4.8909732\\ 4.9048681\\ 4.9186847\\ 4.9324242\end{array}$	$\begin{array}{r} \cdot 008620690\\ \cdot 008547009\\ \cdot 008474576\\ \cdot 008403361\\ \cdot 008333333\end{array}$

No.	Squares.	Cubes.	Square Roots.	Cube Roots.	Reciprocals.
$121 \\ 122 \\ 123 \\ 124 \\ 125$	14641 14884 15129 15376 15625	1771561 1815848 1860867 1906624 1953125	$\begin{array}{c} 11\cdot 0000000\\ 11\cdot 0453610\\ 11\cdot 0905365\\ 11\cdot 1355287\\ 11\cdot 1803399\end{array}$	$\begin{array}{r} 4.9460874\\ 4.9596757\\ 4.9731898\\ 4.9866310\\ 5.0000000\end{array}$	· 008264463 · 008196721 · 008130081 · 008064516 · 008000000
126 127 128 129 130	15876 16129 16384 16641 16900	2000376 2048383 2097152 2146689 2197000	$\begin{array}{r} 11.2249722\\ 11.2694277\\ 11.3137085\\ 11.3578167\\ 11.4017543\\ \end{array}$	5.0132979 5.0265257 5.0396842 5.0527743 5.0657970	-007936508 -007874016 -007812500 -007751938 -007692308
131 132 133 134 135	17161 17424 17689 17956 18225	2248091 2299968 2352637 2406104 2460375	$\begin{array}{c} 11.4455231 \\ 11.4891253 \\ 11.5325626 \\ 11.5758369 \\ 11.6189500 \end{array}$	$5.0787531 \\ 5.0916434 \\ 5.1044687 \\ 5.1172299 \\ 5.1299278 $	·007633588 ·007575758 ·007518797 ·007462687 ·007407407
136 137 138 139 140	18496 18769 19044 19321 19600	$\begin{array}{r} 2515456\\ 2571353\\ 2628072\\ 2685619\\ 2744000 \end{array}$	11.6619038 11.7046999 11.7473401 11.7898261 11.8321596	5.1425632 5.1551367 5.1676493 5.1801015 5.1924941	$\begin{array}{r} \cdot 007352941 \\ \cdot 007299270 \\ \cdot 007246377 \\ \cdot 007194245 \\ \cdot 007142857 \end{array}$
$141 \\ 142 \\ 143 \\ 144 \\ 145$	19881 20164 20449 20736 21025	2803221 2863288 2924207 2985984 3048625	$11.8743421 \\11.9163753 \\11.9582607 \\12.0000000 \\12.0415946$	$5 \cdot 2048279 \\ 5 \cdot 2171034 \\ 5 \cdot 2293215 \\ 5 \cdot 2414828 \\ 5 \cdot 2535879$	007092199 007042254 006993007 006944444 006896552
146 147 , 148 149 150	21316 21609 21904 22201 22500	3112136 3176523 3241792 3307949 3375000	$\begin{array}{r} 12.0830460\\ 12.1243557\\ 12.1655251\\ 12.2065556\\ 12.2474487\end{array}$	$\begin{array}{r} 5\cdot 2656374\\ 5\cdot 2776321\\ 5\cdot 2895725\\ 5\cdot 3014592\\ 5\cdot 3132928\end{array}$	$\begin{array}{r} 0.06849315\\ 0.06802721\\ 0.06756757\\ 0.06711409\\ 0.066666667\end{array}$
151 152 153 154 155	22801 23104 23409 23716 24025	3442951 3511808 3581577 3652264 3723875	12.288205712.328828012.369316912.409673612.4498996	$\begin{array}{r} 5\cdot 3250740\\ 5\cdot 3368033\\ 5\cdot 3484812\\ 5\cdot 3601084\\ 5\cdot 3716854\end{array}$	$\begin{array}{r} \cdot 006622517\\ \cdot 006578947\\ \cdot 006535948\\ \cdot 006493506\\ \cdot 006451613\end{array}$
156 157 158 159 160	24336 24649 24964 25281 25600	3796416 3869893 3944312 4019679 4096000	12.4899960 12.5299641 12.5698051 12.6095202 12.6491106	$\begin{array}{r} 5\cdot 3832126\\ 5\cdot 3946907\\ \cdot\ 5\cdot 4061202\\ 5\cdot 4175015\\ 5\cdot 4288352\end{array}$	$\begin{array}{c} \cdot 006410256\\ \cdot 006369427\\ \cdot 006329114\\ \cdot 006289308\\ \cdot 006250000\end{array}$
$161 \\ 162 \\ 163 \\ 164 \\ 165$	25921 26244 26569 26896 27225	4173281 4251528 4330747 4410944 4492125	$12.6885775 \\ 12.7279221 \\ 12.7671453 \\ 12.8062485 \\ 12.8452326$	$\begin{array}{r} 5.4401218\\ 5.4513618\\ 5.4625556\\ 5.4737037\\ 5.4848066\end{array}$	$\begin{array}{r} \cdot 006211180 \\ \cdot 006172840 \\ \cdot 006134969 \\ \cdot 006097561 \\ \cdot 006060606 \end{array}$
166 167 168 169 <b>170</b>	27556 27889 28224 28561 28900	4574296 4657463 4741632 4826809 4913000	12.8840987 12.9228480 12.9614814 13.0000000 13.0384048	$\begin{array}{c} 5.4958647\\ 5.5068784\\ 5.5178484\\ 5.5287748\\ 5.5396583\end{array}$	$\begin{array}{r} \cdot 006024096 \\ \cdot 005988024 \\ \cdot 005952381 \\ \cdot 005917160 \\ \cdot 005882353 \end{array}$
171 172 173 174 175	29241 29584 29929 30276 30625	$\begin{array}{c} 5000211\\ 5088448\\ 5177717\\ 5268024\\ 5359375\end{array}$	$\begin{array}{r} 13.0766968\\ 13.1148770\\ 13.1529464\\ 13.1909060\\ 13.2287566\end{array}$	$\begin{array}{c} 5.5504991\\ \cdot 5.5612978\\ 5.5720546\\ 5.5827702\\ 5.5934447\end{array}$	$\begin{array}{r} \cdot 005847953 \\ \cdot 005813953 \\ \cdot 005780347 \\ \cdot 005747126 \\ \cdot 005714286 \end{array}$
176 177 178 179 <b>180</b>	30976 31329 31684 32041 32400	5451776 5545233 5639752 5735339 5832000	$\begin{array}{c} 13\cdot 2664992\\ 13\cdot 3041347\\ 13\cdot 3416641\\ 13\cdot 3790882\\ 13\cdot 4164079\end{array}$	$\begin{array}{c} 5\cdot 6040787\\ 5\cdot 6146724\\ 5\cdot 6252263\\ 5\cdot 6357408\\ 5\cdot 6462162\end{array}$	$\begin{array}{r} \cdot 005681818\\ \cdot 005649718\\ \cdot 005617978\\ \cdot 005586592\\ \cdot 005555556\end{array}$

No.	Squares.	Cubes.	Square Roots.	Cube Roots.	Reciprocals.
181 182 183 184 185	32761 33124 33489 33856 34225	5929741 6028568 6128487 6229504 6331625	$13.4536240\\13.4907376\\13.5277493\\13.5646600\\13.6014705$	$5.6566528 \\ 5.6670511 \\ 5.6774114 \\ 5.6877340 \\ 5.6980192$	$\begin{array}{r} \cdot 005524862 \\ \cdot 005494505 \\ \cdot 005464481 \\ \cdot 005434783 \\ \cdot 005405405 \end{array}$
186 187 188 189 190	34596 34969 35344 35721 36100	$\begin{array}{r} 6434856\\ 6539203\\ 6644672\\ 6751269\\ 6859000 \end{array}$	$\begin{array}{r} 13.6381817\\ 13.6747943\\ 13.7113092\\ 13.7477271\\ 13.7840488 \end{array}$	5.7082675 5.7184791 5.7286543 5.7387936 5.7488971	$\begin{array}{r} 005376344\\ 005337594\\ 005319149\\ 005291005\\ 005263158\end{array}$
191 192 193 194 195	36481 36864 37249 37636 38025	6967871 7077888 7189057 7301384 7414875	$\begin{array}{r} 13.8202750\\ 13.8564065\\ 13.8924440\\ 13.9283883\\ 13.9642400\end{array}$	5.7589652 5.7689982 5.7789966 5.7889604 5.7988900	$\begin{array}{r} \cdot 005235602\\ \cdot 005208333\\ \cdot 005181347\\ \cdot 005154639\\ \cdot 005128205\end{array}$
196 197 198 199 200	38416 38809 39204 39601 40000	7529536 7645373 7762392 7880599 8000000	$\begin{array}{r} 14.0000000\\ 14.0356688\\ 14.0712473\\ 14.1067360\\ 14.1421356\end{array}$	5 · 8087857 5 · 8186479 5 · 8284767 5 · 8382725 5 · 8480355	$\begin{array}{r} .005102041\\ .005076142\\ .005050505\\ .005025126\\ .005000000\end{array}$
201 202 203 204 205	40401 40804 41209 41616 42025	8120601 8242408 8365427 8489664 8615125	$14.1774469\\14.2126704\\14.2478068\\14.2828569\\14.3178211$	$\begin{array}{c} 5.8577660\\ 5.8674643\\ 5.8771307\\ 5.8867653\\ 5.8963685\end{array}$	$\begin{array}{r} \cdot 004975124\\ \cdot 004950495\\ \cdot 004926108\\ \cdot 004901961\\ \cdot 004878049\end{array}$
206 207 208 209 <b>210</b>	42436 42849 43264 43681 44100	8741816 8869743 8998912 9129329 9261000	$14.3527001\\14.3874946\\14.4222051\\14.4568323\\14.4913767$	$\begin{array}{c} 5.9059406\\ 5.9154817\\ 5.9249921\\ 5.9344721\\ 5.9439220\end{array}$	$\begin{array}{r} .004854369\\ .004830918\\ .004807692\\ .004807692\\ .004784689\\ .004761905\end{array}$
211 212 213 214 215	44521 44944 45369 45796 46225	9393931 9528128 9663597 9800344 9938375	$14.5258390 \\ 14.5602198 \\ 14.5945195 \\ 14.6287388 \\ 14.6628783$	$\begin{array}{r} 5.9533418\\ 5.9627320\\ 5.9720926\\ 5.9814240\\ 5.9907264\end{array}$	$\begin{array}{r} \cdot 004739336 \\ \cdot 004716981 \\ \cdot 004694836 \\ \cdot 004672897 \\ \cdot 004651163 \end{array}$
216 217 218 219 220	46656 47089 47524 47961 48400	10077696 10218313 10360232 10503459 10648000	$14.6969385\\14.7309199\\14.7648231\\14.7986486\\14.8323970$	6.000000 6.0092450 6.0184617 6.0276502 8.0368107	$\begin{array}{r} \cdot 004629630\\ \cdot 004608295\\ \cdot 004587156\\ \cdot 004566210\\ \cdot 004545455\end{array}$
221 222 223 224 225	48841 49284 49729 50176 50625	10793861 10941048 11089567 11239424 11390625	$\begin{array}{r} 14.8660687\\ 14.8996644\\ 14.9331845\\ 14.9666295\\ 15.000000\\ \end{array}$	$\begin{array}{c} 6 \cdot 0459435 \\ 6 \cdot 0550489 \\ 6 \cdot 0641270 \\ 6 \cdot 0731779 \\ 6 \cdot 0822020 \end{array}$	$\begin{array}{r} \cdot 004524887 \\ \cdot 004504505 \\ \cdot 004484305 \\ \cdot 004464286 \\ \cdot 004444444 \end{array}$
226 227 228 229 230	51076 51529 51984 52441 52900	11543176 11697083 11852352 12008989 12167000	$\begin{array}{r} 15.0332964 \\ 15.0665192 \\ 15.0096689 \\ 15.1327460 \\ 15.1657509 \end{array}$	$\begin{array}{c} 6\cdot 0911994\\ 6\cdot 1001702\\ 6\cdot 1091147\\ 6\cdot 1180332\\ 6\cdot 1269257\end{array}$	$\begin{array}{r} \cdot 004424779 \\ \cdot 004405286 \\ \cdot 004385965 \\ \cdot 004366812 \\ \cdot 004347826 \end{array}$
231 232 233 234 235	53361 53824 54289 54756 55225	12326391 12487168 12649337 12812904 12977875	$\begin{array}{r} 15\cdot 1986842\\ 15\cdot 2315462\\ 15\cdot 2643375\\ 15\cdot 2970585\\ 15\cdot 3297097\end{array}$	$\begin{array}{c} 6\cdot 1357924\\ 6\cdot 1446337\\ 6\cdot 1534495\\ 6\cdot 1622401\\ 6\cdot 1710058\end{array}$	$\begin{array}{r} \cdot 004329004 \\ \cdot 004310345 \\ \cdot 004291845 \\ \cdot 004273504 \\ \cdot 004255319 \end{array}$
236 237 238 239 240	55696 56169 56644 57121 57600	13144256 13312053 13481272 13651919 13824000	$\begin{array}{c} 15\cdot 3622915\\ 15\cdot 3948043\\ 15\cdot 4272486\\ 15\cdot 4596248\\ 15\cdot 4919334\\ \end{array}$	$\begin{array}{c} 6.1797466\\ 6.1884628\\ 6.1971544\\ 6.2058218\\ 6.2144650\\ \end{array}$	.004237288 .004219409 .004201681 .004184100 .004166667

No.	Squares.	Cubes.	Square Roots.	Cube Roots.	Reciprocals.
241 242 243 244 245	58081 58564 59049 59536 60025	13997521 14172488 14348907 14526784 14706125	$15.5241747\\15.5563492\\15.5884573\\15.6204994\\15.6524758$	$\begin{array}{c} 6\cdot 2230843\\ 6\cdot 2316797\\ 6\cdot 2402515\\ 6\cdot 2487998\\ 6\cdot 2573248\end{array}$	004149378 004132231 004115226 004098361 004081633
246 247 248 249 250	60516 61009 61504 62001 62500	$\begin{array}{r} 14886936\\ 15069223\\ 15252992\\ 15438249\\ 15625000\\ \end{array}$	$\begin{array}{c} 15\cdot 6843871\\ 15\cdot 7162336\\ 15\cdot 7480157\\ 15\cdot 7797338\\ 15\cdot 8113883\end{array}$	$\begin{array}{c} 6\cdot 2658266\\ 6\cdot 2743054\\ 6\cdot 2827613\\ 6\cdot 2911946\\ 6\cdot 2996053\end{array}$	$\begin{array}{r} \cdot 004065041 \\ \cdot 004048583 \\ \cdot 004032258 \\ \cdot 004016064 \\ \cdot 004000000 \end{array}$
251 252 253 254 255	63001 63504 64009 64516 65025	15813251 16003008 16194277 16387064 16581375	$\begin{array}{c} 15.8429795\\ 15.8745079\\ 15.9059737\\ 15.9373775\\ 15.9687194 \end{array}$	$\begin{array}{c} 6\cdot 3079935\\ 6\cdot 3163596\\ 6\cdot 3247035\\ 6\cdot 3330256\\ 6\cdot 3413257\end{array}$	$\begin{array}{r} .003984064\\ .003968254\\ .003952569\\ .003937008\\ .003921569\end{array}$
256 257 258 259 <b>260</b>	65536 66049 66564 67081 67600	16777216 16974593 17173512 17373979 17576000	$\begin{array}{c} 16.000000\\ 16.0312195\\ 16.0623784\\ 16.0934769\\ 16.1245155\end{array}$	$6 \cdot 3496042$ $6 \cdot 3578611$ $6 \cdot 3660968$ $6 \cdot 3743111$ $6 \cdot 3825043$	$\begin{array}{r} \cdot 003906250 \\ \cdot 003891051 \\ \cdot 003875969 \\ \cdot 003861004 \\ \cdot 003846154 \end{array}$
261 262 263 264 265	68121 68644 69169 69696 70225	17779581 17984728 18191447 18399744 18609625	$16.1554944\\16.1864141\\16.2172747\\16.2480768\\16.2788206$	$\begin{array}{c} 6\cdot 3906765\\ 6\cdot 3988279\\ 6\cdot 4069585\\ 6\cdot 4150687\\ 6\cdot 4231583\end{array}$	$\begin{array}{r} \cdot 003831418 \\ \cdot 003816794 \\ \cdot 003802281 \\ \cdot 003787879 \\ \cdot 003773585 \end{array}$
266 267 268 269 270	70756 71289 71824 72361 72900	18821096 19034163 19248832 19465109 19683000	$\begin{array}{c} 16\cdot 3095064\\ 16\cdot 3401346\\ 16\cdot 3707055\\ 16\cdot 4012195\\ 16\cdot 4316767\end{array}$	$\begin{array}{r} 6\cdot 4312276\\ 6\cdot 4392767\\ 6\cdot 4473057\\ 6\cdot 4553148\\ 6\cdot 4633041 \end{array}$	.003759398 .003745318 .003731343 .003717472 .003703704
271 272 273 274 275	73441 73984 74529 75076 75625	19902511 20123648 20346417 20570824 20796875	$16.4620776 \\ 16.4924225 \\ 16.5227116 \\ 16.5529454 \\ 16.5831240$	$\begin{array}{r} 6\cdot 4712736\\ 6\cdot 4792236\\ 6\cdot 4871541\\ 6\cdot 4950653\\ 6\cdot 5029572\end{array}$	$\begin{array}{r} .003690037\\ .003676471\\ .003663004\\ .003649635\\ .00363636364\end{array}$
276 277 278 279 280	76176 76729 77284 77841 78400	21024576 21253933 21484952 21717639 21952000	$\begin{array}{r} 16.6132477\\ 16.6433170\\ 16.6733320\\ 16.7032931\\ 16.7332005 \end{array}$	$\begin{array}{r} 6\cdot 5108300\\ 6\cdot 5186839\\ 6\cdot 5265189\\ 6\cdot 5343351\\ 6\cdot 5421326\end{array}$	$\begin{array}{r} \cdot 003623188 \\ \cdot 003610108 \\ \cdot 003597122 \\ \cdot 003584229 \\ \cdot 003571429 \end{array}$
281 282 283 284 285	78961 79524 80089 80656 81225	22188041 22425768 22665187 22906304 23149125	$\begin{array}{r} 16.7630546\\ 16.7928556\\ 16.8226038\\ 16.8522995\\ 16.8819430\end{array}$	$\begin{array}{r} 6.5499116\\ 6.5576722\\ 6.5654144\\ 6.5731385\\ .6.5808443 \end{array}$	$\begin{array}{r} .003558719\\ .003546099\\ .003533569\\ .003521127\\ .003508772\end{array}$
286 287 288 289 290	81796 82369 82944 83521 84100	23393656 23639903 23887872 24137569 24389000	$16.9115345 \\ 16.9410743 \\ 16.9705627 \\ 17.0000000 \\ 17.0293864$	$\begin{array}{c} 6 \cdot 5885323 \\ 6 \cdot 5962023 \\ 6 \cdot 6038545 \\ 6 \cdot 6114890 \\ 6 \cdot 6191060 \end{array}$	$\begin{array}{r} \cdot 003496503 \\ \cdot 003484321 \\ \cdot 003472222 \\ \cdot 003460208 \\ \cdot 003448276 \end{array}$
291 292 293 294 295	84681 85264 85849 86436 87025	24642171 24897088 25153757 25412184 25672375	$\begin{array}{c} 17\cdot0587221\\ 17\cdot0880075\\ 17\cdot1172428\\ 17\cdot1464282\\ 17\cdot1755640\end{array}$	$\begin{array}{r} 6\cdot 6267054\\ 6\cdot 6342874\\ 6\cdot 6418522\\ 6\cdot 6493998\\ 6\cdot 6569302\end{array}$	$\begin{array}{r} \cdot 003436426\\ \cdot 003424658\\ \cdot 003412969\\ \cdot 003401361\\ \cdot 003389831\end{array}$
296 297 298 299 <b>300</b>	87616 88209 88804 89401 90000	25934336 26198073 26463592 26730899 27000000	$\begin{array}{c} 17\cdot 2046505\\ 17\cdot 2336879\\ 17\cdot 2626765\\ 17\cdot 2916165\\ 17\cdot 3205081\end{array}$	$\begin{array}{c} 6\cdot 6644437\\ 6\cdot 6719403\\ 6\cdot 6794200\\ 6\cdot 6868831\\ 6\cdot 6943295\end{array}$	$\begin{array}{r} \cdot 003378378\\ \cdot 003367003\\ \cdot 003355705\\ \cdot 003344482\\ \cdot 0033333333\end{array}$

No.	Squares.	Cubes.	Square Roots.	Cube Roots.	Reciprocals.
301 302 303 304 305	90601 91204 91809 92416 93025	27270901 27543608 27818127 28094464 28372625	$17.3493516 \\ 17.3781472 \\ 17.4068952 \\ 17.4355958 \\ 17.4642492$	$\begin{array}{c} 6\cdot7017593\\ 6\cdot7091729\\ 6\cdot7165700\\ 6\cdot7239508\\ 6\cdot7313155\end{array}$	.003322259 .003311258 .003300330 .003289474 .003278689
306 307 308 309 310	93636 94249 94864 95481 96100	28652616 28934443 29218112 29503629 29791000	17.4928557 17.5214155 17.5499288 17.5783958 17.6068169	6.7386641 6.7459967 6.7533134 6.7606143 6.7678995	$\begin{array}{r} \cdot 003267974 \\ \cdot 003257329 \\ \cdot 003246753 \\ \cdot 003236246 \\ \cdot 003225806 \end{array}$
811 812 813 314 815	96721 97344 97969 98596 99225	30080231 30371328 30664297 30959144 31255875	17.6351921 17.6635217 17.6918060 17.7200451 17.7482393	6.7751690 6.7824229 6.7896613 6.7968844 6.8040921	$\begin{array}{r} \cdot 003215434 \\ \cdot 003205128 \\ \cdot 003194888 \\ \cdot 003184713 \\ \cdot 003174603 \end{array}$
316 317 318 319 320	99856 100489 101124 101761 102400	31554496 31855013 32157432 32461759 32768000	17.7763888 17.8044938 17.8325545 17.8605711 17.8885438	6.8112847 6.8184620 6.8256242 6.8327714 6.8399037	$\begin{array}{r} \cdot 003164557 \\ \cdot 003154574 \\ \cdot 003144654 \\ \cdot 003134796 \\ \cdot 003125000 \end{array}$
321 322 323 324 325	103041 103684 104329 104976 105625	33076161 33386248 33698267 34012224 34328125	17.9164729 17.9443584 17.9722008 18.0000000 18.0277564	$\begin{array}{r} 6\cdot 8470213\\ 6\cdot 8541240\\ 6\cdot 8612120\\ 6\cdot 8682855\\ 6\cdot 8753443 \end{array}$	$\begin{array}{r} \cdot 003115265 \\ \cdot 003105590 \\ \cdot 003095975 \\ \cdot 003086420 \\ \cdot 003076923 \end{array}$
326 327 328 829 330	106276 106929 107584 108241 108900	34645976 34965783 35287552 35611289 35937000	18.0554701 18.0831413 18.1107703 18.1383571 18.1659021	$\begin{array}{r} 6\cdot 8823888\\ 6\cdot 8894188\\ 6\cdot 8964345\\ 6\cdot 9034359\\ 6\cdot 9104232\end{array}$	$\begin{array}{r} \cdot 003067485 \\ \cdot 003058104 \\ \cdot 003048780 \\ \cdot 003039514 \\ \cdot 00303030303 \end{array}$
331 332 333 334 335	$109561 \\ 110224 \\ 110889 \\ 111556 \\ 112225$	36264691 36594368 36926037 37259704 37595375	$18.1934054\\18.2208672\\18.2482876\\18.2756669\\18.3030052$	$\begin{array}{c} 6\cdot 9173964\\ 6\cdot 9243556\\ 6\cdot 9313008\\ 6\cdot 9382321\\ 6\cdot 9451496\end{array}$	$\begin{array}{r} \cdot 003021148 \\ \cdot 003012048 \\ \cdot 003003003 \\ \cdot 002994012 \\ \cdot 002985075 \end{array}$
336 337 338 339 340	112896 113569 114244 114921 115600	37933056 38272753 38614472 38958219 39304000	$18.3303028 \\ 18.3575598 \\ 18.3847763 \\ 18.4119526 \\ 18.4390889 $	$\begin{array}{c} 6.9520533\\ 6.9589434\\ 6.9658198\\ 6.9726826\\ 6.9795321\end{array}$	002976190 002967359 002958580 002949853 002941176
341 342 343 344 345	116281 116964 117649 118336 119025	39651821 40001688 40353607 40707534 41063625	$\begin{array}{r} 18.4661853\\ 18.4932420\\ 18.5202592\\ 18.5472370\\ 18.5741756\end{array}$	6.9863681 6.9931906 7.0000000 7.0067962 7.0185791	·002932551 ·002923977 ·002915452 ·002906977 ·002898551
346 347 348 349 350	119716 120409 121104 121801 122500	41421736 41781923 42144192 42508549 42875000	$18.6010752 \\ 18.6279360 \\ 18.6547581 \\ 18.6815417 \\ 18.7082869$	7.0203490 7.0271058 7.0338497 7.0405806 7.0472987	002890173 002881844 002873563 002865330 002857143
351 352 353 354 355	123201 123904 124609 125316 126025	43243551 43614208 43986977 44361864 44738875	18.7349940 18.7616630 18.7882942 18.8148877 18.8414437	$\begin{array}{r} 7.0540041 \\ 7.0606967 \\ 7.0673767 \\ 7.0740440 \\ 7.0806988 \end{array}$	$\begin{array}{r} \cdot 002849003 \\ \cdot 002840909 \\ \cdot 002832861 \\ \cdot 002824859 \\ \cdot 002816901 \end{array}$
356 357 358 359 <b>360</b>	$126736 \\ 127449 \\ 128164 \\ 128881 \\ 129600$	45118016 45499293 45882712 46268279 46656000	$\begin{array}{c} 18.8679623\\ 18.8944436\\ 18.9208879\\ 18.9472953\\ 18.9736660\end{array}$	7.0873411 7.0939709 7.1005885 7.1071937 7.1137866	.002808989 .002801120 .002793296 .002785515 .002777778

No.	Squares.	Cubes.	Square Roots.	Cube Roots.	Reciprocals.
361 362 363 364 365	130321 131044 131769 132496 133225	47045881 47437928 47832147 48228544 48627125	19.0000000 19.0262976 19.0525589 19.0787840 19.1049732	7.1203674 7.1269360 7.1334925 7.1400370 7.1465695	002770083 002762431 002754821 002754821 002747253 002739726
366	133956	49027896	19.1311265	7.1530901	·002732240
367	134689	49430863	19.1572441	7.1595988	·002724796
368	135424	49836032	19.1833261	7.1660957	·002717391
369	136161	50243409	19.2093727	7.1725809	·002710027
370	136900	50653000	19.2353841	7.1790544	·002702703
371	137641	51064811	19.2613603	$7.1855162 \\7.1919663 \\7.1984050 \\7.2048322 \\7.2112479$	·002695418
372	138384	51478848	19.2873015		·002688172
373	139129	51895117	19.3132079		·002680965
374	139876	52313624	19.3390796		·002673797
375	140625	52734375	19.3649167		·002666667
376	141376	53157376	19.3907194	7.2176522	·002659574
377	142129	53582633	19.4164878	7.2240450	·002652520
378	142884	54010152	19.4422221	7.2304268	·002645503
379	143641	54439939	19.4679223	7.2367972	·002638522
380	144400	54872000	19.4935887	7.2431565	·002631579
381	145161	55306341	19.5192213	$\begin{array}{r} 7.2495045\\ 7.2558415\\ 7.2621675\\ 7.2684824\\ -7.2747864 \end{array}$	·002624672
382	145924	55742968	19.5448203		·002617801
383	146689	56181887	19.5703858		·002610966
384	147456	56623104	19.5959179		·002604167
385	148225	57066625	19.6214169		·002597403
386	148996	57512456	19.6468827	7.2810794	•002590674
387	149769	57960603	19.6723156	7.2873617	•002583979
388	150544	58411072	19.6977156	7.2936330	•002577320
389	151321	58863869	19.7230829	7.2998936	•002570694
390	152100	59319000	19.7484177	7.3061436	•002564103
391	152881	$\begin{array}{c} 59776471 \\ 60236288 \\ 60698457 \\ 61162984 \\ 61629875 \end{array}$	19.7737199	7.3123828	.002557545
392	153664		19.7989899	7.3186114	.002551020
393	154449		19.8242276	7.3248295	.002544529
394	155236		19.8494332	7.3310369	.002538071
395	156025		19.8746069	7.3372339	.002531646
396	156816	62099136	19.8997487	7.3434205	.002525253
397	157609	62570773	19.9248588	7.3495966	.002518892
398	158404	63044792	19.9499373	7.3557624	.002512563
399	159201	63521199	19.9749844	7.3619178	.002506266
400	160000	64000000	20.0000000	7.3680630	.002500000
401 402 403 404 405	160801 161604 162409 163216 164025	64481201 64964808 65450827 65939264 66430125	$\begin{array}{c} 20.0249844\\ 20.0499377\\ 20.0748599\\ 20.0997512\\ 20.1246118 \end{array}$	7.3741979 7.3803227 7.3864373 7.3925418 7.3986363	$\begin{array}{r} \cdot 002493766 \\ \cdot 002487562 \\ \cdot 002481390 \\ \cdot 002475248 \\ \cdot 002469136 \end{array}$
406 407 408 409 410	164836 165649 166464 167281 168100	66923416 67419143 67917312 68417929 68921000	$\begin{array}{r} 20.1494417\\ 20.1742410\\ 20.1990099\\ 20.2237484\\ 20.2484567\end{array}$	7.4047206 7.4107950 7.4168595 7.4229142 7.4289589	$\begin{array}{r} \cdot 002463054 \\ \cdot 002457002 \\ \cdot 002450980 \\ \cdot 002444988 \\ \cdot 002439024 \end{array}$
411 412 413 414 415	168921 169744 170569 171396 172225	69426531 69934528 70444997 70957944 71473375	$\begin{array}{r} 20.2731349\\ 20.2977831\\ 20.3224014\\ 20.3469899\\ 20.3715488 \end{array}$	7.4349938 7.4410189 7.4470342 7.4530399 7.4590359	$\begin{array}{r} \cdot 002433090 \\ \cdot 002427184 \\ \cdot 002421308 \\ \cdot 002415459 \\ \cdot 002409639 \end{array}$
416	173056	71991296	$\begin{array}{c} 20.3960781\\ 20.4205779\\ 20.4450483\\ 20.4694895\\ 20.4939015\end{array}$	7.4650223	.002403846
417	173889	72511713		7.4709991	.002398082
418	174724	73034632		7.4769664	.002392344
419	175561	73560059		7.4829242	.002386635
420	176400	74088000		7.4888724	.00238635

No.	Squares.	Cubes.	Square Roots.	Cube Roots.	Reciprocals.
421 422 423 424 425	177241 178084 178929 179776 180625	74618461 75151448 75686967 76225024 76765625	$\begin{array}{c} 20.5182845\\ 20.5426386\\ 20.569638\\ 20.5912603\\ 20.6155281 \end{array}$	7.4948113 7.5007406 7.5066607 7.5125715 7.5184730	$\begin{array}{c} .002375297\\ .002369668\\ .002364066\\ .002358491\\ .002352941 \end{array}$
426 427 428 429 430	181476 182329 183184 184041 184900	77308776 77854483 78402752 78953589 79507000	$\begin{array}{c} 20.6397674\\ 20.6639783\\ 20.6881609\\ 20.7123152\\ 20.7364414 \end{array}$	7.5243652 7.5302482 7.5361221 7.5419867 7.5478423	$\begin{array}{r} \cdot 002347418 \\ \cdot 002341920 \\ \cdot 002336449 \\ \cdot 002331002 \\ \cdot 002325581 \end{array}$
431 432 433 434 435	185761 186624 187489 188356 189225	80062991 80621568 81182737 81746504 82312875	$\begin{array}{c} 20.7605395\\ 20.7846097\\ 20.8086520\\ 20.8326667\\ 20.8566536\end{array}$	7.5536888 7.5595263 7.5653548 7.5711743 7.5769849	$\begin{array}{r} \cdot 002320186\\ \cdot 002314815\\ \cdot 002309469\\ \cdot 0023094147\\ \cdot 002298851\end{array}$
436 437 438 439 440	190096 190969 191844 192721 193600	82881856 83453453 84027672 84604519 85184000	20.8806130 20.9045450 20.9284495 20.9523268 20.9761770	$\begin{array}{r} 7.5827865\\ 7.5885793\\ 7.5943633\\ 7.6001385\\ 7.6059049\end{array}$	.002293578 .002288330 .002283105 .002277904 .002272727
441 442 443 444 - 445	194481 195364 196249 197136 198025	85766121 86350888 86938307 87528384 88121125	$\begin{array}{c} 21.0000000\\ 21.0237960\\ 21.0475652\\ 21.0475652\\ 21.0713075\\ 21.0950231 \end{array}$	$\begin{array}{r} 7.6116626\\ 7.6174116\\ 7.6231519\\ 7.6288837\\ 7.6346067\end{array}$	$\begin{array}{r} \cdot 002267574 \\ \cdot 002262443 \\ \cdot 002257336 \\ \cdot 002252252 \\ \cdot 002247191 \end{array}$
446 447 448 449 450	198916 199809 200704 201601 202500	88716536 89314623 89915392 90518849 91125000	$\begin{array}{c} 21\cdot 1187121\\ 21\cdot 1423745\\ 21\cdot 1660105\\ 21\cdot 1896201\\ 21\cdot 2132034 \end{array}$	$\begin{array}{c} 7.6403213\\ 7.6460272\\ 7.6517247\\ 7.6574138\\ 7.6630943 \end{array}$	$\begin{array}{r} .002242152\\ .002237136\\ .002232143\\ .002227171\\ .0022222222\end{array}$
451 452 453 454 455	203401 204304 205209 206116 207025	91733851 92345408 92959677 93576664 94196375	$\begin{array}{r} 21.2367606\\ 21.2602916\\ 21.2837967\\ 21.3072758\\ 21.307290\end{array}$	7.6687665 7.6744303 7.6800857 7.6857328 7.6913717	.002217295 .002212389 .002207506 .002202643 .002197802
456 457 458 459 460	207936 208849 209764 210681 211600	94818816 95443993 96071912 96702579 97336000	$\begin{array}{r} 21\cdot 3541565\\ 21\cdot 3775583\\ 21\cdot 4009346\\ 21\cdot 4242853\\ 21\cdot 4476106\end{array}$	$\begin{array}{c} 7.6970023\\ 7.7026246\\ 7.7082388\\ 7.7138448\\ 7.7194426\end{array}$	002192982 002188184 002183406 002178649 002173913
461 462 463 464 465	212521 213444 214369 215296 216225	97972181 98611128 99252847 99897344 100544625	$\begin{array}{r} 21.4709106\\ 21.4941853\\ 21.5174348\\ 21.5406592\\ 21.5638587\end{array}$	7 · 7250325 7 · 7306141 7 · 7361877 7 · 7417532 7 · 7473109	$\begin{array}{r} .002169197\\ .002164502\\ .002159827\\ .002155172\\ .002150538\end{array}$
466 467 468 469 470	217156 218089 219024 219961 220900	$\begin{array}{c} 101194696\\ 101847563\\ 102503232\\ 103161709\\ 103823000 \end{array}$	21.5870331 21.6101828 21.6333077 21.6564078 21.6794834	$7 \cdot 7528606$ $7 \cdot 7584023$ $7 \cdot 7639361$ $7 \cdot 7694620$ $7 \cdot 7749801$	002145923 002141328 002136752 002132196 002127660
471 472 473 474 475	221841 222784 223729 224676 225625	$\begin{array}{r} 104487111\\ 105154048\\ 105823817\\ 106496424\\ 107171875 \end{array}$	21.7025344 21.7255610 21.7485632 21.7715411 21.7944947	$\begin{array}{c} 7\cdot7804904\\ 7\cdot7859928\\ 7\cdot7914875\\ 7\cdot7969745\\ 7\cdot8024538\end{array}$	$\begin{array}{r} .002123142\\ .002118644\\ .002114165\\ .002109705\\ .002105263\end{array}$
476 477 478 479 480	226576 227529 228484 229441 230400	107850176 108531333 109215352 109902239 110592000	$\begin{array}{c} 21\cdot 8174242\\ 21\cdot 8403297\\ 21\cdot 8632111\\ 21\cdot 8860686\\ 21\cdot 9089023 \end{array}$	7.8079254 7.8133892 7.8188456 7.8242942 7.8297353	$\begin{array}{r} .002100840\\ .002096436\\ .002092050\\ .002087683\\ .002083333\end{array}$

No.	Squares.	Cubes.	Square Roots.	Cube Roots.	Reciprocals.
481	231361	111284641	<b>21.</b> 9317122	7.8351688	·002079002
482	232324	111980168	21.9544984	7.8405949	·002074689
483	233289	112678587	21.9772610	7.8460134	·002070393
484	234256	113379904	22.0000000	7.8514244	·002066116
485	235225	114084125	22.0227155	7.8568281	·002061856
486	236196	114791256	$\begin{array}{r} 22.0454077\\ 22.0680765\\ 22.0907220\\ 22.1133444\\ 22.1359436 \end{array}$	7.8622242	•002057613
487	237169	115501303		7.8676130	•002053388
488	238144	116214272		7.8729944	•002049180
489	239121	116930169		7.8783684	•002044990
490	240100	117649000		7.8837352	•002040816
491	241081	118370771	22.1585198	7.8890946	•002036660
492	242064	119095488	22.1810730	7.8944468	•002032520
493	243049	119823157	22.2036033	7.8997917	•002028398
494	244036	120553784	22.2261108	7.9051294	•002024291
495	245025	121287375	22.2485955	7.9104599	•002020202
496	246016	122023936	22.2710575	7.9157832	.002016129
497	247009	122763473	22.2934968	7.9210994	.002012072
498	248004	123505992	22.3159136	7.9264085	.002008032
499	249001	124251499	22.3383079	7.9317104	.002004008
500	250000	125000000	22.3606798	7.9370053	.002000000
501	251001	$\begin{array}{r} 125751501\\ 126506008\\ 127263527\\ 128024064\\ 128787625\\ \end{array}$	22.3830293	7.9422931	.001996008
502	252004		22.4053565	7.9475739	.001992032
503	253009		22.4276615	7.9528477	.001988072
504	254016		22.4499443	7.9581144	.001984127
505	255025		22.4722051	7.9633743	.001980198
506	256036	129554216	22.4944438	7.9686271	.001976285
507	257049	130323843	22.5166605	7.9738731	.001972387
508	258064	131096512	22.5388553	7.9791122	.001968504
509	259081	131872229	22.5610283	7.9843444	.001964637
510	260100	132651000	22.5831796	7.9895697	.001960784
511	261121	133432831	22.6053091	7.9947883	$\begin{array}{r} .001956947\\ .001953125\\ .001949318\\ .001945525\\ .001941748\end{array}$
512	262144	134217728	22.6274170	8.0000000	
513	263169	135005697	22.6495033	8.0052049	
514	264196	135796744	22.6715681	8.0104032	
515	265225	136590875	22.6936114	8.0155946	
516	266256	137388096	22.7156334	$\begin{array}{r} 8.0207794 \\ 8.0259574 \\ 8.0311287 \\ 8.0362935 \\ 8.0414515 \end{array}$	.001937984
517	267289	138188413	22.7376340		.001934236
518	268324	138991832	22.7596134		.001930502
519	269361	139798359	22.7815715		.001926782
520	270400	140608000	22.8035085		.001923077
521	271441	141420761	22.8254244	8.0466030	·001919386
522	272484	142236648	22.8473193	8.0517479	·001915709
523	273529	143055667	22.8691933	8.0568862	·001912046
524	274576	143877824	22.8910463	8.0620180	·001908397
525	275625	144703125	22.9128785	8.0671432	·001904762
526	276676	145531576	22.9346899	8.0722620	$\begin{array}{r} .001901141\\ .001897533\\ .001893939\\ .001890359\\ .001886792\end{array}$
527	277729	146363183	22.9564808	8.0773743	
528	278784	147197952	22.9782508	8.0824800	
529	279841	148035889	23.0000000	8.0875794	
530	280900	148877000	23.0217289	8.0926723	
531	281961	149721291	23.0434372	8.0977589	.001883239
532	283024	150568768	23.0651252	8.1028390	.001879699
533	284089	151419437	23.0867928	8.1079128	.001876173
534	285156	152273304	23.1084400	8.1129803	.001872659
535	286225	153130375	23.1300670	8.1180414	.001869159
536	287296	153990656	$\begin{array}{r} 23.1516738\\ 23.1732605\\ 23.1948270\\ 23.2163735\\ 23.2379001 \end{array}$	8.1230962	.001865672
537	288369	154854153		8.1281447	.001862197
538	289444	155720872		8.1331870	.001858736
539	290521	156590819		8.1382230	.001855288
540	291600	157464000		8.1432529	.001855288

No.	Squares.	Cubes.	Square Roots.	Cube Roots.	Reciprocals.
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541	292681	$\begin{array}{r} 158340421\\ 159220088\\ 160103007\\ 160989184\\ 161878625 \end{array}$	$23 \cdot 2594067$	8.1482765	.001848429
542	293764		$23 \cdot 2808935$	8.1532939	.001845018
543	294849		$23 \cdot 3023604$	8.1583051	.001841621
544	295936		$23 \cdot 3238076$	8.1633102	.001838235
545	297025		$23 \cdot 3452351$	8.1683092	.001834862
546	298116	$162771336 \\ 163667323 \\ 164566592 \\ 165469149 \\ 166375000$	23.3666429	8.1733020	·001831502
547	299209		23.3880311	8.1782888	·001828154
548	300304		23.4093998	8.1832695	·001824818
549	301401		23.4307490	8.1882441	·001821494
550	302500		23.4520788	8.1932127	·001818182
551	303601	167284151	23 • 4733892	8.1981753	.001814882
552	304704	168196608	23 • 4946802	8.2031319	.001811594
553	305809	169112377	23 • 5159520	8.2080825	.001808318
554	306916	170031464	23 • 5372046	8.2130271	.001805054
555	308025	170953875	23 • 5584380	8.2179657	.001801802
556	309136	171879616	23.5796522	8 · 2228985	$\begin{array}{r} \cdot 001798561 \\ \cdot 001795332 \\ \cdot 001792115 \\ \cdot 001788909 \\ \cdot 001785714 \end{array}$
557	310249	172808693	23.6008474	8 · 2278254	
558	311364	173741112	23.6220236	8 · 2327463	
559	312481	174676879	23.6431808	8 · 2376614	
560	313600	175616000	23.6643191	8 · 2425706	
561	314721	176558481	23.6854386	8.2474740	.001782531
562	315844	177504328	23.7065392	8.2523715	.001779359
563	316969	178453547	23.7276210	8.2572633	.001776199
564	318096	179406144	23.7486842	8.2621492	.001773050
565	319225	180362125	23.7697286	8.2670294	.001769912
566	320356	181321496	23.7907545	8.2719039	.001766784
567	321489	182284263	23.8117618	8.2767726	.001763668
568	322624	183250432	23.8327506	8.2816355	.001760563
569	323761	184220009	23.8537209	8.2864928	.001757469
570	324900	185193000	23.8746728	8.2913444	.001754386
571 572 573 574 575	326041 327184 328329 329476 330625	186169411 187149248 188132517 189119224 190109375	23.8956063 23.9165215 23.9374184 23.9582971 23.9791576	$\begin{array}{r} 8.2961903\\ 8.3010304\\ 8.3058651\\ 8.3106941\\ 8.3155175\end{array}$	$\begin{array}{r} \cdot 001751313\\ \cdot 001748252\\ \cdot 001745201\\ \cdot 001742160\\ \cdot 001739130\end{array}$
576	331776	191102976	$\begin{array}{r} 24.0000000\\ 24.0208243\\ 24.0416306\\ 24.0624188\\ 24.0831891 \end{array}$	8.3203353	·001736111
577	332929	192100033		8.3251475	·001733102
578	334084	193100552		8.3299542	·001730104
579	335241	194104539		8.3347553	·001727116
580	336400	195112000		8.3395509	·001724138
581 582 583 584 585	337561 338724 339889 341056 342225	196122941 197137368 198155287 199176704 200201625	$\begin{array}{r} 24.1039416\\ 24.1246762\\ 24.1453929\\ 24.1660919\\ 24.1867732 \end{array}$	$\begin{array}{r} 8.3443410\\ 8.3491256\\ 8.3539047\\ 8.3586784\\ 8.3634466\end{array}$	.001721170 .001718213 .001715266 .001712329 .001709402
586	343396	201230056	$\begin{array}{r} 24.2074369\\ 24.2280829\\ 24.2487113\\ 24.2693222\\ 24.2899156\end{array}$	8.3682095	.001706485
587	344569	202262003		8.3729668	.001703578
588	345744	203297472		8.3777188	.001700680
589	346921	204336469		8.3824653	.001697793
590	348100	205379000		8.3872065	.001694915
591	349281	206425071	$\begin{array}{r} 24\cdot 3104916\\ 24\cdot 3310501\\ 24\cdot 3515913\\ 24\cdot 3721152\\ 24\cdot 3926218\end{array}$	8.3919423	.001692047
592	350464	207474688		8.3966729	.001689189
593	351649	208527857		8.4013981	.001686341
594	352836	209584584		8.4061180	.001683502
595	354025	210644875		8.4108326	.001680672
596	355216	211708736	$\begin{array}{r} 24.4131112\\ 24.4335834\\ 24.4540385\\ 24.4744765\\ 24.4948974 \end{array}$	8.4155419	.001677852
597	356409	212776173		8.4202460	.001675042
598	357604	213847192		8.4249448	.001672241
599	358801	214921799		8.4296383	.001669449
<b>600</b>	360000	216000000		8.4343267	.001666667

No.	Squares.	Cubes.	Square Roots.	Cube Roots.	Reciprocals.
601 602 603 604 605	361201 362404 363609 364816 366025	217081801 218167208 219256227 220348864 221445125	$\begin{array}{r} 24.5153013\\ 24.5356883\\ 24.5560583\\ 24.5764115\\ 24.5967478\end{array}$	$\begin{array}{r} 8.4390098\\ 8.4436877\\ 8.4436877\\ 8.4483605\\ 8.4530281\\ 8.4576906\end{array}$	.001663894 .001661130 .001658375 .001655629 .001652893
606 607 608 609 610	367236 368449 369664 370881 372100	222545016 223648543 224755712 225866529 226981000	$\begin{array}{r} 24.6170673\\ 24.6373700\\ 24.6576560\\ 24.6779254\\ 24.6981781\end{array}$	8.4623479 8.4670001 8.4716471 8.4762892 8.4809261	$\begin{array}{r} \bullet 001650165\\ \bullet 001647446\\ \bullet 001644737\\ \bullet 001642036\\ \bullet 001639344\end{array}$
611	373321	228099131	24.7184142	8.4855579	·001636661
612	374544	229220928	24.7386338	8.4901848	·001633987
613	375769	230346397	24.7588368	8.4948065	·001631321
614	376996	231475544	24.7790234	8.4994233	·001628664
615	378225	232608375	24.7991935	8.5040350	·001626016
616	379456	233744896	24.8193473	8.5086417	.001623377
617	380689	234885113	24.8394847	8.5132435	.001620746
618	381924	236029032	24.8596058	8.5178403	.001618123
619	383161	237176659	24.8797106	8.5224321	.001615509
620	384400	238328000	24.8997992	8.5270189	.001612903
621	385641	$\begin{array}{r} 239483061\\ 240641848\\ 241804367\\ 242970624\\ 244140625 \end{array}$	24.9198716	8.5316009	.001610306
622	386884		24.9399278	8.5361780	.001607717
623	388129		24.9599679	8.5407501	.001605136
624	389376		24.9799920	8.5453173	.001602564
625	390625		25.0000000	8.5498797	.001600000
626 627 628 629 630	391876 393129 394384 395641 396900	$\begin{array}{r} 245314376\\ 246491883\\ 247673152\\ 248858189\\ 250047000\\ \end{array}$	$\begin{array}{r} 25.0199920\\ 25.0399681\\ 25.0599282\\ 25.0798724\\ 25.0998008 \end{array}$	8.5544372 8.5589899 8.5635377 8.5680807 8.5726189	•001597444 •001594896 •001592357 •001589825 •001587302
631	398161	251239591	$\begin{array}{r} 25.1197134\\ 25.1396102\\ 25.1594913\\ 25.1793566\\ 25.1992063\end{array}$	8.5771523	.001584786
632	399424	252435968		8.5816809	.001582278
633	400689	253636137		8.5862047	.001579779
634	401956	254840104		8.5907238	.001577287
635	403225	256047875		8.5952380	.001574803
636 637 638 639 640	404496 405769 407044 408321 409600	$\begin{array}{r} 257259456\\ 258474853\\ 259694072\\ 260917119\\ 262144000 \end{array}$	$25 \cdot 2190404$ $25 \cdot 2388589$ $25 \cdot 2586619$ $25 \cdot 2784493$ $25 \cdot 2982213$	8.5997476 8.6042525 8.6087526 8.6132480 8.6177388	$\begin{array}{r} \cdot 001572327 \\ \cdot 001569859 \\ \cdot 001567398 \\ \cdot 001564945 \\ \cdot 001562500 \end{array}$
641	410881	263374721	25.3179778	8.6222248	001560062
642	412164	264609288	25.3377189	8.6267063	001557632
643	413449	265847707	25.3574447	8.6311830	001555210
644	414736	267089984	25.3771551	8.6356551	001552795
645	416025	268336125	25.3968502	8.6401226	001550388
646	417316	269586136	25.4165301	$8 \cdot 6445855$	.001547988
647	418609	270840023	25.4361947	$8 \cdot 6490437$	.001545595
648	419904	272097792	25.4558441	$8 \cdot 6534974$	.001543210
649	421201	273359449	25.4754784	$8 \cdot 6579465$	.001540832
650	422500	274625000	25.4950976	$8 \cdot 6623911$	.001538462
651	423801	275894451	25.5147016	8.6668310	•001536098
652	425104	277167808	25.5342907	8.6712665	•001533742
653	426409	278445077	25.5538647	8.6756974	•001531394
654	427716	279726264	25.5734237	8.6801237	•001529052
655	429025	281011375	25.5929678	8.6845456	•001526718
656	430336	282300416	25.6124969	8.6889630	.001524390
657	431649	283593393	25.6320112	8.6933759	.001522070
658	432964	284890312	25.6515107	8.6977843	.001519757
659	434281	286191179	25.6709953	8.7021882	.001517451
<b>660</b>	435600	287496000	25.6904652	8.7065877	.001515152

No.	Squares.	Cubes.	Square Roots.	Cube Roots.	Reciprocals.
661	$\begin{array}{r} 436921\\ 438244\\ 439569\\ 440896\\ 442225\end{array}$	288804781	25.7099203	8.7109827	•001512859
662		290117528	25.7293607	8.7153734	•001510574
663		291434247	25.7487864	8.7197596	•001508296
664		292754944	25.7681975	8.7241414	•001506024
665		294079625	25.7875939	8.7285187	•001503759
666	443556	295408296	$\begin{array}{r} 25\cdot8069758\\ 25\cdot8263431\\ 25\cdot8456960\\ 25\cdot8650343\\ 25\cdot8843582\end{array}$	8.7328918	001501502
667	444889	296740963		8.7372604	001499250
668	446224	298077632		8.7416246	001497006
669	447561	299418309		8.7459846	00149768
670	448900	300763000		8.7503401	001492537
671	450241	302111711	25.9036677	8.7546913	.001490313
672	451584	303464448	25.9229628	8.7590383	.001488095
673	452929	304821217	25.9422435	8.7633809	.001485884
674	454276	306182024	25.9615100	8.7677192	.001483680
675	455625	307546875	25.9807621	8.7720532	.001481481
676	456976	308915776	26.000000	8.7763830	001479290
677	458329	310288733	26.0192237	8.7807084	001477105
678	459684	311665752	26.0384331	8.7850296	001474926
679	461041	313046839	26.0576284	8.7893466	001472754
680	462400	314432000	26.0768096	8.7936593	001470588
681	463761	315821241	26.0959767	8.7979679	.001468429
682	465124	317214568	26.1151297	8.8022721	.001466276
683	466489	318611987	26.1342687	8.8065722	.001464129
684	467856	320013504	26.1533937	8.8108681	.001461988
685	469225	321419125	26.1725047	8.8151598	.001459854
686	470596	322828856	26.19160.7	8.8194474	001457726
687	471969	324242703	26.2106848	8.8237307	001455604
688	473344	325660672	26.22975 1	8.8280099	001453488
689	474721	327082769	26.24880\$5	8.8322850	001451379
690	476100	328509000	26.2678511	8.8365559	001449275
691	477481	329939371	26.286° 89	8.8408227	001447178
692	478864	331373888	26.3058,29	8.8450854	001445087
693	480249	332812557	26.3248932	8.8493440	001443001
694	481636	334255384	26.3438797	8.8535985	001440922
695	483025	335702375	26.3628527	8.8578489	001438849
696	484416	337153536	26.3818119	8.8620952	$\begin{array}{r} \cdot 001436782 \\ \cdot 001434720 \\ \cdot 001432665 \\ \cdot 001430615 \\ \cdot 001428571 \end{array}$
697	485809	338608873	26.4007576	8.8663375	
698	487204	340068392	26.4196896	8.8705757	
699	488601	341532099	26.4386081	8.8748099	
700	490000	343000000	26.4575131	8.8790400	
701	491401	344472101	26.4764046	8.8832661	$\begin{array}{r} \bullet 001426534 \\ \bullet 001424501 \\ \bullet 001422475 \\ \bullet 001420455 \\ \bullet 001418440 \end{array}$
702	492804	345948408	26.4952826	8.8874882	
703	494209	347428927	26.5141472	8.8917063	
704	495616	348913664	26.5329983	8.8959204	
705	497025	350402625	26.5518361	8.9001304	
706	498436	351895816	$\begin{array}{r} 26.5706605\\ 26.5894716\\ 26.6082694\\ 26.6270539\\ 26.6458252 \end{array}$	8.9043366	.001416431
707	499849	353393243		8.9085387	.001414427
708	501264	354894912		8.9127369	.001412429
709	502681	356400829		8.9169311	.001410437
710	504100	357911000		8.9211214	.001408451
711	505521	$\begin{array}{r} 359425431\\ 360944128\\ 862467097\\ 363994344\\ 365525875\end{array}$	26.6645833	8.9253078	.001406470
712	506944		26.6833281	8.9294902	.001404494
713	508369		26.7020598	8.9336687	.001402525
714	509796		26.7207784	8.9378433	.001400560
715	511225		26.7394839	8.9420140	.001399501
716	512656	367061696	26.7581763	8.9461809	.001396648
717	514089	368601813	26.7768557	8.9503438	.001394700
718	515524	370146232	26.7955220	8.9545029	.001392758
719	516961	371694959	26.8141754	8.9586581	.001390821
720	518400	373248000	26.8328157	8.9628095	.001388889

No.	Squares.	Cubes.	Square Roots.	Cube Roots.	Reciprocals.
721	519841	374805361	$\begin{array}{r} 26.8514432\\ 26.8700577\\ 26.8886593\\ 26.9072481\\ 26.9258240 \end{array}$	8.9669570	.001386963
722	521284	376367048		8.9711007	.001385042
723	522729	377933067		8.9752406	.001383126
724	524176	379503424		8.9793766	.001381215
725	525625	381078125		8.9835089	.001379310
726	527076	382657176	$\begin{array}{c} 26.9443872\\ 26.9629375\\ 26.9814751\\ 27.0000000\\ 27.0185122\end{array}$	8.9876373	.001377410
727	528529	384240583		8.9917620	.001375516
728	529984	385828352		8.9958829	.001373626
729	531441	387420489		9.0000000	.001371742
730	532900	389017000		9.0041134	.001369863
731	534361	390617891	$\begin{array}{r} 27.0370117\\ 27.0554985\\ 27.0739727\\ 27.0924344\\ 27.1108834 \end{array}$	9.0082229	•001367989
732	535824	392223168		9.0123288	•001366120
733	537289	393832837		9.0164309	•001364256
734	538756	395446904		9.0205293	•001362398
735	540225	397065375		9.0246239	•001360544
736 737 738 739 740	$\begin{array}{r} 541696\\ 543169\\ 544644\\ 546121\\ 547600\\ \end{array}$	398688256 400315553 401947272 403583419 405224000	$\begin{array}{r} 27 \cdot 1293199 \\ 27 \cdot 1477439 \\ 27 \cdot 1661554 \\ 27 \cdot 1845544 \\ 27 \cdot 2029410 \end{array}$	9.0287149 9.0328021 9.0368857 9.0409655 9.0450419	.001358696 .001356852 .001355014 .001353180 .001351351
741	549081	406869021	$\begin{array}{r} 27\cdot 2213152\\ 27\cdot 2396769\\ 27\cdot 2580263\\ 27\cdot 2763634\\ 27\cdot 2946881\end{array}$	9.0491142	001349528
742	550564	408518488		9.0531831	001347709
743	552049	410172407		9.0572482	001345895
744	553536	411830784		9.0613098	001344086
745	555025	413493625		9.0653677	001342282
746	556516	415160936	27.3130006	9.0694220	·001340483
747	558009	416832723	27.3313007	9.0734726	·001338688
748	559504	418508992	27.3495887	9.0775197	·001336898
749	561001	420189749	27.3678644	9.0815631	·001335113
750	562500	421875000	27.3861279	9.0856030	·001333333
751 752 753 754 755	564001 565504 567009 568516 570025	423564751 425259008 426957777 428661064 430368875	$\begin{array}{r} 27\cdot 4043792\\ 27\cdot 4226184\\ 27\cdot 4408455\\ 27\cdot 4590604\\ 27\cdot 4772633\end{array}$	9.0896392 9.0936719 9.0977010 9.1017265 9.1057485	$\begin{array}{r} .001331558\\ .001329787\\ .001328021\\ .001326260\\ .001324503\end{array}$
756	571536	432081216	27.4954542	9.1097669	$\begin{array}{r} \cdot 001322751 \\ \cdot 001321004 \\ \cdot 001319261 \\ \cdot 001317523 \\ \cdot 001315789 \end{array}$
757	573049	433798093	27.5136330	9.1137818	
758	574564	435519512	27.5317998	9.1177931	
759	576081	437245479	27.5499546	9.1218010	
<b>760</b>	577600	438976000	27.5680975	9.1258053	
761	579121	440711081	$27 \cdot 5862284$	9.1298061	.001314060
762	580644	442450728	$27 \cdot 6043475$	9.1338034	.001312336
763	582169	444194947	$27 \cdot 6224546$	9.1377971	.001310616
764	583696	445943744	$27 \cdot 6405499$	9.1417874	.001308901
765	585225	447697125	$27 \cdot 6586334$	9.1457742	.001307190
766	586756	449455096	27.6767050	9.1497576	•001305483
767	588289	451217663	27.6947648	9.1537375	•001303781
768	589824	452984832	27.7128129	9.1577139	•001302083
769	591361	454756609	27.7308492	9.1616869	•001300390
770	592900	456533000	27.7488739	9.1656565	•001298701
771 772 773 774 775	594441 595984 597529 599076 600625	$\begin{array}{r} 458314011\\ 460099648\\ 461889917\\ 463684824\\ 465484375\end{array}$	27 · 7668868 27 · 7848880 27 · 8028775 27 · 8208555 27 · 8388218	9.1696225 9.1735852 9.1775445 9.1815003 9.1854527	$\begin{array}{r} \cdot 001297017 \\ \cdot 001295337 \\ \cdot 001293661 \\ \cdot 001291990 \\ \cdot 001290323 \end{array}$
776	$\begin{array}{c} 602176\\ 603729\\ 605284\\ 606841\\ 608400 \end{array}$	467288576	27.8567766	9.1894018	.001288660
777		469097433	27.8747197	9.1933474	.001287001
778		470910952	27.8926514	9.1972897	.001285347
779		472729139	27.9105715	9.2012286	.001283697
780		474552000	27.9284801	9.2051641	.001282051

No.	Squares.	Cubes.	Square Roots.	Cube Roots.	Reciprocals.
781	$\begin{array}{c} 609961\\ 611524\\ 613089\\ 614656\\ 616225 \end{array}$	476379541	27.9463772	9.2090962	.001280410
782		478211768	27.9642629	9.2130250	.001278772
783		480048687	27.9821372	9.2169505	.001277139
784		481890304	28.0000000	9.2208726	.001275510
785		483736625	28.0178515	9.2247914	.001273885
786	617796	485587656	28.0356915	$9 \cdot 2287068$	.001272265
787	619369	487443403	28.0535203	$9 \cdot 2326189$	.001270648
788	620944	489303872	28.0713377	$9 \cdot 2365277$	.001269036
789	622521	491169069	28.0891438	$9 \cdot 2404333$	.001267427
790	624100	493039000	28.1069386	$9 \cdot 2443355$	.001265823
791	625681	494913671	28.1247222	9.2482344	001264223
792	627264	496793088	28.1424946	9.2521300	001262626
793	628849	498677257	28.1602557	9.2560224	001261034
794	630436	500566184	28.1780056	9.2599114	001259446
795	632025	502459875	28.1957444	9.2637973	001257862
796	$\begin{array}{r} 633616\\ 635209\\ 636804\\ 638401\\ \underline{640000}\\ \end{array}$	504358336	$28 \cdot 2134720$	9.2676798	.001256281
797		506261573	$28 \cdot 2311884$	9.2715592	.001254705
798		508169592	$28 \cdot 2488938$	9.2754352	.001258133
799		510082399	$28 \cdot 2665881$	9.2793081	.001251564
800		512000000	$28 \cdot 2842712$	9.2831777	.001250000
801	$\begin{array}{r} 641601 \\ 643204 \\ 644809 \\ 646416 \\ 648025 \end{array}$	513922401	28 · 3019434	9.2870440	.001248439
802		515849608	28 · 3196045	9.2909072	.001246883
803		517781627	28 · 3372546	9.2947671	.001245330
804		519718464	28 · 3548938	9.2986239	.001243781
805		521660125	28 · 3725219	9.3024775	.001242236
806 807 808 809 810	649636 651249 652864 654481 656100	523606616 525557943 527514112 529475129 531441000	$\begin{array}{r} 28\cdot 3901391\\ 28\cdot 4077454\\ 28\cdot 4253408\\ 28\cdot 4429253\\ 28\cdot 4604989\end{array}$	$\begin{array}{r}9.3063278\\9.3101750\\9.3140190\\9.3178599\\9.3216975\end{array}$	001240695 001239157 001237624 001236094 001234568
811	657721	533411731	$\begin{array}{r} -28.4780617\\ 28.4956137\\ 28.5131549\\ 28.5306852\\ 28.5482048\end{array}$	9.3255320	.001233046
812	659344	535387328		9.3293634	.001231527
813	660969	537367797		9.3331916	.001230012
814	662596	539353144		9.3370167	.001228501
815	664225	541343375		9.3408386	.001226994
816	665856	543338496	28.5657137	9.3446575	.001225490
817	667489	545338513	28.5832119	9.3484731	.001223990
818	669124	547343432	28.6006993	9.3522857	.001222494
819	670761	549353259	28.6181760	9.3560952	.001221001
820	672400	551368000	28.6356421	9.3599016	.001219512
821	674041	553387661	28.6530976	9.3637049	.001218027
822	675684	555412248	28.6705424	9.3675051	.001216545
823	677329	557441767	28.6879766	9.3713022	.001215067
824	678976	559476224	28.7054002	9.3750963	.001213592
825	680625	561515625	28.7228132	9.3788873	.001212121
826	682276	563559976	28.7402157	9.3826752	.001210654
827	683929	565609283	28.7576077	9.3864600	.001209190
828	685584	567663552	28.7749891	9.3902419	.001207729
829	687241	569722789	28.7923601	9.3940206	.001206273
830	688900	571787000	28.8097206	9.3977964	.001204819
831	690561	573856191	28.8270706	9.4015691	.001203369
832	692224	575930368	28.8444102	9.4053387	.001201923
833	693889	578009537	28.8617394	9.4091054	.001200480
834	695556	580093704	28.8790582	9.4128690	.001199041
835	697225	582182875	28.8963666	9.4166297	.001197605
836	698896	584277056	28.9136646	9.4203873	.001196172
837	700569	586376253	28.9309523	9.4241420	.001194743
838	702244	588480472	28.9482297	9.4278936	.001193317
839	703921	590589719	28.9654967	9.4316423	.001191895
840	705600	592704000	28.9827535	9.4353880	.001190476

No.	Squares.	Cubes.	Square Roots.	Cube Roots.	Reciprocals.
841	707281	594823321	29.0000000	9.4391307	.001189061
842	708964	596947688	29.0172363	9.4428704	.001187648
843	710649	599077107	29.0344623	9.446072	.001186240
844	712336	601211584	29.0516781	9.4503410	.001184834
845	714025	603351125	29.0688837	9.4540719	.001183432
846 847 848 849 850	715716 717409 719104 720801 722500	605495736 607645423 609800192 611960049 614125000	$\begin{array}{r} 29\cdot0860791\\ 29\cdot1032644\\ 29\cdot1204396\\ 29\cdot1376046\\ 29\cdot1547595\end{array}$	$\begin{array}{r} 9.4577999\\ 9.4615249\\ 9.4652470\\ 9.4689661\\ 9.4726824\end{array}$	.001182033 .001180638 .001179245 .001177856 .001176471
851	724201	$\begin{array}{r} 616295051\\ 618470208\\ 620650477\\ 622835864\\ 625026375\\ \hline\end{array}$	29.1719043	9.4763957	.001175088
852	725904		29.1890390	9.4801061	.001173709
853	727609		29.2061637	9.4838136	.001172333
854	729316		29.2232784	9.4875182	.001170960
855	731025		29.2403830	9.4912200	.001169591
856	732736	627222016	29.2574777	9.4949188	.001168224
857	734449	629422793	29.2745623	9.4986147	.001166861
858	736164	631628712	29.2916370	9.5023078	.001165501
859	737881	633839779	29.3087018	9.5059980	.001164144
860	739600	636056000	29.3257566	9.5096854	.001162791
861	741321	$\begin{array}{r} 638277381 \\ 640503928 \\ 642735647 \\ 644972544 \\ 647214625 \end{array}$	29.3428015	9.5133699	.001161440
862	743044		29.3598365	9.5170515	.001160093
863	744769		29.3768616	9.5207303	.001158749
864	746496		29.3938769	9.5244063	.001157407
865	748225		29.4108823	9.5280794	.001156069
866	749956	649461896	29.4278779	9.5317497	.001154734
867	751689	651714363	9.4448637	9.5354172	.001153403
868	753424	653972032	29.4618397	9.5390818	.001152074
869	755161	656234909	29.4788059	9.5427437	.001150748
870	756900	658503000	29.4957624	9.5464027	.001149425
871	758641	660776311	29.5127091	9.5500589	$\begin{array}{r} .001148106\\ .001146789\\ .001145475\\ .001145475\\ .001144165\\ .001142857\end{array}$
872	760384	663054848	29.5296461	9.5537123	
873	762129	665338617	29.5465734	9.5573630	
874	763876	667627624	29.5634910	9.5610108	
875	765625	669921875	29.5803989	9.5646559	
876	767376	672221376	$\begin{array}{r} 29.5972972\\ 29.6141858\\ 29.6310648\\ 29.6479342\\ 29.6647939\\ \end{array}$	9.5682982	.001141553
877	769129	674526133		9.5719377	.001140251
878	770884	676836152		9.5755745	.001138952
879	772641	679151439		9.5792085	.001137656
880	774400	681472000		9.5828397	.001136364
881	776161	683797841	29.6816442	9.5864682	$\begin{array}{r} .001135074\\ .001133787\\ .001132503\\ .001131222\\ .001129944 \end{array}$
882	777924	686128968	29.6984848	9.5900939	
883	779689	688465387	29.7153159	9.5937169	
884	781456	690807104	29.7321375	9.5973373	
885	783225	693154125	29.7489496	9.6009548	
886	784996	695506456	29.7657521	9.6045696	.001128668
887	786769	697864103	29.7825452	9.6081817	.001127396
888	788544	700227072	29.7993289	9.6117911	.001126126
889	790321	702595369	29.8161030	9.6153977	.001124859
890	792100	704969000	29.8328678	9.6190017	.001123596
891	793881	707347971	29.8496231	9.6226030	.001122334
892	795664	709732288	29.8663690	9.6262016	.001121076
893	797449	712121957	29.8831056	9.6297975	.001119821
894	799236	714516984	29.8998328	9.6333907	.001118568
895	801025	716917375	29.9165506	9.6369812	.001117318
896	802816	719323136	29.9332591	9.6405690	.001116071
897	804609	721734273	29.9499583	9.6441542	.001114827
898	806404	724150792	29.9666481	9.6477367	.001113586
899	808201	726572699	29.9833287	9.6513166	.001112347
<b>900</b>	810000	729000000	30.0000000	9.6548938	.00111111

No.	Squares.	Cubes.	Square Roots.	Cube Roots.	Reciprocals.
901	811801	731432701	$\begin{array}{c} 30.0166620\\ 30.0333148\\ 30.0499584\\ 30.0665928\\ 30.0832179\end{array}$	9.6584684	.001109878
902	813604	733870808		9.6620403	.001108647
903	815409	736314327		9.6656096	.001107420
904	817216	738763264		9.6691762	.001106195
905	819025	741217625		9.6727403	.001104972
906	820836	743677416	30.0998339	9.6763017	.001103753
907	822649	746142643	30.1164407	9.6798604	.001102536
908	824464	748613312	30.1330383	9.6834166	.001101322
909	826281	751089429	30.1496269	9.6869701	.001100110
910	828100	753571000	30.1662063	9.6 05211	.001098901
911	829921	756058031	30.1827765	9.6940694	·001097695
912	831744	758550528	30.1993377	9.6976151	·001096491
913	833569	761048497	30.2158899	9.7011583	·001095290
914	835396	763551944	30.2324329	9.7046989	·001094092
915	837225	766060875	30.2489669	9.7082369	·001092896
916	839056	768575296	30.2654919	9.7117723	.001091703
917	840889	771095213	30.2820079	9.7153051	.001090513
918	842724	773620632	30.2985148	9.7188354	.001089325
919	844561	776151559	30.3150128	9.7223631	.001088139
920	846400	778688000	30.3315018	9.7258883	.001086957
921	848241	781229961	30.3479818	9.7294109	001085776
922	850084	783777448	30.3644529	9.7329309	001084599
923	851929	786330467	30.3809151	9.7364484	001083423
924	853776	788889024	30.3973683	9.7399634	001082251
925	855625	791453125	30.4138127	9.7434758	001081081
926	857476	794022776	30.4302481	9.7469857	.001079914
927	859329	796597983	30.4466747	9.7504930	.001078749
928	861184	799178752	30.4630924	9.7539979	.001077588
929	863041	801765089	30.4795013	9.7575002	.001076428
930	864900	804357000	30.4959014	9.7610001	.001075269
931	866761	806954491	$\begin{array}{r} 30.5122926\\ 30.5286750\\ 30.5450487\\ 30.5614136\\ 30.5777697\end{array}$	9.7644974	001074114
932	868624	809557568		9.7679922	001072961
933	870489	812166237		9.7714845	001071811
934	872356	814780504		9.7749743	001070664
935	874225	817400375		9.7784616	001069519
936	876096	820025856	30.5941171	9.7819466	001068376
937	877969	822656953	30.6104557	9.7854288	001067236
938	879844	825293672	30.6267857	9.7889087	001066098
939	881721	827936019	30.6431069	9.7923861	001064963
940	883600	830584000	30.6594194	9.7958611	001063830
941	885481	833237621	30.6757233	9.7993336	$\begin{array}{r} .001062699\\ .001061571\\ .001060445\\ .001059322\\ .001058201 \end{array}$
942	887364	835896888	30.6920185	9.8028036	
943	889249	838561807	30.7083051	9.8062711	
944	891136	841232384	30.7245830	9.8097362	
945	893025	843908625	30.7408523	9.8131989	
946	894916	846590536	30.7571130	9.8166591	$\begin{array}{r} \cdot 001057082 \\ \cdot 001055966 \\ \cdot 001054852 \\ \cdot 001053741 \\ \cdot 001052632 \end{array}$
947	896809	849278123	30.7733651	9.8201169	
948	898704	851971392	30.7896086	9.8235723	
949	900601	854670349	30.8058436	9.8270252	
950	902500	857375000	30.8220700	9.8304757	
951	904401	860085351	30.8382879	9.8339238	$\begin{array}{r} \cdot 001051525 \\ \cdot 001050420 \\ \cdot 001049318 \\ \cdot 001048218 \\ \cdot 001047120 \end{array}$
952	906304	862801408	30.8544972	9.8373695	
953	908209	865523177	30.8706981	9.8408127	
954	910116	868250664	30.8868904	9.8442536	
955	912025	870983875	30.9030743	9.8476920	
956	913936	873722816	30.9192497	9.8511280	.001046025
957	915849	876467493	30.9354166	9.8545617	.001044932
958	917764	879217912	30.9515751	9.8579929	.001043841
959	919681	881974079	30.9677251	9.8614218	.001042753
<b>960</b>	921600	884736000	30.9838668	9.8648483	.001041667

## TABLE XXXII.—SQUARES, CUBES, ETC.

No.	Squares.	Cubes.	Square Roots.	Cube Roots.	Reciprocals.
961	923521	887503681	31.0000000	9.8682724	.001040583
962	925444	890277128	31.0161248	9.8716941	.001039501
963	927369	893056347	31.0322413	9.8751135	.001038422
964	929296	895841344	31.0483494	9.8785305	.001037344
965	931225	898632125	31.0644491	9.8819451	.001036269
966	933156	901428696	31.0805405	9.8853574	.001035197
967	935089	904231063	31.0966236	9.8887673	.001034126
968	937024	907039232	31.1126984	9.8921749	.001033058
969	938961	909853209	31.1287648	9.8955801	.001031992
970	940900	912673000	31.1448230	9.8989830	.001030928
971	942841	915498611	31.1608729	9.9023835	.001029866
972	944784	918330048	31.1769145	9.9057817	.001028807
973	946729	921167317	31.1929479	9.9091776	.001027749
974	948676	924010424	31.2089731	9.9125712	.001026694
975	950625	926859375	31.2249900	9.9159624	.001025641
976	952576	929714176	31.2409987	9.9193513	.001024590
977	954529	932574833	31.2569992	9.9227379	.001023541
978	956484	935441352	31.2729915	9.9261222	.001022495
979	958441	938313739	31.2889757	9.9295042	.001021450
980	960400	941192000	31.3049517	9.9328839	.001020408
981	962361	944076141	31.3209195	9.9362613	.001019368
982	964324	946966168	31.3368792	9.9396363	.001018330
983	966289	949862087	31.3528308	9.9430092	.001017294
984	968256	952763904	31.3687743	9.9463797	.001016260
985	970225	955671625	31.3847097_	9.9497479	.001015228
986	972196	958585256	31.4006369	9.9531138	•001014199
987	974169	961504803	31.4165561	9.9564775	•001013171
988	976144	964430272	31.4324673	9.9598389	•001012146
989	978121	967361669	31.4483704	9.9631981	•001011122
990	980100	970299000	31.4642654	9.9665549	•001010101
991 992 993 994 995	982081 984064 986049 988036 990025	973242271 976191488 979146657 982107784 985074875	$\begin{array}{r} 31.4801525\\ 31.4960315\\ 31.5119025\\ 31.5277655\\ 31.5436206 \end{array}$	9.9699095 9.9732619 9.9766120 9.9799599 9.9833055	$\begin{array}{r} \cdot 001009082 \\ \cdot 001008065 \\ \cdot 001007049 \\ \cdot 001006036 \\ \cdot 001005025 \end{array}$
996	992016	988047936	$     \begin{array}{r}       31.5594677 \\       31.5753068 \\       31.5911380 \\       31.6069613 \\       31.6227766 \\     \end{array} $	9.9866488	.001004016
997	994009	991026973		9.9899900	.001003009
998	996004	994011992		9.9933289	.001002004
999	998001	997002999		9.9966656	.001001001
<b>1000</b>	1000000	1000000000		10.0000000	.001000000
1001 1002 1003 1004 1005	1002001 1004004 1006009 1008016 1010025	$\begin{array}{c} 1003003001\\ 1006012008\\ 1009027027\\ 1012048064\\ 1015075125 \end{array}$	31.6385840 31.6543836 31.6701752 31.6859590 31.7017349	$\begin{array}{c} 10.0033322\\ 10.0066622\\ 10.0099899\\ 10.0133155\\ 10.0166389 \end{array}$	.0009990010 .0009980040 .0009970090 .0009960159 .0009950249
1006 1007 1008 1009 1010	1012036 1014049 1016064 1018081 1020100	$\begin{array}{r} 1018108216\\ 1021147343\\ 1024192512\\ 1027243729\\ 1030301000\\ \end{array}$	31.7175030 31.7332633 31.7490157 31.7647603 31.7804972	$\begin{array}{r} 10.0199601\\ 10.0232791\\ 10.0265958\\ 10.0299104\\ 10.0332228 \end{array}$	$\begin{array}{r} .0009940358\\ .0009930487\\ .0009920635\\ .0009910803\\ .0009900990\end{array}$
1011 1012 1013 1014 1015	$\begin{array}{r} 1022121\\ 1024144\\ 1026169\\ 1028196\\ 1030225 \end{array}$	$\begin{array}{r} 1033364331\\ 1036433728\\ 1039509197\\ 1042590744\\ 1045678375\end{array}$	$     \begin{array}{r}       31.7962262 \\       31.8119474 \\       31.8276609 \\       31.8433666 \\       31.8590646 \\     \end{array} $	$\begin{array}{c} 10.0365330\\ 10.0398410\\ 10.0431469\\ 10.0464506\\ 10.0497521 \end{array}$	.0009891197 .0009881423 .0009871668 .0009861933 .0009852217
1016 1017 1018 1019 <b>1020</b>	$\begin{array}{c} 1032256\\ 1034289\\ 1036324\\ 1038361\\ 1040400\\ \end{array}$	$\begin{array}{c} 1048772096\\ 1051871913\\ 1054977832\\ 1058089859\\ 1061208000 \end{array}$	31.8747549 31.8904374 31.9061123 31.9217794 31.9374388	$\begin{array}{c} 10.0530514\\ 10.0563485\\ 10.0596435\\ 10.0629364\\ 10.0662271 \end{array}$	$\begin{array}{r} .0009842520\\ .0009832842\\ .0009823183\\ .0009813543\\ .0009803922\end{array}$

# TABLE XXXIII.—CUBIC YARDS PER 100 FEET OF LEVEL SECTIONS. SLOPE 1:1.

					/11/1.1			
$\operatorname{Depth}_{d}$	Base	Base	Base	Base	Base	Base	Base	Base
	12 feet.	14 feet.	16 feet.	18 feet.	20 feet.	28 feet.	30 feet.	32feet.
1 23 4 5 6 7 8 9 10	48 104 167 237 315 400 493 593 700 815	56 119 189 267 352 444 544 652 767 889	63 133 211 296 389 489 596 711 833 963	70 148 233 326 426 533 648 770 900 1037	78 163 256 356 463 578 700 830 967 1111	107 222 344 474 611 756 907 1067 1233 1407	115 237 367 504 648 800 959 1126 1300 1481	122 252 389 533 685 844 1011 1185 1367 1556
11	937	1019	1100	1181	1263	1589	1670	1752
12	1067	1156	1244	1333	1422	1778	1867	1956
13	1204	1300	1396	1493	1589	1974	2070	2167
14	1348	1452	1556	1659	1763	2178	2281	2385
15	1500	1611	1722	1833	1944	2839	2500	2611
16	1659	1778	1896	2015	2133	2607	2726	2844
17	1826	1952	2078	2204	2330	2833	2959	3085
18	2000	2133	2267	2400	2533	3067	3200	3333
19	2181	2322	2463	2604	2744	3307	3448	3589
20	2370	2519	2667	2815	2963	3556	3704	3852
21	2567	2722	2878	3033	3189	3811	3967	4122
22	2770	2933	3096	3259	3422	4074	4237	4400
23	2981	3152	3322	3493	3663	4344	4515	4685
24	3200	3378	3556	3733	3911	4907	4800	4978
25	3426	3611	3796	3981	4167	5200	5093	5585
26	3659	3852	4044	4237	4430	5500	5393	5585
27	3900	4100	4300	4500	4700	5500	5700	5900
28	4148	4356	4563	4770	4978	5807	6015	6222
29	4404	4619	4833	5048	5263	6122	6337	6552
80	4667	4889	5111	5333	5556	6444	6667	6889
<b>31</b>	4937	5167	5396	5626	5856	6774	7004	7233
32	5215	5452	5689	-5926	6163	7111	7348	7585
33	5500	5744	5989	6233	6478	7456	7700	7944
34	5793	6044	6296	6548	6800	7807	8059	8311
35	6093	6352	6611	6870	7130	8167	8426	8685
<b>36</b>	6400	6667	6933	7200	7467	8533	8800	9067
<b>57</b>	6715	6989	7263	7537	7811	8907	9181	9456
38	7037	7319	7600	7881	8163	9289	9570	9852
39	7367	7656	7944	8233	8522	9678	9967	10256
40	7704	8000	8296	8593	8889	10074	10370	10667
41 42 43 44 45 48 47 48 49 50	8048 8400 9126 9500 9881 10270 10667 11070 11481	8352 8711 9078 9452 9833 10222 10619 11022 11433 11852	8656 9022 9396 9778 10167 10563 10967 11378 11796 12222	8959 9333 9715 10104 10500 10904 11315 11733 12159 12593	9263 9644 10033 10430 10833 11244 11663 12089 12522 12963	10478 10889 11307 11733 12167 12607 13056 13511 13974 14444	10781 11200 11626 12059 12500 12948 13404 13867 14337 14815	11085 11511 11944 12385 12833 13289 13752 14222 14706 15185
51 52 53 54 55 56 57 58 59 60	11900 12326 12759 13200 13648 14104 14567 15037 15515 16000	12278 12711 13152 13600 14056 14519 14989 15467 15952 16444	12656 13096 13544 14000 14463 14933 15411 15896 16389 16889	13033 13481 13937 14400 14870 15348 15833 16326 16826 17333	13411 13867 14330 14800 15278 15763 16256 16756 17263 17778	14922 15407 15900 16400 16907 17422 17944 18474 18474 19011 19556	15300 15793 16293 16800 17315 17837 18367 18904 19448 20000	15678 16178 16685 17200 17722 18252 18789 19333 19885 20444

#### TABLE XXXIII.—CUBIC YARDS PER 100 FEET OF LEVEL, SECTIONS. SLOPE 1.5;1.

-		~	LOIION	5. 510	1.1.1.1.0.	1.		
$\overset{ ext{Depth}}{d}$	Base	Base	Base	Base	Base	Base	Base	Base
	12 feet.	14 feet.	16 feet.	18 feet.	20 feet.	28 feet.	30 feet.	32 feet.
1223456 <b>7</b> 890	50 111 183 267 361 467 583 711 850 1000	57 126 206 398 511 635 770 917 1074	65 141 228 326 435 556 687 830 983 1148	72 156 250 356 472 600 739 889 1050 1222	80 170 272 385 509 644 791 948 1117 1296	109 230 361 504 657 822 998 1185 1383 1593	117 244 383 533 694 867 1050 1244 1450 1667	124 259 406 563 731 911 1102 1304 1517 1741
11	1161	1243	1324	1406	1487	$1813 \\ 2044 \\ 2287 \\ 2541 \\ 2806 \\ 3081 \\ 3369 \\ 3667 \\ 3976 \\ 4296 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ 1000 \\ $	1894	1976
12	1333	1422	1511	1600	1689		2133	2222
13	1517	1613	1709	1806	1902		2383	2480
14	1711	1815	1919	2022	2126		2644	2748
15	1917	2028	2139	2250	2361		2917	3028
16	2133	2252	2370	2489	2607		3200	3319
17	2361	2487	2613	2739	2865		3494	3620
18	2600	2733	2867	3000	3133		3800	3933
19	2850	2991	3131	3272	3413		4117	4257
20	3111	3259	3407	3556	3704		4444	4593
21 223 224 225 226 227 289 299 30	3383 3667 3961 4267 4583 4911 5250 5600 5961 6333	3539 3830 4131 4444 4769 5104 5450 5807 6176 6556	3694 3993 4302 4622 4954 5296 5650 6015 6391 6778	3850 4156 4472 4800 5139 5489 5850 6222 6606 7000	4006 4319 4642 4978 5324 5681 6050 6430 6820 7222	4628 4970 5324 5689 6065 6452 6850 7259 7680 8111	4783 5133 5494 5867 6250 6644 7050 7467 7894 8333	4939 5296 5665 6044 6435 6837 7250 7674 8109 8556
81 32 334 35 36 37 88 39 40	6717 7111 7517 7933 8361 8800 9250 9711 10183 10667	6946 7348 7761 8185 8620 9067 9524 9993 10472 10963	7176 7585 8006 8437 8880 9333 9798 10274 10761 11259	7406 7822 8250 8689 9139 9600 10072 10556 11050 11556	7635 8059 8494 9398 9867 10346 10837 11339 11852	8554 9007 9948 10435 10933 11443 11963 12494 13037	8783 9244 9717 10200 10694 11200 11717 12244 12783 13333	9013 9481 9961 10452 10954 11467 11991 12526 13072 13630
41	11161	11465	11769	12072	12376	13591	13894	14198
42	11667	11978	12289	12600	12911	14156	14467	14778
43	12183	12502	12820	13139	13457	14731	15050	15369
44	12711	13037	13363	13689	14015	15319	15644	15970
45	13250	13583	13917	14250	14583	15917	16250	16583
46	13800	14141	14481	14822	15163	16526	16867	17207
47	14361	14709	15057	15406	15754	17146	17494	17843
48	14933	15289	15644	16000	16356	17778	18133	18489
49	15517	15880	16243	16606	16969	18420	18783	19146
50	16111	16481	16852	17222	17593	19074	19444	19815
<b>51</b>	16717	17094	17472	17850	18228	19739	20117	20494
<b>52</b>	17333	17719	18104	18489	18874	20415	20800	21185
<b>53</b>	17961	18354	18746	19139	19531	21102	21494	21887
<b>54</b>	18600	19000	19400	19800	20200	21800	22200	22600
<b>55</b>	19250	19657	20065	20472	20880	22509	22917	23324
<b>56</b>	19911	20326	20741	21156	21570	23230	23644	24059
<b>57</b>	20583	21006	21428	21850	22272	23961	24383	24805
<b>58</b>	21267	21696	22126	22556	22985	24704	25133	25563
<b>59</b>	21961	22398	22835	23272	23709	25457	25894	26331
<b>60</b>	22667	23111	23556	24000	24444	26222	26667	27111

# TABLE XXXIII.—CORRECTIVE PERCENTAGE FACTORS FOR TABLES OF LEVEL SECTIONS. TABLES OF LEVEL SECTIONS. FOR FOR

To be applied when cross-sections are not level. See § 95.

ve	ans- rse face pe.	-	=12 fee and d=			= 20 fee and $d =$			=30 fe and d=	
α°	Per- cent	10 feet.	20 feet.	50 feet.	10 feet.	20 feet.	50 feet.	10 feet.	20 feet.	50 feet.
5 10 15 20 <b>3</b> 0	9 18 27 36 57	% 1.9 8.2 21 46 327		% 1.8 7.5 19 43 317	% 2.1 9.0 23 51 358	7% 1.8 8.0 21 45 336		% 2.3 10.0 26 57 400	% 2.0 8.4 22 48 354	% 1.8 7.7 20 44 326

## Side slope = 1.5:1 or $\beta$ = 33°41′.

Side slope=1:1 or  $\beta$ =45°.

ve suri	ns- rse face pe.		=12 fee and d=			=20 fee and d=			=30 fee nd <i>d</i> =	
α°	Per- cent	10 feet.	20 feet.	50 feet.	10 feet.	20 feet.	50 feet.	10 feet.	20 feet.	50 feet.
5 10 15 20 30	9 18 27 36 57	% 0.9 3.7 9.0 18 58	% 0.8 3.4 8.2 16 53	% 0.8 3.2 7.8 15 50	% 1.0 4.3 10.3 20 67	% 0.9 3.6 8.7 17 56	% 0.8 3.3 8.0 16 51	$     \begin{array}{r} & & & \\ & & 1.2 \\ & 5.0 \\ 12.1 \\ & 24 \\ & 78 \end{array} $	% 0.9 4.0 9.5 19 61	% 0.8 3.4 8.2 16 53

TABLE XXXIV.—ANNUAL CHARGE AGAINST A TIE, BASED ON THE ORIGINAL COST AND ASSUMED LIFE OF THE TIE: INTEREST COMPOUNDED AT 5%. (See § 217.)

k b

" I

								Life	Life of tie in years	in vea	7							
Original cost									0m 10	m yea								
or the in cents.	ø	4	ß	8	2	8	8	10	11	12	13	14	15	16	17	18	39	8
20	7.34	5.64	4.62	3.94	3.46	3.09	2.81	2.59	2.41	2.26	2.13	2.02	1.93	1.85	1.77	1.7	1.65	1.60
25	9.18		5.77	4.92	4.32	3.87	3 52	3.24	3.01	2.82	2.66	2.53	2.41	2.31	2.22	2.14	2.07	2.01
30	11.02		6.93	5.91	5.18	4.64	4.22	3.89	3.61	3.38	3.19	3.03	2.89	2.77	2.66	2.57	2.48	2.41
85	12.85		8.08	6.90	6.05	5.42	4.92	4.53	4.21	3.95	3.73	3.54	3.37	3.23	3.10	2.99	2.90	2.81
40	14.69		9.24	7.88	6.91	6.19	5.63	5.18	4.81	4.51	4.26	4.04	3.85	3.79	3.55	3.42	3.31	3.21
45	16.52	12.69	10.39	8.87	7.78	6.96	6.33	5.83	5.42	5.08	4.79	4.55	4.34	4.15	3.99	3.85	3.72	3.61
20	18.36	14.10	11.55	9.85	8.64	7.74	7.03	6.48	6.02	5.64	5.32	5.05	4.82	4.61	4.43	4.28	4.14	4.01
55	20.20	15.51		10.84	9.51	8.51	7.74	7.12	6.62	6.21	5.86	5.56	5.30	5.07	4.88	4.71	4.55	4.41
60	22.03	16.92		11.82		9.28	8.44	7.77	7.22	6.77	6.39	6.06	5.78	5.54	5.32	5.13	4.96	4.81
65	23.87	18.33		12.81		10.06	9.14	8.42	7.83	7.33	6.92	6.57	6.26	6.00	5.77	5.56	5.38	5.22
04	25.70	19.74			12.10	10.83	9.85	9.07	8.43	7.90	7.45	7.07	6.74	6.46	6.21	5.99	5.79	5.62
52	27.54	21.15		14.78	12.96	11.60	10.55	9.72	9.03	8.46	7.98	7.58	7.22	6.92	6.65	6.42	6.20	6.02
80	29.38	22.56		15.76	13.83		11.25	10.36	9.63	9.03	8.52	8.08	7.71	7.38	7.10	6.84	6.62	6.42
85	31.21					13.15	11.96	11.01	10.23	9.59	9.05	8.59	8.19	7.84	7.54	7.27	7.03	6.82
60	33.05				15.55		12.66	11.66	10.84	10.15	9.58	9.09	8.67	8.30	7.98	7.70	7.45	7.23
95	34.88		21.94	18.71	16.42	14.70	13.37		11.44	10.72	10.12	9.60	9.15	8.76	8.42	8.12	7.86	7.62
100	36.72	28.20	23.10	19.70	17.28	15.47	14.07	12.95	12.04	11.28	10.65	10.10	9.63	9.23	8.87	8.55	8.27	8.02
For each 5 cents, add	1.836	1.410	1.410 1.155	.985	.864	.774	.703	.648	.602	.564	.532	.505	.482	.461	.443	.428	.414	401
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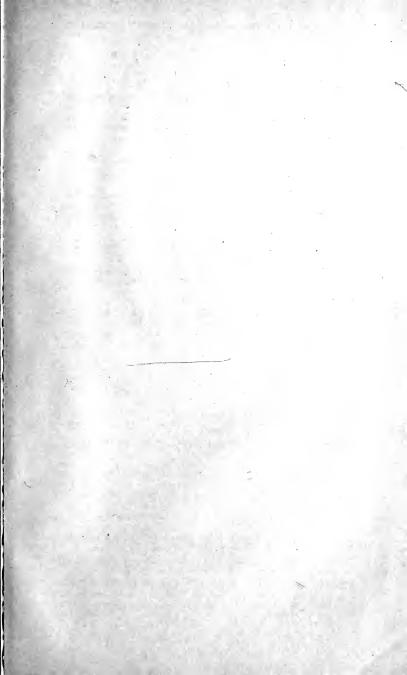
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